1	Determination of the parameters of the triaxial earth ellipsoid as derived from present-day
2	geospatial techniques
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10	Abstract. This investigation implements a least-squares methodology to fit a triaxial ellipsoid to
11	a set of three-dimensional Cartesian coordinates obtained from present-day geospatial techniques,
12	materializing the terrestrial frame ITRF2014. To approximate, as much as possible previous
13	research on this topic, the original spatial values of the station coordinates were "reduced" to the
14	surface of the EGM2008 geoid model by introducing a simple and straightforward procedure. The
15	mathematical model adopted in all LS solutions is the standard quadric polynomial equation
16	parameterizing a triaxial ellipsoid. Functionally related to these polynomial coefficients are nine
17	geometric parameters: the three ellipsoid semi-axes, its origin location with respect to the current
18	conventional geocentric terrestrial frame, and the three rotations defining its spatial orientation.
19	The final results are compatible with the pioneering work started by Burša in 1970 and, lately, by
20	a recent publication by Panou and colleagues in that incorporates updated geoid models.
21	

Keywords: triaxial ellipsoid fitting; ITRF2014 coordinates; geoid model EGM2008; least-squares
 solution

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- 31

32 Introduction

Leaving aside the convenience or not of adopting a triaxial ellipsoid as a replacement to the two-33 parameter rotational ellipsoid GRS80 presently adopted by the International Association of 34 Geodesy (Moritz 1992), scientists have calculated, using different initial assumptions, the 35 36 parameters of a supposedly best-fitting triaxial earth ellipsoid. Table 1 shows, chronologically, the most recent set of semi-axis values $(\overline{a}, \overline{b}, \overline{c})$ that different authors have published to date to 37 specify the size and shape of a presumed triaxial earth ellipsoid. Krasovsky, also known as 38 Krassovsky and Krasovski, mainly published all his work in Russian. His results of 1902 and 1972, 39 were cited in the English geodetic literature by Zhuravlev (1972) and Geodetic Glossary (1986). 40 The tabulated quantities credited to Eitschberger were recently recounted by Grafarend et al. 41 (2014). Finally, Panou et al. (2020) report a myriad of solutions; their values in Table 1 correspond 42 to the solution derived from the EGM2008 (Earth Gravimetric Earth Model of 2008) geoid model 43 (Pavlis et al. 2012). The final listed triaxial ellipsoid determined by Soler and Han, also based on 44 EGM2008, is presented herein for the first time. 45

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Table 1. Semi-axes of some published triaxial earth ellipsoids

	\overline{a} (m)	\overline{b} (m)	\overline{c} (m)
Krasovsky (1902)	6378250.	6378050.	6356730.
Krasovsky (1972)	6378245.	6378033.	6356863.019

Schliephake (1956)	6378245.	6378032.4	6356863.0
Burša (1970)	6378173.±10	$6378105. \pm 16.21$	$6356754. \pm 10.01$
Eitschberger (1978)	6378173.43	6378103.9	6356754.4
Panou et al.(2020)	6378171.88 ± 0.06	6378102.03 ± 0.06	6356752.24 ± 0.06
Soler and Han (Table 3)	6378187.20 ± 3.97	6378092.31±3.92	6356763.60 ± 3.78

48

It should be mentioned here that triaxial ellipsoids are often used in planetology to 49 represent mathematical models of celestial bodies; e.g., Drummond and Christou (2008), Diaz-50 Toca et al. (2019) where a few examples identifying the corresponding sources are tabulated. 51 52 However, normally only the three semi-axes of the triaxial ellipsoid are provided and rarely do they include attached standard deviations. Notice that in Table 1 only a few lines include 53 54 uncertainties. Incidentally, Burša (1970) provides the semi-major axis (\bar{a}) and two eccentricities $(e \text{ and } e_1)$ with their corresponding standard deviations. These known values were transformed 55 before inserting them in Table 1 after making use of the following well-established conventional 56 formulation: 57

58
$$\overline{b} = \overline{a}\sqrt{1-e^2}$$
 and $\sigma_{\overline{b}}^2 = \left(\frac{\partial\overline{b}}{\partial\overline{a}}\right)^2 \sigma_{\overline{a}}^2 + \left(\frac{\partial\overline{b}}{\partial e^2}\right)^2 \sigma_{e^2}^2 = (1-e^2)\sigma_{\overline{a}}^2 + \frac{\overline{a}^2}{4(1-e^2)}\sigma_{e^2}^2$ (1)

that assumes no correlations between the semi-major axis \bar{a} and eccentricity *e*.

Similar equations apply to the semi-minor axis $\overline{c} = \overline{a}\sqrt{1-e_1^2}$. By the way, these values were revised on several occasions in Burša (1971), Burša and Pícha (1972), Burša and Šíma (1980) and Burša and Fialová (1993). These alternative solutions are tabulated in Panou et al. (2020). However, the differences with respect to his very first determination, considered by most scientists to be the gold standard for the triaxial earth, are not significant in the context of this investigation.

66 Methodology

The methodology describing in detail the mathematical theory executed to achieve the final results presented in this document was recently published in Soler et al. (2020). However, to facilitate the full comprehension of the particulars by the reader, the primary steps contained in the process will be briefly described below to make the narrative self-inclusive:

The original LS mathematical model is the standard quadric polynomial equation
 parameterizing the definition of the surface of a triaxial ellipsoid, namely (see e.g. Bektaş 2014,
 2015; Soler et al. 2020),

74
$$F(x, y, z) = ax^{2} + by^{2} + cz^{2} + 2dxy + 2exz + 2fyz + 2gx + 2hy + 2iz - 1 = 0$$
 (2)

The coefficients *a*, *b*, *c*, ... *i* are the parameters to be solved for, while the (x, y, z) coordinates at each point are the observations to which the triaxial ellipsoid surface is fitted to.

2) Once the polynomial coefficients and their variance-covariance matrix are known they are transformed into the nine geometric constants defining the size and shape of the triaxial ellipsoid, mainly, the three semi-axes $(\overline{a}, \overline{b}, \overline{c})$, the coordinates of the origin of the ellipsoid with respect to the (x, y, z) frame and, finally, the counterclockwise rotations about the three ellipsoid axes (x_E, y_E, z_E) to make it parallel to the terrestrial frame (x, y, z). The complete procedure was unambiguously explained in Soler et al. (2020) following some of the ideas presented in Bektaş (2014).

3) Finally, the variance-covariance (v-c) matrices for the nine ellipsoidal parameters are computed.
This is the most intricate calculation of the three steps. Principally, because it involves the
determination of the v-c matrices of three eigenvalues and six eigenvectors applying the
procedure originally introduced in Soler and van Gelder (1991, 2006) and later expanded and
improved in Han et al. (2007). Considering that the typical reader may not be familiar with the
practical implementation of this process, the mathematical background required to accomplish
this specific goal will be succinctly covered.

91 Recall that as a byproduct of the LS solution, the v-c matrix of the nine polynomial coefficients 92 denoted as $[\Sigma]_{(a,b,c,...,i)}$, is known. With this in mind, the complete solution of the problem is 93 described in the following two subsections.

94

95 Variance-covariance matrix of the origin of the ellipsoid

96 The coordinates of the origin of the ellipsoid can be computed using the following matrix equation97 (Soler et al. 2020):

$$98 \qquad \begin{cases} x_{0} \\ y_{0} \\ z_{0} \end{cases} = -\begin{bmatrix} a & d & e \\ d & b & f \\ e & f & c \end{bmatrix}^{-1} \begin{cases} g \\ h \\ i \end{cases} = \frac{-1}{abc + 2dfe - be^{2} - af^{2} - cd^{2}} \begin{bmatrix} bc - f^{2} & -cd + ef & df - be \\ -cd + ef & ac - e^{2} & -af + de \\ df - be & -af + de & ab - d^{2} \end{bmatrix} \begin{cases} g \\ h \\ i \end{cases}$$
(3)

99 The above equation shows that if the polynomial coefficients g, h, and i are equal to zero 100 in (2) the ellipsoid is centered at the origin of the (x, y, z) reference frame. Otherwise, by standard 101 propagation of errors, one has:

102
$$[\Sigma]_{(x_0,y_0,z_0)} = [J][\Sigma]_{(a,b,c...i)}[J]^T$$
 (4)

103 where the mathematical expression for the Jacobian matrix $\begin{bmatrix} J \\ 3\times 9 \end{bmatrix} = \begin{bmatrix} \frac{\partial(x_0, y_0, z_0)}{\partial(a, b, c...i)} \end{bmatrix}$ was given explicitly 104 in (46) of Soler et al. (2020).

105

106 Variance-covariance matrices of the semi-axes and rotations

107 A symmetric matrix [S] is constructed having the following value:

108
$$[S] = \begin{bmatrix} s_{11} & s_{12} & s_{13} \\ s_{21} & s_{22} & s_{23} \\ s_{31} & s_{32} & s_{33} \end{bmatrix} = -\frac{1}{F(x_0, y_0, z_0)} \begin{bmatrix} a & d & e \\ d & b & f \\ e & f & c \end{bmatrix}$$
 (5)

109 Notice that $F(x_0, y_0, z_0)$ is equal to a scalar that results from particularizing (2) to the 110 coordinates of the origin of the ellipsoid (thus, it is also a function of variables *a*, *b*, *c*,*i*). Thus, 111 one can immediately arrange the six distinct elements of the symmetric matrix [*S*] as a column 112 vector, essentially:

113
$$\begin{cases} s_{11} \\ s_{22} \\ s_{33} \\ s_{21} \\ s_{31} \\ s_{32} \end{cases} = -\frac{1}{F(x_0, y_0, z_0)} \begin{cases} a \\ b \\ c \\ d \\ e \\ f \end{cases} = \begin{cases} F_1(a, b, c, ..., i) \\ F_2(a, b, c, ..., i) \\ F_3(a, b, c, ..., i) \\ F_4(a, b, c, ..., i) \\ F_5(a, b, c, ..., i) \\ F_6(a, b, c, ..., i) \end{cases}$$
(6)

114 The v-c matrix of these six elements can be obtained by calculating the following matrix equation:

115
$$[\Sigma]_{(s_{11},s_{22},...,s_{32})} = [J]]\Sigma]_{(a,b,c,...,i)}[J]^T$$
 (7)

116 where the Jacobian
$$\begin{bmatrix} J \\ 6\times9 \end{bmatrix} = \begin{bmatrix} \frac{\partial(F_1, F_2, \dots, F_6)}{\partial(a, b, c, \dots, i)} \end{bmatrix}$$
 computed from (6) was given explicitly by (52) in

By eigen-decomposition theory, the symmetric matrix [*S*] takes the form:

119
$$[S] = [E]^T [\Lambda] [E]$$
 (8)

120 where

121
$$[E] = \begin{bmatrix} \vec{e}_1 \\ \vec{e}_2 \\ \vec{e}_3 \end{bmatrix} = \begin{bmatrix} e_{11} & e_{12} & e_{13} \\ e_{21} & e_{22} & e_{23} \\ e_{31} & e_{32} & e_{33} \end{bmatrix}$$
(9)

122 contains the three eigenvectors (row vectors) and $[\Lambda]$ is the diagonal matrix

123
$$[\Lambda] = \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix}$$
(10)

where λ_1, λ_2 and λ_3 are the three eigenvalues of the matrix [*S*]. Then, the three semi-axes of the triaxial ellipsoid are defined by the equations:

126
$$\overline{a} = \frac{1}{\sqrt{\lambda_1}}, \ \overline{b} = \frac{1}{\sqrt{\lambda_2}}, \ \overline{c} = \frac{1}{\sqrt{\lambda_3}}$$
 (11)

Furthermore, the three rotation (counterclockwise positive) angles, respectively around the semi-major, semi-middle and semi-minor axes, are computed as a function of the eigenvectors using the expressions:

130
$$\varepsilon_1 = \tan^{-1}\left(\frac{-e_{32}}{e_{33}}\right), \quad \varepsilon_2 = \sin^{-1}\left(e_{31}\right), \quad \varepsilon_3 = \tan^{-1}\left(\frac{-e_{21}}{e_{11}}\right)$$
 (12)

131 The v-c matrix of the eigenvalues and eigenvectors of a 3×3 symmetric matrix such as [S] 132 will be denoted here as $[\Sigma]_{(\lambda_1, \lambda_2, \lambda_3, vec[E])}$ where $vec[E] = \{e_{11}, e_{21}, e_{31}, \dots, e_{33}\}^T$ or explicitly:

133
$$[\Sigma]_{(\lambda_1,\lambda_2,\lambda_3,vec[E])} = \begin{bmatrix} [\Sigma]_{(\lambda_1,\lambda_2,\lambda_3)} & [\bullet] \\ 3\times3 & \\ & \\ \hline \begin{bmatrix} \bullet \end{bmatrix}_{g\times3}^T & [\Sigma]_{(e_{11},e_{21},e_{31},\dots,e_{33})} \end{bmatrix}$$

Note that this is a full symmetric matrix that contains the variances of the eigenvalues and eigenvectors along the diagonal, the covariances of the eigenvalues and eigenvectors (nondiagonal elements on the 3×3 and 9×9 diagonal blocks) and the cross-covariances of the eigenvalues and eigenvectors (non-diagonal blocks). For the purpose of this investigation, only the variances of the eigenvalues and eigenvectors are of interest.

The analytical way of how to compute the variance-covariance matrix of the eigenvalues and eigenvectors of a general 3×3 symmetric matrix, to the authors' knowledge, was first shown in Soler and van Gelder (1991, 2006) and later extended and enhanced in Han et al. (2007). This sought-after objective is accomplished through the following propagation of the error matrix equation

146
$$[\Sigma]_{(\lambda_1,\lambda_2,\lambda_3,vec[E])} = [K][\Sigma]_{(s_{11},s_{22},...,s_{32})}[K]^T$$
 (14)

147 where

149 The symbol \otimes denotes the Kronecker Product, defined by $[A] \otimes [B] = [a_{ij}[B]]$ if $[A] = [a_{ij}]$. The 150 symbol \Box denotes the Khatri–Rao product defined by $[A] \Box [B] = [A_1 \otimes B_1, \dots, A_p \otimes B_p]$ if $[A_j]$ 151 and $[B_j]$ ($j = 1, \dots, p$) are (column) partitioned matrices of [A] and [B], respectively (see Rao & 152 Mitra 1971, pp. 12–13 and the illustration in the Appendix). The matrices $[D_E]$, $[D_S]$ and $[D_\Omega]$ were 153 explicitly given in Han et al. (2007) as

156 Once the values of the v-c matrix of eigenvalues and eigenvectors $\sum_{(\lambda_1, \lambda_2, \lambda_3, vec[E])}$ is known, the

157 final v-c matrices of the semi-axes and rotations is given by

158
$$\sum_{6\times6} \sum_{(\bar{a},\bar{b},\bar{c},\varepsilon_1,\varepsilon_2,\varepsilon_3)} = \begin{bmatrix} \mathbf{J} \\ \mathbf{J} \end{bmatrix} \sum_{12\times12} \sum_{(\lambda_1,\lambda_2,\lambda_3,vec[E])} \begin{bmatrix} \mathbf{J} \\ \mathbf{J} \end{bmatrix}^T$$
(17)

159 and

$$\mathbf{160} \qquad \begin{bmatrix} \mathbf{J} \\ \mathbf{J} \end{bmatrix} = \frac{\partial(\overline{a}, \overline{b}, \overline{c}, \varepsilon_{1}, \varepsilon_{2}, \varepsilon_{3})}{\partial(\lambda_{1}, \lambda_{2}, \lambda_{3}, \operatorname{vec}[E])} = \begin{bmatrix} \frac{\partial\overline{a}}{\partial\lambda_{2}} & \frac{\partial\overline{a}}{\partial\lambda_{3}} & \frac{\partial\overline{a}}{\partial\epsilon_{11}} & \frac{\partial\overline{a}}{\partial\epsilon_{21}} & \frac{\partial\overline{a}}{\partial\epsilon_{21}} & \frac{\partial\overline{a}}{\partial\epsilon_{21}} & \frac{\partial\overline{a}}{\partial\epsilon_{22}} & \frac{\partial\overline{a}}{\partial\epsilon_{22}} & \frac{\partial\overline{a}}{\partial\epsilon_{23}} & \frac{\partial\overline{a}}{\partial\epsilon_{23}} & \frac{\partial\overline{a}}{\partial\epsilon_{33}} \\ \frac{\partial\overline{b}}{\partial\lambda_{1}} & \frac{\partial\overline{b}}{\partial\lambda_{2}} & \frac{\partial\overline{b}}{\partial\lambda_{3}} & \frac{\partial\overline{b}}{\partial\epsilon_{11}} & \frac{\partial\overline{b}}{\partial\epsilon_{21}} & \frac{\partial\overline{b}}{\partial\epsilon_{21}} & \frac{\partial\overline{b}}{\partial\epsilon_{22}} & \frac{\partial\overline{b}}{\partial\epsilon_{22}} & \frac{\partial\overline{b}}{\partial\epsilon_{22}} & \frac{\partial\overline{b}}{\partial\epsilon_{22}} & \frac{\partial\overline{b}}{\partial\epsilon_{23}} & \frac{\partial\overline{b}}{\partial\epsilon_{23}} & \frac{\partial\overline{b}}{\partial\epsilon_{23}} \\ \frac{\partial\overline{b}}{\partial\lambda_{1}} & \frac{\partial\overline{b}}{\partial\lambda_{2}} & \frac{\partial\overline{c}}{\partial\lambda_{3}} & \frac{\partial\overline{c}}{\partial\epsilon_{11}} & \frac{\partial\overline{c}}{\partial\epsilon_{21}} & \frac{\partial\overline{c}}{\partial\epsilon_{21}} & \frac{\partial\overline{c}}{\partial\epsilon_{22}} & \frac{\partial\overline{c}}{\partial\epsilon_{22}} & \frac{\partial\overline{c}}{\partial\epsilon_{23}} & \frac{$$

162 It should be noted that the nonlinearity of any LS process could always be a concern if a rigorous 163 estimation is anticipated. Several authors have treated this topic at length (Teunissen 1989). The 164 formulation to determine the degree of approximation involved depends on the second partial 165 derivative of the design matrix. Using the values already published in our previous paper (Soler et

166 al. 2020) it is immediately seen that
$$\frac{\partial^2 F}{\partial \{x\}^2}\Big|_{\{x\}_0,\{l\}_0} = \begin{bmatrix} 0\\ n \times 9 \end{bmatrix}$$
. Consequently, the linearized first order

167 approximation invoked in our LS solution is necessary and sufficient.

Summarizing, equations (3), (11) and (12) solve for the sought after nine triaxial ellipsoid parameters as a function of the values of the polynomial coefficients *a*, *b*, *c*, ..., *i* which are the unknowns in the least-squares solution processing. The variance-covariance matrices of the ellipsoidal parameters are obtained, respectively by (4), and (17) all of them derived directly from the value of $[\Sigma]_{(a,b,c,...,i)}$ computed originally from the LS procedure and the intermediate equations (7) and (14).

By the way, equations (14) and (15) provide the solution for obtaining the full variancecovariance matrix of the eigenvalues and eigenvectors of any 3×3 symmetric matrix which is given on its general form by (13).

Here is a final note related to this topic. A recent publication by Panou and Agatza Balodimou (2020) elaborates on the advantages and disadvantages of the direct versus indirect (the

one proposed herein) methodologies to estimate the variance-covariance of the parameters 179 involved in the fitting of a triaxial ellipsoid. As we related in this work and in our previous 180 publication (Soler et al. 2020), our main intent was to explain in detail to the reader how to compute 181 the v-c matrix of the eigenvalues and eigenvectors of a 3×3 symmetric matrix. As far as the authors 182 are aware of, this operation is impossible to be performed without introducing the Kronecker and 183 Khatri-Rao products, which, by the way, are an important part of the matrix algebra arsenal. 184 Furthermore, although the correlations between eigenvalues and eigenvectors is determined, the 185 authors, nevertheless, concur with Panou and Agatza-Balodimou (2020) that the full set of 186 correlations between the different parameters of the triaxial ellipsoid cannot be estimated through 187 our step-by-step indirect procedure. To obtain the correlations between shifts and semi-axes and 188 rotations one needs to use their direct approach. 189

190 Data used in the calculations

The original data are the Cartesian coordinates of the ITRF2014 geodetic stations and their corresponding standard deviations that were extracted from the Software INdependent EXchange Format (SINEX) files (IERS Message 103 2006) of the latest solutions disseminated by the IERS (International Earth Rotation and Reference Systems Service; see Altamimi et al. 2016). This information was used to obtain the values of the Cartesian coordinates along the ellipsoid height on the surface of the EGM2008 geoid model (Pavlis et al. 2012) according to the schematic illustration depicted in Fig. 1.



Fig. 1. Graphic relationship between different geodetic parameters

The triaxial ellipsoid is actually fitted to a cluster of $(x, y, z)_G$ coordinates, which in the example 201 shown in Fig. 1 corresponds to the point of intersection between the ellipsoid height h and the 202 geoid model EGM2008. Notice that the standard assumption $h \approx N + H$ was introduced. 203 According to Fig. 1 one can write: 204

Note the distinction between 3D coordinates of points referred to the ITRF2014 frame such as $(x, y, z)_G$ and coordinates of the stations belonging to the definition of the ITRF2014 frame: $(x, y, z)_{ITRF2014}$ (Altamimi et al. 2016).

In the above equation the value of *h* is rigorously known with respect to the GRS80 ellipsoid. On the other hand, the value of *N* could also be computed, at a certain level of accuracy, using the EGM2008 geoid model. In any event, the only errors affecting this "reduction" of the $(x, y, z)_{ITRF2014}$ coordinates to the value of $(x, y, z)_G$ on the surface of the geoid model are contained along the geodetic height and are mainly caused by the uncertainty on the value of *N*. Smaller errors, not affecting the final results, are introduced by the assumption that $h \approx N + H$

The 3D coordinates defining the ITRF20014 frame (Altamimi et al. 2016) which was initially 215 used in this investigation, resulted from an accurate, up-to-date combination of four geospatial 216 techniques: VLBI (Very Long Baseline Interferometry, Bachmann et al. 1915), GNSS (Global 217 218 Navigation Satellite System, Rebischung et al 2016, SLR (Satellite Laser Ranging, Luceri and Pavlis (2016), and DORIS (Doppler Orbitography and Radiopositioning Integrated by Satellite, 219 Moreaux et al. (2016). Thus, it should be considered the leading edge on the determination of 220 accurate 3D geocentric Cartesian coordinates at a certain number of geodetic stations around the 221 globe. From these sets of coordinates the values of $(x, y, z)_G$, see Fig. 1, "reduced" (downward 222 continued) to the geoid were computed and used as available observations to which the sought 223 triaxial ellipsoid was fitted. 224

The $(x, y, z)_{ITRF2014}$ coordinate data set was downloaded from the ITRF Website at the following URL address: http://itrf.ensg.ign.fr/ ITRF_solutions/2014/ITRF2014_files.php. All coordinates refer to the 2010.0027 epoch. The undulations of the EGM2008 geoid model, without accompanied statistics, were interactively accessible at the following Web platform with URL: https://geographiclib.sourceforge.io/cgi-bin/GeoidEval?input=39.35+-74.41666&option=Submit

230

232 Least Squares (LS) Solutions

Among all LS minimization options described in Soler et al. (2020) the so-called "general LS 233 solution" was the strategy selected for the reasons outlined in that publication. It must be stressed 234 that this sort of solution is based on a mathematical model, which is an implicit function of 235 unknowns and observations schematically written as F(X,L) = 0. However, the reader should be 236 aware that in the specialized literature dedicated to the theory of least-squares, this functional 237 relationship receives other names as, for example, "mixed adjustment model" in Leick et al. (2015). 238 239 The unknowns X in this particular instance are the nine coefficients of equation (2) defining the quadric surface of the fitted triaxial ellipsoid, while the observations L is the set of 3D $(x, y, z)_G$ 240 coordinates, which are also referred to the ITRF2014 frame although they are not part of the IERS 241 ITRF2014 solution. Following the account in the methodology section presented previously, once 242 243 the nine coefficients of the polynomial are known one is able to determine, using several sequential algebraic steps described previously, the corresponding nine parameters that fully define the 244 triaxial ellipsoid in space, that is: three semi-axes $(\overline{a}, \overline{b}, \overline{c})$, the three shifts of its origin with respect 245 to the ITRF2014 terrestrial frame (x_0, y_0, z_0) and, finally, the positive counterclockwise rotations 246 $(\varepsilon_1, \varepsilon_2, \varepsilon_3)$ about a Cartesian frame initially coinciding with the semi-axes of the ellipsoid that is 247 rotated to attain parallelism with the geocentric terrestrial frame. Lastly, after implementing a 248 propagation of errors strategy explained in the section Methodology, their associated statistics for 249 these nine parameters are also estimated. 250

251

252 LS solution fundamentals

Figure 2 depicts with dots the location of stations around the globe involved in the definition of the ITRF2014 frame. In contrast, denoted with small circles are shown the 1163 stations participating in the LS solution. This selected number of stations was used because the accurate errors of the geoid heights around the planet are not well-known; therefore, an upper limit for Hwas established and only stations with values of H < 500 m were used. This specific cutoff value was chosen to eliminate possible unknown errors on the modeled undulations of the geoid in

mountainous regions were, by obvious reasons, it is more difficult to produce rigorous values of 259 the geoid height. At the same time, the greater the value of H is, the larger the error that may disturb 260 the approximation $h \approx N + H$ on account of the unpredictability of the curvature of the plumb line. 261 Nonetheless, notice from Fig. 2 that an adequate coverage of ITRF2014 stations with the restriction 262 H < 500 is scattered around the earth and dispersed to a great extent among the four quadrants of 263 the planet. It should be emphasized once more that no values of the undulations of the EGM2008 264 geoid model were used as observations, although the knowledge of N at each station was required 265 as an intermediate quantity to determine the 3D coordinates $(x, y, z)_G$, the actual observables to 266 which the triaxial ellipsoid was fitted to. Precisely, this fact certainly makes the procedure 267 implemented in this article to be markedly different to any other previous investigation that 268 attempted to unravel the characteristics of the best triaxial ellipsoid parameters of an earth model. 269 In the experiment elaborated here, the only errors in the position of the 3D points are counted along 270 the geodetic height mainly due to uncertainties on the undulations, otherwise, the position of the 271 coordinates of the observables in space are as rigorous as feasible. 272



Fig. 2. Geographic distributions of the 1163 geodetic stations (H < 500 m) on the surface of the geoid used in the LS solution

Recall that the values of (λ, φ) shown in Fig. 1 are rigorously known with respect to the GRS80 reference ellipsoid, and with *H* they are merely used to determine the values of the coordinates $(x, y, z)_G$ in space. Once all ITRF20014 selected station was corrected by the displacement in Cartesian coordinates caused by the reduction to the geoid (see Fig. 1) and the coordinates $(x, y, z)_G$ were known, the LS procedure described above was implemented.



Fig. 3. Plot of the residuals (v_x, v_y, v_z) from the LS solution for the $(x, y, z)_G$ coordinates





Fig. 4. Plot of the residuals along the local geodetic frame (v_E, v_N, v_U)

285 The least-squares residual plots pertaining to each one of the used stations are available in Fig. 3, where it is clearly shown that all the residuals along the x, y, and z components is always 286 between ± 100 m. Figure 4 shows the representation of the residuals of Fig. 3 transformed into the 287 local (topocentric) geodetic: frame east, north, up (not shown in Fig. 1). This plot was created to 288 approximately visualize the magnitude of the residuals along the geodetic height (up) component 289 by implementing the well-known equation: 290

291
$$\begin{cases} v_E \\ v_N \\ v_U \end{cases} = \begin{bmatrix} -\sin\lambda & \cos\lambda & 0 \\ -\cos\lambda\sin\varphi & -\sin\lambda\sin\varphi & \cos\varphi \\ \cos\lambda\cos\varphi & \sin\lambda\cos\varphi & \sin\varphi \end{bmatrix} \begin{cases} v_x \\ v_y \\ v_z \end{cases}$$
(20)

292 As expected, the conversion of residuals from Cartesian to curvilinear coordinates shows that the geodetic height residual along the local frame v_{μ} obviously presents the maximum scatter 293 of the three residual components (v_E, v_N, v_U) . Having said that, observe that according to Fig. 4, 294 the resultant standard deviation of about 20 m for v_{U} definitely exhibits a reasonable triaxial 295 ellipsoid fitting to the cluster of generated three-dimensional points $(x, y, z)_G$. 296

297

298 **Results from the LS solutions**

Table 2 presents the estimates of the nine coefficients of equation (2) resulting from the LS solution using the set of coordinates $(x, y, z)_G$ as observations with their corresponding standard deviations. The statistics in Table 2 resulted directly from the LS process and the assumption of a diagonal weight matrix extracted from the ITRF2014 SINEX file.

Parameters	Estimates [×10 ⁻¹³]
а	$0.24581357 \pm 0.00000016$
b	$0.24582046 \pm 0.00000014$
С	$0.24747303 \pm 0.00000015$
d	$0.00000124 \pm 0.00000010$
е	$-0.00000067 \pm 0.00000010$
f	$-0.00000119 \pm 0.00000010$
g	$-0.50342905 \pm 0.34889404$
h	$0.74081758 \pm 0.34570154$
i	$-1.86086692 \pm 0.32974988$
Root-mean-squared distances (m)	20.1977

Table 2. Estimates of the parameters of the quadric equation of the fitted triaxial ellipsoid

Because the coefficients in Table 2 are difficult to interpret geometrically, the following 306 step was to transform them into the parameters shown in Table 3 after following the algebraic 307 operations described in the Methodology section. This table presents in column arrangement the 308 resultant nine spatial parameters defining the geometric characteristics (see Fig. 5) of the triaxial 309 ellipsoid mainly: the three shifts of the origin (x_0, y_0, z_0) , three semi-axes $(\overline{a}, \overline{b}, \overline{c})$, and the three 310 rotations $(\varepsilon_1, \varepsilon_2, \varepsilon_3)$ with accompanying standard deviations. The column on the left contains the 311 results obtained from this investigation. The middle column tabulates the results published in 312 313 Panou et al. (2020), and finally, the column on the right shows the original values reported by Burša (1970). The standard deviations in Table 3 resulted after a step-by-step procedure following 314 a conventional propagation of errors strategy. 315



Parameters	This study	Panou et al.	<mark>Burša</mark> Ellipsoid
$x_0(m)$	-2.05 ± 1.42		0
$y_0(\mathbf{m})$	3.01 ± 1.41		0
$z_0(m)$	7.52 ± 1.32		0
$\overline{a}(\mathbf{m})$	6378187.20 ± 3.97	6378171.88 ± 0.06	6378173.00 ± 10.00
\overline{b} (m)	6378092.31 ± 3.92	6378102.03 ± 0.06	6378105.15 ± 16.21
\overline{c} (m)	6356763.60 ± 3.78	6356752.24 ± 0.06	6356754.36 ± 10.01
$\mathcal{E}_1({}^0)$	-0.0447 ± 0.0035		0
$\mathcal{E}_2({}^0)$	0.0157 ± 0.0034		0
$\mathcal{E}_3({}^0)$	9.8894 ± 0.7059	14.9356740±0.0000005W	$14.8\pm5W$

Table 3. Ellipsoidal parameters $(\pm 1 \sigma)$ derived from the coefficients in Table 2

322

323 Several conclusions could be inferred from the tabulated values. In what follows, they are going324 to be analyzed in order of their level of importance.

1) Semi-axes of the triaxial ellipsoid $(\overline{a}, \overline{b}, \overline{c})$. Obviously, the three most important parameters of 325 the fitted triaxial ellipsoid are the semi-axes. Our results show good consistency with the values 326 previously published by Burša (1970), which are almost identical to the results recently made 327 available by Panou et al. (2020). In this respect, it should be pointed out that the conceptual 328 methodology used by Burša and Panou et al. is very similar except that the latter incorporated 329 into their calculations contemporary geoid models. Keeping this in mind is not surprising that 330 they reached similar results. However, the procedure implemented here departs from the other 331 two because instead of using geoid undulations as observations Cartesian coordinates directly 332 derived from the latest IERS solution: ITRF2014 were employed. Nevertheless, as the reader 333

can attest, the answers are sufficiently close to considering them physically plausible. Perhaps 334 it could be speculated that the detected reasonable discrepancies are mainly caused by the 335 variants in methodology introduced in this research for determining the best fitting triaxial 336 ellipsoid. Among all geoid models used by Panou et al. (2020), the comparisons should 337 concentrate on their solution "D2.1, G-T6 I" that best fit the triaxial ellipsoid to the EGM2008 338 geoid model undulations which is the model used in our investigation. If one contrasts the last 339 two results in Table 1, both reinforced by cutting-edge geospatial data-bases and modern 340 advances in digital and computational software, one finds the following differences (Soler and 341 Han minus Panou et al.): $\delta \overline{a} = 15.32$ m; $\delta \overline{b} = -9.72$ m; and $\delta \overline{c} = 11.36$ m. In the authors' 342 opinion, these differences should not be considered significant amid the complexity of the 343 problem at hand and merely convey the distinct methodologies between the two procedures. 344 The results of this investigation produces a triaxial ellipsoid which shape has slightly less 345 rotational symmetry and polar flattening that the one from Panou et al. (2020). Perhaps with 346 more optimum symmetric global coverage of ITRF2014 stations, our results could be improved 347 further and better approximation, or not, to those of Panou et al. (2020) and Burša could be 348 validated. However, at present, this is merely a postulated hypothesis difficult to be confirmed 349 until more station coordinates data becomes available. 350

Finally, it is important to emphasize at this juncture that Burša's values were not used as initial approximations at any stage of the least-squares process. The original approximations of the parameters of the coefficients in equation (2) were set to zero during the first iteration.

2) Rotation angles $(\varepsilon_1, \varepsilon_2, \varepsilon_3)$. The second main resultant product to the fitting of a cluster of 3D 354 points $(x, y, z)_G$ to a quadric surface, in particular a triaxial ellipsoid, is the spatial orientation 355 of the ellipsoid such as the general example depicted in Fig. 5. The ellipsoid in question is 356 randomly located in space, having its center (CE), generally speaking, not coinciding with the 357 origin of the (x, y, z) terrestrial frame and with its coordinate axes (x_E, y_E, z_E) initially aligned 358 with the three semi-axes also arbitrarily oriented in space (see Fig. 5). The precise spatial 359 position of the ellipsoid is facilitated by the knowledge of the values of three rotations (positive 360 counterclockwise) denoted $(\varepsilon_1, \varepsilon_2, \varepsilon_3)$ respectively performed around the three Cartesian axes of 361

the frame (x_E, y_E, z_E) . Notice that these rotations are passive rotations (Soler 2018) meaning that 362 the axes rotate and the ellipsoid remains fixed in space. The rotations by amounts $(\varepsilon_1, \varepsilon_2, \varepsilon_3)$ 363 about the axes (x_E, y_E, z_E) are performed until they achieve a position of parallelism with 364 respect to the geocentric (x, y, z) terrestrial frame. These three rotations will physically 365 determine the orientation of the semi-axes in space. The values of these rotations are calculated 366 as a function of the unequivocal components of the eigenvectors using equations. (12). For 367 example, the rotation about the third axis is $\mathcal{E}_3 = 9.8894^0 \pm 0.7059^0$. Because this is a 368 counterclockwise rotation around the z_E axis after achieving parallelism with the (x, y, z)369 geocentric frame, it means that the \overline{a} axis (which, as mentioned before, is fixed with the 370 ellipsoid in space) is located approximately at an angle of 9.8894° in a direction opposite to the 371 rotation, that is, west of the $//x_E$ axis. The same logic could be applied to understand the 372 physical meaning of the other two rotations ε_2 and ε_3 . 373

3) Coordinates of the center of the ellipsoid (x_0, y_0, z_0) . As Fig. 5 shows, in general, the center of 374 the ellipsoid (CE) should not necessarily coincide, in a LS sense, with the origin of the frame 375 defined by the cluster of $(x, y, z)_G$ points. It must be stressed here that in Burša (1970) was 376 implicitly assumed that his triaxial ellipsoid was geocentric. Our research also solved for the 377 shifts of the origin of the ellipsoid on the frame defined by the corresponding collection of 378 $(x, y, z)_G$ observations that should be considered a realization of the ITRF2014 frame. As 379 previously explained, these shifts are a byproduct of the solution of the general quadric equation 380 and were determined afterwards through the implementation of equation (3). It is axiomatic to 381 think that the three shifts should be primarily affected by the global symmetry of the 382 observational data. That is, if the set of points $(x, y, z)_G$ was completely symmetric with 383 respect to the origin of the (x, y, z) frame, the origin of the fitted ellipsoid will likely be centered 384 at the origin of the frame. This is perfectly seen in the exercise presented in Soler et al. (2020) 385 where the coordinates of the given points are biased by certain amounts and this is directly 386 reflected on the solution of the shifts. With the set of coordinates at our disposal in the present 387 case, from Table 3 one gets the following ellipsoid center displacements: $x_0 = -2.05 \text{ m} \pm 1.42$ 388

m; $y_0 = 3.01 \text{ m} \pm 1.41 \text{ m}$; $z_0 = 7.52 \text{ m} \pm 1.32 \text{ m}$. This appears to indicate that the distribution of points between the northern and southern hemispheres is distinctively more asymmetric than any other distribution. For example, to clarify this concept, a geoid which figure is slightly pearshaped in the north-south direction will conceivably support a non-geocentricity shift along the z component. It is not simply that the norther hemisphere may have more stations than the southern hemisphere as Fig. 1 appears to indicate but that, overall, the geoid heights on the northern hemisphere are slightly larger than the ones in the southern hemisphere.

396

397 LS with ellipsoid shifts constrained to zero

Considering that the values of the shifts could be easily constrained to zero, an alternative LS solution was implemented, forcing the values of (x_0, y_0, z_0) to zero. This is readily done by assuring that in equation (2) g = h = i = 0. The results of this constrained adjustment are presented in Tables 401 4 and 5. The asterisks in both tables indicate that the corresponding parameters were constrained 402 to zero.

403

404 **Table 4.** Parameter estimates using the ITRF2014 stations for the case of constraining

405

Parameters	Estimates [×10 ⁻¹³]
а	$0.24581350 \pm 0.00000016$
b	$0.24582049 \pm 0.00000014$
С	$0.24747249 \pm 0.00000011$
d	$0.00000115 \pm 0.00000010$
е	$-0.00000062 \pm 0.00000008$

g = h = i = 0

f	$-0.00000125 \pm 0.00000008$	
g	0*	
h	0*	
i	0*	
Root-mean-squared distances (m)	20.2915	

Table 5. Ellipsoidal parameters $(\pm 1 \sigma)$ derived from the constrained solutions in Table 3

Parameters	This study	<mark>Burša</mark> Ellipsoid
$x_0(m)$	$0.0000 \pm 0.0000*$	0
$y_0(\mathbf{m})$	$0.0000 \pm 0.0000*$	0
$Z_0(\mathbf{m})$	$0.0000 \pm 0.0000*$	0
$\overline{a}(\mathbf{m})$	6378187.7495 ± 3.9840	6378173.0000 ± 10.0000
\overline{b} (m)	6378092.2282 ± 3.7801	6378105.1518 ± 16.2088
\overline{c} (m)	6356770.5975 ± 2.8694	6356754.3618 ± 10.0125
$\mathcal{E}_1({}^0)$	-0.0461 ± 0.0028	0
$\mathcal{E}_2({}^0)$	0.0143 ± 0.0027	0
$\mathcal{E}_{3}(^{0})$	9.1338 ± 0.7083	$14.8\ensuremath{^{\scriptscriptstyle 0}}\xspace\pm5\ensuremath{^{\scriptscriptstyle 0}}\xspace$ W

The resulting values forcing the shifts of the origin of the ellipsoid to zero are presented in 409 columns form in Tables 5 and 6 using the same format that the unconstrained case. Furthermore, 410 the results of this constrained LS adjustment solution unequivocally show a slight increase on the 411 root-mean-squared distance from the observation points to the surface of the fitted ellipsoid. This 412 may indicate that the observations do not fit the model as well when the ellipsoid is forced to be 413 geocentric. Thus, it can be inferred that the best triaxial earth ellipsoid fitted to the observed 414 geospatial data at locations on the geoid is not necessarily geocentric. Indeed, although the shifts 415 are not significantly large, the change in position of the ellipsoid also generates small changes in 416 its orientation. The semi-axes remain practically unchanged, they are actually (constrained minus 417 unconstrained): $\delta \overline{a} = 0.45$ m; $\delta \overline{b} = -0.10$ m; and $\delta \overline{c} = 7.00$ m. Except for the semi-minor axis \overline{c} 418 which absorbs a change of about 7m away from the Burša value to compensate for constraining 419 the ellipsoid to be geocentric thus eliminating a shift of about 7m along the third axis. This 420 corroborates that the values of the coordinates used are very accurate whereas imposing the 421 geocentricity of the ellipsoid will not fit equally well the observations and gives the worst value 422 for the third semi-minor axis. In conclusion, the results obtained by the general LS adjustment 423 hints to an earth's best fitting triaxial ellipsoid that is not perfectly geocentric. 424

Additionally, after imposing the triaxial ellipsoid to be geocentric, and implementing the LS constrained solution, the rotation angle about the third axis does not change by much. This confirms, somewhat, that the semi-major axis of the best fitting triaxial ellipsoid to the irregular undulating surface of the geoid is located, approximately, parallel to the *x*-*y* plane, shifted by about 7m from the origin of the terrestrial frame at an angle of about 10 degrees of longitude west from the zero-meridian.

431

432 Rotations attributes

Under the assumption that the general unconstrained LS solution, as listed in Table 3, is more realistic than the one fixing to zero the coordinates of the origin of the ellipsoid, a few words will be said about the rotation results. Burša (1970) is credited with calculating, for the first time, as a function of the earth's spherical harmonics derived from early satellite observations the orientation of the equatorial semi-major axis of a triaxial best-fitting ellipsoid. From this dynamical solution, he obtained a value for the longitude of the semi-major axis of $-14.8^{\circ} \pm 5^{\circ} \equiv 14.8^{\circ} W \pm 5^{\circ}$. Later, Burša (1977), reintroduced the following equations borrowed from Darwing (1877) giving the rotations about the three axes according to the equations:

441
$$\delta \alpha_1 = \frac{D}{C-B}; \ \delta \alpha_2 = \frac{E}{A-C}; \ \delta \alpha_3 = \frac{F}{B-A}$$
 (22)

where A, B, and C, are the earth's moments of inertia and D, E, and F are its products of inertia. 442 Expressing these values as a function of the best spherical harmonics determined from satellite 443 observations at that time (GEM 5 and GEM 6) Burša arrived at a value of $\delta \alpha_3 = -14.8^{\circ}$. Therefore, 444 he proved that the angle he had previously published roughly coincided with the orientation of the 445 principal semi-major axis of the Earth inertia ellipsoid. Subsequently, other authors corroborated 446 this figure. For example, Soler and Mueller (1978) rigorously solving for the eigenvalues and 447 eigenvectors of the earth's second-rank inertia tensor also determined from satellite observations, 448 the orientation of the earth first principal inertia axis as $\delta \alpha_3 = -14^{\circ} 55^{\circ}$. More recently, following 449 slightly different analytical methods, Groten (2007), Vîlcu (2009), and Chen and Shen (2010) 450 451 reached practically the same conclusions.

The point we are trying to convey here is that all of these longitudinal angular values are 452 referred to the orientation of the earth's first principal inertia axes, and that this is not exactly 453 equivalent to determine the best fitting triaxial ellipsoid to the earth, or more specifically, the best 454 fitting ellipsoid to the EGM2008 geoid model. The principal moments of inertia are affected by 455 the total mass distribution of the earth. The irregular surface of the geoid is also affected by mass 456 distributions; however, there is not any known theory to rigidly tie the physical shape of the geoid 457 (materialized by its undulations) with the earth's major principal axes of inertia. This is an area 458 459 that should be investigated further. Nevertheless, it appears that the semi-major axis of the earth's 460 best fitting terrestrial triaxial ellipsoid is approximately oriented in the same regional area that the earth's major principal axis of inertia, at least the historical research proves that. 461

462 Recapitulating, nobody has yet attempted an investigation along the premises presented in 463 this article where the earth's triaxial ellipsoid is fitted to a collection of Cartesian points accurately located on the ITRF2014 frame. From the values in Table 3 containing the unconstrained solution, it can be deduced that the third axis of the physically fitted ellipsoid will approximately be located at a spherical curvilinear distance of only 4.68 km from the north pole of the ITRF2014 frame along the meridian of longitude 240.6963°. Recall that this axis has only geometric meaning and is not directly related to the instantaneous rotation axis of the earth or its third principal inertia axis.

Actually, because the rotations around the first and second axes are close to zero, the rotation 470 around the third axis comprises an angle of about 10° (in our solution) that can be translated into 471 the plane of the equator of the triaxial ellipsoid. However, the rigorous computation of this angle 472 will require the solution of a spherical triangle (see Appendix II). In Fig. A1, the three positive 473 counterclockwise rotations about their corresponding axis are shown. The figure depicts the last 474 sequence of a rotation \mathcal{E}_2 about the second axis followed by the final rotation \mathcal{E}_3 about the third 475 axis. Notice that, at this point, the axes y_E and z_E have changed the location pictured in the figure. 476 Of our interest is the spherical triangle α drawn in the figure. This is the angle in space between 477 the axis parallel to the geocentric x-axis and the location of the semi-mayor axis \overline{a} of the triaxial 478 ellipsoid. Using standard spherical trigonometry and following the steps outlined in Appendix II 479 (Fig. A2) one reaches the answer $\alpha = 9.8994^{\circ} \approx 10^{\circ}$. Consequently, the true angle that one is after 480 is 9.8994° versus the value of the rotation about the third axis $\mathcal{E}_3 = 9.8894°$ directly determined in 481 482 the least-squares solution of Table 3. The difference between both is so small because the values of the other two rotations \mathcal{E}_1 and \mathcal{E}_2 are very close to zero. Although the result is practically 483 identical, the intention of the authors was to emphasize the rigorous mathematical discrepancy 484 between the two angular solutions considering that this distinction is never treated in all 485 discussions related to the fitting of earth's triaxial ellipsoids. One thing is to resolve the orientation 486 487 of the triaxial ellipsoid in space through the determination of three rotation angles and the other to publish the angle between the semi-major axis with respect to the geocentric (terrestrial) x-axis. 488 Therefore, to mention simply that the semi-major axis is 14° W = -14° is not 100% correct. This 489 assertion is only rigorous if the other two rotation angles are zero, meaning that the semi-minor 490 491 axis of the triaxial ellipsoid is parallel (or coincides) with the third axis of the geocentric frame, a very singular and improbable circumstance. 492

493

494 Conclusions

In this investigation, a set of 3D Cartesian coordinates given in the ITRF2014 frame at geodetic 495 stations located on the surface of the EGM2008 geoid model were used to fit a triaxial ellipsoid 496 after implementing a LS procedure. A trivial scheme was devised to "reduce from terrain to geoid" 497 the coordinates that were primarily based on the computation of orthometric heights (H) from the 498 499 rigorous knowledge of the geodetic height h and the value of the undulation of the geoid N $(H \approx h - N)$. Results comparable to previous investigations dating back about 50 years were 500 reached. However, the procedure developed for the preparation of this work is different from the 501 preceding aforementioned research. While other authors have used the undulations of modeled 502 geoids as observations, our research uses 3D rigorous, up-to-date geospatial-determined Cartesian 503 coordinates as observables. Nevertheless, it should be pointed out that, as in previous 504 investigations, possible errors in the undulations of the geoid models (EGM2008 in our case) may 505 affect the results. Consequently, in this research, an upper bound of H < 500 m was enforced to 506 reduce, as much as feasible, unknown uncertainties on the values of the undulations. Concentrating 507 now on the findings obtained for the best fitting triaxial ellipsoid, the reader is addressed to Table 508 3. The general LS solution gives the following results involving 1163 ITRF2014 stations 509 disseminated around the world: for the three semi-axes: $\bar{a} = 6378187.20 \text{m} \pm 3.97 \text{m}$, $\bar{b} =$ 510 6378092.3m ± 3.92m, $\overline{c} = 6356763.60$ m ± 3.78m; for the three shifts $x_0 = -2.05 \pm 1.42$ m, $y_0 = -2.05 \pm 1.42$ 511 $3.01m \pm 1.41m$, $z_0 = 7.52m \pm 1.32m$; and for the three rotations $\mathcal{E}_1 = -0.0447^\circ \pm 0.0035^\circ$, $\mathcal{E}_2 = -0.0447^\circ \pm 0.0035^\circ$ 512 $0.0157^{\circ} \pm 0.0034^{\circ}, \quad \mathcal{E}_3 = 9.8894^{\circ} \pm 0.7059^{\circ}.$ 513

Because the results might be slightly dependent on the distribution of points on the earth surface, in the future, when some of the geographic regions in Fig. 2 that currently lack ITRF2014 points, e.g. northern Siberia, central Africa, and Antarctica, are filled, the outcomes presented herein could be improved. This enhancement should advance further the scientific knowledge of the best closed mathematical expression of our planet.

It has been found that the entire methodology is founded, at least, on two demanding premises, a general LS solution and a rigorous eigentheory determination of the variance-covariance matrix

of the semi-axes and rotations of the fitted triaxial ellipsoid. As far as the authors' are concerned, 521 no approach scientifically equivalent to the one introduced here has been published or attempted 522 to date. On the contrary, the standard procedure to determine the best earth's triaxial ellipsoid 523 through the years follows the path of the innovative ideas advanced by Burša originally in 1970. 524 Our proposal appears to be a viable alternative but lacks the availability of a denser network of 525 geodetic stations around the world. It is plausible to speculate that in the course of time, this 526 existent weakness will be strengthened and, without any doubt, it can be predicted that much better, 527 528 improved and accurate results could be attained.

529

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533

534 Data Availability

535 Data containing the station coordinates and their standard deviations used in this study were 536 obtained from the SINEX files publicly available at the ITRF web site http://itrf.ensg.ign.fr/ 537 ITRF_solutions/2014/ITRF2014_files.php. Processing logs and result files are available from the 538 corresponding author on reasonable request.

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 6(3): 255-267.
- 625
- 626 <u>Appendix I</u>. A practical example of the Khatri–Rao product

Assume that one wants to compute the following Khatri-Rao product, as it appears in (15),

$$628 \qquad \begin{bmatrix} E \end{bmatrix}^T \Box \quad \begin{bmatrix} E \end{bmatrix}^T \\ _{3\times 3} \qquad _{3\times 3}$$

629 where [E] is the following matrix of eigenvectors:

$$[E] = \begin{bmatrix} e_{11} & e_{12} & e_{13} \\ e_{21} & e_{22} & e_{23} \\ e_{31} & e_{32} & e_{33} \end{bmatrix} \Rightarrow [E]^{T} = \begin{bmatrix} e_{11} & e_{21} & e_{31} \\ e_{12} & e_{22} & e_{32} \\ e_{13} & e_{23} & e_{33} \end{bmatrix} = \begin{bmatrix} e_{11} \\ e_{12} \\ e_{13} \end{bmatrix} \cdot \begin{bmatrix} e_{21} \\ e_{22} \\ e_{23} \end{bmatrix} \cdot \begin{bmatrix} e_{31} \\ e_{32} \\ e_{33} \end{bmatrix}$$
 (A.2)

(A.1)

631 Then, by definition:

$$632 \qquad [E]^{T} \square [E]^{T} = \begin{bmatrix} e_{11} \begin{pmatrix} e_{11} \\ e_{12} \\ e_{13} \end{pmatrix} \begin{pmatrix} e_{21} \\ e_{22} \\ e_{23} \end{pmatrix} \begin{pmatrix} e_{31} \\ e_{32} \\ e_{33} \end{pmatrix} \\ e_{22} \begin{pmatrix} e_{31} \\ e_{22} \\ e_{33} \end{pmatrix} = e_{32} \begin{pmatrix} e_{31} \\ e_{32} \\ e_{33} \end{pmatrix} \\ e_{12} e_{12} e_{22} e_{23} e_{31} e_{32} \\ e_{11} e_{12} e_{22} e_{23} e_{31} e_{32} \\ e_{12} e_{13} e_{22} e_{23} e_{23} e_{23} \\ e_{12} e_{13} e_{22} e_{23} e_{23} \\ e_{12} e_{13} e_{23} e_{22} e_{23} \\ e_{12} e_{13} e_{23} e_{22} e_{23} \\ e_{12} e_{13} e_{23} e_{22} e_{23} \\ e_{12} e_{13} e_{22} e_{23} e_{23} \\ e_{13} e_{11} e_{23} e_{21} e_{33} e_{31} \\ e_{13} e_{12} e_{23} e_{22} e_{33} e_{33} \\ e_{13} e_{12} e_{23} e_{22} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{22} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{23} e_{23} e_{33} \\ e_{13} e_{12} e_{23} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{23} e_{23} e_{33} \\ e_{13} e_{12} e_{23} e_{23} e_{23} e_{33} \\ e_{13} e_{12} e_{23} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{23} e_{23} \\ e_{13} e_{12} e_{23} e_{23} e_{23} \\ e_{13} e_{23}$$

633

Appendix II. Direct angle between the semi-major axis of the fitted triaxial ellipsoid and the //x axis

636 When solving for the orientation of the semi-major axis of the triaxial ellipsoid, the angle that 637 should be reported is not ε_3 but α depicted in the right angle spherical triangle of Fig. A1.



639Fig. A1. Relationship between rotation angles and the angle α between the semi-major axis \overline{a} 640and the $\Box x$ axis

642 According to the well-known Napier's rules (Fig. A2):



Fig. A2. Practical solution of right angle spherical triangles

645
$$sin(middle part) = cos(opposit part) \times cos(opposit part)$$
 (A.4)

646 Consequently,

647
$$\sin\left(\frac{\pi}{2} - \alpha\right) = \cos\varepsilon_2 \times \cos\varepsilon_3 \Longrightarrow \cos\alpha = \cos\varepsilon_2 \times \cos\varepsilon_3$$
 (A.5)

648
$$\alpha = \cos^{-1}(\cos\varepsilon_2 \times \cos\varepsilon_3)$$
 (A.6)

649 And after substituting $\varepsilon_2 = 0.0157^\circ$ and $\varepsilon_3 = 9.8894^\circ$ in equation (A.6) one finally gets the angle 650 between the semi-major axis and the axis //x equal to: $\alpha = 9.8994^\circ \approx 10^\circ$.

651

652 Author Biography



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Tomás Soler holds a Ph.D. from The Ohio State University. He worked at the National Geodetic
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