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7
8 **A Probabilistic, Parcel-Level Inundation Prediction Tool for Medium-Range Flood**
9 **Forecasting in Large Lake Systems**

10
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15
16 **Research Impact Statement:** Incorporating uncertainty into inundation predictions provides a
17 conservative forecast of flood risk for shoreline property owners on large lakes.

18
19 **Abstract:** This study contributes a bathtub-style inundation prediction model with abstractions
20 of coastal processes (i.e. storm surge and wave runup) for flood forecasting at medium-range
21 (weekly to monthly) timescales along the coastline of large lakes. Uncertainty from multiple data
22 sources are propagated through the model to establish probabilistic bounds of inundation,
23 providing a conservative measure of risk. The model is developed in a case study of the New
24 York Lake Ontario shoreline, which has experienced two record-setting floods over the course of
25 three years (2017-2019). Predictions are developed at a parcel-level and are validated using
26 inundation accounts from an online survey and flyover imagery taken during the recent flood
27 events. Model predictions are compared against a baseline, deterministic model that accounts for
28 the same processes but does not propagate forward data uncertainties. Results suggest that a
29 probabilistic approach helps capture observed instances of inundation that would otherwise be
30 missed by a deterministic inundation model. However, downward biases are still present in

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31 probabilistic predictions, especially for parcels impacted by wave runup. The goal of the tool is
32 to provide community planners and property owners with a conservative, parcel-level assessment
33 of flood risk to help inform short-term emergency response and better prepare for future flood
34 events.

35
36 **(KEYWORDS:** *probabilistic predictions; Great Lakes; inundation verification; flood hazard*)
37

38

39

INTRODUCTION

40 Damage from coastal flooding is growing rapidly around the world (Jongman, *et al.*, 2012;
41 Paprotny *et al.*, 2018). Along ocean coasts, flood frequency is projected to more than double in
42 certain regions with sea level rise and increased storm activity (Vitousek *et al.*, 2017). Along the
43 coastline of large inland lakes, the situation is complicated by fluctuations in climate and
44 hydrology that alter water level variability in different ways and over multiple timescales
45 (Gronewold *et al.*, 2013; Woolway *et al.*, 2020). In the Laurentian Great Lakes, coastal
46 communities have experienced record-setting high water levels over the last several years,
47 leading to inundation of near-shore homes and businesses and flash floods during storm surge
48 and high wave events (IJC-LOSLR Board, 2018; Gronewold and Rood, 2019). These record-
49 setting floods highlight the need for information that can help communities reduce coastal flood
50 impacts, especially information tailored for the unique hazards present in large lake systems.

51

52 Coastal communities make decisions regarding flood-risk reduction on various time scales,
53 including short-term emergency response and long-term risk management. Short-term
54 emergency response actions include alerting residents in low-lying regions (including seasonal
55 residents), moving belongings to higher elevation, sealing low-elevation storm drains to avoid
56 backflow, securing pumps to remove ponded water, and sandbagging homes and key
57 infrastructure to reduce flood damages. These activities often require days or even weeks to
58 implement. Long-term risk management actions include investing in shoreline protection and
59 stabilization structures (e.g. vertical walls, revetments), elevating structures, retrofitting
60 mechanical systems to operate under submerged conditions, installing sewer systems to avoid
61 septic system failure, and retrofitting existing storm sewer outlets with control valves to avoid

62 backflow. The necessary information and tools needed to make informed flood-risk decisions
63 vary depending on the relevant time scales. In this study, we focus on developing a probabilistic
64 inundation model that is designed to support medium-range (i.e. weekly to monthly) flood
65 forecasting and short-term emergency response along lake coastlines but can also be adapted for
66 screening-level assessments of long-term flood risk. This model is developed in a case study of
67 the New York coastline of Lake Ontario, the 13th largest inland lake in the world and the last of
68 the five Laurentian Great Lakes.

69
70 There are several commonly employed techniques to model inundation that range in complexity,
71 from simplified conceptual models to 2-D and 3-D hydrodynamic models (Teng *et al.*, 2017).
72 Deterministic, single-value water surface models (or “bathtub” models) predict inundation by
73 comparing land elevation and static water level (NOAA-CSC, 2010). Because of their simplicity,
74 bathtub models forego coastal process calculations such as storm surge and wave runup.
75 However, on large lakes, wind fields can propagate significant wave runup and storm surge
76 during periods of increased storm activity, and flood events can be induced by high static water
77 levels, storm activity, or a combination of the two (Kreutzwiser *et al.*, 1992; Angel, 1995).
78 Therefore, bathtub models often miss important factors that contribute to inundation.

79
80 Higher dimensional hydrodynamic models can accurately capture coastal processes at a fine
81 temporal and spatial resolution using the governing laws of hydraulics and fluid motion (Bates *et*
82 *al.*, 2010; Favaretto *et al.*, 2019). Given the importance of storm-related activities in inundation
83 prediction (Spaulding *et al.*, 2017), a fine resolution hydrodynamic model is being used as the
84 basis to update FEMA flood insurance rate maps for the entire Great Lakes shoreline (FEMA,
85 2014). While hydrodynamic models can capture accurately the coastal processes that contribute
86 to inundation, they require granular meteorological inputs that are often unavailable when
87 forecasting inundation at medium-range lead times (e.g., winds fields are typically forecasted out
88 only a few days; Chu *et al.*, 2011). This complicates the direct use of predictions from
89 hydrodynamic models in month-ahead flood risk estimates. However, we argue that these models
90 still provide valuable information for medium-range forecasting. In this work, we forward an
91 approach that develops statistical summaries of storm surge and wave runup from hindcasts of

92 hydrodynamic model output, and then adds those components into bathtub models to provide a
93 better characterization of flood risk at extended lead times.

94

95 Beyond accounting for multiple inundation processes, components of model error should be
96 quantified and propagated to provide estimates of uncertainty around inundation predictions. It is
97 important to account for data and model uncertainties to prevent decision-makers from relying
98 on “precise, but potentially inaccurate” (Alfonso *et al.*, 2016) data. This is particularly true
99 during extreme high-water events, when relatively small uncertainties in water levels and
100 elevation data can result in significantly different flooding impacts. This is demonstrated in
101 Figure 1, which shows the range of properties along the shoreline of Lake Ontario that are
102 inundated when water level and elevation uncertainties are considered and water levels are high
103 (as during recent floods in 2017 and 2019).

104

105 Several uncertainties confound inundation predictions. For instance, there is underlying
106 uncertainty in the vertical accuracy of elevation data, which is often derived from Light
107 Detection and Ranging (LiDAR) data or digital elevation models (DEMs). Elevation data that
108 overestimate the true land elevation would result in an underestimation of flood risk (Van de
109 Sande *et al.*, 2012). Similarly, inaccuracies in water levels from gage measurement error,
110 interpolation to ungaged sites, datum conversion, or forecasts of hydrologic inputs can impact
111 the accuracy of inundation predictions. Propagation and interactions in meteorologically induced
112 surges, coastal seiches, and wave set-up, set-down, and runup further increase the uncertainty in
113 total water levels that can induce coastal flooding (Mazas *et al.*, 2014). Probabilistic approaches
114 for predicting inundation seek to account for these uncertainties by reporting the likelihood of
115 inundation, rather than a deterministic, binary estimate of inundation occurrence (Leon *et al.*,
116 2014). These approaches have grown in popularity over the past decade (Gesch, 2009; NOAA-
117 CSC, 2010; Gesch, 2013; Schmid *et al.*, 2014; Kane *et al.*, 2015; Alfonso *et al.*, 2016; Gesch,
118 2018; Kovanen *et al.*, 2018; West *et al.*, 2018), in part because they relay the reliability of
119 inundation predictions and better communicate flood risk to shoreline communities (Di
120 Baldassarre *et al.*, 2010; Moser, 2014). For instance, the National Oceanic and Atmospheric
121 Administration (NOAA) developed the Lake Level Viewer (coast.noaa.gov/llv) for each of the
122 Great Lakes to incorporate uncertainty into bathtub-style predictions via the z-score method

123 (Schmid *et al.*, 2014), albeit with limited resolution that could hinder its use for flood risk
124 management at the local level (Komolafe *et al.*, 2018).

125
126 In addition to uncertainty propagation, model validation is another critical step needed to ensure
127 that decision-makers understand the accuracy of predicted flood risk information. Inundation
128 models are often validated using observed water levels and streamflow (for riverine flooding)
129 rather than accounts of property inundation due to data availability (Horritt, 2006). However,
130 many recent studies have relied on crowdsourcing and citizen science to gather reports of
131 flooding to use in the validation process (Horritt, 2006; Kutija *et al.*, 2014; Blumberg *et al.*,
132 2015; Yu *et al.*, 2016; Loftis *et al.*, 2017; Assumpção *et al.*, 2018; Loftis *et al.*, 2019), although
133 this methodology is still not common practice (See, 2019). In addition, to the authors'
134 knowledge, model validation has only been used to test deterministic inundation predictions; the
135 verification of probabilistic inundation predictions using observed accounts of flooding is
136 underexplored.

137
138 In order for inundation predictions to be utilized in coastal decision-making, such as emergency
139 response actions, they must capture the underlying inundation-driving mechanisms while also
140 quantifying uncertainty and stakeholder confidence in the predictions. Currently, medium-range
141 inundation prediction techniques in lacustrine coastal regions do not take into account all of these
142 factors. To address this gap, this study forwards a novel, probabilistic, and parcel-level
143 inundation prediction and mapping tool that is used to address three underlying research
144 questions: 1) How accurate are inundation predictions based on a deterministic bathtub model
145 with abstractions of coastal processes (i.e., storm surge and wave runup) in large lake systems?
146 2) Under what conditions can predictions be improved by incorporating uncertainty? and 3) How
147 does this accuracy vary depending on the mechanisms driving the inundation event?

148
149 The proposed model is adapted from an existing model (The Flood Tool) previously used for
150 inundation predictions along the Great Lakes shoreline (Baird, 2005). The model estimates
151 parcel-level inundation based on deterministic bathtub-style modeling with added modules to
152 abstract storm surge and wave runup processes. This work provides three primary contributions
153 over the original Flood Tool and to the broader literature. First, we provide an updated version of

154 the model that can develop conservative probabilistic inundation predictions under retrospective
155 and forecasted water level conditions while accounting for storm surge and wave runup
156 processes. Second, we verify inundation predictions using flyover imagery and citizen-science
157 reports of inundation via an online survey during recent flood events. As part of this work, we
158 explore the spatial heterogeneity of prediction accuracy and its relation to the mechanisms that
159 drive inundation along different areas of the shoreline. Finally, we demonstrate the use of the
160 model for medium-range, probabilistic inundation forecasts along the New York Lake Ontario
161 shoreline that can be updated with operational, multi-week forecasts of static water levels issued
162 at sub-weekly timescales. The study concludes with a discussion of limitations of the proposed
163 model, future research needs, and the potential of the model to be adapted for use in long-term
164 planning efforts for lake level management.

165 166 DATA AND METHODS

167 The proposed model requires four components to probabilistically predict inundation at the
168 parcel level: structure elevation, static water level, storm surge, and wave runup (Figure 2).
169 Inundation predictions are based on a bathtub-style modeling framework, where the elevation of
170 a structure on a parcel is compared against the total water level (i.e., the sum of static levels,
171 storm surge, and wave runup) to estimate inundation. However, instead of a binary prediction of
172 inundation, the model estimates the probability of inundation following the NOAA (or z-score)
173 method (Schmid *et al.*, 2014).

174
175 In this method, uncertainty is quantified for data associated with each component, which when
176 taken together quantifies the cumulative uncertainty in the inundation calculation. This technique
177 assumes that all data sources are unbiased, that the error in each data source is independent of
178 errors for other data sources, and that the cumulative uncertainty can be approximated by a
179 normal distribution. If these assumptions hold, then the cumulative uncertainty can be calculated
180 by taking the root of the sum of the squares of the individual root mean square errors (RMSEs)
181 for each data source. The cumulative RMSE is then used to calculate the z-score at a given
182 structure using Equation 1.

183

184
$$Z \text{ Score} = \frac{\text{Structure Elevation} (\text{Static Water Level} + \text{Storm Surge} + \text{Wave Runup})}{RMSE_{cumulative}} \quad (1)$$

185

186 with

187

188
$$RMSE_{cumulative} = \sqrt{RMSE_{elev}^2 + RMSE_{static.level}^2 + RMSE_{surge}^2 + RMSE_{runup}^2} \quad (2)$$

189

190 The z-score translates into a probability of inundation based on the cumulative distribution of a
191 standard normal distribution evaluated at the z-score. Although some studies have shown not all
192 errors are normally distributed, the assumption of normality of the NOAA method tends to more
193 conservatively predict inundation (Gesch, 2009; Schmid *et al.*, 2014). While over-predictions of
194 flood risk might result in unnecessarily high flood protection costs, a conservative quantification
195 of flood risk supports the risk-adverse nature of water managers and flood risk planners
196 (O'Connor *et al.*, 2005).

197

198 In the proposed model, the NOAA method and its components can be used to predict inundation
199 for past events (verification mode) or future events (forecast mode). Some of the individual
200 elements in Equation 1 will vary depending on the application (or mode) of inundation
201 prediction. These elements, their data sources, and their associated uncertainties are described in
202 more detail below. Geographic coverage for each data source is shown in Figure 3.

203

204 *Structure Elevation*

205 Structure elevation is defined as the elevation of the lakeward side of the structure of interest.
206 For a conservative inundation prediction, the minimum elevation of the lakeward side of the
207 structure is included in the z-score calculation. Elevation information is available in the form of
208 digital elevation models (DEMs). There are seven New York counties with shorelines on Lake
209 Ontario (Niagara, Orleans, Monroe, Wayne, Cayuga, Oswego, and Jefferson). All Lake Ontario
210 shoreline counties, excluding Monroe County and Niagara County, are covered by a publicly
211 available FEMA 1-meter DEM (FEMA, 2014. NYS Elevation Data. Accessed July 2018,
212 <https://gis.ny.gov/elevation>). Monroe County is covered by a 1-foot DEM (Monroe County
213 Department of Environmental Services, 2017. GIS Data. Accessed March 2019,
214 <https://www2.monroecounty.gov/gis-Data.php>). Niagara County is covered by a publicly

215 available 3-meter DEM (NOAA Office for Coastal Management, 2014. Coastal Digital Elevation
216 Model: Lake Ontario. Accessed March 2019, <https://inport.nmfs.noaa.gov/inport/item/48114>).

217
218 Elevations were extracted for shoreline homes using tax parcel shapefiles in GIS software. Tax
219 parcel information is publicly available for Niagara, Orleans, Wayne, Cayuga, and Jefferson
220 counties. Tax parcel information for Monroe and Oswego counties were obtained from their
221 respective GIS departments. The tax parcel shapefiles were used to identify the footprint of the
222 structure of interest from the Microsoft Footprint Database (Microsoft, 2019.
223 USBuildingFootprints. Accessed August 2019 - October 2019,
224 <https://github.com/microsoft/USBuildingFootprints>), which was then used to extract the base
225 elevation of the foundation of the structure from the compiled elevation dataset.

226
227 The uncertainty in the DEM elevations is assumed to be equal to the vertical error determined
228 for the associated LiDAR data used to develop that DEM. These values are reported as a RMSE
229 for each DEM dataset (Table 1).

230
231 *Static Water Level*
232 Static water level is defined as the still water level without any influence of storm related
233 activities such as wave runup or storm surge. These data are input into the tool as either a lake-
234 wide average of gage observations for a particular historic date (verification mode) or a
235 forecasted static water level for a future date (forecast mode).

236
237 **Verification Mode.** In verification mode, gage observations on Lake Ontario are
238 averaged to ensure there are no surge or seiche impacts when estimating the static water level.
239 The six gages used in the calculation are located in both the United States and Canada (NOAA
240 Great Lakes Environmental Research Laboratory, 2019. Great Lakes Water Levels Monitoring
241 Network. Accessed August 2019, <https://www.glerl.noaa.gov/data/wlevels/#monitoringNetwork>)
242 and include two long-term gages managed by NOAA at Rochester and Oswego, NY, as well as
243 four long-term gages at Kingston, Cobourg, Toronto, and Port Weller, located in the Province of
244 Ontario and managed by Fisheries and Oceans Canada. The static water level for a given date is

245 calculated as the 5-day rolling average water level between the six gages in the monitoring
246 network.

247
248 The uncertainty associated with static water levels in verification mode is the combination of
249 gage measurement error (RMSE of 0.006 m (EPA, 2016)) and the error introduced by converting
250 between datums. As static water level is calculated by averaging across six gages, the RMSE for
251 the lake-wide average static level is approximately 0.002 m via the Central Limit Theorem. Error
252 is introduced in datum conversion because all DEM-based elevations are reported with respect to
253 the North American Vertical Datum of 1988 (NAVD88), while all water levels are reported with
254 respect to the International Great Lakes Datum of 1985 (IGLD85). NOAA has calculated and
255 reported the potential error associated with converting between these two datums (RMSE of 0.20
256 m (NOAA, 2016. VDatum. Accessed January 2019,
257 https://vdatum.noaa.gov/docs/est_uncertainties.html#estTransform)).

258
259 **Forecast Mode.** Weekly water level forecasts are produced by the US Army Corps of
260 Engineers – Detroit District (USACE) and Environment and Climate Change Canada (ECCC)
261 and released every Friday ([ire.usace.army.mil/Missions/Great-Lakes-Information/Great-Lakes-](http://ire.usace.army.mil/Missions/Great-Lakes-Information/Great-Lakes-Water-Levels/Water-Level-Forecast/Weekly-Great-Lakes-Water-Levels)
262 [Water-Levels/Water-Level-Forecast/Weekly-Great-Lakes-Water-Levels](http://ire.usace.army.mil/Missions/Great-Lakes-Information/Great-Lakes-Water-Levels/Water-Level-Forecast/Weekly-Great-Lakes-Water-Levels)). The forecasting
263 system employs an ensemble of input hydroclimatic (e.g. precipitation, temperature, evaporation,
264 runoff) forecasts at 1-4 week lead times and estimated inflows from the upper Great Lakes to
265 Lake Ontario and from the Ottawa River to the St. Lawrence River. This ensemble of inputs is
266 used to produce an ensemble of projected water levels on Lake Ontario.

267
268 In forecast mode, the ensemble mean is used as the static water level when predicting inundation.
269 Uncertainty in the forecasted static level is quantified as the combination of datum conversion
270 uncertainty and the 95% confidence interval of the ensemble, which is assumed to be +/- 2
271 standard deviations of a normal distribution centered around the mean forecast. From this
272 confidence interval, we infer the standard deviation of the forecast and use it in the cumulative
273 uncertainty term in Equation 1. The standard deviation will vary for each forecast issue, but at a
274 4-week lead time it is generally on the order of 0.10 m.

275

276 *Storm Surge*

277 Storm surge is defined as the increase in water level over the static mean level due to high wind
278 activity or seiche events. In this study, hourly storm surge is taken from the Lake Ontario
279 Operational Forecast System (LOOFS) that is managed by NOAA's National Ocean Service
280 (NOS). The LOOFS is based on a gridded hydrodynamic model that uses atmospheric
281 observations and weather prediction guidance to produce three dimensional predictions of water
282 temperature and two-dimensional forecasts of water levels for Lake Ontario (Chu *et al.*, 2011).
283 The LOOFS also predicts deviations from the average lake level, i.e. seiche and storm surge
284 events. The LOOFS provides two sources of data, short-term (1-48 hour) forecasts and nowcasts,
285 the latter which is based on near real-time observations and provides a continuous estimate of
286 present conditions across the lake. For any location along the shoreline, we utilize the nowcast
287 data for hourly water level deviations from the lake level average (i.e., storm surge) at the grid
288 cell nearest the location of interest. These gridded data are available along the entire coastline at
289 a 5 km resolution from 2006 to present.

290

291 **Verification Mode.** When comparing model predictions of inundation to observed
292 inundation events, we use the maximum LOOFS nowcast storm surge associated with the date of
293 observed inundation. Because these are modeled data, we estimated their uncertainty by
294 comparing nowcast surge values to surge values at hourly observations at gages across the
295 shoreline, including those listed in Section 2.2.1 but also including additional gages managed by
296 NOAA and the USGS. The observed hourly surge values were calculated by taking hourly
297 observed water levels for each gage and subtracting from them a 3-day rolling average to
298 estimate the water level deviation (i.e., surge) for each hour. The RMSE between the nowcast
299 and observed surge was calculated for each gage for data between May 24, 2017 and July 19,
300 2019 (when all gages had available data), and then the RMSE values were averaged across gages
301 to estimate an average RMSE for nowcast surge estimates that could be applied anywhere along
302 the shoreline (RMSE of 0.026 m).

303

304 We also considered an alternative method to calculate storm surge at an arbitrary location along
305 the shoreline based on the interpolation of hourly gaged observations to ungaged sites using an
306 inverse distance weighting approach. This approach was compared against the LOOFS storm

307 surge values under cross-validation. A determination was made to use the LOOFS surge data
308 because it performed similarly to the interpolation approach and provided a longer dataset on
309 which to base probabilistic estimates of surge. More detail is provided on this comparison in the
310 Supplemental Material (Section S1, Figure S1).

311
312 **Forecast Mode.** When developing medium-range (weekly to monthly) forecasts of storm
313 surge, there are not reliable weather forecasts of wind speed and direction at long lead times on
314 which to base a forecasted surge event. Therefore, the user is provided with the option to select a
315 scenario of wind speed and direction, and the tool then estimates the potential storm surge (with
316 uncertainty) conditional on those wind parameters and the LOOFS nowcast data. This is
317 accomplished for any grid cell along the shoreline using the following procedure:

- 318 1. Hourly wind speeds from the LOOFS nowcast data are categorized into bins ranging from 0
319 miles per hour (mph) to 100 mph by increments of 10 mph for a total of 10 wind speed bins.
- 320 2. Hourly wind directions are classified as the cardinal and intercardinal directions for a total
321 of 8 wind direction bins.
- 322 3. Each combination of wind speed and wind direction is classified as a wind event (80 total
323 wind events).
- 324 4. Each wind event is associated with some number n of hourly occurrences in the nowcast
325 dataset, and each of those n occurrences has its own nowcast surge value at the grid cell of
326 interest. This produces an empirical distribution of surge values for a given wind event and
327 location. In addition, there is additional uncertainty in each individual nowcast surge value
328 (as quantified in 2.3.1). We employ a mixture distribution (Figure 4) to compound the error
329 in the modelled nowcast surge data with the uncertainty of potential surge values for any
330 given wind event:

$$331 \quad p(s|w) = \int p(s|\hat{s}) p(\hat{s}|w) d\hat{s} \quad (3)$$

332
333
334 Here, $p(s|w)$ is the distribution of the true surge value for a given wind event, $p(\hat{s}|w)$ is the
335 distribution of modelled nowcast surge values for a given wind event, and $p(s|\hat{s})$ is the
336 distribution of the true surge value around a particular nowcast surge value. We assume p
337 ($s|w$) can be approximated as a mixture of normal distributions, i.e., we assume normality

338 in the nowcast surge values under any given wind event and in the errors of the nowcast
339 surge values.

340 5. The mixture distribution allows us to determine the expected value of a surge event for any
341 given wind event, as well as an estimate of its standard deviation. Here, the standard
342 deviation quantifies uncertainty in both nowcast estimates of surge as well as the spread in
343 surge events for a selected wind field. The expected surge value is input into the numerator
344 of Equation 1 and the standard deviation is incorporated into the cumulative uncertainty in
345 the denominator.

346

347 *Wave Runup*

348 Wave runup is defined as the water level increase resulting from near-shore wave breaking that
349 propagates water up the shoreline. The method to calculate wave runup is adapted from the
350 original formulation presented in the Flood Tool (Baird, 2005), which is based on the Mase
351 method and is outlined by FEMA in the Guidelines and Specifications for Flood Hazard
352 Mapping Partners (FEMA, 2009):

353

$$354 \quad R = Mase(h_0) = 1.1 \times \xi^{0.7} \times h_0 \quad (4)$$

355

356 Here, R is the wave height that exceeds the low bluff or vertical wall height, ξ is the surf
357 similarity parameter, and h_0 is the offshore wave height. The surf similarity parameter is defined
358 as:

359

$$360 \quad \xi = \frac{\tan \theta}{\sqrt{\frac{h_0}{L_0}}} \quad (5)$$

361

362 where $\tan \theta$ is the nearshore slope of the property and L_0 is the peak wave period. The vertical
363 water depth added by wave runup on top of static water level and storm surge at a particular
364 parcel is calculated using the shoreline profile slope and the vertical height, R .

365

366 The Mase equation in Eq. 4 is written as a function of h_0 to emphasize its dependence on
367 offshore wave heights, which are assumed to be the primary source of uncertainty in this work.

368 Simulated offshore wave height and wave period data were collected from the US Army Corps
369 of Engineers Wave Information Studies (WIS) dataset (United States Army Corps of Engineers
370 (USACE), 2010. Wave Information Studies. Accessed February 2019,
371 <http://wis.usace.army.mil>). The WIS uses discrete spectral wave models and input wind fields to
372 provide estimates of wave height, period, and direction for gridded locations across the Lake
373 Ontario shoreline (see Figure 3). These data, available from January 1, 1979 to December 31,
374 2014, were validated against a limited set of hourly observed wave heights measured at a buoy
375 near Oswego, NY and were determined to be relatively unbiased, at least for that location (see
376 Supplemental Material; Section S2, Figures S2-S3).

377
378 For inundation predictions in either verification or forecast mode, the average monthly wave
379 height for the given date and WIS location nearest the parcel of interest is used as input into the
380 wave runup calculation. The uncertainty of the monthly wave height (as quantified by the
381 variance of WIS wave heights for that month and location, $\sigma_{h_0}^2$) is propagated into the wave
382 runup calculation via the delta method:

$$\sigma_R^2 = \text{Mase}(h_0)^2 \sigma_{h_0}^2 \quad (6)$$

383
384
385
386 Here, σ_R^2 is the variance of the vertical height and $\text{Mase}(h_0)$ is the derivative of the Mase
387 equation with respect to h_0 .

388
389 Shoreline profile information was retrieved from the Flood and Erosion Prediction System
390 (FEPS) database (Baird, 2005) available for a large portion of the New York shoreline on Lake
391 Ontario. This database includes parcel-level information for vertical wall/bluff height, distance
392 from the structure to the vertical wall/bluff, and nearshore and backshore slope based on
393 elevation data.

394 395 APPLICATION

396 *Model Verification*

397 **Verification Data.** Four datasets were used in model verification. The first was an online
398 survey developed by Cornell University and New York Sea Grant (NYSG) and distributed to

399 shoreline communities during the 2017 flood event that requested written and visual accounts of
400 inundation (Steinschneider *et al.*, 2019). Responses were collected from approximately 500
401 participants. Survey responses were pre-screened to ensure that inundation occurred due to Lake
402 Ontario water levels, rather than a connected waterway. Redundancy was purposefully included
403 for key survey questions to ensure respondents fully understood the question and, to the best
404 of their ability, answered it accurately. The survey included several questions about foundation
405 inundation, which are used here as the basis to evaluate the inundation model. Some respondents
406 provided the approximate date that foundation inundation began. In other cases, this field was
407 left blank and the inundation event was associated with the date the survey was submitted. For
408 each report of inundation, the maximum hourly water level at the associated tax parcel in the
409 four weeks prior to and including the date of inundation was collected and used in the inundation
410 prediction. We use this hourly water level, rather than the water level on the specific date of
411 inundation, because there was often a lag between the inundation occurrence and survey
412 reporting and some degree of uncertainty around the true date that foundation inundation began.

413
414 Imagery from three flyovers was collected and used as another source of observational data. One
415 flyover was conducted on June 12, 2017 and was organized by the Eastern Lake Ontario Dune
416 Coalition (hereafter abbreviated DUNE). This flyover included coverage of the entire southern
417 shoreline of Lake Ontario. Another unmanned flyover on July 12, 2017 was conducted by the
418 USGS. This flyover focused primarily along the coast of Wayne County, NY near the village of
419 Sodus Point. The third flyover was completed June 15, 2019 by the non-profit group Save Our
420 Sodus Inc. (SOS) with coverage of the entire New York shoreline. These images were provided
421 to the research team through personal communication and can be made available upon request to
422 SOS.

423
424 All of the flyover images were used to visually identify cases of foundation inundation along the
425 shoreline. For each flyover product, images were scanned to identify properties with primary
426 structures that could clearly be identified as having their foundation inundated or not inundated.
427 These properties were assigned binary indicators (0,1) to record the inundation state of the
428 structure foundation. A total of 63, 13, and 77 observations were collected from the DUNE,
429 USGS, and SOS flyovers, respectively. Sample images with positive instances of foundation

430 inundation from each of these flyovers can be found in the Supplemental Material (Section S3).
431 Using Google Earth, the addresses of these properties were identified, and then they were aligned
432 with the corresponding tax parcel data and building footprint using GIS software. The minimum
433 elevation of the foundation of the home was then collected as well as the latitude and longitude.
434 The date of inundation of the structure was input as the date of the flyover. For each image of
435 inundation, the maximum hourly water level at the associated tax parcel on the date of
436 inundation was collected and used in the inundation prediction.

437
438 Due to data availability, 458 of the 687 verification accounts (across both the survey and flyover
439 images) were able to be fully validated and included in the results.

440
441 **Verification Procedure.** Model predictions of inundation were developed for all parcels
442 where observations of inundation were available (i.e., parcels from the Cornell-NYSG survey,
443 DUNE flyover, USGS flyover, and SOS flyover). It is highly unlikely that the flyover images
444 capture waves in the still imagery; therefore, the wave runup calculation was not included in
445 inundation predictions for these accounts. The wave runup calculation is included in predictions
446 made for the survey accounts of inundation.

447
448 The tool produced probabilistic predictions of inundation for each property on the given date of
449 inundation. These probabilistic predictions were also converted into deterministic predictions
450 based on the sign of the numerator in Eq. 1 (e.g., a positive (negative) numerator in Eq. 1 was
451 associated with a positive (negative) deterministic prediction of inundation).

452
453 We used these deterministic and probabilistic predictions to answer the first two research
454 questions of this work: 1) How accurate are inundation predictions based on a deterministic
455 bathtub model? and 2) Under what conditions can predictions be improved by incorporating
456 uncertainty? The deterministic and probabilistic predictions were compared with the observed
457 cases of inundation using a Brier Score (BS):

458
459
$$BS = \frac{1}{N} \sum_{i=1}^N (p_i - o_i)^2 \quad (7)$$

460

461 Here, p_i is a value between zero and one that reflects the predicted probability of inundation for
462 the i^{th} parcel (e.g., $p_i = 0.57$ implies a predicted probability of inundation of 57%). We note that a
463 deterministic prediction of inundation and no inundation is equivalent to a probabilistic
464 prediction of 100% and 0% chance of inundation, respectively. The binary indicator o_i reflects
465 the observed state of inundation for the i^{th} parcel (0 implies no inundation, 1 implies inundation).
466 A BS of zero is ideal as it means that the predictions and the observed data are the same, whereas
467 a BS closer to one indicates that the model is often either underpredicting or overpredicting cases
468 of inundation.

469
470 The BS for the probabilistic and deterministic predictions were compared using a Brier Skill
471 Score (BSS):

$$472 \quad BSS = 1 - \frac{BS_{prob}}{BS_{det}} \quad (8)$$

473
474
475 The BSS quantifies the degree to which probabilistic predictions outperform deterministic
476 predictions of inundation. A score of zero suggests that the probabilistic and deterministic
477 predictions perform equally well, whereas a score above or below zero indicates that the
478 probabilistic predictions are outperforming or underperforming the deterministic predictions,
479 respectively. We note that if there is a large difference between structure elevation and total
480 water levels for most parcels, the deterministic predictions will very often be correct and the
481 deterministic BS score will likely be lower than the score for the probabilistic predictions (i.e.,
482 BSS will be negative). However, if in many cases the total water level and structure elevation are
483 sufficiently close so that data uncertainty will significantly impact the inundation prediction, it is
484 likely that the BSS will be positive and probabilistic predictions are needed to accurately assess
485 and communicate inundation risk.

486
487 The BSS was calculated separately for each of the different observational datasets, as well as for
488 observations associated with different shoreline types (i.e. open coastline or embayment). In
489 addition, spatial patterns in the error between probabilistic predictions and observed inundation
490 were analyzed to better determine regions along the shoreline where the model was more or less
491 accurate. This analysis provided insight into which inundation-driving mechanisms were

492 accurately being captured by the tool. Wave runup calculations solely impact open coastline
493 properties, whereas static water level and storm surge calculations impact both open coastline
494 and embayment properties. Therefore, geographic clustering of accurate or inaccurate model
495 predictions in particular locations is important in diagnosing model performance.

496

497 *Demonstration of Medium-Range Inundation Forecasts*

498 To demonstrate inundation predictions under a medium-range water level forecast, we use the
499 May 16, 2019 issue date for a June 14, 2019 forecast date. This water level forecast was chosen
500 since it nearly overlaps with the SOS flyover, conducted on June 15, 2019. This allows us to
501 compare known cases of inundation with month-ahead inundation predictions. The tool is
502 publicly available online as a Google Earth Engine web application
503 (<https://kts48.users.earthengine.app/view/lake-ontario-flood-mapper>).

504

505 There are two options for displaying inundation predictions based on forecasted water levels: a
506 continuous map based on DEM grid cells or a parcel-specific inundation map based on structure
507 polygons. Shoreline information required for wave runup calculations is only available for
508 parcels in the FEPS database, not at the DEM grid cell resolution, and therefore wave runup is
509 not included in continuous forecast maps at the DEM grid cell level. For each water level
510 forecast, inundation predictions are made using the follow steps (shown here for DEM-based
511 inundation maps):

512

- 513 1. The tool automatically retrieves the point forecast and uncertainty range (i.e. RMSE) of
514 the USACE/ECCC issued static water level forecast at a month lead time.
- 515 2. The user selects a wind speed and wind direction (i.e. a wind event).
- 516 3. For the entire shoreline, that wind speed and direction is used to develop a storm surge
517 distribution (via Eq. 3), providing a mean value and an RMSE.
- 518 4. These terms are included in Eqs. 1-2 to estimate the probability of inundation for every
519 DEM grid cell.

520

521 A similar procedure is followed for parcel-specific inundation maps, but with an added step to
522 include wave runup based on offshore wave heights for the month of interest.

523

524

RESULTS

525 *Verification of Inundation Predictions*

526 The reference model performance is based on deterministic inundation predictions, shown in
527 Table 2. When all of the datasets are pooled together (Table 2a), the deterministic model
528 accurately predicts no inundation and inundation for approximately 37% and 29% of the
529 observations, respectively. However, the deterministic model underpredicts and overpredicts
530 inundation for 21% and 13% verification accounts, respectively. If a conservative approach to
531 inundation modeling is preferred, the underprediction rate of observed inundation events
532 (approximately one in five) is concerning.

533

534 Model performance varies significantly across the different observational products. When
535 compared to the survey verification product, the model shows a large percentage of
536 underpredictions (Table 2b). It is worthwhile to reiterate that the survey is likely the only
537 observational set that captures inundation events caused by wave processes in addition to static
538 levels and storm surge. When compared to the USGS flyover, the model also has a similarly high
539 rate of underpredictions, albeit based on a much smaller sample size (Table 2e). The model
540 rarely underpredicts observations based on the SOS flyover, but overpredictions are common
541 (the model predicts inundation when none is observed in 29% of all observations; Table 2d). No
542 such overpredictions are reported for the DUNE flyover, and the rate of underpredictions is also
543 relatively low (13%; Table 2c).

544

545 The probabilistic model provides a way to embed some degree of conservatism into the
546 inundation predictions. Table 3 displays probabilistic inundation predictions (split into 10%
547 increments) along with the reported inundation state for all observations pooled across
548 verification products. Table 3 shows that the majority of observations that did not experience
549 inundation were predicted to have a very low probability of being inundated (0-10% chance).
550 The 98 observations that did experience inundation but were underpredicted by the deterministic
551 model (see Table 2a) fall into the 0 – 50% range for the probabilistic predictions. Approximately
552 40% of these underpredicted properties have non-trivial flood-risk (i.e., 40 of the 98
553 underpredicted observations have a 10-50% chance of inundation). This demonstrates the need to

554 propagate uncertainty into inundation predictions, so as to better represent flood risk for
555 properties that may be underestimated using a deterministic approach. Still, 58 observations
556 (~13%) that reported inundation were predicted to have a low likelihood of inundation (0-10%
557 chance), suggesting some downward bias in the probabilistic predictions.

558
559 While Tables 2 and 3 highlight the potential value of probabilistic predictions as compared to a
560 deterministic approach, this value is quantified using the BSS. Figure 5 shows the BSS for all
561 verification accounts and the breakdown of skill between verification product (survey reports and
562 SOS, DUNE, and USGS flyovers) and shoreline type (open coast versus embayment). Almost all
563 products show an increase of prediction skill in probabilistic over deterministic predictions (i.e.,
564 a positive BSS). The largest BSS score is associated with the USGS product for embayments, but
565 this result is only based on one observation. For categories with more observations, positive BSS
566 scores range from 0.06 to 0.39. Embayment properties associated with the DUNE flyover are the
567 only exception where deterministic predictions outperform probabilistic predictions (negative
568 BSS). In this case, the deterministic predictions are very accurate; there are only 12
569 underpredictions and no overpredictions (Table 2c). Therefore, the incorporation of uncertainty
570 is often not needed to explain discrepancies in the deterministic predictions.

571
572 When considering the full set of observations, the BSS score is higher for observations in
573 embayments versus those on the open coast. This result is almost entirely driven by the survey
574 verification product, which also shows better probabilistic predictions (as compared to a
575 deterministic baseline) for embayment properties versus those on open coastline. Conversely, for
576 the DUNE flyover product, probabilistic predictions tend to provide a larger improvement over a
577 deterministic baseline for open coastline properties. For the SOS flyover, the BSS scores do not
578 differ significantly between open coastline and embayments, and little can be said for the
579 USGS flyover because the sample size of embayment properties is too small.

580
581 The tendency for probabilistic predictions to more strongly outperform deterministic predictions
582 in embayments for the survey, but not the flyovers, may reflect the processes captured by the
583 different verification products. The flyovers provide still imagery taken on clear days with low
584 wind activity to best capture images along the shoreline, and therefore do not likely capture

585 inundation associated with wave activity. Conversely, the written survey reports integrate
586 respondents' observations of flooding over a period of time prior to the survey date, and
587 therefore can account for wave-related inundation. These wave-related flood events would be
588 mostly limited to the open coast, since barrier beaches often protect properties within
589 embayments from wave activity. Therefore, a lower BSS along the open coastline compared to
590 embayments for the survey reports, but not for the flyover products, suggests that the tool may be
591 systematically underestimating wave-related flooding.

592
593 To assess the spatial distribution of model prediction skill, Figure 6a shows the difference
594 between the predicted probability of inundation and the binary inundation observation (hereafter
595 the Inundation Probability – Observation (IPO) score) for all observations mapped across the
596 Lake Ontario shoreline. Highly accurate and precise predictions are associated with IPO scores
597 near zero, whereas IPO scores greater than and less than zero are indicative of probabilistic
598 overpredictions and underpredictions, respectively. Figures 5b-d show the spatial distribution of
599 IPO scores within specific regions of the shoreline in more detail. The distribution of IPO scores
600 are shown for the full verification dataset and for each verification product in Figure 6e.

601
602 The probabilistic model is performing well along most of the shoreline, with IPO scores most
603 often within a narrow range (-0.3, 0.3) around zero. While the median IPO score for most
604 datasets (except the USGS) is approximately zero, the full dataset, survey, DUNE, and USGS
605 products have IPO scores that tend to range below zero, indicating more underpredictions in
606 these products. In contrast, most of the IPO scores for the SOS verification product are positive,
607 indicating more overpredictions.

608
609 Model predictions along the eastern shoreline, such as regions around North Pond (Figure 6b)
610 and Jefferson County, tend to be the most accurate. While large underpredictions and
611 overpredictions ($|IPO| > 0.9$) do occur, they are more infrequent compared to other areas of the
612 shoreline.

613
614 The largest concentration of underpredictions is located along the shoreline of Monroe County
615 (Figure 6c) and are predominately from the survey verification product. Along the shoreline in

616 this region, houses are located within close proximity to the waterfront with relatively
617 unprotected shorelines. Survey accounts for these properties also reported significant wave
618 activity as a major contributor to inundation, suggesting that model underpredictions in this area
619 are linked to poorly characterized wave runup processes.

620
621 In Sodus Point (Figure 6d), there is a clustering of overpredictions along the peninsula (IPO >
622 0.9). All of the overpredictions in this region (n = 7) are from the SOS flyover verification
623 product. In Wayne County, there is only 1 underprediction (IPO < - 0.9) for the SOS product,
624 with the model doing a relatively accurate job of representing flood risk (- 0.9 < IPO < 0.9) for
625 118 verification accounts (94%). The modelled static water level used in the verification
626 procedure for these accounts is 75.91 meters, which is the all-time high daily water level on Lake
627 Ontario. In addition, the nowcast identified a positive surge anomaly in this area on the SOS
628 flyover date. However, the observed water level at a USGS gage near Sodus Bay was 75.85
629 meters, suggesting the total water level used for verification was higher than that observed. This
630 again illustrates that at high water levels, small discrepancies in measured data can result in
631 significant uncertainty in predicted inundation.

632 633 *Demonstration of Medium Range Inundation Forecasts*

634 Figure 7 shows a medium range forecast of inundation for June 14, 2019, issued approximately a
635 month beforehand (May 16, 2019). These inundation predictions are associated with a mean
636 static water level forecast of 75.87 meters. The map displays inundation risk as low-, moderate-,
637 and high-risk, which corresponds to probabilistic inundation predictions of 1-5% (yellow), 5-
638 50% (orange), and 50-100% (red), respectively. The ranges for these categories were based on
639 stakeholder feedback.

640
641 Under the static water level forecast, key locations in Wayne County NY were at moderate to
642 high risk of inundation. The probabilistic inundation predictions for the SOS flyover
643 observations on June 15, 2019 are shown in Table 4. At this lead time, the uncertainty in the
644 static water level forecast is a major driver of the uncertainty in inundation predictions. There is
645 only one property being significantly underpredicted (inundation probability < 10%). The model
646 is overpredicting inundation significantly (inundation probability > 90%) for seven properties.

647 The probabilistic model has a BS of 0.20, which indicates the probabilistic model fits the
648 observed data relatively well, even when based on the month-ahead forecasted static water level.
649 The BSS for these observations is 0.35, which further demonstrates the benefits of the
650 probabilistic predictions over a deterministic approach for medium range forecasts.

651

652

DISCUSSION

Model Limitations and Future Research Needs

654 The proposed model attempts to improve risk characterization over a deterministic approach by
655 propagating known vertical errors into inundation predictions. However, some key uncertainties
656 were not included in the model, particularly those related to structural uncertainties and biases in
657 certain datasets and models. For instance, while our model accounts for an abstraction of wave
658 runup processes via the Mase equation (Eq. 4), Melby *et al.* (2012) showed that these empirical
659 models parameterized by deep-water wave conditions “will yield significant uncertainty in
660 application to shallow water conditions with varied bathymetry.” Improved results could be
661 possible using different empirical approaches (Stockdon or EuroTop formula), or using
662 hydrodynamic models capable of capturing wave transformation into shallow water regions, but
663 these approaches were not considered. The abstractions of wave runup used here may be
664 responsible for some regions of key underpredictions (e.g. Monroe County) and should be taken
665 as a caution against using this model for precise inundation predictions in key areas susceptible
666 to coastal processes that are difficult to characterize. Future work is needed to identify which
667 components of the model lead to systematic biases and whether computationally efficient
668 alternatives can be found. The model does not account for the duration of wind speeds on storm
669 surge heights, nor the correlation of storm surge and waves. To more accurately capture flood risk,
670 future work should determine how flood risk varies with the persistence and co-occurrence of
671 extreme coastal events. Additionally, a variety of non-lake level processes (e.g. riverine flooding,
672 ponding in nearshore areas, etc.) are excluded from the tool and are therefore not included in
673 potential inundation impacts. Stakeholder communication is critical to ensure communities
674 understand how this tool can (and cannot) be used to forecast their flood risk.

675

676 In an effort to present a robust verification of the model, multiple observational products were
677 used to assess model predictions. However, these observational products all have measurement

678 error, which should be considered when interpreting the results. For instance, while the flyover
679 products are associated with precise dates, the survey information has more uncertainty in the
680 date of the actual inundation event being reported. Survey responses could have been submitted
681 at any time following an inundation event, and not all survey responses reported the date of
682 flooding. There is also the possibility of human error in the survey product, as homeowners may
683 have reported inundation for a different part of their property (e.g. utility shed, detached garage,
684 etc.) when asked about foundation inundation for their primary residential structure. Further,
685 while flyover images were carefully screened to ensure observations of inundation (or lack
686 thereof) were accurate, there is the possibility that certain observations were incorrectly
687 categorized.

688
689 When used in forecast mode, medium-range forecasts of static lake levels contribute a large
690 portion of the uncertainty to inundation predictions. Any potential to improve the accuracy and
691 precision of these forecasts could have significant value to coastal communities. Recent work has
692 sought to improve water level forecasts in the Great Lakes region (Durnford *et al.*, 2018). This
693 effort requires that data and models be seamlessly integrated across the international border of
694 the US and Canada (Gronewold *et al.*, 2018), as demonstrated in the expansion of the National
695 Water Model across the Great Lakes region (Mason *et al.*, 2019). Forecasting efforts could also
696 benefit from the assimilation of state-of-the-art measurements of antecedent conditions (e.g.
697 snowpack (Arslan *et al.*, 2019), soil moisture (Entekhabi *et al.*, 2010)), as well as additional
698 runoff model intercomparisons (Gaborit *et al.*, 2017) and improvements in models of open-water
699 evapotranspiration (Charusombat *et al.*, 2018). Medium-range water level forecasts would
700 further improve with increased skill in precipitation and temperature forecasts at subseasonal to
701 seasonal lead times (Vitart *et al.*, 2017); recent efforts in the Great Lakes region have focused on
702 developing a suite of seasonal forecast tools for this purpose (Bolinger *et al.*, 2017). One of the
703 strongest signals is related to the El Niño-Southern Oscillation (ENSO), which provides forecast
704 information at the end of the fall season for winter and early spring water supplies. This
705 coincides with the timing needed to prepare for and potentially reduce flood risk. While ENSO
706 forecasts can be noisy over the Great Lakes, recent work suggests that non-linearity in the
707 underlying teleconnections could be used to improve forecast skill (Carter *et al.*, 2018; Fu *et al.*,
708 2019).

709

710 *Implications for Lake Level Management*

711 Municipal-level decision-making for flood risk mitigation on Lake Ontario is complicated by
712 water level management that influences flooding on the lake. Since the late 1950's, water levels
713 on Lake Ontario have been regulated by the International Joint Commission (IJC) at the Moses-
714 Saunders Power Dam, located downstream of Lake Ontario on the St. Lawrence River. The dam
715 has been used to stabilize water levels on the lake for a variety of stakeholder interests, including
716 domestic water use, navigation, hydropower, riparian protection, and recreational boating.
717 However, water level stabilization caused significant stress to coastal wetlands and other
718 ecosystems (Wang *et al.*, 2015; Wilcox *et al.*, 2018), leading the IJC to introduce a new water
719 level management plan (Plan 2014) on January 1, 2017 that reintroduced some of the natural
720 variability in water levels that had been reduced under the previous plan (IJC, 2014). A few
721 months after Plan 2014 was implemented, Lake Ontario experienced the 2017 flood, and then the
722 2019 flood occurred two years later. These floods have caused significant public backlash
723 against Plan 2014, threatening the environmental benefits promised under the plan. This has
724 sparked a review of Plan 2014 and considerations of whether an alternative management regime
725 could improve the tradeoff between riparian flood risk and environmental restoration.

726

727 To effectively quantify risk and expected benefits to multiple stakeholder interests, any candidate
728 management plan needs to be assessed under an ensemble of plausible water supply scenarios.
729 The proposed inundation prediction tool lends itself to aid in quantifying flood damages under a
730 large ensemble of water supply scenarios due to its low computational cost. In addition,
731 uncertainty propagation would lead to a conservative estimate of riparian flood risk, which
732 would help address stakeholder concerns in the tense political environment. This is particularly
733 important given the non-linear damage curve (see Figure 1), where small changes in peak water
734 levels can lead to large changes in potential impacts. Therefore, the probabilistic inundation tool
735 is well suited to assist in flood impact quantification in future lake level management studies
736 (both on Lake Ontario and the upper Great Lakes). However, more work is needed to support
737 this effort, e.g., regional extreme value models of storm surge and offshore wave heights
738 anywhere along the shoreline. This effort is left for future work.

739

CONCLUSION

This study contributes a novel, probabilistic, and parcel-level inundation prediction and mapping tool that combines multiple flood-related processes (static water levels, storm surge, wave run-up) relevant to large lake systems while also accounting for and propagating uncertainty in each through to inundation predictions. The model acts as a computationally efficient complement to other inundation prediction tools in the Great Lakes that is well adapted for repeated and conservative inundation prediction, as is needed for frequently issued flood forecasts during extreme high water events or in planning studies with large ensembles of water supply scenarios.

The tool was validated in a case study along the New York Lake Ontario shoreline with accounts of inundation from four separate observational products covering the record floods of 2017 and 2019. Validation efforts showed that the probabilistic tool provided more accurate inundation predictions than deterministic predictions. The probabilistic tool had areas of concentrated underpredictions, which were attributed to deficiencies in capturing wave runup and overtopping of shoreline protection structures (e.g. vertical walls). However, in most locations the probabilistic nature of the tool allowed for conservative inundation estimates that helps to avoid major underestimation of inundation risk.

The fully validated model will be made available to stakeholders as an online forecasting tool with the goal of supporting proactive risk management and accelerating community response to potential inundation. This tool joins a larger suite of models emerging to help communities mitigate heightened flood risk along the Great Lakes shoreline.

SUPPORTING INFORMATION

Additional supporting information may be found online under the Supporting Information tab for this article: a comparison of modelled and spatially-interpolated, observation storm surge data, an assessment of modelled wave height data, and sample images used for model validation.

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775

776

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1005 FIGURE LEGENDS

1006 **Figure 1.** The distribution of home elevations along the Lake Ontario shoreline (see Data).
1007 Under a high water level scenario (75.9 m, the average peak level between the floods of 2017
1008 and 2019), 15% of homes on the Lake Ontario shoreline fall below that water level and are
1009 projected to be inundated. However, after propagating vertical errors in the mean water level and
1010 home elevations (see Methods), up to 43% of homes are at risk to be impacted.

1011 **Figure 2.** Flowchart of probabilistic inundation predictions.

1012 **Figure 3.** Map of study region and data sources.

1013 **Figure 4.** Mixture distribution for storm surge at a particular location and for a particular wind
1014 event (e.g., 10 - 20 mph winds from the northeast). In this example, there are $n = 9$ hourly
1015 occurrences associated with this wind event, each with a different nowcast surge value. The
1016 distribution of true surge around any particular nowcast surge value is shown with dotted blue
1017 lines. The final mixture distribution of storm surge is shown in yellow.

1018 **Figure 5.** The BSS for each combination of verification product and shoreline type. The BSS of
1019 all verification properties (orange line), open coastline properties (red line), and embayment
1020 properties (blue line) is displayed as the reference BSS for all product and shoreline
1021 combinations (shown numerically).

1022 **Figure 6.** IPO scores mapped along the Lake Ontario shoreline (a). Negative values correspond
1023 to model underpredictions, while positive values correspond to model overpredictions. IPO
1024 scores are shown for Sandy Creek, Oswego County (b), Greece, Monroe County (c), and Sodus
1025 Point, Wayne County (d). The boxplot of IPO scores broken down by verification product is
1026 shown in (e).

1027 **Figure 7.** The Google Earth Engine user interface of the online inundation prediction tool.
1028 Inundation predictions are shown for the June 2019 forecasted water level in Wayne County,
1029 New York.

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TABLE CAPTIONS

Table 1. The reported RMSE for each DEM covering the Lake Ontario shoreline.

Source	County Coverage	RMSE (m)
FEMA 1-meter DEM	Orleans, Wayne, Cayuga, Oswego, Jefferson	0.127
Monroe County 1-foot DEM	Monroe	0.106
NOAA 3-meter DEM	Niagara	0.2

1052 **Table 2.** Contingency tables for deterministic inundation predictions versus reported inundation
 1053 accounts, shown by verification product (percentages of total sample size shown in parentheses).

a)

Full Data (n = 458)		Reported	
		No	Yes
Predicted	No	171 (37%)	98 (21%)
	Yes	57 (13%)	132 (29%)

b)

Survey (n = 226)		Reported	
		No	Yes
Predicted	No	55 (24%)	76 (34%)
	Yes	20 (9%)	75 (33%)

c)

DUNE (n = 89)		Reported	
		No	Yes
Predicted	No	53 (60%)	12 (13%)
	Yes	0 (0%)	24 (27%)

d)

SOS (n = 126)		Reported	
		No	Yes
Predicted	No	63 (50%)	4 (3%)
	Yes	37 (29%)	22 (18%)

e)

USGS (n = 17)		Reported	
		No	Yes
Predicted	No	0 (0%)	6 (35%)
	Yes	0 (0%)	11 (65%)

1054 **Table 3.** Probabilistic inundation predictions for data from all verification products (n = 458).

Probability of Inundation (%)	Reported	
	No	Yes
0 - 10	131 (29%)	60 (13%)
10 - 20	12 (3%)	14 (3%)
20 - 30	10 (2%)	9 (2%)
30 - 40	9 (2%)	9 (2%)
40 - 50	9 (2%)	6 (1%)
50 - 60	10 (2%)	14 (3%)
60 - 70	8 (2%)	17 (4%)
70 - 80	7 (1%)	6 (1%)
80 - 90	12 (3%)	19 (4%)
90 - 100	20 (4%)	76 (17%)

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1063 **Table 4.** Probabilistic inundation predictions based on the month-ahead water level forecast for

1064 the SOS flyover verification product (n = 126).

Probability of Inundation (%)	Reported	
	No	Yes
0 - 10	41 (32%)	1 (1%)
10 - 20	7 (6%)	0 (0%)
20 - 30	8 (6%)	0 (0%)
30 - 40	5 (4%)	3 (2%)
40 - 50	8 (6%)	3 (2%)
50 - 60	7 (6%)	3 (2%)
60 - 70	6 (5%)	1 (1%)
70 - 80	8 (6%)	2 (2%)
80 - 90	3 (2%)	2 (2%)
90 - 100	7 (6%)	11 (9%)

1065