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To cite this article: Tarang Khangaonkar *et al* 2024 *Environ. Res. Lett.* **19** 104039

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RECEIVED
6 June 2024REVISED
26 August 2024ACCEPTED FOR PUBLICATION
29 August 2024PUBLISHED
6 September 2024

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Mixing and dilution controls on marine CO₂ removal using alkalinity enhancement

Tarang Khangaonkar^{1,2,*} , Brendan R Carter^{2,3}, Lakshitha Premathilake^{1,2}, Su Kyong Yun¹ , Wenfei Ni¹, Mary Margaret Stoll², Nicholas D Ward⁴ , Lenaïg G Hemery⁴ , Carolina Torres Sanchez⁴, Chinmayee V Subban¹, Mallory C Ringham⁷, Matthew D Eisaman^{5,6}, Todd Pelman⁷, Krti Tallam⁷  and Richard A Feely³

¹ Energy and Environment Directorate, Pacific Northwest National Laboratory, Seattle, WA 98109, United States of America

² University of Washington, Seattle, WA, United States of America

³ Pacific Marine Environmental Laboratory, NOAA, Seattle, WA, United States of America

⁴ Marine and Coastal Research Laboratory, PNNL, Sequim, WA, United States of America

⁵ Department of Earth & Planetary Sciences, Yale University, New Haven, CT, United States of America

⁶ Yale Center for Natural Carbon Capture, Yale University, New Haven, CT, United States of America

⁷ Ebb Carbon, Inc., San Carlos, CA, United States of America

* Author to whom any correspondence should be addressed.

E-mail: Tarang.Khangaonkar@pnnl.gov

Keywords: ocean alkalinity enhancement, modeling, marine carbon dioxide removal, zone of influence, mixing, dilution, carbon dioxide outgassing reduction

Supplementary material for this article is available [online](#)

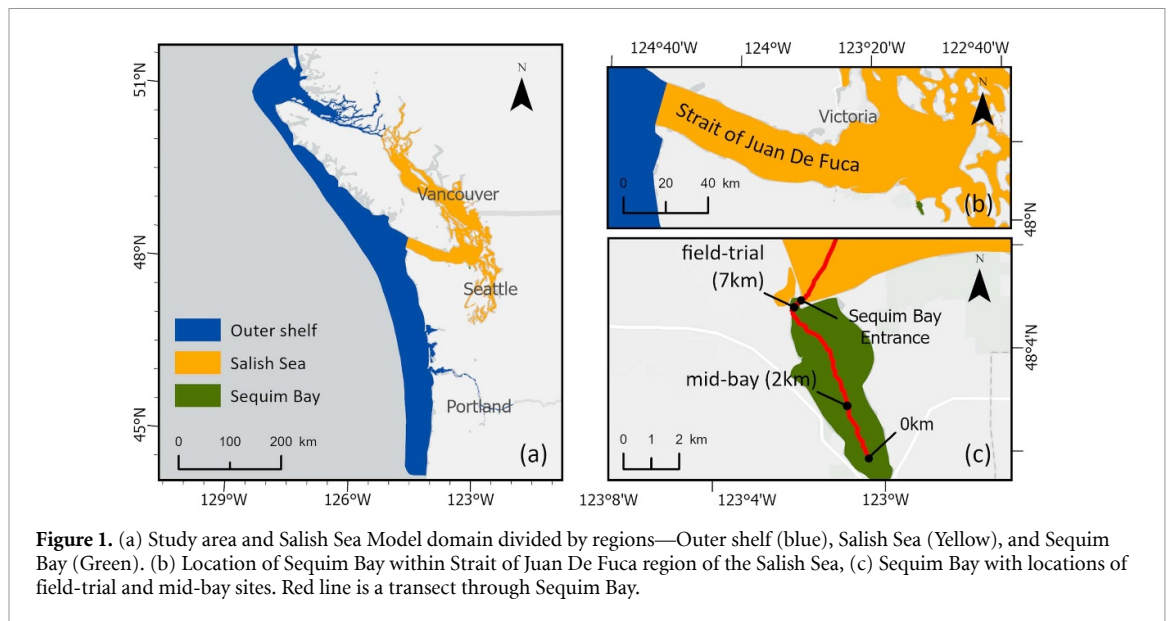
Abstract

Marine CO₂ removal (CDR) using enhanced-alkalinity seawater discharge was simulated in the estuarine waters of the Salish Sea, Washington, US. The high-alkalinity seawater would be generated using bipolar membrane electro dialysis technology to remove acid and the alkaline stream returned to the sea. Response of the receiving waters was evaluated using a shoreline resolving hydrodynamic model with biogeochemistry, and carbonate chemistry. Two sites, and two deployment scales, each with enhanced TA of 2997 mmol m⁻³ and a pH of 9 were simulated. The effects on air-sea CO₂ flux and pH in the near-field as well as over the larger estuary wide domain were assessed. The large-scale deployment (addition of 164 Mmoles TA yr⁻¹) in a small embayment (Sequim Bay, 12.5 km²) resulted in removal of 2066 T of CO₂ (45% of total simulated) at rate of 3756 mmol m⁻² yr⁻¹, higher than the 63 mmol m⁻² yr⁻¹ required globally to remove 1.0 GT CO₂ yr⁻¹. It also reduced acidity in the bay, ΔpH ≈ +0.1 pH units, an amount comparable to the historic impacts of anthropogenic acidification in the Salish Sea. The mixing and dilution of added TA with distance from the source results in reduced CDR rates such that comparable amount 2176 T CO₂ yr⁻¹ was removed over >1000 fold larger area of the rest of the model domain. There is the potential for more removal occurring beyond the region modeled. The CDR from reduction of outgassing between October and May accounts for as much as 90% of total CDR simulated. Of the total, only 375 T CO₂ yr⁻¹ (8%) was from the open shelf portion of the model domain. With shallow depths limiting vertical mixing, nearshore estuarine waters may provide a more rapid removal of CO₂ using alkalinity enhancement relative to deeper oceanic sites.

1. Introduction

At the current level of human emissions estimated at ≈40 GT (giga tons) CO₂ yr⁻¹, the target of limiting global warming to 1.5 °C–2.0 °C by 2100 set by the Paris Agreement of 2015 [1] will require proactive and deliberate CO₂ removal (CDR) of ≈10 GT CO₂ yr⁻¹ from the atmosphere by mid-century, and ≈20 GT

CO₂ yr⁻¹ by mid-to-late century [2]. Oceanic capture of CO₂ from the atmosphere through air-sea gas exchange alone will not be sufficient [3, 4]. The natural processes would eventually reduce atmospheric CO₂ levels to nearly the preindustrial levels, but only at an unacceptably long timescale of ≈100–200 × 10³ years [5–7]. Even after reducing emissions to net-zero levels, marine CDR efforts will be needed



to accelerate the oceanic carbon capture processes to shorter timescales of decades, to meet the 2100 target.

Ocean alkalinity enhancement (OAE) approach is an emerging technology, that has the potential to accelerate oceanic CO₂ uptake while providing the added benefit of local ocean acidity reduction. OAE techniques include direct addition of alkalinity through minerals such as pulverized carbonate/silicate rocks [8, 9], or releasing high-alkalinity aqueous streams (e.g. NaOH) generated via electrochemical splitting [10, 11] or electrodialysis [12–14]. Modeling studies ranging from simplified box models to spatially resolved models have examined the potential effectiveness of these alkalinity enhancement techniques [15–18]. Results in general indicate that extreme large-scale additions of alkalinity would be required to have a noticeable global scale effect on CDR. Keller *et al* [19] highlighted the challenge using scenarios limiting the alkalinity addition to ≈ 6 GT Ca²⁺ yr⁻¹ as Ca(OH)₂, an amount that could be delivered by modern fleet of ships, resulting in only modest uptake of CO₂ (20 GT by 2030 and 180 GT by 2100). Ilyina *et al* [20] pointed out that alkalization could still provide CO₂ uptake benefits on a nearshore subregional scale, and simultaneously help counteract local ocean acidification.

Simulated global-scale perturbations often do not accurately reflect the scale of the alkalinity enhancement strategies that will likely be employed in practice. Wang *et al* [21] tested a hypothetical total alkalinity (TA) release of 1.67×10^{10} mol TA yr⁻¹ (equivalent to 667 950 T NaOH yr⁻¹) in Unimak Pass, Alaska using a 100 km grid size global-scale model, resulting in 639 905 T CO₂ yr⁻¹ removed from the air. The authors noted that even for these seemingly large rates of TA release, the region over which surface pCO₂ mitigation was > 10 ppm was limited to a single model

cell. The scale of mixing zones associated with plumes from typical point source discharges ≈ 0.01 – 0.1 km² is considerably smaller than a typical regional/global ocean model cell ≈ 30 – 100 km². The coarse resolution of the large-scale models likely induces excessive numerical dilution due to instantaneous numerical mixing within the receiving cell. High resolution modeling, at the scale of near-field zone of mixing and tidal transport is needed to accurately resolve the expected benefits of practical full-scale deployment and to support feasibility assessment; design; siting; establishment of monitoring, reporting, and verification procedures; and evaluation of any potential ecosystem effects. Given costs of transportation, access to required electrical power, and potential ecosystem benefits, nearshore settings are an important consideration for the transition of technology from theory to practical deployment.

In this study, we examine the biogeochemical response of Sequim Bay, within the fjord-like estuarine waters of the Salish Sea, Washington, US (see figure 1) to OAE at the local scale of a planned field trial and hypothetical full-scale deployments. An existing electrochemical system located onshore would deliver an enhanced-alkalinity stream at a TA of 2929 $\mu\text{mol kg}^{-1}$ or 2997 mmol m^{-3} (mmol m⁻³) and pH of 9 with $\Delta\text{pH} \approx 1.06$, and $\Delta\text{TA} \approx 869$ mmol m^{-3} relative to average ambient conditions) for the duration of one year. We use a regional scale model with sub-regional/site specific refinement to quantify the increase in CO₂ flux and pH over the domain. OAE via delivery of excess base in the form of hydroxide ions is expected to induce a rapid reduction in dissolved CO₂* [expressed collectively with H₂CO₃ as CO_{2(aq)}]. The resulting increase in the gradient between CO_{2(air)} and CO_{2(aq)} should provide a corresponding increase in

the net air-to-water CO₂ flux. However, equilibration occurs over a timescale of weeks or longer, during which turbulent mixing and dilution with ambient water with higher background CO_{2(aq)} could rapidly diminish the gradient and rate of CO₂ capture away from the source. We use these simulations to assess how mixing and dilution impact CDR associated with OAE in a realistic nearshore estuarine setting relative to ideal open ocean conditions.

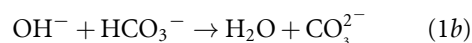
2. Methods and experimental design

2.1. Electrodialysis system—OAE field trial

A planned field trial of a bipolar electro dialysis (BPED) system at the US Department of Energy's Pacific Northwest National Laboratory, in Sequim Bay, Washington provided the setting and the opportunity for this modeling-based assessment. Figure 2 shows a schematic process diagram of the system developed by Ebb Carbon, Inc. consisting of withdrawal of seawater and electrochemical extraction of acid using BPED [12–14, 22, 23]. The extracted acid is diverted away for other beneficial uses and seawater with increased alkalinity is returned to surface waters.

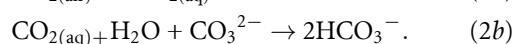
The system is designed to generate a highly concentrated stream (mostly NaOH) at a pH \approx 13.9. Blending with seawater is needed to reduce the pH to 9 prior to discharge in compliance with the local water quality standards, resulting in TA of 2929 $\mu\text{mol kg}^{-1}$ (2997 mmol m^{-3}). Delivered at the field trial flow rate of 0.001 75 $\text{m}^3 \text{s}^{-1}$, this corresponds to TA addition of 0.164 Mmol yr^{-1} . Using CO2SYS [24], an ambient $T = 14$ °C, $S = 30$ psu, equilibrium $p\text{CO}_2$ of 398 ppm, and the ratio $\Delta\text{CO}_2/\Delta\text{TA} = 0.84$ [7, 23], the carbon capture potential for this added alkalinity is 6.1 ton yr^{-1} .

Alkalinity is a primary control for the carbon content in the ocean on long timescales, and the carbon capture potential is proportional to the alkalinity enhancement in seawater under equilibrium $p\text{CO}_2$ at the sea surface [7]. The addition of alkalinity to seawater results in a rapid reduction of CO_{2(aq)} levels, governed by oceanic carbonate chemistry [22]. The net reactions are as follows,



Equations (1a) and (1b) occur over a short/immediate time scale [25].

Depleted CO_{2(aq)} and bicarbonate (HCO₃⁻) are replenished from the atmosphere over a longer time frame of weeks to months through air-sea CO₂ gas exchange described by equations (2a) and (2b) below,



Return to full equilibrium state with CO_{2(aq)} replenished from air-to-sea transfer provides the theoretical maximum CO₂ capture. This assumes ideal conditions where added alkalinity remains at the surface and contributes fully towards CO₂ capture.

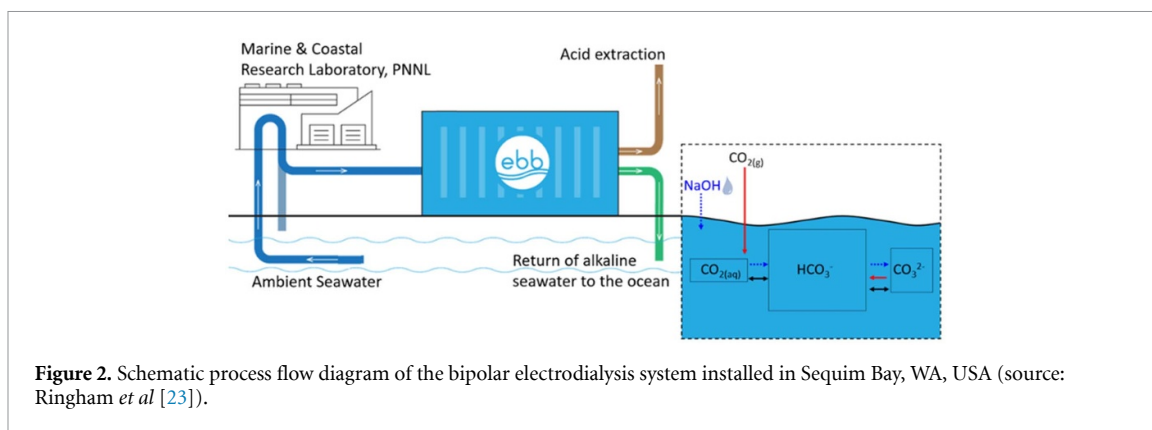
We leveraged the existing finite volume coastal ocean model (FVCOM [26]) hydrodynamics coupled to the FVCOM-ICM [27] biogeochemistry-based implementation of the *Salish Sea Model* [28, 29]. The model was refined within Sequim Bay region (see figure 1) to seamlessly resolve the mixing-zone-scale processes at the OAE site (25–100 m) where the process impacts will be most acute, to the local-scale (Sequim Bay wide) chronic impacts on ocean biogeochemistry that are relevant for assessing co-benefits such as local ocean acidification mitigation, to the larger regional-scale (Salish Sea wide) impacts on ocean carbon uptake and storage.

The model tracks the variations of TA and dissolved inorganic carbon (DIC) in the water column by considering the kinetic processes that contribute to the changes of TA and DIC acting as sources or sinks. Without a parameterization for carbonate mineral cycling, the modeled biological change in TA in the water column is proportional to the summation of the changes in NH₄⁺ and NO₃⁻ concentrations due to primary production, remineralization of dissolved organic nitrogen constituents, denitrification, and sediment fluxes of NH₄⁺ and NO₃⁻. The model computes the DIC change by accounting for the changes in primary production, remineralization of dissolved organic carbon constituents, nitrification, denitrification, sediment fluxes, and air-sea exchange [30]. The model computes the CO₂ exchange between the atmosphere and the sea surface based on the equilibrium condition,

$$Q_c = K_v (\text{CO}_{2(\text{aq})\text{sat}} - \text{CO}_{2(\text{aq})\text{surf}}) A_{\text{tce}} \quad (3)$$

$$K_v = 0.251 W_{\text{wind}}^2 \left(\frac{660}{Sc} \right)^{1/2} \frac{24}{100} \quad (4)$$

In equation (3), Q_c ($\text{mmol CO}_2 \text{ d}^{-1}$) is the CO₂ gas exchange rate over A_{tce} . The area associated with the model grid node for tracer transport in FVCOM-ICM; $\text{CO}_{2(\text{aq})\text{surf}}$ (mmol m^{-3}) is the concentration of CO_{2(aq)} at the sea surface; $\text{CO}_{2(\text{aq})\text{sat}}$ (mmol m^{-3}) is the saturated concentration of CO_{2(aq)} at the sea surface; K_v (m d^{-1}) is the gas transfer velocity calculated based on the Wanninkhof (equation (4)) where W_{wind} (m s^{-1}) is the wind speed; Sc is the Schmidt number for CO₂ [31]. CO_{2(aq)} is computed using CO2SYS [24] formulations built into FVCOM-ICM. Further, FVCOM-ICM computes pH as a state variable based on the TA, DIC, and rate constants from CO2SYS using Newton–Raphson iterative method, which is an adaptation of the approach used in pyCO2SYS [32]. The selection of K1, K2 and KSO₄ dissociation constants are based on the formulation of Lueker *et al* [33].



In typical summer conditions when the ocean surface is undersaturated [$\text{CO}_{2(\text{aq})\text{surf}} < \text{CO}_{2\text{atm}}$], the ocean absorbs CO_2 from the atmosphere resulting in a positive Q_c . For the Sequim Bay field trial with TA of $2929 \mu\text{mol kg}^{-1}$ the maximum carbon capture rate in the form of increase in CO_2 absorption flux (Q_c/A) is estimated at $2822 \text{ mmol CO}_2 \text{ m}^{-2} \text{ yr}^{-1}$ at the source. This value was computed using the equilibrium condition-based gas exchange (equations (3) and (4) together with CO2SYS, and average summertime Salish Sea surface conditions ($T = 17^\circ\text{C}$, $S = 27$ psu, $\text{TA} = 1914 \mu\text{mol kg}^{-1}$, and $\text{DIC} = 1758 \mu\text{mol kg}^{-1}$) [34], corresponding $p\text{CO}_2$ level of 375 ppm, and average summer wind condition of 3.2 m s^{-1} for year 2014 from the University of Washington Weather Research Forecasting Model. However, in the winter, Salish Sea is supersaturated with $\text{CO}_{2(\text{aq})}$ substantially exceeding the saturation levels [35]. The maximum CDR rate for the same alkalinity enhancement under the high- $p\text{CO}_2$ winter conditions ($T = 7^\circ\text{C}$, $S = 29$ psu, $\text{TA} = 2020 \mu\text{mol kg}^{-1}$, and $\text{DIC} = 1971 \mu\text{mol kg}^{-1}$), $p\text{CO}_2$ level of 685 ppm and average winter wind condition of 5.3 m s^{-1} for year 2014 is significantly (five-fold) higher with a reduction in outgassing CO_2 flux of $14832 \text{ mmol CO}_2 \text{ m}^{-2} \text{ yr}^{-1}$ at the release point. CO_2 flux determined with equations (3) and (4) is sensitive to lower T , higher TA, DIC, and particularly, wind and $p\text{CO}_2$.

2.2. Baseline, field trial and scale-up sensitivity tests

We designed four OAE scenarios, each with a two-year long simulation period consisting of continuous high alkalinity discharge for the first year followed by a second year with no discharge. The Sequim Bay discharge location and the greater Salish Sea have e-folding flushing times of about ten days, and about one year respectively [36]. A dynamic steady state within Sequim Bay is reached after ten days of discharge and a high alkalinity plume is continuously transported out into the Strait of Juan de Fuca and the Salish Sea. The effects of released excess residual alkalinity in the Salish Sea are accounted for until they are flushed out of the domain. The baseline conditions

selected were based on Year 2014 model [37], with a validation completed previously, with zero discharge to serve as the reference for comparison to scenarios. The following scenarios were tested with enhanced TA addition in million mols (Mmol) over a 1 year duration (see figure 1 for site locations):

- SCN1 = field-trial site, 0.164 Mmol of TA added
- SCN2 = field-trial site, 164 Mmol of TA added
- SCN3 = mid-bay site, 0.164 Mmol of TA added
- SCN4 = mid-bay site, 164 Mmol of TA added

Scenarios SCN1 and SCN2 correspond to field trial site discharges, located near the western shoreline at the entrance of Sequim Bay. SCN3 and SCN4 evaluate the response to releasing enhanced-alkalinity seawater from the mid-bay site in quiescent conditions. SCN2 and SCN4 represent 1000 fold scale up from the field trial flow rate corresponding to potential full-scale deployment, with a realistic discharge rate of 40 million gallons per day (MGD) ($1.75 \text{ m}^3 \text{ s}^{-1}$), comparable to large municipal or industrial wastewater discharges in the region.

Only direct TA addition was considered, introduced as a TA flux (mmol s^{-1}) during these simulations. Addition of TA flux was only done in the first year, but the simulation continued over the second year with TA source shut off to allow residual enhanced TA within the domain to continue the CDR. The transports of mass and heat that could accompany industrial outfalls were not also parameterized to ensure that the physical circulation and characteristics within the baseline simulation remain directly comparable to those in the various scenarios.

3. Results and discussion

3.1. Nearfield mixing and dilution

Irrespective of the alkalinity delivery method, bulk release from a vessel or metered out through an outfall, the process of initial dilution from hydraulic mixing with the ambient is unavoidable. The concentrations during this near-field dilution phase reduce from the end-of-pipe levels by the dilution factor

that is directly proportional to ambient currents, inversely proportional to the flow rate, and affected by outfall/diffuser configuration. Dilution factor (ψ) is defined by the equation $\Delta Cf = \Delta C/\psi$ where ΔCf is the increase in ambient concentration after mixing in the field and ΔC is the difference between end of pipe concentration and the ambient.

In this case, relative to annual average ambient $TA_a = 2128 \text{ mmol m}^{-3}$, the end-of-pipe TA (TA_e) corresponding to the scenarios of 2997 mmol m^{-3} corresponds to $\Delta TA = 869 \text{ mmol m}^{-3}$. The final TA_f after mixing would be controlled by ψ . For a preliminary estimate, we used UM3, an analytical plume model that simulates jet and buoyancy induced dilution and mixing of fluids released through submerged outfalls [38]. Average ambient conditions ($T = 9.3 \text{ }^\circ\text{C}$, and $S = 30$) were used to estimate the expected nearfield dilution factors, within 100 m radius mixing zone (typical regulatory mixing zone size in Washington) for the respective scenarios. The nearfield dilutions for SCN1 and SCN2 at the shallow high current environment field-trial site were 388 and 13 respectively, while for SCN3 and SCN4 at the deeper mid-bay site, the dilutions are estimated at 336, and 65 respectively.

This is also reflected in the surface TA, pH, aragonite saturation state (Ω_{arag}), $p\text{CO}_2$, and ΔCO_2 flux plots shown in figure 3. At the low discharge rate of 0.164 Mmol, the dilutions are so high that the elevation of TA, pH, and Ω_{arag} levels, and reduction in $p\text{CO}_2$ are not detectable above ambient. However, at the full-scale deployment 164 Mmol, the spikes or drops in concentrations near the source location are the dominant feature. The increase in alkalinity (and pH) from the discharge causes a drop in $p\text{CO}_2$ resulting in an increase in CDR flux. The control exerted by the dilution process on TA, pH, and $p\text{CO}_2$ levels and therefore ΔCO_2 flux or CDR rate is seen in figure 3 (also see figures S1 and S2 in supplementary materials).

Although $\Delta\text{pH} \approx 0.6$ is high near the source and has the potential to cause localized ecosystem impacts [39, 40], the pH levels of 8.6 is still well below the water quality protective standard of 9 in Washington, US, and drops rapidly to 8.1 or lower within the nearfield mixing zone $\approx 100 \text{ m}$ (0.01 km^2), which lies within natural variability of pH in Sequim Bay [41]. The transects show that within Sequim Bay, there is elevation in background levels of pH and TA due to the longer residence and constrained flushing, but levels drop off further once the plume travels outside of Sequim Bay. While the CDR rate in Sequim Bay drops from the very high values near the source within the mixing zone, it is still elevated relative to baseline. CDR therefore continues at a lower rate, but over a much larger Sequim Bay area (13 km^2).

3.2. Change in CO_2 flux and pH in Sequim Bay

We focused our attention on the full-scale scenarios SCN2 and SCN4, the $1.75 \text{ m}^3 \text{ s}^{-1}$ discharges at a TA of 2997 mmol m^{-3} . These cases correspond to an addition of $165 \text{ Mmols yr}^{-1}$ of TA. As shown in figure 3, in addition to the peak TA increase near the source, the sustained discharges achieve a dynamic steady state resulting in an elevation of the background TA levels over a larger zone of influence. Over this zone, the $\text{CO}_{2(\text{aq})}$ levels in surface waters are reduced relative to baseline and the CO_2 capture process occurs at an enhanced level.

As discussed previously, most coastal estuaries including the Salish Sea are in a state of outgassing during the winter months [34, 35, 42]. The OAE effect on the gas exchange represents CDR irrespective of whether it helps enhance carbon capture from the atmosphere during the summer or reduce degassing to atmosphere from water during the winter. Figure 4 presents annual average ΔCO_2 flux in $\text{mmol CO}_2 \text{ m}^{-2} \text{ yr}^{-1}$. The mid-bay discharge allows greater retention of the enhanced alkalinity, resulting in greater increase in air-sea CO_2 flux within Sequim Bay (depth range: 0–38 m). The CDR benefit is realized over a long duration of (weeks to months) and covers a domain well beyond Sequim Bay, including the Salish Sea and the continental shelf to which alkalinity is exported. The annual average increases in CO_2 flux over the Sequim Bay domain are $1785 \text{ mmol CO}_2 \text{ m}^{-2} \text{ yr}^{-1}$ (SCN2) and $3266 \text{ mmol m}^{-2} \text{ yr}^{-1}$ (SCN4). These differences are primarily due to location of SCN2 near the mouth of Sequim Bay in high current environment that allows faster transport of enhanced TA into the Salish Sea.

The addition of large volumes of basic water at the water quality standard limit of 9 pH to the Salish Sea also provides an immediate reduction of acidity broadly across the bay. Figures 3 and 5 show that the elevation of pH levels of up to 0.6 units appears feasible within the mixing zone near the mid-bay source for SCN4 after accounting for nearfield dilution. The annual average ocean acidification reduction for Sequim Bay is also significant with ≈ 0.1 units increase in pH. This improvement is comparable to the estimated reduction in pH of 0.11–0.06 due to global anthropogenic acidification processes in the region [43–45]. Qualitatively, these results indicate that application of OAE technology in protected environments with limited flushing has the potential to provide embayment-wide ocean acidification mitigation benefits. We note, however, that this increase in pH is accompanied by a drop in $p\text{CO}_2$ of over 200 ppm, which has the potential to affect the ecosystem through carbon limitation impacts to primary production [46].

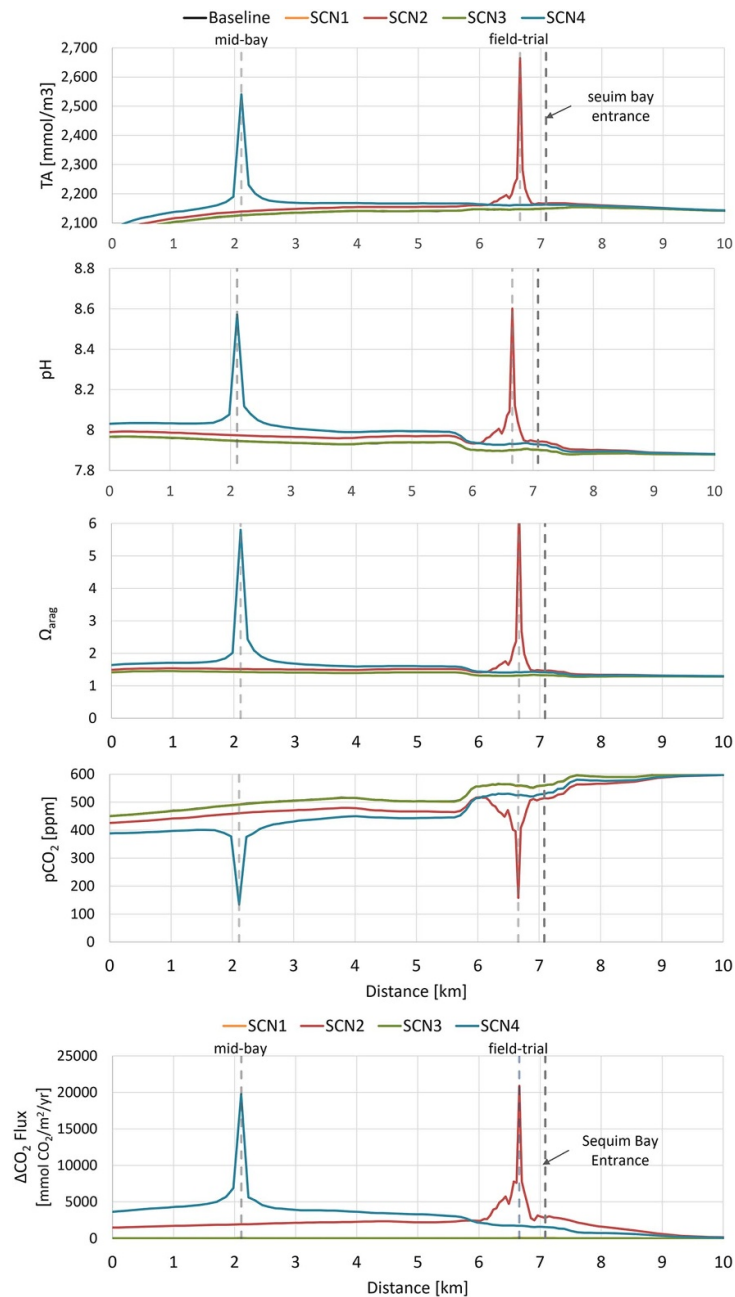
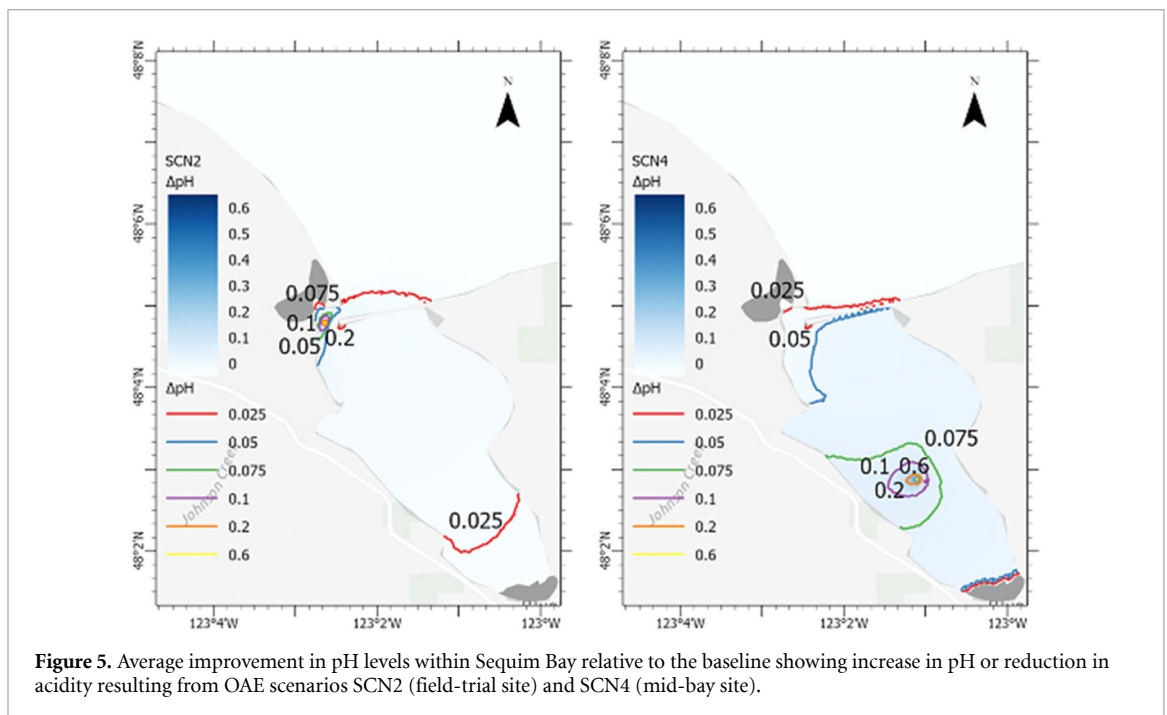
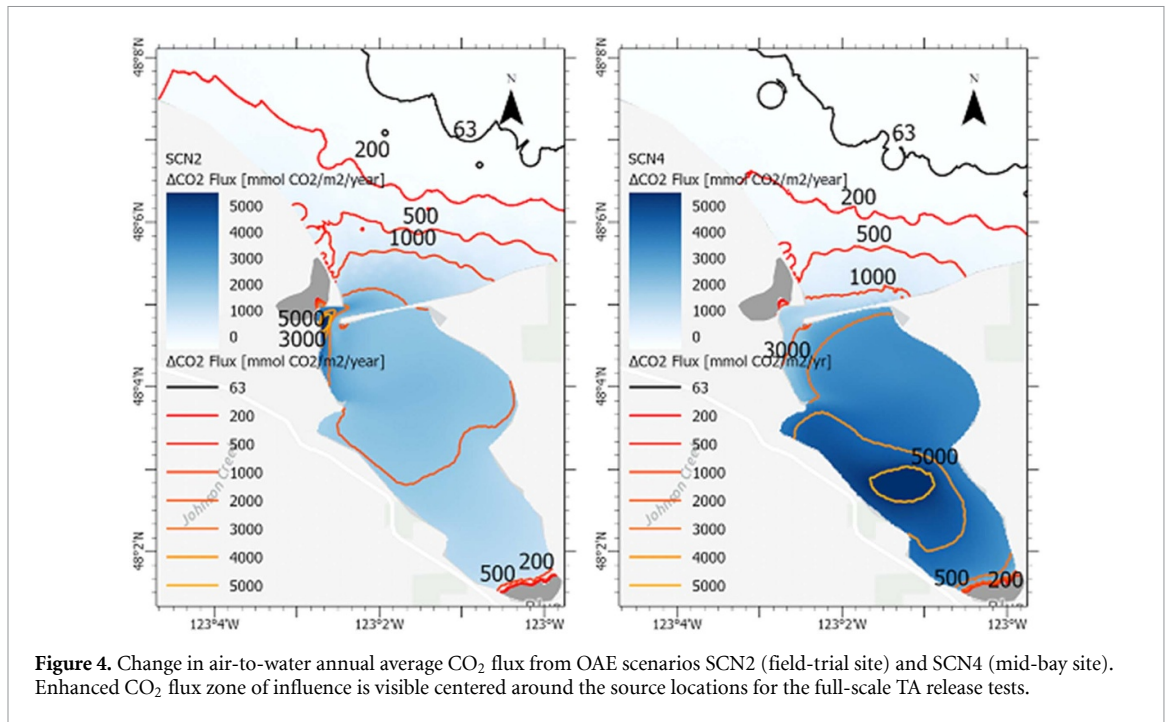


Figure 3. Total alkalinity (TA), pH, $p\text{CO}_2$, Ω_{arag} , and ΔCO_2 flux in the surface layer along the transect from southern end of Sequim Bay (0 m) through Sequim Bay entrance into the Strait of Juan De Fuca (see figure 1). Results are plotted for Baseline conditions along with the four scenarios averaged over a year of simulation. The mouth of Sequim Bay is marked by the dashed line.

3.3. CO_2 mass removal/capture in the Salish Sea

The CDR away from the source occurs at a slower rate but over a larger area and longer timeframe. Figure 6 shows a domain-wide distribution of enhanced alkalinity and higher ΔCO_2 flux for the full-scale mid-bay release scenario SCN4. While the domain-wide rates are a fraction of their levels relative to source location, the associated active area is considerably larger. The exported alkalinity from Sequim Bay mixes with the exchange flow in the Strait of Juan de Fuca and is transported landwards through the deeper layers, while alkalinity in the surface layers makes its way out to the continental shelf and to the Pacific Ocean

through the open boundary. Figure 6 shows that CDR magnitudes over the shelf region with deeper waters drop significantly compared to the estuarine and relatively shallow stratified regions of the domain. The study area domain was divided into three regions (1) Outer shelf, (2) Salish Sea, and (3) Sequim Bay (see figure 1). Figure 7 shows composite bar charts representing total mass of CO_2 removed from the respective regions. The effects of residual alkalinity from the second year as it is flushed out of the system are also shown. The annual average alkalinity enhancement over the continental shelf and along the ocean boundary is reduced to trace levels $<0.01 \text{ mmol m}^{-3}$.



This alkalinity at a low-enhancement concentration is transported out of the domain through the open ocean boundary and will continue to capture carbon at a much lower rate asymptotically until reaching background TA concentrations.

The results show that although Sequim Bay occupies a small fraction of the study area (0.02%), it accounts for 24% and 45% of CDR relative to the entire domain for SCN2 and SCN4 respectively. The Salish Sea captures 66% and 47% of the CDR while the outer shelf accounts for 10% and 8% relative to the entire domain for SCN2 and SCN4 respectively.

In addition, CDR associated with residual alkalinity is lower in the 2nd year at $\approx 38\%$ relative to Year 1. This is consistent with the estimates of one-year e -folding Salish Sea flushing characteristics expected to flush down to $1/e$ (37%) level of alkalinity change in Year 2.

At a global scale, OAE is attributed a medium-high potential for CDR, with expectations of >0.1 – 1.0 GT CO₂ yr⁻¹ [4]. At the upper limit of the range, at 1.0 GT CO₂ yr⁻¹, OAE represents a significant fraction of the 10 GT yr⁻¹ global target for limiting global warming to 1.5 °C by 2100. This corresponds to a

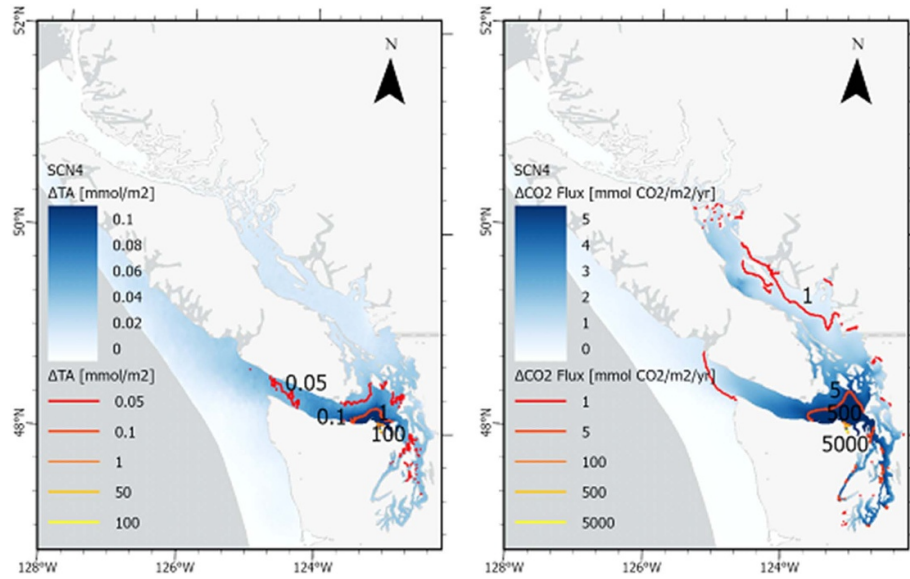


Figure 6. Enhanced alkalinity and CO₂ removal flux over the entire study domain from continuous high alkalinity discharge (SCN4) in Sequim Bay. The plot shows the effect of OAE extending beyond the confines of Sequim Bay release site to Salish Sea and the outer shelf.

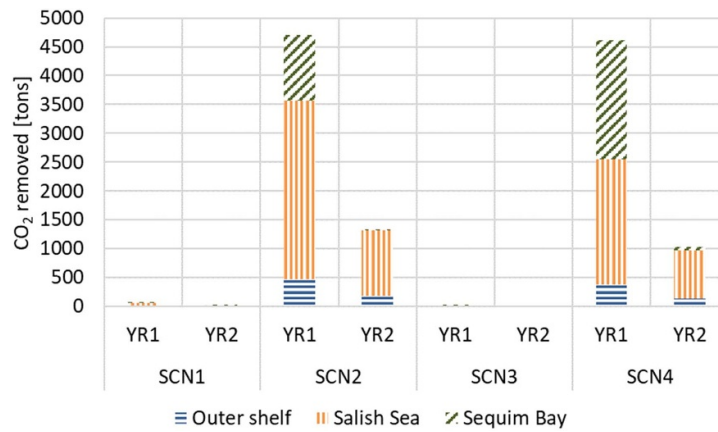


Figure 7. Mass of CO₂ removed through OAE scenarios SCN 1–4 distributed by regions within the study domain. Outer shelf—blue, Salish Sea (minus Sequim Bay)—yellow, and Sequim Bay—green. Stacked plots of CO₂ mass removed are shown for year 1 with the alkaline discharge and year 2 with discharge terminated.

global average increase in air-to-water CO₂ flux of $\approx 63 \text{ mmol m}^{-2} \text{ yr}^{-1}$ (using total ocean area [47] of 361.84 million km²). Therefore, carbon capture must ideally occur at rates $\geq 63 \text{ mmol m}^{-2} \text{ yr}^{-1}$ to have the potential to meet the demand for accelerated CDR and can serve as the OAE system design target and a point of reference for defining the optimum zone of influence.

The concern over the dilution control is straightforward in that physical mixing process may reduce the alkalinity concentration and/or divert the alkalinity away from the surface thereby reducing the carbon capture rates well below the ideal target. To illustrate this further, we used carbonate chemistry equilibrium kinetics (equations (1) and (2)) in CO₂SYS, to compute the increase in CO₂ flux for varying dilution without considering vertical mixing. Baseline CO₂

flux was computed for $T = 14 \text{ }^\circ\text{C}$, $S = 30 \text{ psu}$ and, average alkalinity of $2096 \text{ } \mu\text{mol kg}^{-1}$ and DIC of $2030 \text{ } \mu\text{mol kg}^{-1}$ using equations (3) and (4). Nine different levels of enhanced alkalinities were simulated, ranging from 2400 to 4000 $\mu\text{mol kg}^{-1}$. The parameter values $A_{\text{ice}} (1.0 \text{ m}^2)$ and $W_{\text{wind}} (5.0 \text{ m s}^{-1})$ were kept constant.

Figure 8 shows the sensitivity of the change in air-to-water CO₂ flux to dilution of TA. ΔQ_{ce} represents end-of-pipe peak change (increase) in CO₂ exchange rate relative to baseline ($\text{mmol CO}_2 \text{ m}^{-2} \text{ yr}^{-1}$). ΔQ_c is the increase in CO₂ flux after dilution. The plot shows that normalized CO₂ flux change declines with increasing dilution, indicating that the CDR rate reduces as the high alkaline plume travels away from the source and gets diluted due to ocean currents and tides-induced mixing.

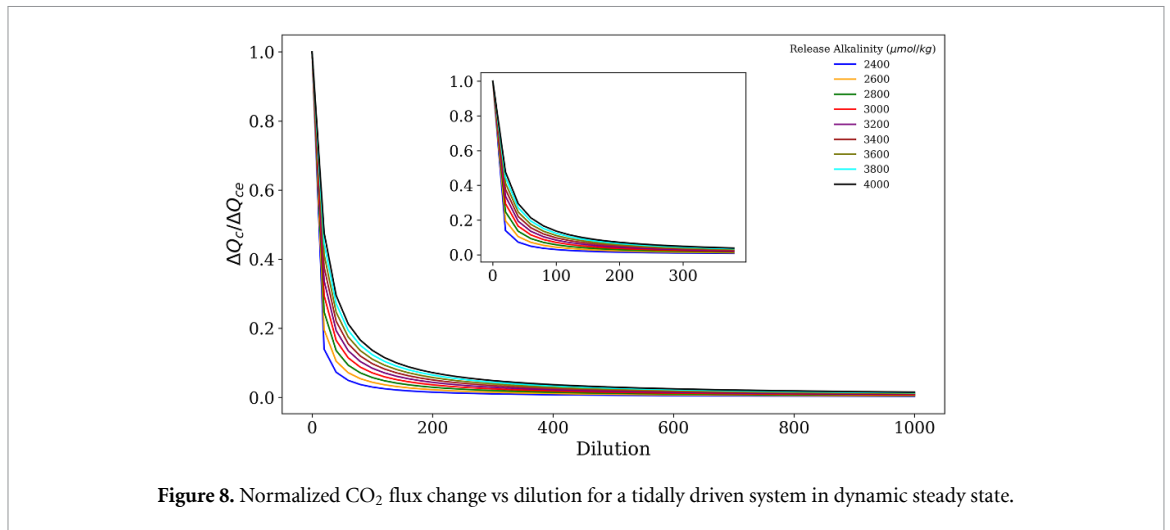


Figure 8. Normalized CO₂ flux change vs dilution for a tidally driven system in dynamic steady state.

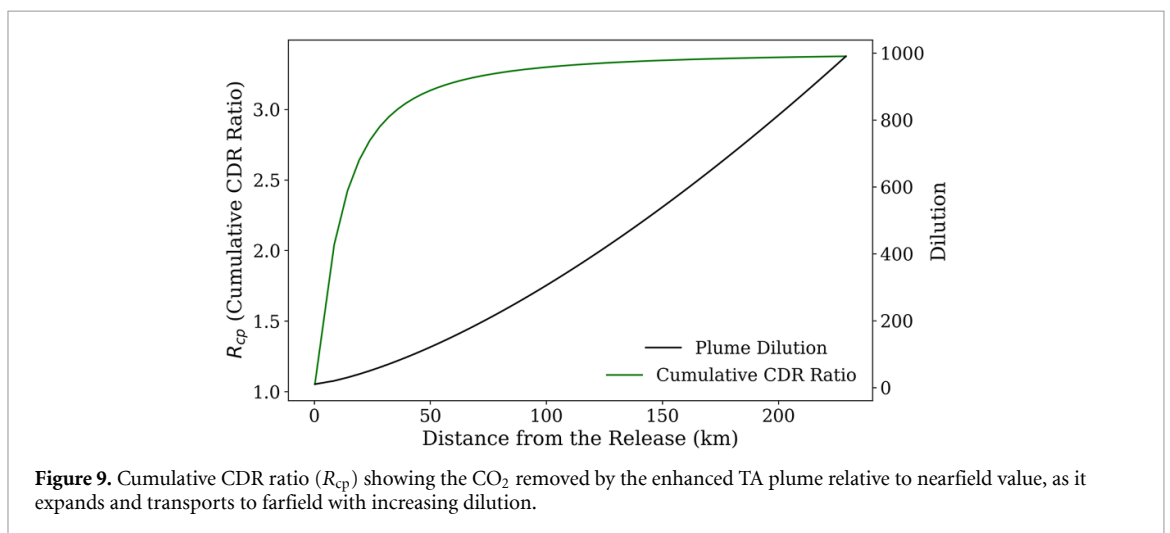


Figure 9. Cumulative CDR ratio (R_{cp}) showing the CO₂ removed by the enhanced TA plume relative to nearfield value, as it expands and transports to farfield with increasing dilution.

However, dilution due to lateral spreading has little influence on total CDR. While the lateral spreading increases dilution, the CDR occurs over a correspondingly larger area. This is shown in figure 9 using ratio R_{cp} defined as the cumulative CDR (farfield) at a distance x -km after dilution (ψ), relative to CDR (nearfield) at the source. Cumulative CDR in this example was computed using a hypothetical release of TA = 4000 $\mu\text{mol kg}^{-1}$, and assuming lateral spreading only using the 4/3rd power law (Brooks, 1960). In figure 8, relative increase in CO₂ flux $\Delta Q_c/\Delta Q_e$ drops rapidly by $\approx 90\%$ within a short distance and a dilution ψ of >200 . However, figure 9 shows that the cumulative CDR increases well up to over three fold increase, until $\psi = 900$ before plateauing out, in this case at distance of >50 km.

For the full-scale tests SCN2 and SCN4, the CO₂ flux drops below 63 $\text{mmol m}^{-2} \text{yr}^{-1}$ within short a distance of ≈ 5 km (SCN2) and 8 km (SCN4) from the source locations, outside of Sequim Bay. Therefore, Sequim Bay and the 8 km boundary, shallow nearshore regions depths ≈ 0 –40 m represents an optimum zone of influence for the scenarios tested that provides rapid CDR at above the global

ideal. Interestingly, the CDR continues to be effective at lower rate but distributed over the larger Salish Sea area. It is not until the alkalinity plume is outside the shallower estuarine reaches, and out in the open ocean, that the CDR removal drops significantly, likely due to drop in surface TA concentrations from increased vertical diffusion in addition to lateral spreading relative to the confines of the Salish Sea. Relative to open ocean deeper waters, the estuarine stratified conditions and shallow depths limit the vertical mixing and dilution. This could be a benefit for coastal implementations, but further simulations would be required to directly address this possibility. It is worth noting that estuarine environments only represent a small fraction of the overall ocean surface area, and would therefore need large perturbations to be able to make quantitatively meaningful contributions to global CDR.

In addition, we found that OAE CDR benefit is more rapidly attained during the winter outgassing conditions typical of most estuaries and the Salish Sea. Here, the CDR benefit is realized in the form of reduction of outgassing through alkalinity addition. Table 1 below shows CO₂ removed from the Salish Sea

Table 1. Total CO₂ (tons) removed from the Salish Sea region using OAE scenarios SCN2 (field trial site) and SCN4 (mid-bay site), with enhanced TA additions of 164 million mols (Mmols) in 1 year.

| Total CO ₂ removed from the Salish Sea (T of CO ₂ yr ⁻¹) ^a | | |
|--|-------------|-------------|
| Summer (in-gassing period, April–September) | SCN2 | SCN4 |
| | 363 | 404 |
| 2014 Summer—Salish Sea average: $T = 14$ °C, TA = 1884 mmol m ⁻³ , DIC = 1695 mmol m ⁻³ , pH = 8.2, $p\text{CO}_2 = 263$ ppm | | |
| Winter (out-gassing period, October—March) | SCN2 | SCN4 |
| | 3926 | 3872 |
| 2014 Winter—Salish Sea average: $T = 9$ °C, TA = 1977 mmol m ⁻³ , DIC = 1888 mmol m ⁻³ , pH = 7.9, $p\text{CO}_2 = 523$ ppm | | |
| Total | 4289 | 4276 |

^a Total CO₂ from one year model simulation for SCN2 and SCN4.

region of the model domain in tons for the full-scale tests separated into summer in-gassing vs. winter out-gassing periods. Nearly 90% of the CDR for all scenarios is associated with a reduction of outgassing during the months from October to March in the Salish Sea. The difference is due to sensitivity of the of air-water CO₂ exchange rate to lower winter temperatures and higher TA, DIC, and $p\text{CO}_2$, and stronger wind.

4. Conclusion

The results show that an enhanced-alkalinity stream released to surface waters at the local water quality standards limit of 9 pH, TA 2997 mmol m⁻³ s⁻¹ at full-scale deployment (at flow rates typical of large municipal or industrial wastewater outfalls ≈ 40 MGD) can provide significant marine CDR of ≈ 0.4 KT CO₂ yr⁻¹ from the atmosphere. However, when carbon capture benefits of reduced degassing are included, the value increases to ≈ 4.2 KT CO₂ yr⁻¹.

The results highlight the control exerted on the quantity of CDR by the mixing and dilution of the added alkalinity plume, demonstrating a sharp decline in CDR rates per unit area with increasing dilution. Carbon removal at higher dilution is not affected if it simply occurs over larger area at a proportionally lower rate. This is the case in shallow estuarine waters where mixing is restricted to lateral spreading limited by depth. However, as the plume spreads to deeper oceanic water, the diffusion over depth could potentially result in a decrease in the CDR rate.

In naturally outgassing estuarine conditions stronger CDR benefit may be through reduction of degassing of CO₂ to the atmosphere. The CDR associated with reduction of outgassing between October and March accounts for as much as 90% of total simulated CDR in Salish Sea.

In addition, our analysis indicates that the application of OAE in protected environments

with limited flushing has the potential to provide embayment-wide local acidification mitigation benefits. The results showing improvement in pH levels comparable to the estimated reduction in pH of 0.11–0.06 due to global anthropogenic acidification processes in the region is a very encouraging finding.

These results indicate that nearshore estuarine waters may provide a better performance and attractive setting for full-scale OAE systems relative to deeper oceanic sites. While the results are promising, the biogeochemical feedback and impacts on biota of releasing enhanced-alkalinity streams at large flow rates in estuarine environments are largely unknown and require further investigation. As shown in panel 3 of figure 3, the drop in $p\text{CO}_2$ by more than 200 ppm (locally) could lead to severe carbon limitation and has the potential impact primary production.

It is important to note that the model does not consider loss of DIC from ‘runaway precipitation’. As shown in panel 4 of figure 3, average Ω_{arag} levels peak at ≈ 6 and limited to a small footprint of ≈ 100 m. However, daily maximum values can reach as high as 15 and can have a larger footprint ≈ 500 m in diameter (see supplementary material figures S3 and S4). The assumption is that associated outfall diffuser will be designed to provide sufficient initial dilution such that aragonite saturation state (Ω_{arag}) remains below the threshold of 5 and the concern managed within the constraints of an authorized mixing zone [48]. Intermittent dosing could be another option to address this risk. Thresholds of concern for runaway precipitation are a subject of ongoing research [23].

The simulated TA variations only consider the effects of NH₄⁺ and NO₃⁻ changes due to biogeochemical processes. The Salish Sea however does exhibit blooms of bioalkalifiers such as coccolithophores [49] that also affect TA. While the model used is locally refined, the Sequim Bay resolving version is based on previously calibrated models [28, 36], it has not yet been validated using data from Sequim Bay. Due to these limitations, there is a high

level of uncertainty, particularly during outgassing in the estuarine setting.

Data availability statement

The data and model results that support the findings of this study will be made available upon request through the *Salish Sea Modeling Center* data portal at URL/DOI: <https://ssmc-uw.org/salish-sea-modeling-center/data-portal/>

Acknowledgments

This research was primarily supported by the Climate Works Foundation Grant Number 22-2361. Partial support was received from the US Department of Energy's Waterpower Technologies Office Laboratory Research Program at Pacific Northwest National Laboratory (PNNL). BRC and MMS thank the National Oceanographic Partnership Program (NOPP) under the National Oceanic and Atmospheric Administration's Ocean Acidification Program (Crossref Funder ID: 100018228; ROR ID: <https://ror.org/02bfn4816>) award to University of Washington CICOES. The CICOES and PMEL contributions are Numbers 2024-1381 and 5645, respectively.

Conflict of interest

MDE is Co-Founder and Chief Scientific Advisor at Ebb Carbon, Inc., MCR, TP, and KT are employees of Ebb Carbon.


ORCID iDs

Tarang Khangaonkar  <https://orcid.org/0000-0003-2881-9467>

Su Kyong Yun  <https://orcid.org/0009-0004-9505-7778>

Nicholas D Ward  <https://orcid.org/0000-0001-6174-5581>

Lenaig G Hemery  <https://orcid.org/0000-0001-5337-4514>

Krti Tallam  <https://orcid.org/0000-0002-4509-4157>

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