

Rigorous estimation of local accuracies revisited

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Abstract. New insights about the concept of local accuracies are elaborated in this article. Recently found evidence supports the mathematical rigor of equations previously published in this journal as the unique alternative to rigorously estimate local accuracies. A mathematical algorithm to compute the averaged local accuracies at a point using the full network statistics of a preselected cluster of surrounding points is introduced. The relationship between eigenvalues and eigenvectors of error ellipsoids among different local frames is also addressed.

Introduction

As far as one can determine, the rigorous formulation for the estimation of local accuracies was introduced twenty years ago. “Local” in this context implies that the final variance-covariance (v-c) matrix (or its error ellipsoid) is referred to the local horizon geodetic frame while incorporating statistics (variances and covariances) from nearby points. The intent is clearly to determine, as much as possible, the influence of observational errors inherent to near-by points to

24 the precision and/or accuracy of any other arbitrary survey mark in the network (horizontal, 3D,
25 Global Navigation Satellite System (GNSS) determined, etc.) to which, in the opinion of the
26 authors, they are observationally connected. The first published rigorous treatment of the subject
27 matter was given explicitly, without derivation, in Appendix A by Geomatics Canada (1996,
28 p.19-20). The same set of equations were reproduced verbatim by Craig and Wahl (2003)
29 supporting the same general methodology concept for cadastral applications. A few years later,
30 identical ideas were posted on the Web by Wallace (2009). The same set of rigorous equations
31 has been used by several authors in practical engineering applications (e.g. Marendić et al. 2011;
32 Lee and Seo 2012).

33 However, in a book published by Burkholder (2008), perhaps unaware of the aforementioned
34 references, that author introduces a new approximate approach that is not as rigorous as the
35 original written formulations of local accuracies that were previously available in print. The
36 inaccuracy and limitation of this approximation has been confirmed in Soler and Smith (2010) by
37 introducing a novel independent derivation. The controversy was further cleared and settled in a
38 discussion and closure published in this journal (Burkholder 2012; Soler and Smith 2012).
39 Unfortunately, a recent publication by the same author still overlooked the general scientific
40 consensus and a plethora of earlier established facts and again insisted on a similar
41 approximation (Burkholder 2014). To finally settle this issue, we feel obligated to revisit the
42 subject matter and close this chapter once and for all by introducing new alternative
43 mathematical proofs, supported by easy to understand concepts, corroborating to the reader
44 interested in mathematical veracity that Burkholder's derivation is merely an approximation for
45 computing local accuracies. It is now left to the geospatial engineering community to judge the

46 substance of the two approaches and decide which method is better reinforced by the
47 fundamental principles of theoretical rigor and thoroughness.

48

49 **Theoretical background**

50 Figure 1 depicts two points denoted 1 and 2 on the surface of a preselected reference ellipsoid.

51 To clarify our arguments, it is assumed that the two points are located along the same meridian

52 which is presumed contained on the plane of the paper. This restriction is introduced to

53 illuminate the comprehension of the concepts although this simplification will not affect the final

54 interpretation of results. A current (e.g. GNSS-defined) global terrestrial geocentric frame ($x, y,$

55 z), is assumed at the origin of the ellipsoid (not shown in Fig. 1). At point 1 two local

56 (topocentric) frames have been drawn. A local frame (x_1, y_1, z_1) which is parallel to the global

57 terrestrial geocentric frame is identified at point 1 and would be referred herein as the “local

58 terrestrial frame” at point 1. Similarly, the so-called local horizon geodetic frame (e_1, n_1, u_1) at

59 point 1 is also depicted in the figure. By definition (see e.g. Soler 1988), the direction e points

60 towards the geodetic positive east, n points to the geodetic positive north, and u (up) points to the

61 geodetic zenith, positive up. Notice that all local frames are right-handed; furthermore, it follows

62 from the assumptions mentioned above that the e -axis is perpendicular to the plane of the paper,

63 with positive direction pointing towards the reader, the n -axis is also on the plane of the selected

64 meridian and is tangent to the ellipsoid at the point and the u -axis is normal to the ellipsoid

65 forming a right-handed triad. It should be made clear also that the z -axis is on the plane of the

66 meridian while the y - and z -axes are not.

67 The same logic is applied to point 2 where in a similar way two local frames denoted ($x_2, y_2,$

68 z_2) and (e_2, n_2, u_2) are pictured. Recall that the axes of the local terrestrial frames, by definition,

69 are parallel to the global geocentric frame and thus, to themselves. However, the (e_i, n_i, u_i) , $i = 1,$
70 2, local geodetic frames have different spatial orientation anywhere on the surface of the
71 ellipsoid.

72 It is well-know (e.g. Soler 1988) that the transformation of frames (or its coordinates) between
73 the two described local frames at points 1 and 2 follows immediately from:

$$74 \quad (x_1, y_1, z_1) \begin{matrix} \xrightarrow{R_1} \\ \xleftarrow{R_1^T} \end{matrix} (e_1, n_1, u_1) : \begin{matrix} \left\{ e_1 \right\} \\ \left\{ n_1 \right\} \\ \left\{ u_1 \right\} \end{matrix} = R_1 \begin{matrix} \left\{ x_1 \right\} \\ \left\{ y_1 \right\} \\ \left\{ z_1 \right\} \end{matrix} \quad (1)$$

$$75 \quad (x_2, y_2, z_2) \begin{matrix} \xrightarrow{R_2} \\ \xleftarrow{R_2^T} \end{matrix} (e_2, n_2, u_2) : \begin{matrix} \left\{ e_2 \right\} \\ \left\{ n_2 \right\} \\ \left\{ u_2 \right\} \end{matrix} = R_2 \begin{matrix} \left\{ x_2 \right\} \\ \left\{ y_2 \right\} \\ \left\{ z_2 \right\} \end{matrix} \quad (2)$$

76 where the symbol T indicates matrix transpose. The orthogonal matrix that rotates the local
77 terrestrial frame into the local horizon geodetic frame at any point i can be written explicitly as
78 (see e.g. Soler 1976):

$$79 \quad R_i = \begin{bmatrix} -\sin \lambda & \cos \lambda & 0 \\ -\cos \lambda \sin \varphi & -\sin \lambda \sin \varphi & \cos \varphi \\ \cos \lambda \cos \varphi & \sin \lambda \cos \varphi & \sin \varphi \end{bmatrix}_i ; i = 1, 2 \quad (3)$$

80 With this information, it can be proved that the variance covariance matrix (v-c) of the local
81 horizon geodetic frame (e_i, n_i, u_i) determined as a function of the v-c matrix of the local
82 terrestrial frame (x_1, y_1, z_1) can be written as (Soler and Smith 2010):

$$83 \quad \Sigma_{(e_1, n_1, u_1)} = R_1 \Sigma_{(x_1, y_1, z_1)} R_1^T \quad (4)$$

84 and similarly at point 2:

$$85 \quad \Sigma_{(e_2, n_2, u_2)} = R_2 \Sigma_{(x_2, y_2, z_2)} R_2^T \quad (5)$$

86 The local accuracies are also referred to in the geodetic-surveying literature as an average of
 87 some set of relative accuracies. However, to avoid any possible confusion, in this article one is
 88 going to restrict the name of relative local accuracies to the ones referred only to the (x, y, z)
 89 frame leaving the nomenclature of “local accuracies” exclusively to the relative accuracies
 90 referred to the local geodetic frames (e, n, u) .

91 Let us propagate errors to the basic equation defining the concept of relative local accuracies
 92 between two points:

$$93 \left. \begin{aligned} \Delta e &= e_1 - e_2 \\ \Delta n &= n_1 - n_2 \\ \Delta u &= u_1 - u_2 \end{aligned} \right\} \quad (6)$$

94 The equation written above is also the starting point of the whole mathematical development
 95 followed by Burkholder (2012). To facilitate the understanding, and in order to simplify as much
 96 as possible the mathematical derivation, the assumption is made that the full v-c matrix of the
 97 original terrestrial coordinates (the so-called network accuracies), is restricted to two points and,
 98 furthermore, that it is block diagonal (the cross-correlations between points are assumed zero),
 99 therefore, one can write explicitly:

$$100 \Sigma_{(x,y,z)}^* = \left[\begin{array}{c|c} \Sigma_{(x_1,y_1,z_1)}^{3 \times 3} & 0 \\ \hline 0 & \Sigma_{(x_2,y_2,z_2)}^{3 \times 3} \end{array} \right] = \left[\begin{array}{c|c} \Sigma_{11} & 0 \\ \hline 0 & \Sigma_{22} \end{array} \right] \quad (7)$$

101 The asterisk * indicates that the assumption of zero cross-correlations is enforced implying that
 102 the v-c matrix is block diagonal. In other words, although there are correlations between the
 103 coordinates of each point, nevertheless, the points themselves are not correlated. This situation
 104 appears in practice when one combines in a v-c matrix points that belong to two different
 105 adjustments with no common observations.

106 Applying the propagation of errors law to Eq. (6), immediately follows

$$107 \quad \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}}^* = \Sigma_{(e_1, n_1, u_1)} + \Sigma_{(e_2, n_2, u_2)} = \Sigma_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 1}}^* \quad (8)$$

108

109 This undoubtedly shows that the variances and covariances at points 1 and 2 are scalar quantities
110 that could be added. Finally, substituting Eqs. (4) and (5) in Eq. (8) one arrives, under the stated
111 assumptions, to the rigorous expression to determine the local (relative) accuracies between two
112 arbitrary points 1 and 2 (recall that cross-correlations were assumed zero):

$$113 \quad \text{Rigorous} \Rightarrow \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}}^* = R_1 \Sigma_{11} R_1^T + R_2 \Sigma_{22} R_2^T = \Sigma_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 1}}^* \quad (9)$$

114 The above equation can be approximated as follows (Burkholder, 2008). However, as we will
115 see later, [this](#) formulation is just an approximation of Eq. (9):

$$116 \quad \text{Approximate} \Rightarrow \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}}^* = R_1 \Sigma_{11} R_1^T + R_1 \Sigma_{22} R_1^T \neq \Sigma_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 1}}^* \quad (10)$$

117 The first immediate conclusion comparing Eqs. (9) and (10) is that while Eq. (9) satisfies the
118 commutative property, Eq. (10) does not. It is very instinctive to comprehend that the “relative
119 accuracy” between two points 1 and 2 should be equal to the “relative accuracy” between points
120 2 and 1 independent of if one is talking about (x, y, z) or (e, n, u) coordinates. Rigorously
121 speaking, they should be identical. Nevertheless, this condition is not enforced by Burkholder’s
122 Eq. (10).

123

124 **Consequences of using the approximation equation**

125 Although in practice, primarily for short distances, Eqs. (9) and (10) may return the same or
126 similar values, mathematically and conceptually speaking, Eq. (10) is **an** approximation. Let us
127 concentrate further in the differences inherent to Eqs. (9) and (10). The consequences of

128 implementing the rigorous or the approximate equations could be described explicitly by the two
129 procedures outlined below.

130 Figure 2 schematically shows hypothetical error ellipsoids referred to the local terrestrial
131 frames at points 1 and 2. This is the original information available when using modern three-
132 dimensional GNSS techniques.

133 In the rigorous derivation of local accuracies (Soler and Smith 2010), the following steps are
134 executed:

- 135 1) Transform the v-c matrix referred to the local terrestrial frame at point 1 to the local
136 horizon geodetic frame at point 1 (Eq. (4))
- 137 2) Transform the v-c matrix referred to the local terrestrial frame at point 2 to the local
138 horizon geodetic frame at point 2 (Eq. (5))
139 or vice versa
- 140 3) Add up the v-c matrices obtained in 1) and 2) (see Eq. (9))

141 The resultant value is a unique v-c matrix termed the v-c matrix of local accuracies between
142 points 1 and 2 or between point 2 and 1, both are identical. This definition and the corresponding
143 final equations are supported by many publications, among them, Geomatics Canada (1996),
144 Craig and Wahl (2003), Wallace (2009), Soler and Smith (2010; 2012) and Soler et al. (2012).

145 The alternative procedure suggested by Burkholder in his book (Burkholder 2008)
146 although not clearly demonstrated mathematically, in practical terms, performs the following
147 steps:

- 148 1) Transform the v-c matrix referred to the local terrestrial frame at point 1 to the local
149 horizon geodetic frame at point 1 (Eq. (4))

150 2) Transform the v-c matrix referred to the local terrestrial coordinates at point 2 to the local
151 horizon geodetic frame at point 1

152 3) Add up the v-c matrices obtained in 1) and 2) (see Eq. (10))

153 However, in this case the resultant relative value of the v-c matrix between two points is not
154 unique as it should be.

155 Notice nevertheless, that this second approach is mathematically, as well as intuitively, an
156 approximation. Why should the error ellipsoid of the terrestrial coordinates at point 2 be
157 transformed into the local horizon geodetic frame at point 1, when the actual observations and
158 reductions were performed at point 2? For example, the local plumb line (or the normal to the
159 ellipsoid), meridian, etc. at point 2 are generally different to the ones at point 1, furthermore the
160 local environment of point 2 (e.g. GNSS atmospheric corrections, etc.) has nothing to do with
161 point 1. It does not make sense to assume that the local observational errors at point 2 could be
162 transferred to point 1! There exists a unique “combined” local (relative) accuracy value between
163 any two points, period! And this fact is obtained rigorously by propagating errors to Eq. (6). If
164 the definition of local accuracies is to be changed, one first should explain the mathematical rigor
165 of the equations and convince general audience of the intrinsic characteristics of the final product
166 that one wants to propose. That will require a theoretical derivation that starts with propagating
167 errors appropriately from Eq. (6) avoiding the risk of mixing up concepts in the process.

168

169 **Local accuracies at points in networks**

170 Let us assume a simple spatial network like the one shown in Fig. 3. Considering that every two
171 points produces a single local accuracy value, the total number of unique local accuracies
172 between n points grouped by sets of $m = 2$ points ($n > m$) is:

$$173 \quad \binom{n}{m} = \frac{n!}{m!(n-m)!} \quad (11)$$

174

175 In the example of Fig. 3, $n = 5$ and $m = 2$. Then, substituting these values in Eq. (11), the total
 176 number of unique two-point local accuracies for the network in Fig. 3 will be equal to 10.

177 Written them explicitly:

$$178 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}}^* = R_1 \sum_{11} R_1^T + R_2 \sum_{22} R_2^T = \sum_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 1}}^* \quad (12)$$

$$179 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 3}}^* = R_1 \sum_{11} R_1^T + R_3 \sum_{33} R_3^T = \sum_{(\Delta e, \Delta n, \Delta u)_{3 \rightarrow 1}}^* \quad (13)$$

$$180 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 4}}^* = R_1 \sum_{11} R_1^T + R_4 \sum_{44} R_4^T = \sum_{(\Delta e, \Delta n, \Delta u)_{4 \rightarrow 1}}^* \quad (14)$$

$$181 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 5}}^* = R_1 \sum_{11} R_1^T + R_5 \sum_{55} R_5^T = \sum_{(\Delta e, \Delta n, \Delta u)_{5 \rightarrow 1}}^* \quad (15)$$

$$182 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 3}}^* = R_2 \sum_{22} R_2^T + R_3 \sum_{33} R_3^T = \sum_{(\Delta e, \Delta n, \Delta u)_{3 \rightarrow 2}}^* \quad (16)$$

$$183 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 4}}^* = R_2 \sum_{22} R_2^T + R_4 \sum_{44} R_4^T = \sum_{(\Delta e, \Delta n, \Delta u)_{4 \rightarrow 2}}^* \quad (17)$$

$$184 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 5}}^* = R_2 \sum_{22} R_2^T + R_5 \sum_{55} R_5^T = \sum_{(\Delta e, \Delta n, \Delta u)_{5 \rightarrow 2}}^* \quad (18)$$

$$185 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{3 \rightarrow 4}}^* = R_4 \sum_{44} R_4^T + R_3 \sum_{33} R_3^T = \sum_{(\Delta e, \Delta n, \Delta u)_{4 \rightarrow 3}}^* \quad (19)$$

$$186 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{3 \rightarrow 5}}^* = R_3 \sum_{33} R_3^T + R_5 \sum_{55} R_5^T = \sum_{(\Delta e, \Delta n, \Delta u)_{5 \rightarrow 3}}^* \quad (20)$$

$$187 \quad \sum_{(\Delta e, \Delta n, \Delta u)_{4 \rightarrow 5}}^* = R_4 \sum_{44} R_4^T + R_5 \sum_{55} R_5^T = \sum_{(\Delta e, \Delta n, \Delta u)_{5 \rightarrow 4}}^* \quad (21)$$

188 Then, the average local accuracy at one point (point 1, for example) in a network could be
 189 defined as the average of all local accuracies connecting points radiating from that point.

190 Therefore, in this particular example, the average local accuracy at point 1 can be computed from
 191 the following equation:

$$192 \quad \bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2,3,4,5}}^* = \frac{\Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}}^* + \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 3}}^* + \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 4}}^* + \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 5}}^*}{4} \quad (22)$$

194 And substituting the values of Eqs. (12), (13), (14) and (15) above, after simplification one gets

$$195 \quad \bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2,3,4,5}}^* = R_1 \Sigma_{11} R_1^T + \frac{R_2 \Sigma_{22} R_2^T + R_3 \Sigma_{33} R_3^T + R_4 \Sigma_{44} R_4^T + R_5 \Sigma_{55} R_5^T}{4} \quad (23)$$

196 which clearly makes a lot of sense. The maximum contribution rests on the accuracy of point 1
 197 while the remaining contributions are averaged out. For this main reason, its averaged local
 198 accuracy error ellipsoid could be assumed that corresponds to the radiating point, in this case
 199 point 1. Consequently, at every point one can assume two error ellipsoids, the original network
 200 ellipsoid and the averaged local accuracy error ellipsoid for that point. The averaged local
 201 terrestrial error ellipsoid (referred to a frame parallel to the global (x, y, z) frame) is not
 202 considered as intuitive as the averaged local accuracy error ellipsoid, because of the difficulty of
 203 visualizing in space the x -, y -, and z -axis, therefore, it is neglected in this discussion. This is
 204 simply because to know the statistics (variances and covariances) referred to a local north and
 205 east in the local horizon plane is more practical and can be easily envisioned. Furthermore, it is
 206 clear from Fig. 3 that the averaged local accuracies for points such as number 5, that has other
 207 points around it, should get a more realistic value of the quality of the survey at this point in that
 208 local area. This is precisely the advantage of providing local accuracies, the observational errors
 209 inherent to **a** points radiating from an arbitrary point also contribute to the final quality of the
 210 estimation of its accuracy.

211 Recall now that equation (23) assumes that the v-c matrix of the points referred to the global
 212 terrestrial frame was block diagonal. Otherwise, the contribution of the non-diagonal blocks
 213 $(\Sigma_{12}, \Sigma_{13}, \Sigma_{14}, \Sigma_{15})$ and their transposes should be accounted for. For example, the rigorous
 214 (complete) average local accuracies at point 1 (see Fig. 3) with only connections to point 2 and 3
 215 takes the form (Soler et al. 2012):

$$\begin{aligned}
 216 \quad \bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2,3}} &= \frac{\Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2}} + \Sigma_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 3}}}{2} \\
 &= \frac{R_1 \Sigma_{11} R_1^T + R_2 \Sigma_{22} R_2^T - R_1 \Sigma_{12} R_2^T - R_2 \Sigma_{21} R_1^T + R_1 \Sigma_{11} R_1^T + R_3 \Sigma_{33} R_3^T - R_1 \Sigma_{13} R_3^T - R_3 \Sigma_{31} R_1^T}{2} \\
 217 \quad &= R_1 \Sigma_{11} R_1^T + \frac{1}{2} [R_2 \Sigma_{22} R_2^T + R_3 \Sigma_{33} R_3^T - R_1 \Sigma_{12} R_2^T - R_2 \Sigma_{21} R_1^T - R_1 \Sigma_{13} R_3^T - R_3 \Sigma_{31} R_1^T] \\
 218 \quad & \tag{24}
 \end{aligned}$$

219 A further clarification is in order: the U.S. Federal Geographic Data Committee (FGDC) (1998)
 220 specifies that “local accuracy” be provided as a 95% confidence interval. A practical numerical
 221 example of equation (24) applied to three points resulting from a 3D GNSS network computed at
 222 the 95% confident levels was explained in Soler et al. (2012).

223

224 **Computation of the average local accuracies in a network using matrix algebra**

225 A simple matrix procedure to compute the average local accuracies from the original “network
 226 accuracy” variance-covariance matrix could be written as follows:

$$227 \quad \bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{1 \rightarrow 2,3 \dots n-1}} = \frac{1}{n-1} \text{Trace}_b \left[[\mathfrak{S}_1][\mathfrak{R}] \begin{bmatrix} \Sigma_{11} & \Sigma_{12} & \cdots & \Sigma_{1n} \\ \Sigma_{21} & \Sigma_{22} & \cdots & \Sigma_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ \text{sym.} & & & \Sigma_{nn} \end{bmatrix} [\mathfrak{R}]^T [\mathfrak{S}_1]^T \right] \tag{25}$$

228 In the above equation the following operator has been introduced:

229 $\text{Trace}_b = \text{Sum of the diagonal } 3 \times 3 \text{ blocks of a square matrix formed by } 3 \times 3 \text{ blocks}$

230 The explicit form of the other matrices in equation (25) are:

$$231 \quad [\mathfrak{S}_1]_{3(n-1) \times 3n} = \begin{bmatrix} [I] & -[I] & [0] & [0] & \cdots & [0] \\ [I] & [0] & -[I] & [0] & \cdots & [0] \\ [I] & [0] & [0] & -[I] & \cdots & [0] \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ [I] & [0] & [0] & [0] & \cdots & -[I] \end{bmatrix}; \text{ and } [\mathfrak{R}]_{3n \times 3n} = \begin{bmatrix} R_1 & [0] & [0] & [0] & [0] \\ & R_2 & [0] & [0] & [0] \\ & & R_3 & [0] & [0] \\ & & & \ddots & \vdots \\ \text{sym.} & & & & R_n \end{bmatrix} \quad (26)$$

232 where $[I]$ is the 3x3 unit matrix. Similarly for point 2,

$$233 \quad \bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{2 \rightarrow 1, 3 \dots n-1}} = \frac{1}{n-1} \text{Trace}_b \left[[\mathfrak{S}_2][\mathfrak{R}] \begin{bmatrix} \Sigma_{11} & \Sigma_{12} & \cdots & \Sigma_{1n} \\ \Sigma_{21} & \Sigma_{22} & \cdots & \Sigma_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ \Sigma_{nn} \end{bmatrix} [\mathfrak{R}]^T [\mathfrak{S}_2]^T \right] \quad (27)$$

234 where now:

$$235 \quad [\mathfrak{S}_2]_{3(n-1) \times 3n} = \begin{bmatrix} -[I] & [I] & [0] & [0] & \cdots & [0] \\ [0] & [I] & -[I] & [0] & \cdots & [0] \\ [0] & [I] & [0] & -[I] & \cdots & [0] \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ [0] & [I] & [0] & [0] & \cdots & -[I] \end{bmatrix} \quad (28)$$

236 In general one can write:

$$237 \quad [\mathfrak{S}_i]_{i \neq 1} = \begin{array}{c} i \text{ column} \\ \downarrow \\ \begin{bmatrix} -[I] & & & [I] \\ & -[I] & & [I] \\ & & \ddots & \vdots \\ & & & -[I] & [I] \\ \hline & & & [I] & -[I] \\ & & & \vdots & \ddots \\ & & & [I] & & -[I] \end{bmatrix} \\ \leftarrow i \text{ row} \end{array} \quad (29)$$

238 where the rest of the 3x3 blocks not shown in the above matrix are equal to zero. Another

239 important clarification should be stressed; the matrix written above assumes that the averaged

254 (31)

255 “Relative network accuracies” between two points i and j are defined through the mathematical
 256 model:

$$\left. \begin{aligned}
 \Delta x &= x_i - x_j = -(x_j - x_i) \\
 \Delta y &= y_i - y_j = -(y_j - y_i) \\
 \Delta z &= z_i - z_j = -(z_j - z_i)
 \end{aligned} \right\} \quad (32)$$

$$\begin{aligned}
 \Sigma_{(\Delta x, \Delta y, \Delta z)_{i \rightarrow j}} &= [[I] : [-I]] \Sigma_{(x, y, z)_{ij}} \begin{bmatrix} [I] \\ [-I] \end{bmatrix} = [[I] : [-I]] \begin{bmatrix} \Sigma_{ii} & \Sigma_{ij} \\ \Sigma_{ji} & \Sigma_{jj} \end{bmatrix} \begin{bmatrix} [I] \\ [-I] \end{bmatrix} \\
 &= \Sigma_{ii} + \Sigma_{jj} - \Sigma_{ij} - \Sigma_{ji} = \Sigma_{(\Delta x, \Delta y, \Delta z)_{j \rightarrow i}}
 \end{aligned} \quad (33)$$

259 And the explicit form of the above equation can be written:

$$\begin{aligned}
 \Sigma_{(\Delta x, \Delta y, \Delta z)_{i \rightarrow j}} &= \begin{bmatrix} \sigma_{x_i}^2 - 2\sigma_{x_i x_j} + \sigma_{x_j}^2 & \sigma_{x_i y_i} - \sigma_{x_i y_j} - \sigma_{x_j y_i} + \sigma_{x_j y_j} & \sigma_{x_i z_i} - \sigma_{x_i z_j} - \sigma_{x_j z_i} + \sigma_{x_j z_j} \\ & \sigma_{y_i}^2 - 2\sigma_{y_i y_j} + \sigma_{y_j}^2 & \sigma_{y_i z_i} - \sigma_{y_i z_j} - \sigma_{y_j z_i} + \sigma_{y_j z_j} \\ & sym. & \sigma_{z_i}^2 - 2\sigma_{z_i z_j} + \sigma_{z_j}^2 \end{bmatrix} \\
 &= \Sigma_{(\Delta x, \Delta y, \Delta z)_{j \rightarrow i}}
 \end{aligned} \quad (34)$$

262 The original v-c matrix of network accuracies could be referred to the local horizon frames at
 263 each point as was introduced in Soler and Smith (2010):

$$\Sigma_{(e, n, u)} = \begin{bmatrix} \Sigma_{(e, n, u)_{ii}} & \cdots & \Sigma_{(e, n, u)_{ij}} & \cdots \\ \vdots & \ddots & \vdots & \\ \Sigma_{(e, n, u)_{ji}} & \cdots & \Sigma_{(e, n, u)_{jj}} & \cdots \\ sym. & & & \ddots \end{bmatrix} = \begin{bmatrix} R_i \Sigma_{ii} R_i^T & \cdots & R_i \Sigma_{ij} R_j^T & \cdots \\ \vdots & \ddots & \vdots & \\ R_j \Sigma_{ji} R_i^T & \cdots & R_j \Sigma_{jj} R_j^T & \cdots \\ sym. & & & \ddots \end{bmatrix} \quad (35)$$

265 The general form of the rotation matrix R_i is given by Eq. (3). This equation is one of the most
 266 important developments in the theory of local accuracies introduced by Soler and Smith (2010).

267 As we will see below, this matrix equation is critical for the development of the rigorous form of

284 Although some authors represent the local accuracies error ellipses (or ellipsoids) at the center
 285 of the line connecting two arbitrary points i and j , this practice is not recommended. In the first
 286 place because it could be confused with the error ellipse (ellipsoid) computed at the middle point
 287 of the line connecting two arbitrary points. As the reader will see below, the local accuracies
 288 error ellipsoid and the middle point of the line error ellipsoid are not the same.

289

290 **Variance-covariance matrix at the average (middle) point of a spatial segment when the**
 291 **stochastic information at the end points is available**

292 The mathematical model is:

$$\left. \begin{aligned} x_m &= \frac{x_i + x_j}{2} \\ y_m &= \frac{y_i + y_j}{2} \\ z_m &= \frac{z_i + z_j}{2} \end{aligned} \right\} \quad (39)$$

294 As usual, the network full v-c matrix is given by:

$$\Sigma_{(x,y,z)} = \begin{bmatrix} \Sigma_{ii} & \cdots & \Sigma_{ij} & \cdots \\ \vdots & \ddots & \vdots & \\ \Sigma_{ji} & \cdots & \Sigma_{jj} & \cdots \\ sym & & & \ddots \end{bmatrix} \quad (40)$$

296 Then, propagating errors:

$$\Sigma_{(x_m, y_m, z_m)}_{ij} = J \Sigma_{(x,y,z)}_{ij} J^T \quad (41)$$

298 where

$$J = \frac{\partial(x_m, y_m, z_m)}{\partial(x_i, y_i, z_i, x_j, y_j, z_j)} = \frac{1}{2} \begin{bmatrix} 1 & 0 & 0 & | & 1 & 0 & 0 \\ 0 & 1 & 0 & | & 0 & 1 & 0 \\ 0 & 0 & 1 & | & 0 & 0 & 1 \end{bmatrix} = \frac{1}{2} [[I] \parallel [I]] \quad (42)$$

300 and substituting (42) into (41), finally:

$$301 \quad \Sigma_{(x_m, y_m, z_m)_{ij}} = \frac{1}{4} [\Sigma_{ii} + \Sigma_{jj} + \Sigma_{ij} + \Sigma_{ji}] \quad (43)$$

302 This is an interesting result. The v-c matrix at the middle point of a spatial line between points i
 303 and j is equal to one fourth of the sum of the four matrices (two v-c diagonal block matrices and
 304 two non-diagonal cross-covariance matrices) related to the points.

305 If one compares Eq. (43) with Eq. (33) immediately follows:

$$306 \quad \Sigma_{(\Delta x, \Delta y, \Delta z)_{i \rightarrow j}} = 4 \Sigma_{(x_m, y_m, z_m)_{ij}} - 2 [\Sigma_{ij} + \Sigma_{ji}] \quad (44)$$

307 Using Eq. (31) the explicit form of Eq. (43) easily follows:

$$308 \quad \Sigma_{(x_m, y_m, z_m)_{ij}} = \frac{1}{4} \begin{bmatrix} \sigma_{x_i}^2 + 2\sigma_{x_i x_j} + \sigma_{x_j}^2 & \sigma_{x_i y_i} + \sigma_{x_i y_j} + \sigma_{x_j y_i} + \sigma_{x_j y_j} & \sigma_{x_i z_i} + \sigma_{x_i z_j} + \sigma_{x_j z_i} + \sigma_{x_j z_j} \\ & \sigma_{y_i}^2 + 2\sigma_{y_i y_j} + \sigma_{y_j}^2 & \sigma_{y_i z_i} + \sigma_{y_i z_j} + \sigma_{y_j z_i} + \sigma_{y_j z_j} \\ \text{sym.} & & \sigma_{z_i}^2 + 2\sigma_{z_i z_j} + \sigma_{z_j}^2 \end{bmatrix} \quad (45)$$

311 To get the value of Eq. (43) referred to the local horizon plane (e, n, u), in other words
 312 $\Sigma_{(e_m, n_m, u_m)_{ij}}$, following the logic developed from our first paper about local accuracies and
 313 recalled herein, Eq. (43) takes the form:

$$314 \quad \Sigma_{(e_m, n_m, u_m)_{ij}} = \frac{1}{4} [R_i \Sigma_{ii} R_i^T + R_j \Sigma_{jj} R_j^T + R_i \Sigma_{ij} R_j^T + R_j \Sigma_{ji} R_i^T] \quad (46)$$

315 and after replacing the values from Eq. (35) immediately follows:

$$316 \quad \Sigma_{(e_m, n_m, u_m)_{ij}} = \frac{1}{4} \begin{bmatrix} \sigma_{e_i}^2 + 2\sigma_{e_i e_j} + \sigma_{e_j}^2 & \sigma_{e_i n_i} + \sigma_{e_i n_j} + \sigma_{e_j n_i} + \sigma_{e_j n_j} & \sigma_{e_i u_i} + \sigma_{e_i u_j} + \sigma_{e_j u_i} + \sigma_{e_j u_j} \\ & \sigma_{n_i}^2 + 2\sigma_{n_i n_j} + \sigma_{n_j}^2 & \sigma_{n_i u_i} + \sigma_{n_i u_j} + \sigma_{n_j u_i} + \sigma_{n_j u_j} \\ \text{sym.} & & \sigma_{u_i}^2 + 2\sigma_{u_i u_j} + \sigma_{u_j}^2 \end{bmatrix} \quad (47)$$

317 This corroborates, as before, that the symbolic notation equivalence between Eqs. (45) and (47)
 318 is retained. The derivation of Eq. (47) would have been very difficult to compute directly from
 319 the initial math model defined by Eq. (39) after it has been expressed in the (e, n, u) frame
 320 without the introduction of Eq. (35). This validates, once more, that our equations to determine
 321 accurate local accuracies are generally rigorous and correct.

322 Similarly to Eq. (44) it can be written:

$$323 \quad \Sigma_{(\Delta e, \Delta n, \Delta u)_{i \rightarrow j}} = 4 \Sigma_{(e_m, n_m, u_m)_{ij}} - 2 [R_i \Sigma_{ij} R_j^T + R_j \Sigma_{ji} R_i^T] \quad (48)$$

324

325 **On error ellipsoids**

326 As Fig. 3 shows there is a unique error ellipsoid at each point that can be determined from the
 327 original network v-c matrix $\Sigma_{(x_i, y_i, z_i)}$ for any arbitrary point i . For simplicity, only error
 328 ellipsoids at points 1, 2, and 3 have been drawn in the figure. Let's assume that the network v-c
 329 matrix of points 1 and 2 is:

$$330 \quad \Sigma_{(x,y,z)} = \Sigma_{(x_1, y_1, z_1, x_2, y_2, z_2)} = \begin{bmatrix} \begin{bmatrix} 3.003 & 3.508 & -0.743 \\ 3.508 & 34.460 & -17.864 \\ -0.743 & -17.864 & 16.151 \end{bmatrix} & \begin{bmatrix} 1.222 & 0.961 & 0.606 \\ 0.962 & 9.045 & -4.527 \\ 0.593 & -4.537 & 7.046 \end{bmatrix} \\ \begin{bmatrix} 1.222 & 0.962 & 0.593 \\ 0.961 & 9.045 & -4.537 \\ 0.606 & -4.527 & 7.046 \end{bmatrix} & \begin{bmatrix} 4.755 & 6.882 & -2.792 \\ 6.882 & 57.717 & -31.039 \\ -2.792 & -31.039 & 25.470 \end{bmatrix} \end{bmatrix} \quad (\text{cm}^2) \quad (49)$$

331 Point 1 has the following geodetic curvilinear coordinates: $\lambda_1 = 262^\circ 53' 22.1562''$, $\varphi_1 = 31^\circ 34'$
 332 $39.7778''$, $h_1 = 101.712$ m referred to the ITRF2000 frame and GRS80 ellipsoid. Then, if one
 333 computes the eigenvalues and eigenvectors of the first 3x3 diagonal block in Eq. (49) one obtains
 334 the following diagonal matrix of eigenvalues:

$$335 \quad A_{(x_1, y_1, z_1)} = \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix}_{(x_1, y_1, z_1)} = \begin{bmatrix} 45.647 & 0 & 0 \\ 0 & 5.710 & 0 \\ 0 & 0 & 2.258 \end{bmatrix} \text{ (cm}^2\text{)} \quad (50)$$

336 with diagonal elements $\lambda_1 > \lambda_2 > \lambda_3$ and the matrix of column eigenvectors:

$$337 \quad S_{(x_1, y_1, z_1)} = [s_1 \quad s_2 \quad s_3]_{(x_1, y_1, z_1)} = \begin{bmatrix} -0.0791 & 0.3706 & 0.9254 \\ -0.8518 & 0.4571 & -0.2559 \\ 0.5179 & 0.8085 & -0.2795 \end{bmatrix} = \begin{bmatrix} s_{1x} & s_{2x} & s_{3x} \\ s_{1y} & s_{2y} & s_{3y} \\ s_{1z} & s_{2z} & s_{3z} \end{bmatrix} \text{ (cm)} \quad (51)$$

338 The square roots of the diagonal elements of Eq. (50) are the values of the three “principal axes”

339 of the error ellipsoid with semi-axes $a = \sqrt{\lambda_1} = 6.830\text{cm}$; $b = \sqrt{\lambda_2} = 2.389\text{cm}$;

340 $c = \sqrt{\lambda_3} = 1.503\text{cm}$. Notice that the semi-axes of the error ellipsoid are not equal to the standard

341 deviations at the point (square roots of the diagonal elements in the v-c of Eq. (49)), namely,

342 $\sigma_{x_1} = 1.733\text{cm}$; $\sigma_{y_1} = 5.870\text{cm}$; and $\sigma_{z_1} = 4.019\text{cm}$.

343 The angles defining the orientations of the three principal axes in the x - y - z frame are:

$$344 \quad \tan \bar{\lambda}_k = \frac{s_{k_y}}{s_{k_x}}; \quad \tan \varphi_k = \frac{s_{k_z}}{\sqrt{s_{k_x}^2 + s_{k_y}^2}} \quad k = 1, 2, 3 \text{ principal axes}$$

345 $\bar{\lambda}_1 = 84.6959^\circ$; $\varphi_1 = 31.1898^\circ$; $\bar{\lambda}_2 = 50.9696^\circ$; $\varphi_2 = 53.9499^\circ$; $\bar{\lambda}_3 = 344.5452^\circ$; $\varphi_3 = 16.2314^\circ$.

346 Now, as mentioned above, the v-c matrix of point 1 referred to the (e_1, n_1, u_1) local horizon frame

347 can be computed as follows:

$$348 \quad \Sigma_{(e_1 n_1 u_1)} = \begin{bmatrix} \sigma_{e_1}^2 & \sigma_{e_1 n_1} & \sigma_{e_1 u_1} \\ & \sigma_{n_1}^2 & \sigma_{n_1 u_1} \\ \text{sym.} & & \sigma_{u_1}^2 \end{bmatrix} = R_1 \Sigma_{(x_1 y_1 z_1)} R_1^T = \begin{bmatrix} 2.624 & 1.013 & 1.167 \\ 1.013 & 5.377 & -0.291 \\ 1.167 & -0.291 & 45.613 \end{bmatrix} \text{ (cm}^2\text{)} \quad (52)$$

349 Similarly, computing the eigenvalues of the above symmetric matrix, one arrives at:

$$350 \quad A_{(e_1, n_1, u_1)} = \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix}_{(e_1, n_1, u_1)} = \begin{bmatrix} 45.647 & 0 & 0 \\ 0 & 5.710 & 0 \\ 0 & 0 & 2.258 \end{bmatrix} \quad (\text{cm}^2) \quad (53)$$

351 Therefore, as expected, we get exactly the same eigenvalues implying that the network error
 352 ellipsoid is a unique estimating surface although it could be referred to different local frames. In
 353 other words, the magnitudes of the semi-axes of the error ellipsoid are the same independent of
 354 the frame used. Hence, the differences between the matrices in the first diagonal block in Eq. (49)
 355 and the matrix in Eq. (52) are merely due to the fact that the values in Eq. (49) refer to the local
 356 terrestrial frame (x_1, y_1, z_1) while the elements in the matrix of Eq. (52) refer to the local geodetic
 357 horizon frame (e_1, n_1, u_1) . Consequently, the magnitude of the semi-axes of the error ellipsoid
 358 obtained from the two v-c matrices, being scalar quantities, are invariant under rotations and
 359 therefore their size is the same in both local frames, although they are taken along the
 360 corresponding eigenvectors referred to each frame. Obviously, the components of the
 361 eigenvectors look different because they are referred to two different frames. However, only a
 362 rotation is involved.

363 Using the notation introduced above, the analytical proof that the eigenvalues referred to the
 364 two frames are the same follows:

$$365 \quad \Sigma_{(e_1 n_1 u_1)} = R_1 \Sigma_{(x_1 y_1 z_1)} R_1^T = R_1 \left(S_{(x_1 y_1 z_1)} \Lambda_{(x_1 y_1 z_1)} S_{(x_1 y_1 z_1)}^T \right) R_1^T = \left(R_1 S_{(x_1 y_1 z_1)} \right) \Lambda_{(x_1 y_1 z_1)} \left(S_{(x_1 y_1 z_1)}^T R_1^T \right) = S_{(e_1 n_1 u_1)} \Lambda_{(e_1 n_1 u_1)} S_{(e_1 n_1 u_1)}^T \quad (54)$$

367 and consequently,

$$368 \quad S_{e_1 n_1 u_1} = R_1 S_{x_1 y_1 z_1} \quad \text{and} \quad \Lambda_{e_1 n_1 u_1} = \Lambda_{x_1 y_1 z_1}. \quad (55)$$

369 In other words, the components of each eigenvector defining the orientation of the semi-axes of
 370 the error ellipsoid referred to the local horizon frame (e_1, n_1, u_1) could be obtained from the

371 eigenvectors originally computed and referred to the local terrestrial frame (x_1, y_1, z_1) through a
 372 rotation matrix as follow:

$$373 \quad \{s_1\}_{(e_1, n_1, u_1)} = R_1 \{s_1\}_{(x_1, y_1, z_1)}; \quad \{s_2\}_{(e_1, n_1, u_1)} = R_1 \{s_2\}_{(x_1, y_1, z_1)}; \quad \{s_3\}_{(e_1, n_1, u_1)} = R_1 \{s_3\}_{(x_1, y_1, z_1)} \quad (56)$$

374 or, equivalently, using a single matrix multiplication, for point 1, one can write:

$$375 \quad S_{(e_1, n_1, u_1)} = R S_{(x_1, y_1, z_1)} = \begin{bmatrix} 0.9923 & -0.1238 & 0 \\ 0.0648 & 0.5196 & 0.8519 \\ -0.1055 & -0.8454 & 0.5237 \end{bmatrix} \begin{bmatrix} -0.0791 & 0.3706 & 0.9254 \\ -0.8518 & 0.4571 & -0.2559 \\ 0.5179 & 0.8085 & -0.2795 \end{bmatrix} \quad (57)$$

$$= \begin{bmatrix} -0.0270 & -0.3112 & -0.9500 \\ 0.0065 & -0.9504 & 0.3111 \\ -0.9996 & 0.0022 & 0.0277 \end{bmatrix} = \begin{bmatrix} s_{1e} & s_{2e} & s_{3e} \\ s_{1n} & s_{2n} & s_{3n} \\ s_{1u} & s_{2u} & s_{3u} \end{bmatrix} \quad (cm)$$

376 The two angles defining the directions of the orientation in space of the three principal axes in
 377 the $e-n-u$ frame could be computed as follows (α = geodetic azimuth; ν = geodetic vertical
 378 angle):

$$379 \quad \tan \alpha_k = \frac{s_{ke}}{s_{kn}}; \quad \tan \nu_k = \frac{s_{ku}}{\sqrt{s_{ke}^2 + s_{kn}^2}} \quad k = 1, 2, 3 \quad \text{principal axes} \quad (58)$$

$$380 \quad \alpha_1 = 283.6495^0; \nu_1 = -88.4098^0; \alpha_2 = 18.1289^0; \nu_2 = 0.1242^0; \alpha_3 = 288.1323^0; \nu_3 = 1.5853^0 \quad (59)$$

381 Comparing now Eqs. (52) and (53) it is very clear that looking into the magnitudes of the semi-
 382 axes and the variances (diagonal elements of Eq. (52)) that the principal axes of the error
 383 ellipsoid (axes a , b , and c) are almost aligned with the up, north, and east directions where
 384 a along the up direction, b along the north direction, and c along the east direction, clearly
 385 showing that the maximum error is along the height (up) component as it is generally the case
 386 when processing GNSS observations. The actual values are $\sigma_{u_1} = 6.754\text{cm} \approx a$; $\sigma_{n_1} = 2.319\text{cm}$
 387 $\approx b$; $\sigma_{e_1} = 1.612\text{cm} \approx c$. This is corroborated by the direction of the first principal axis that was

388 determined to be: $\alpha_1 = 283.6495^0$; $\nu_1 = -88.4098^0$. Notice that the other two semi-axes are
 389 practically on the plane of the local geodetic horizon (very small ν_2 and ν_3 angles).

390 From Eq. (54) other interesting relationships could be discussed. Taking traces of Eq. (54) one
 391 can write:

$$392 \quad \text{Trace } \Sigma_{(e_1 n_1 u_1)} = \text{Trace } [R_1 \Sigma_{(x_1 y_1 z_1)} R_1^T] = \text{Trace } [S_{(e_1 n_1 u_1)} \Lambda_{(e_1 n_1 u_1)} S_{(e_1 n_1 u_1)}^T] \quad (60)$$

393 By incorporating the cyclic permutation rule into the above equation and reordering terms:

$$394 \quad \text{Trace } \Lambda_{(e_1 n_1 u_1)} = \text{Trace } \Sigma_{(x_1 y_1 z_1)} = \text{Trace } \Sigma_{(e_1 n_1 u_1)} \quad (61)$$

395 Or explicitly:

$$396 \quad \lambda_1 + \lambda_2 + \lambda_3 = a^2 + b^2 + c^2 = \sigma_{x_1}^2 + \sigma_{y_1}^2 + \sigma_{z_1}^2 = \sigma_{e_1}^2 + \sigma_{n_1}^2 + \sigma_{u_1}^2 = \sigma_p^2 \quad (62)$$

397 where the scalar σ_p^2 receives the name of *point variance*. The above expression indicates that
 398 σ_p , *point standard deviation*, is the magnitude of a vector (invariant with respect to rotations)
 399 that could be obtained from the components of any of the vectors: (a, b, c) , $(\sigma_{x_1}, \sigma_{y_1}, \sigma_{z_1})$, or
 400 $(\sigma_{e_1}, \sigma_{n_1}, \sigma_{u_1})$. The orientation of these four vectors is generally not the same but their magnitude
 401 is identical. Therefore, the point variance is unique at any point of a network and thus
 402 independent of local frame selection.

403 The above concepts also apply to the discussion of an “averaged local accuracies error
 404 ellipsoid” except that now the orientation of this error ellipsoid resulting from equations such as
 405 Eq. (27) is always referred to the local frame *e-n-u* (see Fig. 4). This is one of the great
 406 advantages of using “local accuracies”, the v-c matrix at each point *i* refers to the more intuitive
 407 local horizon geodetic frame although it was directly computed from the original full network
 408 (absolute) v-c matrix as written mathematically in Eq. (31). Modern GNSS technology permits
 409 the computation of full network v-c matrices including the variances (diagonal elements),

410 covariances between coordinates (non-diagonal elements of the diagonal 3 x 3 blocks and cross-
 411 covariances between points (non-diagonal 3 x 3 blocks). This is emphasized because “local
 412 accuracy” results are way off the mark when the cross-covariances are assumed zero
 413 ($\Sigma_{ij} = [0]$ if $i \neq j$) in the computations. This important but often ignored fact was already
 414 numerically shown in Soler et al. (2012). However, restricting ourselves now to the example
 415 selected here shown in Eq. (49), if one implements Eq. (8) the resultant eigenvalues are $\lambda_1^* =$
 416 122.9090 cm^2 ; $\lambda_2^* = 12.7917 \text{ cm}^2$; $\lambda_3^* = 5.8556 \text{ cm}^2$. Therefore, if the rigorous Eqs. (37) or (38)
 417 are used for the calculation, the resulting eigenvalues are $\lambda_1 = 97.9413 \text{ cm}^2$; $\lambda_2 = 4.6943 \text{ cm}^2$;
 418 and $\lambda_3 = 4.2999 \text{ cm}^2$, a significant difference. The eigenvalues of a v-c local accuracy matrix
 419 based on a block diagonal network accuracy matrix are larger than the eigenvalues obtained
 420 using the full network v-c matrix. Consequently the availability of the non-diagonal blocks of the
 421 network v-c matrix is essential to obtain rigorous results. Only recently with the incorporation of
 422 GNSS methods and 3D least-squares models has this important achievement been made
 423 routinely available to the engineers and surveyors.

424 Figure 4 shows schematically the parameters involved in the final “averaged local accuracies
 425 error ellipsoid” at an arbitrary point i resulting from implementing the general Eq. (25), denoted
 426 symbolically by $\bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{i \rightarrow j, k, \dots}}$. From this v-c matrix the following parameters are obtained
 427 (see Fig. 4): the averaged standard deviations of the averaged local accuracies along the e , n , and
 428 up -axes ($\bar{\sigma}_{\Delta e}$, $\bar{\sigma}_{\Delta n}$, $\bar{\sigma}_{\Delta u}$); the three semi-axes a , b , and c of the error ellipsoid, and the three
 429 orthonormal eigenvectors \vec{s}_1 , \vec{s}_2 , and \vec{s}_3 (they are perpendicular to each other and with
 430 modulus equal to one) defining the orientation of the principal axes. $\bar{\Sigma}_{(\Delta e, \Delta n, \Delta u)_{i \rightarrow j, k, \dots}}$ contains

431 all the information including cross-correlations between points (see Fig.2 and 3) to determine the
432 most accurate result as a function of the primary statistical information of nearby survey marks.
433 The values of $\bar{\sigma}_{\Delta e}$, $\bar{\sigma}_{\Delta n}$, and $\bar{\sigma}_{\Delta u}$ could be converted to the 95% confidence interval suggested
434 by FGDC (1998, 2008) using the logic described in Soler et al. (2012). Although some scientists
435 advocate the use of a bi-normal radial error (Leenhouts 1985), in the opinion of the authors it
436 will be more rigorous and it takes the same effort computationally speaking to report the
437 corresponding error ellipses, although the values of $\bar{\sigma}_{\Delta e}$, $\bar{\sigma}_{\Delta n}$, and $\bar{\sigma}_{\Delta u}$ is all the information
438 that is practically needed.

439

440 **Conclusions**

441 On the basis of the standard definition of “local accuracies” as announced by scientists more than
442 20 years ago, new insights about their rigorous definition and their differences with an
443 alternative characterization proposed by Burkholder (2008) are detailed. Attention to the
444 calculation of the so-called “mean (averaged) local accuracy” at a survey point is emphasized by
445 presenting a didactic mathematical discussion with theoretical examples.

446 According to the authors, “averaged local accuracies” is the best practical way to indicate the
447 quality of geodetic and/or engineering surveyed points on a particular area. With the advent of
448 GNSS technology the availability of variance-covariance matrices between coordinates and
449 cross-covariance matrices between points have improved the rigorous determination of averaged
450 local accuracies at any arbitrary point i as a function of the accuracies of its selected surrounding
451 points j, k, \dots sharing common observations. This possibility was not attainable before GNSS
452 hardware and 3D methodologies were fully developed. Up until recently, the absence of the
453 knowledge of cross-covariances between points (the non-diagonal 3x3 blocks in the network

454 (absolute) v-c matrix) has impeded the rigorous determination of local accuracies. Furthermore,
455 as explained in previous sections, the assumption that the non-diagonal blocks are zero
456 introduces inaccurate positioning estimates to the results. As Fig. 2 and 3 indicates, presently, we
457 have at our disposal all the information that is need it to compute averaged local accuracies at
458 any point by considering all existing information about the errors implicit in its surrounding
459 survey marks. The approach delineated herein is without any doubt the most accurate way to
460 have a grasp of the overall point-by-point survey quality in local projects where, clearly, the final
461 accuracy of every point is directly affected by the observational errors of their connected
462 neighboring stations. Equation (27) presents a simple mathematical algorithm to implement
463 numerically these concepts using matrix algebra by starting from the original full v-c matrix of
464 the network accuracies given in the usual form of Eq. (31).

465 Subsequently, some ideas related to error ellipsoids and their inherent eigenvalues and
466 eigenvectors are exploited by explaining the different relationships with respect to different
467 (topocentric) local frames and how to transform between them using their corresponding rotation
468 matrices. At this point the different parameters related to the averaged local error ellipsoid are
469 described (see Fig. 4). In the opinion of the authors this is the type of ellipsoid that should be
470 provided in order to determine the best set of local accuracies.

471

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475

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