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# Biological design criteria for juvenile fish passage, 1998:

high-velocity flume development and improved wet-separator efficiency

Fish Ecology Division

Northwest Fisheries Science Center

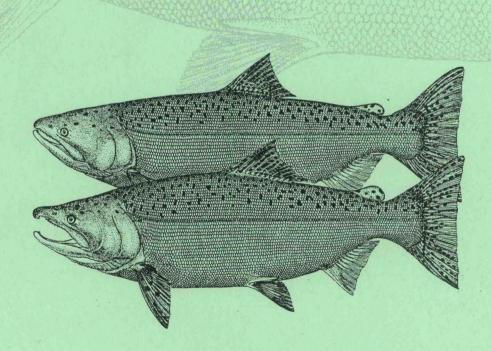
National Marine Fisheries Service

Seattle, Washington

by

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Biological Design Criteria for Juvenile Fish Passage, 1998: High-Velocity Flume Development and Improved Wet-Separator Efficiency F56 M2 1998

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### **EXECUTIVE SUMMARY**

During the 1998 spring and summer juvenile salmonid migrations, we continued research to provide biological design criteria for the improvement of conventional juvenile salmonid wet separators, which are currently in use in fish passage facilities at hydroelectric dams on the Snake and Columbia Rivers. In addition, we conducted evaluations to develop the high-velocity flume (HVF) wet separator and tested a preliminary adult and debris separator designed to remove large fish and debris before they reach the juvenile wet separator. Both the conventional and HVF separator units were used to trap river-run smolts from Gatewell 6B at McNary Dam.

Testing for conventional separator improvement was conducted in a unit simulating the wet-separators presently used at the dams. In this unit, six treatments were evaluated to compare the effects of alternate separation-bar spacings (16, 17, and 19-mm), and flow diverters (with or without diverters) on salmonid separation efficiency, separator exit efficiency fish (passage through the separator unit), and fish condition (descaling).

Results from these tests indicated that separation efficiency values for all salmonid smolts evaluated during the spring migration (total catch) were significantly higher with 19-mm bar spacing than with 16-mm spacing, but were not significantly different between 16- and 17-mm or between 19- and 17-mm bar spacing. For the total catch, separation efficiency was also significantly higher with flow diverters deployed than when they were not used. For subyearling chinook salmon, separation efficiency exhibited a similar trend among bar spacing conditions, but displayed no difference with respect to the flow diverter.

There was a significant interaction between conditions affecting separator exit efficiency for the total catch during the spring, but not for subyearling chinook salmon. Mean descaling values were statistically similar among treatments involving both fish groups, and interaction between conditions was not significant for descaling.

In the high-velocity flume (HVF) separator, separation efficiency, exit efficiency, and descaling were again evaluated. Treatments for the HVF evaluations consisted of 12 combinations of alternate separation-bar spacing (13, 16, and 19 mm), alternate separation-bar array orientation in relation to the water surface (0° and 4° angle), and alternate water velocity (1 and 2 m/s).

Using the HVF during the spring outmigration, we found that mean separation efficiency for the total juvenile salmonid catch showed a significant interaction among all three conditions. Separation was nearly identical using 16-mm and 19-mm bar spacing with 1 m/s water velocity and with a flat separation-bar array, and both values were

significantly higher than mean values for all other treatments. Subyearling chinook salmon separation efficiency values were statistically higher at 1 m/s than at 2 m/s water velocity, and higher using the flat separation-bar array than the angled array.

Most separator exit efficiency comparisons using the HVF revealed a significant interaction between water velocity and separation-bar array angle. Exit efficiency was generally higher at 2 m/s than at 1 m/s, and higher using the flat separation-bar array than the angled array.

Comparisons among descaling values during spring using the HVF were not significantly different among any treatment conditions during the spring, and there were no significant interactions among descaling comparisons during either migration period. However, for fall chinook salmon, descaling values were significantly higher in treatments with water velocity at 2 m/s than at 1 m/s.

Initial evaluation of a prototype adult and debris separator showed the design to be about 85% effective at rerouting large fish before they entered the juvenile wet separator. The design also removed larger or more dendritic debris, but was ineffective at intercepting smaller particles.

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### INTRODUCTION

Separation of smolts by size is a key objective of juvenile bypass systems at hydroelectric dams on the Columbia and Snake Rivers. Juvenile chinook salmon (*Oncorhynchus tshawytscha*) that are transported with juvenile steelhead (*O. mykiss*, which are generally larger than chinook salmon smolts) may experience higher levels of stress than those transported with other chinook salmon (McCabe et al. 1979, Congleton et al. in press). In addition to stress reduction, separation provides management options based on different size classes.

Separation at U.S. Army Corps of Engineers (COE) operated facilities has evolved from an initial 'dry' separation process, where fish were sorted using inclined pipes (McComas et al. 1998), to a wet separation approach. The conventional wet separator used in bypass facilities at COE projects is similar to that developed and evaluated by Gessel et al. (1985). Since the conventional separator keeps fish submerged, it is considered less stressful to migrants; the separation process relies primarily on behavioral responses to induce smolts to attempt to sound (dive) between separation bars just under the water surface.

Details of the wet separation process are described and diagramed by McComas et al. (1998). Briefly, conventional wet separators use a three-stage separation process designed to remove small fish first; then larger smolts; and finally adult salmonids, non-salmonid incidental species, and debris. The spacing of separation bars in successive compartments of the separator determines the size of fish able to sound at each stage. Under ideal conditions, the first compartment, or "A" section, would segregate smaller smolts such as chinook, coho (*O. kisutch*), and sockeye (*O. nerka*) salmon from the larger, predominantly steelhead smolts, which are sorted in the B section.

In practice, there are several problems with conventional wet separators. First, the conventional separators have had sporadic failures in separation efficiency. For example, at McNary Dam in 1994, separation efficiency values from the "A" section of the separator were 32.2, 24.1, and 27.7% for yearling chinook, coho, and sockeye salmon respectively (Brad Eby, U.S. Army Corps of Engineers, McNary Dam Juvenile Fish Passage Facility, Umatilla OR, 97882, Pers. commun., July 1995). These failures may have been caused by flow surges, which carry small fish through the first section with insufficient time to sound through the separation bars, or by inadequate stimulus to generate a sounding (diving) response in fish in the separator unit.

Second, video monitoring associated with behavior and physiology studies has indicated that fish also hold under the separator bars for extended periods, rather than exiting expeditiously from the separator unit (Shreck et al. in prep). This work suggests that fish may exit the separator unit only after becoming fatigued by prolonged resistance to the hydraulic conditions within the unit. If this is the case, the conventional separator may be contributing to increased overall stress, which could ultimately effect survival.

To address these concerns, we continued research during the 1998 spring and summer migration periods to increase salmonid smolt separation efficiency in conventional wet separators. These studies centered on developing biological design criteria for conventional separators by analyses of the spacing between separation bars and by the use of flow deflectors above the bars.

In addition, we continued work on the high-velocity flume (HVF) wet separation concept, which arose from interagency brainstorming sessions. Preliminary studies to evaluate the extent to which smolts will sound between separation bars in a high-velocity environment were conducted in a small flume at McNary Dam during the latter part of the fall chinook migration in 1996 (McComas et al.1998). Results demonstrated that if sufficient separation-bar length is available, a substantial proportion of fall chinook salmon will sound between separation bars at higher velocities than are normally present in existing wet separators.

Preliminary evaluations of a HVF separator design in 1997 compared 24 treatments involving combinations of water velocity, water depth above the separation bars, separation-bar array length, and orientation of separation bars in relation to the water surface. Promising results were obtained at a water velocity of 1 m/s, 5-cm depth over the separation bars and with 12-m-long separation bars oriented parallel to the water surface (McComas et al. 1998). In 1998 we continued to develop HVF criteria by considering the relationship among separation-bar array orientation, spacing between the separation bars, and water velocity.

In currently operating wet-separator units large incidental species, adult salmonids, and debris are delivered to the separator along with outmigrant smolts. Larger fish pass completely through both separator sections to a removal sump at the end of the unit, and debris must be removed by hand before clogging the separator or causing injury to juvenile fish. A more appropriate sequence would be to remove trash and large fish before they enter the juvenile portion of the separator. Therefore, in 1998, we also began evaluating a system for eliminating large fish and debris upstream from the juvenile fish wet separator. Specific research objectives in 1998 were these:

- Evaluate the effects of separation-bar spacing and flow diverters on juvenile salmonid separation, separator exit efficiency, and descaling in a simulated conventional wet separator.
- 2) Evaluate the effects of separation-bar spacing, water velocity, and separation-bar array orientation on juvenile salmonid separation, separator exit efficiency, and descaling in a high-velocity flume wet separator.
- 3) Conduct preliminary evaluation of an experimental device for removing adult salmonids, large incidental species and debris prior to entry into a wet separator.

# OBJECTIVE 1: EVALUATE SEPARATION-BAR SPACING AND FLOW DIVERTERS IN A CONVENTIONAL WET SEPARATOR

### **Approach**

A full-sized separator unit was fabricated to simulate the function of the small fish section of a conventional wet separator, similar to those in use at McNary and Lower Monumental Dams (McComas et al. 1998). A full-sized separator section was used for the simulated unit so that beneficial changes found could be adapted to existing conventional wet separators without requiring major revisions. The simulated conventional wet separator measured 1.52 m wide, 3.96 m long and 1.2 m high (5 x 13 x 4 ft)(Fig. 1). Maximum water depth was 0.8 m, with add-in water supplied through a 25.4-cm (10-in) siphon drawing water from the forebay.

Several modifications were built into the simulated unit to reduce or eliminate functional weaknesses known to impede operation in conventional wet separators. Major modifications to this basic unit involved removal of the downwell sump located in the downstream end of operational separators, and reduction and redirection of add-in water

In operational separators, a downwell sump serves as the entrance to an exit orifice for fish which have sounded between the separation bars (separated fish). However, video recordings of behavior near the sump entrance have shown that accelerating water velocities through the downwell cause smolts to resist entering the sump by swimming vigorously against the flow (James L. Congleton, Pers. commun., Idaho Cooperative Fish and Wildlife Research Unit, Department of Fish and Wildlife, University of Idaho, Moscow, ID 83844-1141, March 1995), suggesting delayed migration and increased stress as a result of hydraulic conditions within the unit.

Therefore, the area containing the downwell sump was eliminated from the simulated unit by installing a vertical partition 61 cm (2 ft) from the downstream end and horizontally across the width of the unit. The partition supported the downstream end of the separation-bar array at a height which allowed approximately 3-cm (1.25 in) water depth over the separation bars, forming the overflow orifice for fish not passing between the bars (non-separated fish, Fig. 1).

The other major difference between the simulated separator unit and an existing operational wet separator involved the make-up water delivery system, and this in turn is linked to placement of the submerged exit orifice. Conventional wet separators presently in operation have a submerged exit orifice approximately 1.5 m (5 ft) below the water surface. In addition to a direct drain supply furnishing water directly to the orifice, the volume of water needed to support a downwell orifice at this depth is furnished by forced

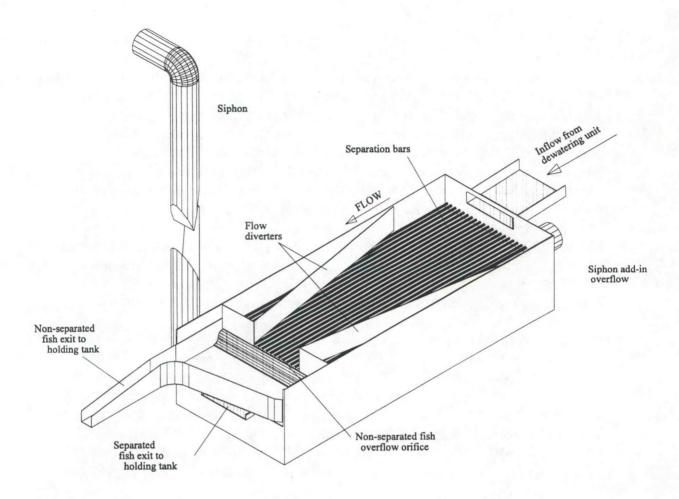


Figure 1. Relationship among components of the simulated conventional wet separator unit used during biological design criteria studies at McNary Dam, 1998.

upward flow through a perforated-plate false bottom at three points along the longitudinal centerline of each separator section. Fish have been seen swimming into this flow, in a head-down orientation toward the perforated plate. This hydraulic situation contributes to increased holding time in the separator and probably to increased fatigue and stress.

Previous studies using test separators have demonstrated that a shallower orifice configuration can be more efficient at passing fish than an orifice deeper in the water column (McComas et al. 1998). The bottom of the submerged orifice in the simulated unit was placed 23 cm (9 in) below the water surface to reduce velocity and volume through the opening. The submerged orifice measured 7.6 by 61 cm (2 x 24 in), and was centered in the partition at the downstream end of the unit. A perforated plate false bottom sloped from the bottom edge of the submerged orifice to 15 cm (6 in) below the water surface at the upstream end of the separator.

Make-up water was also redirected to eliminate the upward flow component that appeared to attract fish. A 24.5-cm (10-in) PVC tube through the longitudinal centerline, and along the floor of the separator under the false bottom, received water from the siphon. Flow was regulated by 24.5-cm (10-in) valves on both ends of this tube. Four lateral 10-cm (4-in) pipes were attached to each side of the 24.5-cm tube, and each pipe was equipped with double rows of 1-cm (3/8-in) holes directed toward the floor at approximately 30° to the vertical. This arrangement dispersed make-up water inflow throughout the separator with no apparent upwelling.

Separation bars were contained in arrays oriented parallel to flow along the long axis of the simulated unit, and sloped from 7.6 cm (3 in) below the water surface at the upstream end to 3 cm (1.25 in) below the surface at the downstream end. Each array consisted of two panels, 0.76 m wide and 3.35 m long (2.5 x 11 ft), with individual bars of 25.4-mm-id (1-in) aluminum tubing. Three interchangeable arrays were constructed, with nominal spacings of 16, 17, and 19 mm (0.625, 0.6875, and 0.75 in) between individual bars.

With the described configuration, fish entering the simulated separator were allowed unrestricted access to the overflow orifice across the entire separator width, similar to conditions in a conventional separator. Poor separation in conventional units results in part from small fish passing over the overflow orifice without attempting to sound between the separation bars. In addition, larger fish tend to hold in the upstream portion of the small fish section for long periods, reducing exit efficiency.

It is possible that this holding behavior may be an avoidance response to the abrupt flow acceleration at the interface between the overflow orifice and the relatively low separator flow. A progressive increase in velocity through the length of the unit could encourage larger smolt egress by making the flow transition less rapid. To test this

possibility, two flow diverters were fabricated to channel flow over the overflow orifice through a smaller area in the center of the orifice (Fig. 1).

Flow diverters were intended to create a gradual increase in velocity along their length, thus avoiding a precipitous increase in velocity at the overflow. Diverters consisted of removable 2.7-m (9-ft) aluminum wings inclined from the sides of the unit across the separator bars so that non-separated fish passage was confined to a 61-cm (2-ft) opening in the center of the unit. A shorter 46-cm (1.5-ft) wing extended horizontally from the side to the angled wing to restrict overflow above the bars to the center opening.

With reduced length due to the downwell modification and without flow diverters in place, total area of the separation bars in the simulated conventional separator unit was  $5.11 \text{ m}^2$  (55 ft²), or approximately 85% of the total area available in one section of an operational separator (5.85 m², 65 ft²). Flow diverters further reduced the available area to 3.86 m² (41.5 ft²), or 64% of the total in an operational unit section.

To evaluate the effects of separation-bar spacing and flow diverters on separation and exit efficiency, treatments were randomized in blocks, each consisting of one of the following 6 combinations of separation-bar spacing and flow diverter conditions:

	Condition		
Treatment	Separation-bar spacing (mm)	Flow Diverters	
1	16	off	
2	16	on	
3	17	off	
4	17	on	
5	19	off	
6	19	on	

Before initiating a replicate, water depth in the separator was stabilized at approximately 2 cm (0.8 in) depth over the overflow orifice. River-run (test) fish were introduced into the simulated conventional separator through an opening in the upper end along with dewatered flows from the north orifice of Gatewell 6B. A replicate was initiated by opening the gatewell orifice, which allowed test fish to enter the unit along with enough additional inflow to raise the depth across the separator overflow orifice to approximately 3 cm (1.25 in). Fish exiting through the two separator orifices were detained in separate holding tanks for examination. Replicate duration was dependent on numbers of fish entering the separator rather than on time. After more than 25 chinook salmon had entered the simulated unit, recruitment was halted by closing the gatewell orifice.

After the replicate was ended, test fish were collected first from above, then from below the separation bars within the separator unit. Animals from the two holding tanks were examined last. Each group was anesthetized separately using tricane methane sulfonate (MS-222) and enumerated by species and categorized by length group as less than 180 mm fork length (<180 mm) or greater than or equal to 180 mm fork length (≥180 mm). Fish condition was also noted as percent descaling for each species using current Fish Transportation Oversight Team descaling criteria (Ceballos et al. 1992). Nearly all salmonid smolts during the spring migration, and a representative portion of the chinook salmon catch from the summer migration, were measured to fork length (FL).

One test series was completed during the spring migration, and one during the summer migration, with both series involving multiple blocks of the six treatments. Blocks and treatments within blocks were performed sequentially. The order of flow diverter treatments within separation bar spacing treatments, and the order of bar spacing treatments within each block, was random. However, for implementation purposes, both flow diverter treatments were completed at a given separation-bar spacing before changing to the next bar spacing in the block.

A total of 54 replicates (9 for each treatment) were completed during the spring migration test period from 27 April through 1 June. From 27 April through 4 May, all work was accomplished between 0600 and 1400. Low fish numbers prompted the addition of a second shift (1400-2200) beginning 5 May, and a third shift beginning 25 May (2200-0600) so that tests were conducted 24 hours each day for the remainder of the spring migration. All testing was completed between 0600 and 1400 during the summer migration period from 22 June through 30 July, resulting in 90 replicates (15 per treatment). No testing was done between 5 June and 22 June.

Separation efficiency (SEF) was calculated similarly for both length groups, as the number of separated fish, by species, in a given length group compared to the total number of smolts from that group entering the separator during the test interval:

$$SEF = \frac{F}{T} \times 100\% \tag{1}$$

Where: SEF= separation efficiency

F = number of separated fish

T = total number of fish entering the evaluation separator

However, separation has a somewhat different behavioral implication for each of the two length groups. For smolts <180 mm, separation efficiency was calculated using the fraction which sounded between the separation bars, whereas separation efficiency of fish  $\geq$ 180 mm was calculated using the fraction which did not sound between the bars.

Total separation efficiency was calculated using the number of fish from each group which separated properly as the number of separated fish.

Separator exit efficiency (SEE) was calculated by species as the proportion of fish in each size group having exited the simulated conventional wet separator compared to the total number of fish in that group that entered the separator during the test interval:

$$SEE = \frac{A}{T} \times 100\% \tag{2}$$

Where: SEE = orifice exit efficiency

A = fish number of fish from size group A exiting orifice T = total number of fish from group A entering the separator

Following recovery from anesthetic, all fish were released directly into the juvenile fish bypass channel.

### **Results and Discussion**

A total of 6,860 smolts were included in treatment comparisons using the simulated conventional wet separator during the spring migration. Yearling chinook salmon <180 mm composed approximately 40% of the catch, while steelhead ≥180 mm composed about 14.9%. For the summer migration period, subyearling chinook salmon made up over 99% of a total catch of 15,535 smolts. Salmonid catch data are presented by replicate in Appendix Table 1, with non-target incidental catch in Appendix Table 2.

Since changing the separation-bar arrays placed practical restrictions on the order of separation-bar treatments, the sequence of treatments within each block was not entirely random. Rather, a given bar spacing was set, and all flow-diverter conditions were evaluated for treatments within a block before the next bar spacing was evaluated. Normally, this non-random effect is analyzed using a split-plot procedure (Petersen 1985). In this case, "large plots" were two consecutive tests and "small plots" were individual tests. Variability in sampled fish stocks and environmental conditions was assumed to differ between "large" and "small" time plots.

However, results from actual field testing precluded the statistical power in distinguishing between these two plot sizes, because the actual time between tests in the same "large time plot" was sometimes longer than the time between tests in different "large time plots." For example, Treatments 1 and 2 could be considered components of Large Time Plot 1, Treatments 3 and 4 of Large Time Plot 2, and Treatments 5 and 6 of Large Time Plot 3. However, in Replicate 5 (Appendix Table 1), because all tests were conducted during a 5-day work week, with interruptions to the series occurring each

weekend, Treatments 3, 4, and 6 were completed on 8 May, and Treatment 5 was not effected until 11 May. Therefore, Treatments 3 and 4 were actually sampled closer in time to Treatment 6 than Treatments 5 and 6. This type of disruption happened often enough that we did not expect the "large time plots" and "small time plots" to differ much in their respective variances. However, there was variation over the course of each migration period. Consequently, data were analyzed using a randomized block analysis of covariance (ANCOVA) statistical design.

A further divergence from the study design was that for several individual replicates, the minimum sample size criteria of 25 fish per test was not met. Therefore, datasets were analyzed using combined data from adjacent replicates (of the same treatment) until that minimum was attained. The analyses for these datasets were thus reduced to completely randomized analyses of variance (ANOVA).

A split-plot block ANOVA analysis (date groupings being the blocks) was conducted where possible (mostly total species) and little difference was found between error terms and/or results from the less restrictive analyses of covariance (date being the covariate). Therefore, the results of the analyses of covariance or the completely randomized ANOVA are presented.

The ANOVA procedure was used to determine the significance of observed mean differences among treatments by length group (<180 mm fork length, ≥180 mm fork length, and total catch) for each species and by length group the for the total salmonid catch. For each group separation efficiency, separator exit efficiency, and descaling were analyzed.

From the spring chinook migration period, significant numbers of smolts were available for analysis for chinook salmon <180 mm, total chinook salmon catch, steelhead ≥180 mm, total steelhead catch, sockeye salmon <180 mm, total salmonids <180 mm, total salmonids ≥180 mm, and total salmonid catch. Subyearling chinook salmon <180 mm comprised the only group with sufficient numbers of valid replicates for analysis during the summer migration. Since virtually all sockeye and subyearling chinook salmon were <180 mm, a separate analysis was not done for total catch for these species.

## **Separation Efficiency**

Complete results of statistical analyses among separation efficiency comparisons using the simulated conventional wet separator are presented in Appendix Table 3. In general, separation efficiency increased for length groups <180 mm and decreased for fish ≥180 as separation-bar spacing increased. Flow diverter conditions showed a similar general increase in separation for fish from smaller fish groups and a decrease for larger fish with diverters on (deployed) compared to the off (not deployed) condition.

Mean yearling chinook salmon separation efficiency for fish <180 mm was significantly different among separation-bar spacing treatments analyzed across flow diverter conditions (F = 13.10, df = 2, P = 0.000) and between flow diverter treatments (F = 14.35, df = 1, P = 0.001). However, there was no interaction among the two conditions (F = 1.53, df = 2, P = 0.230). Mean separation efficiencies were 55% (SE = 2.3), 64% (SE = 2.4), and 72% (SE = 2.4) for the 16, 17, and 19-mm separation-bar treatments, respectively.

Fisher's protected least significant difference (LSD) revealed that all three means were significantly different from each other, indicating that smaller yearling chinook salmon separated differently with as little as 2 mm (0.08 in) difference in separation-bar spacing. Similarly computed values were 59% (SE = 1.9) with flow diverters on and 69% (SE = 1.9) with diverters off. When yearling chinook salmon  $\geq$ 180 mm were combined with the smaller fish group to form the total chinook salmon catch, there were no significant separation efficiency differences among any of the treatment conditions.

Steelhead separation efficiency was significantly lower (F = 9.10, df = 2, P = 0.002) using the 19-mm separation-bar spacing (80%, SE = 2.9) than with either the 16-mm bar spacing (96%, SE = 2.1) or the 17-mm spacing (90.8, SE = 2.9) for fish  $\geq$ 180 mm long. There was no difference among any of the treatments for the total steelhead catch, and no interaction among treatment conditions for either group.

Only sockeye salmon <180 mm exhibited a significant interaction between flow-diverter and bar-spacing conditions (F = 4.15, df = 2, P = 0.025). Among the six treatments, separation efficiency for sockeye salmon was as follows:

Treatment conditions		Separation efficiency (%)	
Separation-bar spacing	Flow diverter	Mean	SE
16 mm	off	66.9	5.2
16 mm	on	79.8	5.6
17 mm	off	78.9	5.6
17 mm	on	62.6	5.6
19 mm	off	77.9	5.6
19 mm	on	87.5	5.2

Fisher's LSD indicated that mean separation using the 16-mm separation-bar spacing without a flow diverter and using 17-mm spacing with a flow diverter were statistically similar, and significantly lower than the other four treatments, which were all similar.

For all salmonid smolts <180 mm (total catch <180 mm), separation efficiency was significantly higher with the 19-mm separation-bar spacing (75%, SE = 2.7) than with the other spacings (F = 7.75, df = 2, P = 0.001), and significantly higher (F = 5.12, df = 1, P = 0.028) with flow diverters in place (71%, SE = 2.1) than when they were not used (64%, SE = 2.1).

For all smolts  $\geq 180$  mm (total catch  $\geq 180$  mm), separation efficiency values for all three separation-bar spacing conditions were significantly different from each other (F = 23.12, df = 2, P = 0.000). Not surprisingly for this group, separation was higher using the 16-mm bar spacing (95%, SE = 1.9). Combined mean separation efficiency values for the total salmonid catch were 69% (SE = 1.9), 72% (SE = 2.0) and 77% (SE = 2.0) using separation bars spaced 16, 17, and 19 mm apart, respectively. Separation using the 19-mm bar spacing was significantly higher than for the 16-mm spacing, but not different from the 17-mm spacing. Summed across bar-spacing treatments, separation efficiency for the total catch was also higher (F = 6.72, df = 1, P = 0.012) with flow diverters on (75%, SE = 1.6) than when they were not used (69%, SE = 1.6).

During the summer migration, subyearling chinook salmon mean separation efficiency exhibited no interaction between flow-diverter and separation-bar-spacing conditions, and no difference between flow-diverter conditions. However, separation was significantly lower (F = 9.99, df = 2 P = 0.000) with the 16-mm separation-bar spacing (83%, SE = 1.2) than with either the 17-mm (90%, SE = 1.2) or 19-mm (89%, SE = 1.2) bar spacing.

## Separator Exit Efficiency

Separator exit efficiency ranged from 85 to 98% for groups analyzed during the spring migration, and from 75 to 86% for subyearling chinook salmon during the summer migration. There was a significant interaction between separation-bar-spacing and flow-diverter conditions only for all smolts combined (total catch, all species) during the spring (F = 4.59, df = 2, P = 0.015), resulting in the following exit efficiency values:

litions	Total salmonid species, total catch		
Flow diverter	Mean separator exit efficiency (%)	SE	
off	87.3	2.1	
on	93.8	2.1	
off	95.1	2.3	
on	94.1	2.1	
off	95.7	2.2	
on	89.4	2.2	
	Flow diverter  off  on  off  on  off	Flow diverter         Mean separator exit efficiency (%)           off         87.3           on         93.8           off         95.1           on         94.1           off         95.7	

Exit efficiency was lower for treatments using 16-mm bar spacing with no flow diverter than for all other treatments except those using 19-mm spacing with flow diverters deployed. The latter treatment had similar exit efficiency to both 17-mm treatments, and to the 16-mm treatments with flow diverters on, but was lower than the 19-mm bar spacing without flow diverters. A complete list of statistical comparisons for exit efficiency using the simulated conventional separator is contained in Appendix Table 4.

Subyearling chinook salmon generally exited the separator less readily than did salmonids during the spring migration. Mean exit efficiency was similar for flow diverter treatments when compared across separation-bar spacing conditions (F = 0.33, df = 1, P = 0.566), but was significantly different among separation-bar spacing conditions (F = 5.32, df = 2, P = 0.007). Fall chinook exit efficiency was higher using the 16-mm separation-bar spacing (88%, SE = 2.4) than the 19-mm spacing (75%, SE = 2.4). Both variations were statistically similar to exit efficiency using 17-mm bar spacing (80%, SE = 2.4).

### **Fish Condition**

During the spring migration, mean descaling ranged from 0.9 to 5.9% for analyzed groups (Table 1). For all salmonids captured, (total catch), mean descaling using 16, 17, and 19-mm bar-spacing was 3.9, 4.1 and 4.0%, respectively. This was somewhat lower than the overall descaling rate of 6.8% posted for all species summarized from the juvenile fish facility annual report (Hoffarth et al. 1999).

Subyearling chinook salmon descaling was typically low throughout the summer migration, averaging 1.1, 1.2, and 1.2% using respective bar spacings of 16, 17, and 19 mm.

Differences among mean descaling values were compared using the ANCOVA and ANOVA procedures for the same groups analyzed for separation and exit efficiency. No interaction was found between flow diverter and separation-bar spacing conditions for any of the groups analyzed, and mean descaling differences among treatments were not significant (Appendix Table 5). Differences among sample date were significant for subyearling chinook salmon (F = 29.17, F = 0.000), but did not explain variability among descaling data for groups during the spring migration.

Table 1. Mean descaling values (%) by species and separation-bar spacing condition for salmonid smolt groups evaluated using a simulated conventional wet separator during biological design criteria studies at McNary Dam, 1998.

	Separation-bar			
Species	Length group	spacing (mm)	Mean	SE
Yearling chinook salmon	<180 mm	16	3.7	1.1
		17	4.4	1.1
		19	4.8	1.1
	total catch	16	3.8	1.1
		17	4.8	1.4
		19	4.8	1.1
Steelhead	≥180 mm	16	2.7	1.0
		17	4.5	1.4
		19	4.9	1.4
	total catch	16	2.4	1.0
		17	4.0	1.2
		19	3.8	1.2
Sockeye salmon	<180 mm	16	5.9	1.0
		17	3.5	1.0
		19	3.5	1.0
Total salmonid species	<180 mm	16	4.7	0.7
(spring migration)		17	3.8	0.7
		19	4.1	0.7
Total salmonid species	≥180 mm	16	0.9	1.3
(spring migration)		17	5.3	1.3
		19	4.9	1.6
Total salmonid species	total catch	16	3.9	0.7
(spring migration)		17	4.1	0.7
		19	4.0	0.7
Subyearling chinook salmon	<180 mm	16	1.1	0.3
		17	1.2	0.3
		19	1.2	0.3

# OBJECTIVE 2: EVALUATE SEPARATION-BAR SPACING, WATER VELOCITY, AND SEPARATION-BAR ARRAY ORIENTATION IN A HIGH-VELOCITY FLUME WET SEPARATOR

### Approach

The HVF wet separator constructed for preliminary evaluation in 1997 (McComas et al. 1998) was used during this series. The separator consists of an aluminum flume 76 cm (30 in) square in cross section with a working separation-bar length of 12 m (40 ft).

Individual separation bars were 25.4-mm-id (1-in-id) aluminum tubing. The 12-m array was consists of 8 removable, interconnecting panels, each 1.5-m long by 0.76-m wide (5 ft x 30 in). This configuration facilitated exchange among bar spacing and slope treatments. To evaluate the effect of separation-bar spacing on separation efficiency and separator exit efficiency, three sets of separation bars were fabricated with spacing of 13, 16, or 19 mm (0.5, 0.625, or 0.75 in) between bars.

Separation-bar panels were supported in the flume at one of two orientations by 2.54 cm (1 in) square aluminum stanchions. Stanchions were placed in pockets set into, and flush with, the inside of the HVF. With the bars at 0° (flat) in relation to the water surface, one set of stanchions maintained the bottom of the array approximately 36 cm (14 in) above the bottom of the flume along the entire array length. The other set of supports increased in length from 0 cm at the upstream end to 36 cm (14 in) at the downstream end, so that the array inclined at a constant positive slope.

For each combination of separation-bar spacing and angle, separation efficiency was evaluated at velocities of 1 and 2 m/s, measured near the downstream end of the separation bars. Flow control in the 12-m working section of the flume was accomplished by varying the height of a lift gate near the downstream end of the flume, and by regulating makeup water volume to a distribution box at the upstream end of the flume. Makeup water was supplied by forebay siphons.

Velocity was measured and adjusted for each replicate using a Swoffer Model 2100 current velocity meter (Swoffer Marine Instruments, Inc., Seattle, Washington<sup>1</sup>) and water depth was adjusted to approximately 5 cm (2 in) over the downstream end of the separation bars for all treatments.

<sup>1</sup> Reference to trade names does not imply endorsement by National Marine Fisheries Service.

Twelve treatments involving combinations of separation-bar spacing, separation-bar array orientation and water velocity were organized in blocks to evaluate the effects of the three conditions on separation and exit efficiency and fish condition as follows:

		Condition	
Treatment	Separation-bar spacing (mm)	Separation-bar orientation	Water velocity (m/s)
1	13	flat	1
2	13	angled	1
3	13	flat	2
4	13	angled	2
5	16	flat	1
6	16	angled	1
7	16	flat	2
8	16	angled	2
9	19	flat	1
10	19	angled	1
11	19	flat	2
12	19	angled	2

Replicates were randomized by separation-bar spacing, so that all treatments at a given spacing were completed before beginning treatments at the next bar spacing.

River-run migrant salmonid smolts (test fish) used during the evaluation were obtained by trapping volitional emigrants from the south orifice of Gatewell 6B. After establishing treatment conditions in the separator, a replicate was initiated by opening the gatewell orifice to introduce test fish into the upstream end of the HVF along with the partially dewatered gatewell-orifice flow. Smolts were allowed to accumulate in the flume and holding tanks until at least 25 chinook salmon had entered the unit. Recruitment from the gatewell was terminated by closing the gatewell orifice, and fish were removed from the unit in four groups (above bars, below bars, large-fish holding tank, small-fish holding tank), and examined similarly to fish for Objective 1.

### **Results and Discussion**

A total of 10,130 smolts were included in high-velocity flume wet separator treatment comparisons for the spring migration. Yearling chinook salmon <180 mm, sockeye salmon <180 mm, and steelhead  $\geq$ 180 mm comprised approximately 48, 25, and 13% of the total catch, respectively. For the summer migration period, nearly 99% of the total catch of 35,136

smolts were subyearling chinook salmon. Salmonid catch data for the HVF are presented by replicate in Appendix Table 6.

ANOVA, rather than the split-plot analysis, was used to determine the significance of differences among means for the treatments; this method was preferred for reasons analogous to those outlined in the discussion under Objective 1. Separation efficiency, separator exit efficiency, and descaling analyses were completed by length group for each species and for the total salmonid catch.

From the spring chinook migration period, sufficient numbers of smolts were available for analyses of each of the following categories: chinook salmon <180 mm, total chinook salmon catch, steelhead ≥180 mm, total steelhead catch, sockeye salmon <180 mm, total salmonid catch <180 mm, total salmonid catch ≥180 mm, and total salmonid catch. Subyearling chinook salmon <180 mm comprised the only group with sufficient numbers of valid replicates for analysis during the summer migration. Since virtually all sockeye and subyearling chinook salmon were <180 mm, a separate analysis was not done for total catch for these species.

A total of 99 replicates were completed over the spring migration. Low numbers of smolts exiting the south gatewell produced a mean replicate duration of 4.4 hours, and by 12 May it became apparent that fewer than the expected 10 replicates per treatment would be realized if all 12 treatments were replicated for the remainder of the season. All four 13-mm separation-bar spacing conditions were discontinued after 12 May in order to complete as many replicates as possible using what at that time appeared to be the more advantageous treatments. This resulted in 4 replicates for each of the 13-mm treatments, and 11 replicates completed for each treatment using 16- and 19-mm separation-bar spacing.

# **Separation Efficiency**

Complete results of ANCOVA and ANOVA comparisons for separation efficiency are presented in Appendix Table 7 by species for each group analyzed.

At a given separation-bar spacing, mean separation efficiency for chinook salmon <180 mm was higher at a water velocity of 1 m/s than at 2 m/s, and generally higher using a separation-bar array orientated flat in relation to the water surface than using the angled orientation (Fig. 2a). Separation of yearling chinook salmon <180 mm was affected by significant interactions between bar spacing and array orientation (F = 3.43, df = 2, P = 0.037) and between bar spacing and water velocity (F = 3.42, df = 2, P = 0.037). For the former interaction, the highest mean separation efficiency was obtained using 19-mm bar spacing with a flat bar array (74%, SE = 3.41). However, this was statistically similar to separation

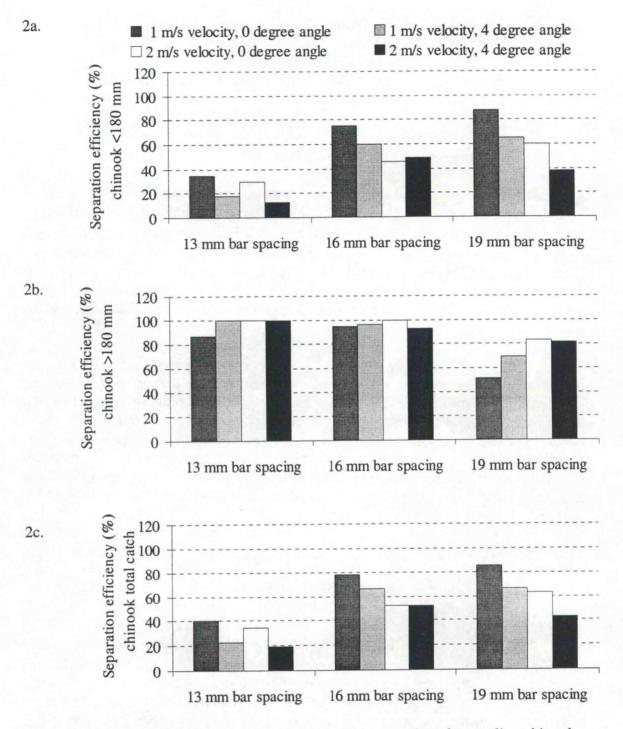


Figure 2. Relationship among mean separation efficiency values for yearling chinook salmon by treatment group for fish captured during separation efficiency evaluations using a high-velocity flume wet separator at McNary Dam, 27 April-6 June, 1998.

efficiency using 16-mm bar spacing with an angled bar array (55%, SE = 3.11) and to 16-mm spacing with a flat array (60%, SE = 3.0). Summed across angle conditions, mean separation efficiency for bar-spacing and velocity treatments was significantly higher using 19-mm spacing and a water velocity of 1 m/s (77%, SE = 3.14) than for any other combination.

The chinook salmon  $\geq 180$  mm group was not formally analyzed because too few replicates were completed with statistically valid numbers of fish. However, summed by treatment, this group showed a reverse trend to that noted for smaller fish (Fig. 2b). When fish  $\geq 180$  mm were included, the total yearling chinook salmon catch displayed a proclivity similar to that of the smaller chinook salmon group with respect to interaction between separation-bar spacing and array angle. Separation efficiency using 19-mm spacing and a flat array (74%, SE = 2.7) was higher than for all other bar-spacing/angle combinations (F = 3.63, df = 2, P = 0.030). Calculated across bar spacing and angle conditions, mean separation efficiency values for the total chinook salmon catch were significantly higher at 1 m/s (60%) than at 2 m/s (44%, F = 31.76, df = 1, P = 0.000) (Fig. 2c).

Steelhead <180 were captured too infrequently for analysis, and there were too few treatments with 13-mm bar spacing to demonstrate trends. However, at the 16- and 19-mm bar spacings, smaller steelhead mean separation efficiency values were at least arithmetically higher with the flat separation bar array, and were generally higher at 2 m/s than at 1 m/s with either array orientation (Fig. 3a).

As with smaller chinook salmon, separation efficiency results for steelhead  $\geq 180$  mm were influenced by a significant interaction between separation-bar spacing and array angle (F = 3.61, df = 2, P = 0.041). Since separation for larger fish is enhanced by not sounding between the bars, conditions which retard sounding favor better separation. Unsurprisingly then, the highest separation for this group occurred using 13-mm bar spacing with the angled bar array (100%, SE = 4.39, Fig. 4b).

Somewhat lower, but statistically similar, values were obtained using 13-mm bar spacing with the flat bar array (90%, SE = 4.4), and also using 16-mm bar spacing with flat (99%, SE = 2.2) and angled (96%, SE = 2.2) bar arrays. With 19-mm spacing, separation efficiency using the flat bar array (68%, SE = 2.2) was statistically lower than that using the angled array (76%, SE = 2.1), and both flat and angled bar treatments with 19-mm spacing were different from those with 13- and 16-mm spacing.

For the total steelhead catch, differences in separation efficiency were significant only for separation-bar spacing, possibly a result of the influence of including smaller steelhead (Fig. 3c). Mean separation efficiency was higher for all 16-mm bar spacing treatments combined (56%, SE = 4.8) than for all 13-mm (28%, SE = 9.8) or 19-mm (43%, SE = 4.8) treatments.

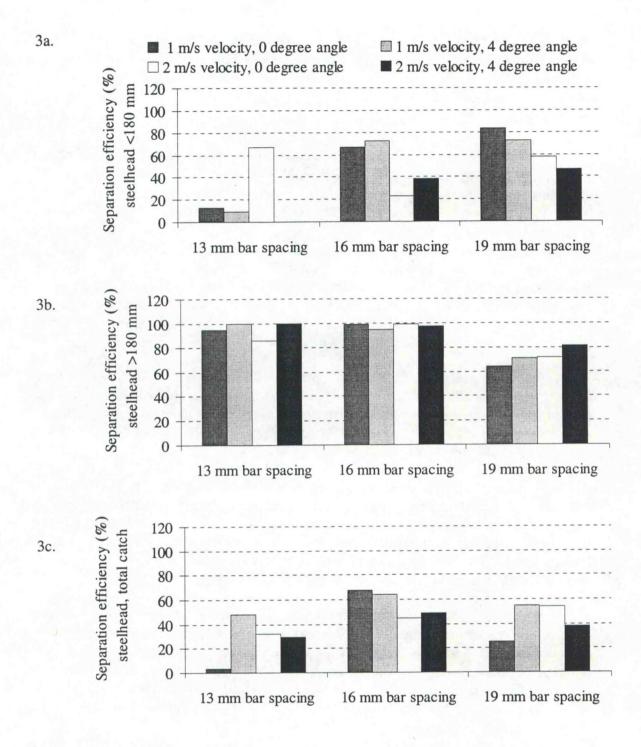


Figure 3. Relationship among mean separation efficiency values for steelhead by treatment group for fish captured during separation efficiency evaluations using a high-velocity flume wet separator at McNary Dam, 27 April-6 June, 1998.

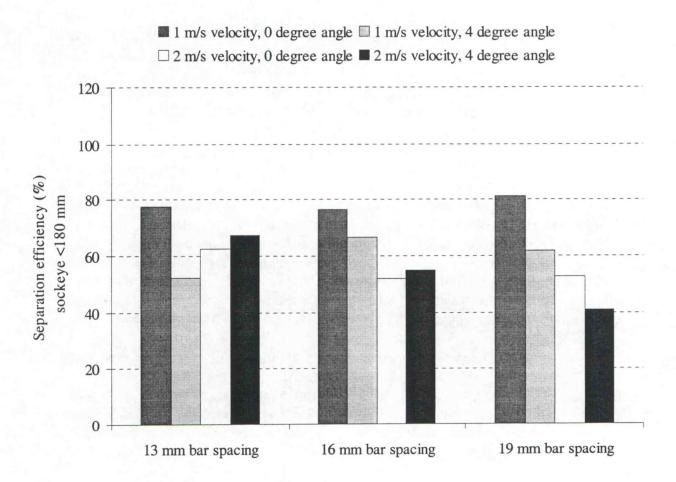


Figure 4. Relationship among mean separation efficiency values by length group for sockeye salmon <180 mm examined during separation efficiency evaluations using a high velocity flume wet separator at McNary Dam, 27 April-6 June 1998.

All but one sockeye salmon captured were <180 mm in length, so that only treatments involving the smaller sockeye salmon group were analyzed for this species (Fig. 4). Separation efficiency values for sockeye salmon were significantly different solely with regard to water velocity (F = 4.63, df = 1, P = 0.037). Combined over separation-bar spacing and array angle conditions, separation efficiency was higher at a water velocity of 1 m/s (69%, SE = 5.1) than 2 m/s (55%, SE = 4.4).

All salmonids captured (total salmonids) during spring were analyzed by length group in a manner parallel to analyses for individual species. Separation efficiency showed a significant interaction among the three conditions evaluated (separation-bar spacing, water velocity, and separation-bar array angle) for fish <180 mm (F = 3.99, df = 2, P = 0.022), and for the total catch (F = 3.69, df = 2, P = 0.029). For both fish groups, the highest values were obtained using flat separation-bar arrays and 1 m/s water velocity.

Also, there was a distinct trend within separation-bar spacing conditions for both groups; measured separation efficiency was higher at 1 m/s water velocity than at 2 m/s velocity, and higher with a flat separation-bar array than with an angled array (Fig. 5). The highest mean separation for fish <180 mm was achieved using the 19-mm spacing (84%, SE = 3.8) which was statistically similar only to the 16-mm separation-bar spacing (75%, SE = 3.8). Separation efficiency for the total catch was nearly identical using 16-mm and 19-mm bar spacing (80.88%, SE = 3.1 and 80.95%, SE = 3.3, respectively), and both estimates were significantly higher than values for all other treatments.

Separation efficiency for the total catch  $\geq 180$  mm was significantly correlated to separation-bar spacing (F = 26.79, df = 2, P = 0.000), with no interaction among treatment conditions. Mean separation using the 13-mm spacing (94%, SE = 5.4) was similar to that using the 16-mm spacing (95%, SE = 2.4), and both the 13- and 16-mm spacing conditions produced significantly higher separation efficiency than the 19-mm spacing (71%, SE = 2.3).

Differences between subyearling chinook salmon separation efficiency values were significant for water velocity (F = 30.40, df = 1, P = 0.000) and separation-bar array angle (F = 22.25, df = 1, P = 0.000). Separation efficiency was statistically higher at 1 m/s (81%, SE = 1.8) than at 2 m/s velocity (67%, SE = 1.8), and higher using the flat separation-bar array (80%, SE = 1.8) than the angled array (68%, SE = 1.8). Separation-bar spacing did not influence fall chinook salmon separation during this study. However, since the subyearling chinook salmon lengths (mean 105 mm, SE = 1.38, range 68-154 mm) over the course of the study were well below the 180-mm threshold, this outcome was not unexpected.

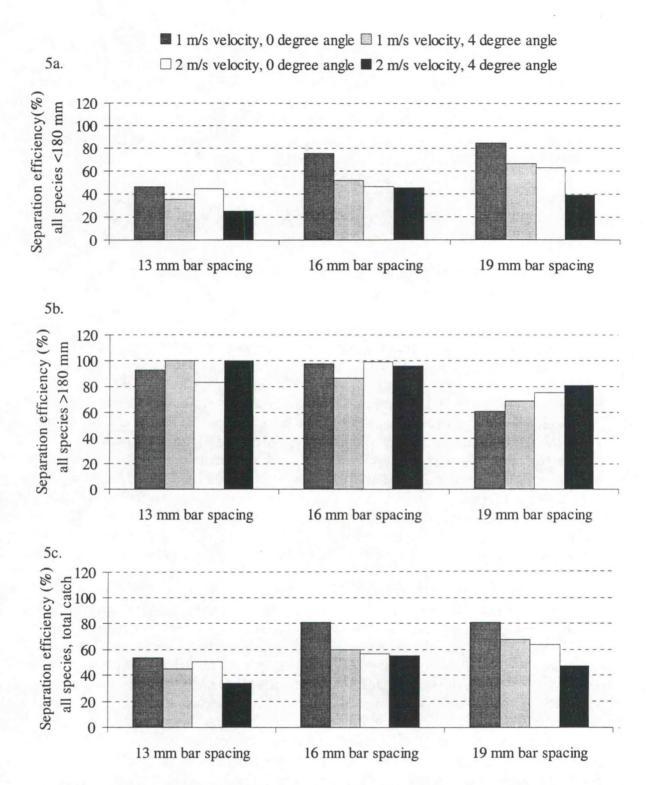


Figure 5. Relationship among mean separation efficiency values by treatment group for all salmonid species captured during separation efficiency evaluations using a high-velocity flume wet separator at McNary Dam, 27 April-6 June, 1998.

Sample date was included as a covariate in analyses of length groups for which sufficient numbers of replicates were available over the entire migration, and/or of groups for which combining adjacent replicates (through time) did not compromise the goal of the procedure. A significant portion of variability in mean separation efficiency was attributable to sample date for yearling chinook salmon <180 mm (F = 26.73, F = 10.000), yearling chinook salmon total catch (F = 24.44, F = 10.000), total salmonid species <180 mm (F = 10.66, F = 10.000), and the total salmonid species total catch (F = 4.06, F = 10.000).

## Separator Exit Efficiency

Statistical analyses of separator exit efficiency data obtained using the HVF was conducted using the methods described in for separation efficiency in Objective I (Appendix Table 8).

Most exit-efficiency comparisons revealed some level of interaction between water velocity and separation-bar array angle. For example, the interaction between velocity and angle was significant for yearling chinook salmon <180 mm (F = 24.20, df = 1, P = 0.000), with the lowest exit efficiency value associated with 1 m/s velocity and angled bars (89%, SE = 0.996). Exit efficiency was similar among treatments using 1 m/s velocity with flat separation bar arrays (99.7%, SE = 1.0), and 2 m/s velocity with flat (99.7%, SE = 1.0) or angled arrays (99%, SE = 1.1). Results were nearly identical in magnitude and direction for the total yearling chinook salmon catch (F = 4.55, df = 1, P = 0.043), and for subyearling chinook salmon (F = 18.20, df = 1, P = 0.000), indicating that fish in the smaller size class were holding in the separator at the lower velocity, possibly using the angle of the separation bars as flow protection. At the higher velocity, or without an angled array for protection, fish exited the separator expeditiously.

Sockeye salmon <180 mm exit efficiency ranged from 97 to 100% over all 12 treatments, and showed a similar overall pattern. However, there was no interaction among conditions and no significant differences among mean values by treatment for this length group. Given the relatively high exit efficiencies and the poorer separation, it is probable that sockeye salmon were unable to sound quickly enough to make use of the array angle as flow protection, unable to hold for sustained periods in water velocities approaching 1 m/s even with the angled bars, or both.

Mean exit efficiency for large fish groups exhibited a similar trend with respect to interaction between velocity and bar angle for steelhead  $\geq 180$  mm (F = 4.55, df = 1 P = 0.43), and for the total salmonid catch  $\geq 180$  mm (F = 5.67, df = 1, P = 0.023), but in the large fish, disparity between efficiencies was greater within each group than for the smaller fish groups. Exit efficiency for steelhead  $\geq 180$  mm at 1 m/s velocity and with an angled separation bar array was 67% (SE = 4.7). This was significantly lower than exit

efficiency with a flat bar array at 1 m/s (97%, SE = 4.8), or with the flat or angled bar array at 2 m/s (99%, SE = 4.8 and 89.5%, SE = 4.98, respectively).

Results were nearly identical for all small smolts ( $\geq 180$  mm), with respective means using angled and flat arrays of 72% (SE = 3.9) and 97% (SE = 4.0) at 1 m/s and 99% (SE = 3.97) and 93% (SE = 3.9) at 2 m/s water velocity. Intuitively, these results reinforced our observations that larger fish are more capable of maintaining position in the separator than smaller animals under similar conditions. It is noteworthy that all groups tended to exit promptly at either velocity when the separation-bar array was flat.

As with separation efficiency, separator exit efficiencies for the total catch <180 mm and for the total catch of all smolts combined were affected by interactions between separation-bar spacing, water velocity and separation-bar array angle. For the total catch <180 mm, exit efficiency was significantly lower using an angled separation-bar array at a velocity of 1 m/s in conjunction with 16-mm bar spacing (84%, SE = 1.2) than for all combinations except that using 19-mm spacing (86%, SE = 1.2), velocity at 2 m/s, and angled separation bars.

For all salmonid smolts evaluated during the spring migration (total catch), the combination of 16-mm bar spacing with an angled bar array and a velocity of 1 m/s produced significantly lower exit efficiency (81%, SE = 1.3) than all other treatment combinations. Exit efficiency was over 90% for all other treatments in both groups except for the total catch with 19-mm spacing, angled bars, and velocity of 1 m/s (88%, SE = 1.3). Among the three separation-bar spacings for both groups, exit efficiency was very similar (range 97.42 to 99.60%) at water velocities of 1 m/s and 2 m/s using flat separation-bar arrays.

#### **Fish Condition**

Results of descaling comparisons using the HVF are presented in Appendix Table 9. There was no significant interaction among treatment conditions and no significant differences among mean descaling values by treatment or condition for any fish group evaluated during the spring migration. Considered by separation-bar spacing, descaling ranged from 0.5 to 5.7% for all groups with sufficient replicate sizes for evaluation (Table 2). Greater variability in data for the 13-mm treatments probably resulted from the lower number of replicates and truncated duration over which replicates for that separation-bar spacing were conducted.

For subyearling chinook salmon, there was a significant difference between mean descaling values at water velocities of 2 m/s (3.4%, SE = 0.4) and 1 m/s (1.5%, SE = 0.4). This relationship is unexplained, and will be watched closely during future investigations.

Table 2. Mean descaling values (%) by species and separation-bar spacing condition for salmonid smolt groups evaluated using a high-velocity flume wet separator during biological design criteria studies at McNary Dam, 1998.

Species	Length group	Separation-bar spacing (mm)	Mean descaling (%)	SE
Yearling chinook salmon	<180 mm	13	5.6	1.2
		16	1.1	0.6
		19	2.9	0.7
	total catch	13	5.7	1.1
		16	4.1	0.6
		19	3.0	0.6
Steelhead	≥180 mm	13	0.7	1.7
		16	3.2	0.8
		19	3.0	0.8
	total catch	13	0.5	1.8
		16	3.2	0.8
		19	2.5	0.9
Sockeye salmon	<180 mm	13	2.6	1.8
		16	3.9	0.9
		19	2.7	0.9
Total salmonid species	<180 mm	13	4.7	0.9
(spring migration)		16	4.0	0.5
		19	3.2	0.5
Total salmonid species	≥180 mm	13	1.8	1.9
(spring migration)		16	3.7	0.8
(opinis inigiation)		19	3.6	0.8
Total salmonid species	total catch	13	4.6	0.9
(spring migration)		16	3.8	0.5
(		19	3.3	0.5
Subyearling chinook	<180 mm	13	2.0	0.5
salmon		16	2.7	0.5
		19	2.8	0.5

# OBJECTIVE 3. EVALUATE A PROTOTYPE ADULT AND DEBRIS SEPARATOR

### Approach

Several techniques were considered for removing trash from the water preceding entry into a wet separator, such as revolving screens, moving inclined plane collectors, and trash dump systems. Since this objective was appended just before the field season began, we implemented a relatively uncomplicated design directed toward removal of primarily larger debris and incidental catch. Also, since there was no duplicate or comparison system available for evaluation, the results were not formally analyzed.

An adult and debris (adult separator) separator was retrofit to the space between the simulated conventional wet separator used in Objective 1 and the gatewell dewatering unit upstream from the wet separator (Fig. 6). The adult separator unit was contained in a rectangular aluminum box 183 cm long and 61 cm wide (6 x 2 ft)(Fig. 6). The separation-bar array within the unit was made of 25.4-mm-id (1-in id) aluminum tubing spaced 32 mm (1.25 in) apart. This spacing allowed water and smolts to pass readily between the bars into a 76-mm (3-in) deep flume beneath, from which they were routed into the simulated conventional juvenile-fish wet separator.

The separation bars sloped downstream 25.4 mm (1 in) along their length. In addition, at the downstream end, the bars sloped 25.4 mm from left to right facing downstream. By this arrangement, adult salmonids and other large incidental fish which were unable to pass between the separation bars were guided toward the right downstream corner of the array as they slid along the separation bars. In addition to the compound slope on the separation bars, a curved, padded wall along the lower end of the unit helped guide intercepted fish toward an exit opening in the right side at the downstream end of the adult separator. The opening routed diverted animals into a flume leading to the juvenile fish bypass channel under the separator platform. A spray bar suspended over the lower end of the separator directed water along separation bars and into the return flume to prevent injury and to provide lubrication.

To determine the number of fish redirected by the adult separator (separated), an attendant counted and recorded, by species, all fish passing through the flume when the unit was operational. Non-separated fish were removed from the juvenile fish wet separator with a dipnet as they accumulated, counted by species, and returned to the bypass channel without delay.

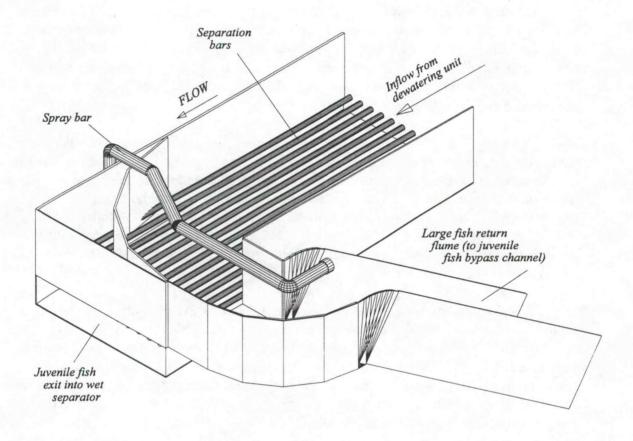


Figure 6. Major components of the adult and debris separator used to remove trash and large fish from flow carrying juvenile salmonid smolts during wet separator biological design criteria studies at McNary Dam, 1998.

Debris which did not pass between the bars (separated debris) accumulated on the adult separator separation bars and was removed manually. Trash which did pass between the bars was collected from the juvenile fish wet separator and holding tanks, and constituted the non-separated contingent.

### **Results and Discussion**

A total of 34 large fish were counted passing through the adult return flume, or were removed from the juvenile wet separator over both the spring and summer migrations. Of these, 1 was an adult steelhead, 29 were adult shad (*Alosa sapidissima*), and four were suckers (*Catostomus* spp.). Twenty nine of the total number (85%) were counted passing through the adult separator return flume. This should be considered the minimum separation efficiency for the unit, since it is possible that some individuals may have escaped visual detection. During all replicates conducted involving juvenile outmigrant salmonids, only one large steelhead smolt was known to have been intercepted and diverted by the adult separator.

The five large fish removed from the juvenile separator were all adult shad. We theorize that the laterally compressed shape of this species allowed some fish to pass between the separation bars when body alignment entering from the dewaterer was favorable.

Debris was retained over one week intervals periodically through the spring migration for comparison. Lacking a quantitative method of classification, comparison of separated and non-separated debris was subjective. The separated fraction (retained on the adult separator) was comprised mainly of larger woody debris, such as twigs and branches (Fig. 7a), while the non-separated fraction was composed largely of smaller wood chips, leaves, grasses, and aquatic plant parts (Fig. 7b). The adult separator was somewhat effective at filtering out larger debris, provided the pieces were either wider in cross section than the bar spacing, dendritic, or not oriented along the longitudinal axis of the separator bars on entering the unit.

The practicality of the adult separator as a debris removal device is dependent on application. For use in a HVF separator, smaller particles would normally pass through the wet separator (between the separation bars of the wet separator and through the submerged orifice, or over the overflow orifice), finally ending up in fish holding facilities. With a simulated conventional separator, the energy moving even small trash fragments dissipates on entering the unit, allowing the particles to accumulate on the perforated plate false bottom under the separation bars near the upstream end of the separator. Sufficiently large deposits of debris in this area could cause unpredictable flow disruption, altering effective function of the unit.

7a.



7b.



Figure 7. Debris recovered from an adult and debris separator (7a) and from a simulated conventional wet separator (7b) while evaluating the adult and debris removal unit during biological design criteria studies at McNary Dam, 1998.

#### CONCLUSIONS AND RECOMMENDATIONS

#### **Conventional Wet Separator**

- 1. Using a simulated conventional wet separator, separation efficiency for the total salmonid catch during the spring migration was highest with a 19-mm separation-bar spacing condition, or with flow diverters deployed. Subyearling chinook salmon separation efficiency was highest using 19- and 17-mm separation-bar spacing. Sockeye salmon <180 mm was the only group which displayed a significant interaction between flow diverter and separation-bar spacing conditions.</p>
- 2. Separator exit efficiency for the total salmonid catch during the spring revealed a significant interaction between flow diverter and separation-bar spacing. Exit efficiency was highest using 19-mm bar spacing without flow diverters. Subyearling chinook salmon exit efficiency was highest using a 16-mm separation-bar spacing, but not different between flow diverter conditions.
- 3. There were no statistically significant differences in mean descaling values for any group analyzed from evaluations using the simulated conventional wet separator.
- 4. Using a conventional wet separator, total salmonid catch separation efficiency was statistically similar between 17- and 19-mm separation-bar spacing conditions. Future separation efficiency studies should include additional comparison to define the distinction in separation efficiency between these separation-bar gaps.

### **High-Velocity Flume Wet Separator**

- 5. There was a significant interaction among separation-bar spacing, separation-bar-array angle and water velocity for the total salmonid catch during the spring migration using a high-velocity flume (HVF) wet separator. Separation efficiency was highest using 16-mm or 19-mm bar spacing, a 0° (flat) separation-bar array, and water velocity of 1 m/s. Fall chinook salmon separation efficiency showed no interaction among conditions, and was higher at 1 m/s water velocity, or using a flat separation-bar array.
- 6. Separator exit efficiency using the HVF displayed a significant interaction between water velocity and orientation of the separation-bar array for all groups except sockeye salmon <180 mm. For the total salmonid catch during the spring

- migration, exit efficiency was generally higher using flat separation-bar arrays regardless of water velocity, and higher at 2 m/s water velocity than at 1 m/s.
- 7. No significant differences were found among mean descaling values for groups analyzed from the spring migration using the HVF. Subyearling chinook salmon descaling was significantly higher for treatments having 2 m/s water velocity than at 1 m/s.
- 8. Using the HVF, separation efficiency for the total salmonid catch was similar between replicates tested with the 16- and 19-mm separation bar gaps. Additional work should focus on determining the separation-bar spacing within this range to determine optimal bar spacing that allows passage of small fish while restricting large fish to the area above the bars.
- 9. To date, separation efficiency evaluations have been short in duration, with replicate tests lasting from approximately 30 minutes to 8 hours. However, since separators in operation at the dams function continuously, the relationship between diel time span and separation efficiency needs to be explored.

### **Adult and Debris Separator**

10. A preliminary adult and debris separator design was at least 85% effective at intercepting and removing large fish prior to entry to a juvenile wet separator. For debris, the adult separator was somewhat effective at intercepting larger debris, but was ineffective at removing smaller particles from the water.

### **ACKNOWLEDGMENTS**

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## APPENDIX

**Data Tables** 

Appendix Table 1. Total catch, by species and length group (by fork length in millimeters) for individual replicates of separation efficiency tests using a simulated conventional wet separator at McNary Dam, 1998.

		rearling nook		arling nook	Ste	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 1, Treatmen	t 1, 27 A	pril, Bar	spacing	g 16 mn	ı, flow o	liverters	on			
Tanks: separated			33						1	
non-separated			30		15			7	1	
Separator: separated			11		1					
non-separated										
Replicate 2, Treatmen	t 1, 30 A	pril, Bar	spacin	g 16 mn	n, flow o	liverters	on			
Tanks: separated		27	1			2				12
non-separated		30	3			15				2
Separator: separated		2								1
non-separated										
Replicate 3, Treatmen	t 1, 5 Ma	y, Bar s	pacing	16 mm,	flow div	verters o	n			
Tanks: separated		75	2		22				27	
non-separated		21	3			13				5
Separator: separated			4							
non-separated		2								
Replicate 4, Treatmen	t 1, 7 Ma	y, Bar s	pacing	16 mm,	flow div	verters o	n			
Tanks: separated			6			1	31			
non-separated			9		5	3	45			
Separator: separated	4									
non-separated										
Replicate 5, Treatmen	nt 1, 11 M	lay, Bar	spacing	16 mm	, flow d	iverters	on			
Tanks: separated			23							34
non-separated			9		5		2			3
Separator: separated			1							
non-separated										
Replicate 6, Treatmer	nt 1, 12 M	Iay, Bar	spacing	16 mm	, flow d	iverters	on			
Tanks: separated			17				2			10
non-separated			14			2	51			4
Separator: separated			5				1			
non-separated										
Replicate 7, Treatmer	nt 1, 14 M	Iay, Bar	spacing	16 mm	, flow d	iverters	on			
Tanks: separated			32			6				68
non-separated			27		3	9	55			20
Separator: separated			14							1
non-separated			1			1	1			

# Appendix Table 1. Continued.

	-	earling inook		arling nook	Stee	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 8, Treatmer	nt 1. 19 M	lav. Bar	spacing	16 mm	flow di	verters	on			
Tanks: separated	, ., .,	uj, Dui	22	20 2222	,	1		1		3
non-separated			29		1	3	8	2		10
Separator: separated			10		1	1	1	_		10
non-separated			10			1	1			
Replicate 9, Treatmer	nt 1, 21 M	lay, Bar	spacing	16 mm	, flow di	verters	on			
Tanks: separated	9		31			1		5		64
non-separated	2		47		8	4	34	11		31
Separator: separated			20			2		1		2
non-separated										
Replicate 10, Treatme	ent 1, 27 I	May, Ba	r spacin	g 16 mr	n, flow o	liverter	s on			
Tanks: separated	24		7		1	2	2	2		19
non-separated	9		16		8	1	10	4		7
Separator: separated	2		1					1		2
non-separated										
Replicate 11, Treatme	ent 6, 23 J	June, Ba	r spacin	g 16 m	n, flow	diverter	s on			
Tanks: separated		189								
non-separated		37								
Separator: separated		12								
non-separated										
Replicate 12, Treatme	ent 6, 26 J	June, Ba	r spacin	g 16 m	n, flow	diverter	s on			
Tanks: separated		160								
non-separated		32								
Separator: separated		16								
non-separated										
Replicate 13, Treatme		June, Ba	r spacin	g 16 m	n, flow	diverter	s on			
Tanks: separated	45									
non-separated	23									
Separator: separated										
non-separated										
Replicate 14, Treatme		June, Ba	r spacin	g 16 m	n, flow	diverter	s on			
Tanks: separated	59									
non-separated	14									
Separator: separated	5									
non-separated										
Replicate 15, Treatme		June, Ba	r spacin	g 16 m	n, flow	diverter	s on			
Tanks: separated	134									
non-separated	56									
Separator: separated	34									
non-separated										

		earling nook		arling inook	Stee	elhead	C	Coho	Soc	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 16, Treatme	nt 6, 1 Ju	ılv, Bar	spacing	16 mm.	flow di	verters	on			
Tanks: separated	56	,			A MA					
non-separated	14									
Separator: separated	11									
non-separated										
Replicate 17, Treatme		ıly, Bar	spacing	16 mm	, flow di	verters	on			
Γanks: separated	161									
non-separated	35									
Separator: separated non-separated	31									
Replicate 18, Treatme		ıly, Bar	spacing	16 mm	, flow di	verters	on			
Γanks: separated	68									
non-separated	9									
Separator: separated	29									
non-separated										
Replicate 19, Treatme		ıly, Bar	spacing	16 mm	, flow di	verters	on			
Γanks: separated	133									
non-separated	9									
Separator: separated non-separated	58									
Replicate 20, Treatme		ıly, Bar	spacing	16 mm	, flow di	verters	on			
Γanks: separated	141									
non-separated	10									
Separator: separated	106									
non-separated										
Replicate 21, Treatme		July, Ba	r spacin	g 16 mm	n, flow o	liverter	son			
Γanks: separated	37		1							
non-separated	14		1							
Separator: separated non-separated	23		1							
Replicate 22, Treatme	ent 6, 22 J	July, Ba	r spacin	g 16 mm	n, flow o	liverters	son			
Γanks: separated	65		1							
non-separated	8		1							
Separator: separated non-separated	56									
Replicate 23, Treatme	nt 6, 15	July, Ba	r spacin	g 16 mr	n, flow	liverter	son			
Γanks: separated	92									
non-separated	34									
Separator: separated non-separated	22									

	Subyearli		Yearling chinook	Stee	lhead	C	oho	Soc	ckeye
Source	<180 ≥18			<180	≥180	<180	≥180	<180	≥180
Replicate 24, Treatme							_100	100	_10,
Fanks: separated	114	Dar spa	icing 10 mi	i, now u	iverter	SOII			
non-separated	19								
Separator: separated	28								
non-separated	20								
Replicate 25, Treatme		r spaci	ng 16 mm,	flow dive	erters o	n			
Γanks: separated	47								
non-separated	14								
Separator: separated									
non-separated									
Replicate 1, Treatmen	nt 2, 27 April,	Bar spa	and the same of th	n, flow d	-				2
Γanks: separated			5 5		3	3 12			2
non-separated			9			12			1
Separator: separated non-separated			9						1
Replicate 2, Treatmen	nt 2, 30 April,	Bar spa	cing 16 mn	ı, flow di	iverters	off			
Γanks: separated			6						5
non-separated		1	1	5		1			3
Separator: separated		1	1						1
non-separated									
Replicate 3, Treatmen	nt 2, 6 May, Ba	ar spaci	ng 16 mm,	flow div	erters o	ff			
Tanks: separated									26
non-separated			8	2		12	1		11
Separator: separated			1		1				8
non-separated									
Replicate 4, Treatmer	nt 2, 7 May, Ba	ar spaci	_	flow dive		ff			
Γanks: separated			9		1	_			42
non-separated			7		2	7			34
Separator: separated non-separated			1						9
Replicate 5, Treatmer	it 2, 11 May, F		_	, flow di	verters	off			07
Γanks: separated			1			0.4			27
non-separated			6		3	24			28
Separator: separated		1	5			,			
						1			
non-separated						- ee			
non-separated Replicate 6, Treatmer	nt 2, 12 May, H	ar spac	ing 16 mm	, flow div	verters	011			
non-separated Replicate 6, Treatmen	nt 2, 12 May, H	1	4		2	2			8
non-separated  Replicate 6, Treatmer  Fanks: separated  non-separated	nt 2, 12 May, I	1	4 9	, flow div	_				8
non-separated  Replicate 6, Treatmer Γanks: separated	nt 2, 12 May, F	1	4		2	2			

		earling nook		arling inook	Stee	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 7, Treatme	ent 2, 15 M	lay, Bar	spacing	16 mm	, flow d	iverters	off			
Tanks: separated			9							56
non-separated			29		4					9
Separator: separated			7							5
non-separated							8			
Replicate 8, Treatme	ent 2, 18 M	lay, Bar	spacing	g 16 mm	, flow d	iverters	off			-
Tanks: separated			50			1	2			25
non-separated			35		8	8	46			2
Separator: separated										
non-separated										
Replicate 9, Treatme	ent 2, 21 M	lay, Bar	spacing	g 16 mm	, flow d	iverters	off			40
Tanks: separated	2		24				2			40
non-separated			39		3	1	3	6		22
Separator: separated			20							8
non-separated										
Replicate 10, Treatn		May, B		ng 16 m	m, flow			1		22
Tanks: separated	13		8		7	1	1	1 14		22
non-separated	4		12		7	4	24	14		1
Separator: separated non-separated	3						1			1
Replicate 11, Treatn	nent 2, 23	June, Ba	ar spaci	ng 16 m	m, flow	diverter	s off			
Tanks: separated	197									
non-separated	67									
Separator: separated	10									
non-separated	10									
Replicate 12, Treatn	nent 2, 24	June, Ba	ar spaci	ng 16 m	m, flow	diverte	rs off			
Tanks: separated	155									
non-separated	49									
Separator: separated	1									
non-separated										
Replicate 13, Treatr	nent 2, 26	June, B	ar spaci	ng 16 m	m, flow	diverte	rs off			
Tanks: separated	60									
non-separated	15									
Separator: separated	1									
non-separated										
Replicate 14, Treatr		June, B	ar spaci	ng 16 m	m, flow	diverte	rs off			
	70									
non-separated	23									

		yearling ninook		arling inook	Sta	elhead	0	Coho	Sa	ckeye
	CI			IIIOOK	310	emead			30	
Source	<180		<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 15, Treat		June, Ba	ır spaciı	ng 16 m	m, flow	diverter	s off			
Γanks: separated	106									
non-separated	55									
Separator: separated										
non-separated										
Replicate 16, Treat	ment 2, 1 J	uly, Bar	spacing	16 mm	, flow di	verters	off			
Tanks: separated	219									
non-separated	64									
Separator: separated	1									
non-separated										
non separated										
Replicate 17, Treat		uly, Bar	spacing	16 mm	, flow di	verters	off			
Γanks: separated	285		1							
non-separated	117				,					
Separator: separated	21									
non-separated										
Replicate 18, Treat	ment 2, 7 J	uly, Bar	spacing	16 mm	, flow di	verters	off			
Tanks: separated	25,413									
non-separated										
Separator: separated	14									
non-separated	4									
Replicate 19, Treat	ment 2 8 I	uly Ror	enacino	16 mm	flow di	verters	off			
Tanks: separated	136	uly, Dai	spacing	, 10 mm	, HOW UI	verters	JII.			
non-separated	12									
	109									
Separator: separated	109									
non-separated										
Replicate 20, Treati			r spacin	g 16 mn	n, flow d	iverters	off			
Γanks: separated	128	1								
non-separated	20	2								
Separator: separated	90									
non-separated										
Replicate 21, Treat	ment 2, 13	July, Ba	r spacin	g 16 mr	n, flow o	liverters	off			
tepineute ma, areas	56		1							
	0									
	8									
Γanks: separated non-separated	24									
Tanks: separated non-separated										
Fanks: separated non-separated Separator: separated non-separated	24 1	July Ro	r snacin	og 16 mr	n flow e	liverters	off			
Fanks: separated non-separated Separator: separated non-separated Replicate 22, Treati	24 1 ment 2, 13	July, Ba	r spacin	ng 16 mr	n, flow o	liverters	off			
Tanks: separated non-separated Separator: separated non-separated Replicate 22, Treation Fanks: separated	24 1 ment 2, 13 269	July, Ba	r spacin	ng 16 mr	n, flow o	liverters	off			
Tanks: separated non-separated Separator: separated non-separated Feplicate 22, Treator Tanks: separated non-separated non-separated	24 1 ment 2, 13	July, Ba	r spacin	ng 16 mr	n, flow o	liverters	off			
Tanks: separated non-separated Separator: separated non-separated Replicate 22, Treation Fanks: separated	24 1 ment 2, 13 269	July, Ba	r spacin	ng 16 mr	n, flow o	liverters	off			

		yearling inook		arling inook	Ste	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 23, Treatm									7100	
Tanks: separated	281	July, Da	spacin	g To IIII	ii, HOW (	aivei ter	3 UII			
non-separated	4									
Separator: separated	61									
non-separated	14									
Replicate 24, Treatm	ent 2, 20	Iulv. Ba	r spacin	g 16 mm	n, flow	liverter	s off			
Tanks: separated	43	, , ,	1	8	,					
non-separated	17									
Separator: separated	7.									
non-separated										
Replicate 25, Treatm	ent 2, 23	July, Ba	r spacin	g 16 mm	n, flow	liverter	s off			
Tanks: separated	43		•	0						
non-separated	13									
Separator: separated	3									
non-separated										
Replicate 1, Treatme	ent 3, 28 A	pril, Ba	r spacin	g 17 mn	n, flow o	liverter	son			
Tanks: separated			74		6		1			
non-separated			56		40		9			
Separator: separated										
non-separated			1							
Replicate 2, Treatme	ent 3, 1 Ma	ay, Bar s	pacing	17 mm,	flow div	verters o	on			
Tanks: separated			46		2					4
non-separated			. 3		5		4			1
Separator: separated						1				
non-separated										
Replicate 3, Treatme	ent 3, 6 Ma	ay, Bar	pacing	17 mm,	flow div					
Tanks: separated			21			2	7			28
non-separated			12		5		21			22
Separator: separated			8							2
non-separated							1			
Replicate 4, Treatme	ent 3, 8 Ma	ay, Bar	pacing	17 mm,	flow div		n			
Tanks: separated			7			2				41
non-separated			2 2		1	2	7			24
Separator: separated			2				1			4
non-separated										
Replicate 5, Treatme	ent 3, 5 Ma	ay, Bar	spacing	17 mm,	flow di	verters o				
Tanks: separated			7				1			14
non-separated			7		1	1	30			3
Separator: separated			2				1			
non-separated										

	Subyearling chinook	Yearling chinook	Stee	lhead	C	oho	Soc	ckeye
Source	<180 ≥180	<180 ≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 6, Treatme	nt 3, 13 May, Bar	spacing 17 mm	, flow di	verters	on			
Tanks: separated		19		3	5			44
non-separated		17	2	2	29			11
Separator: separated		4		2				
non-separated					1			
Replicate 7, Treatme	nt 3, 18 May, Bar	spacing 17 mm	, flow di	verters	on			
Tanks: separated		17						111
non-separated	1	20	2		9	11		29
Separator: separated		13		1				17
non-separated								
Replicate 8, Treatme	nt 3, 19 May, Bar		, flow di	verters	on			
Tanks: separated		19						18
non-separated		6		2	6			1
Separator: separated		1						4
non-separated								
Replicate 9, Treatme	nt 3, 25 May, Bar	spacing 17 mm	, flow di	verters	on			
Tanks: separated	7	15	1		2	3		20
non-separated	1	14	9		30	10		20
Separator: separated		1						4
non-separated								
Replicate 10, Treatm	ent 3, 1 June, Bar	spacing 17 mm	, flow di	verters	on			
Tanks: separated	55	8			2	1		5
non-separated	22	4	2		3	7	1	20
Separator: separated		1						
non-separated			1					
Replicate 11, Treatm	ent 3, 23 June, Ba	ar spacing 17 m	m, flow o	diverter	s on			
Tanks: separated	213	1						
non-separated	24		1					
Separator: separated	1							
non-separated								
Replicate 12, Treatm	ent 3, 25 June, Ba	ar spacing 17 m	m, flow o	diverter	s on			
Tanks: separated	190							
non-separated	30							
Separator: separated	20							
non-separated								
Replicate 13, Treatm	ent 3, 26 June, Ba	ar spacing 17 m	m, flow o	diverte	rs on			
Tanks: separated	54							
non-separated	15							
Separator: separated								
non-separated								
non separated								

		yearling inook		arling nook	Stee	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 14, Treatme	ent 3. 29	Iune. Ba	r spacir	ng 17 m	m. flow	diverter	s on	- 10		THE STATE OF
Tanks: separated	171	,,		8	,					
non-separated	29									
Separator: separated	13									
non-separated	10									
Replicate 15, Treatme		June, Ba	r spacir	ng 17 m	m, flow	diverter	s on			
Γanks: separated	72									
non-separated	24									
Separator: separated	9									
non-separated										
Replicate 16, Treatme		uly, Bar	spacing	17 mm	, flow di	verters	on			
Tanks: separated	71		1							
non-separated	4		1							
Separator: separated	11									
non-separated										
Replicate 17, Treatm		uly, Bar	spacing	17 mm	, flow di	iverters	on			
Tanks: separated	128									
non-separated	22									
Separator: separated non-separated	80									
Replicate 18, Treatm	ent 3, 8 J	uly, Bar	spacing	17 mm	, flow d	iverters	on			
Tanks: separated	151									
non-separated	27									
Separator: separated	79									
non-separated										
Replicate 19, Treatm	ent 3, 9 J	uly, Bar	spacing	17 mm	, flow d	iverters	on			
Tanks: separated	125		3							
non-separated	13									
Separator: separated	60									
non-separated										
	ent 3, 10	July, Ba	r spacin	ıg 17 mı	n, flow	diverter	s on			
	00		1							
Tanks: separated	92									
Γanks: separated non-separated	9		1							
non-separated Separator: separated			1							
Γanks: separated non-separated	9		1							
Tanks: separated non-separated Separator: separated non-separated Replicate 21, Treatm	9 59	July, Ba		ng 17 mi	m, flow	diverter	s on			
Tanks: separated non-separated Separator: separated non-separated Replicate 21, Treatm	9 59	July, Ba		ng 17 mi	m, flow	diverter	s on			
Tanks: separated non-separated Separator: separated non-separated Replicate 21, Treatm	9 59 ent 3, 13	July, Ba		ng 17 mi	m, flow	diverter	s on			
Tanks: separated non-separated Separator: separated non-separated Replicate 21, Treatm Tanks: separated	9 59 ent 3, 13 43	July, Ba		ng 17 mi	m, flow	diverter	s on			

		earling		arling inook	Stee	elhead	C	oho	So	ckeye
Source	<180	≥180		≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatme										-
Tanks: separated	86	uly, Da	spacin	g I / IIII	ii, iiow c	arver ter	3 OII			
non-separated	6		1							
Separator: separated	48		1							
non-separated			•							
Replicate 23, Treatme	nt 3, 15	July, Ba	r spacin	g 17 mr	n, flow o	liverter	s on			
Tanks: separated	58		•							
non-separated	12									
Separator: separated	17									
non-separated										
Replicate 24, Treatme	nt 3, 21	July, Ba	r spacin	g 17 mr	n, flow d	liverter	s on			
Tanks: separated	54									
non-separated	9									
Separator: separated	29									
non-separated										
Replicate 25, Treatme	nt 3, 24	July, Ba	r spacin	g 17 mr	n, flow d	liverter	s on			
Tanks: separated	48									
non-separated	16									
Separator: separated	22									
non-separated										
Replicate 1, Treatmen	t 4, 27 A	pril, Ba	r spacin	g 17 mn	n, flow d	liverter	s off			
Tanks: separated			74		2	2				
non-separated			27		11	3	8			
Separator: separated			1							
non-separated			4		5					
Replicate 2, Treatmen	t 4, 1 Ma	y, Bar s	pacing	17 mm,	flow div	verters o	off			
Tanks: separated			36			1	1			11
non-separated			19			3	12			2
Separator: separated			3							
non-separated			2							
Replicate 3, Treatmen	t 4, 6 Ma	y, Bar s	pacing	17 mm,	flow div	verters o	off			50
Tanks: separated			7							59
announted			6		1		2			
non-separated			9							33
Separator: separated										18
Separator: separated non-separated  Replicate 4, Treatmen	nt 4, 8 Ma	ıy, Bar s	pacing	17 mm,	flow div	verters o	off			
Separator: separated non-separated  Replicate 4, Treatmen Tanks: separated	at 4, 8 Ma	ny, Bar s	3	17 mm,	1	verters o				53
Separator: separated non-separated  Replicate 4, Treatmen Tanks: separated non-separated	nt 4, 8 Ma	ıy, Bar s	-	17 mm,		verters (	off 3	2		53 20
Separator: separated non-separated  Replicate 4, Treatmen Tanks: separated	at 4, 8 Ma	ny, Bar s	3	17 mm,	1	verters (		2		

		earling nook		arling nook	Stee	elhead	C	Coho	So	ckeye	
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180	
Replicate 5, Treatmen	t 4, 12 M	ay, Bar	spacing	17 mm	, flow di	verters	off	MALE			
Tanks: separated			5			2	1			44	
non-separated			4				3	2		8	
Separator: separated			2							4	
non-separated											
Replicate 6, Treatmen	it 4, 13 M	ay, Bar	spacing	17 mm	, flow di	iverters					
Tanks: separated			8				2	1		6	
non-separated			1		6		16	2		4	
Separator: separated			2		1		1				
non-separated											
Replicate 7, Treatmen	nt 4, 15 M	ay, Bar		17 mm	, flow di					27	
Tanks: separated			43		1	2	2			27	
non-separated			36		5	9	44			13	
Separator: separated			1							2	
non-separated							1				
Replicate 8, Treatmen	at 4, 20 M	lay, Bar		17 mm	, flow d	iverters		1.		20	
Tanks: separated	1		19		_	1	1	1		38	
non-separated	1		13		2		1	2		6	
Separator: separated			2							2	
non-separated											
Replicate 9, Treatmen		lay, Bar		17 mm		iverters	off			0.0	
Tanks: separated	8		60		1	_	17	10		88	
non-separated			. 32		17	2	17	12		29	
Separator: separated			11			1				4	
non-separated											
Replicate 11, Treatme		June, Ba	ar spacin	ıg 17 m	m, flow	diverte	rs off				
Tanks: separated	278										
non-separated	26										
Separator: separated						1					
non-separated						1					
Replicate 12, Treatme		June, Ba	ar spacin	ıg 17 m	m, flow	diverte	rs off				
Tanks: separated	130										
non-separated	17										
Separator: separated non-separated											
Replicate 13, Treatme	ent 4, 26	June, Ba	ar spacin	ıg 17 m	m, flow	diverte	rs off				
Tanks: separated	53										
non-separated	12										
Separator: separated											
non-separated											

# Appendix Table 1. Continued.

	Subyearli chinool	-	arling inook	Ste	elhead	С	oho	Soc	ckeye
Source	<180 ≥1	80 <180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 14, Treatme									
Γanks: separated	151	Dur space		11, 110 !!	41,6166	0 011			
non-separated	9								
Separator: separated	5								
non-separated									
Replicate 15, Treatme	ent 4, 30 June,	Bar spaci	ng 17 mr	n, flow	diverter	s off			
Γanks: separated	496								
non-separated	60								
Separator: separated	1								
non-separated									
Replicate 16, Treatme			g 17 mm,	flow di	verters	off			
Γanks: separated	110	3							
non-separated									
Separator: separated									
non-separated									
Replicate 17, Treatme		Bar spacing	g 17 mm,	flow di	verters	off			
Γanks: separated	17								
non-separated	22								
Separator: separated non-separated	45								
Replicate 18, Treatmo	ent 4, 8 July, I	Bar spacing	2 17 mm,	flow di	verters	off			
Tanks: separated	127								
non-separated	20								
Separator: separated	101								
non-separated									
Replicate 19, Treatme		Bar spacing	g 17 mm,	flow di	verters	off			
Γanks: separated	104	Bar spacing	g 17 mm,	flow di	verters	off			
Γanks: separated non-separated	104 25	Bar spacing	g 17 mm,	flow di	verters	off			
Fanks: separated non-separated Separator: separated	104 25 101	Bar spacing	g 17 mm,	flow di	verters	off			
Tanks: separated non-separated	104 25	3ar spacing	g 17 mm,	flow di	verters	off			
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatme	104 25 101 1 ent 4, 10 July,	Bar spacir							
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatmeranks: separated	104 25 101 1 ent 4, 10 July, 56								
Fanks: separated non-separated Separator: separated non-separated Fanks: separated non-separated non-separated non-separated	104 25 101 1 ent 4, 10 July,	Bar spacir							
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatmer Fanks: separated non-separated Separated Separator: separated	104 25 101 1 ent 4, 10 July, 56	Bar spacir							
Fanks: separated non-separated Separator: separated non-separated Fanks: separated non-separated non-separated non-separated	104 25 101 1 ent 4, 10 July, 56	Bar spacir							
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatmer anks: separated non-separated separator: separated non-separated separator: separated non-separated Replicate 21, Treatmer separated Replicate 21, Treatmer separated non-separated Replicate 21, Treatmer separated non-separated Replicate 21, Treatmer separated non-separated separated separated non-separated separated non-separated separated non-separated separated non-separated separated non-separated non-separated non-separated separated non-separated non	104 25 101 1 ent 4, 10 July, 56 3	Bar spacir 1	ng 17 mn	a, flow (	liverter	s off			
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatmeranks: separated non-separated separator: separated non-separated separator: separated non-separated non-separated separated separated separated separated Replicate 21, Treatmeranks: separated	104 25 101 1 ent 4, 10 July, 56 3	Bar spacir 1	ng 17 mn	a, flow (	liverter	s off			
Fanks: separated non-separated Separator: separated non-separated Fanks: separated non-separated non-separated separator: separated non-separated Replicate 21, Treatmeranks: separated non-separated non-separated non-separated non-separated non-separated	104 25 101 1 ent 4, 10 July, 56 3 ent 4, 13 July, 38 5	Bar spacir 1	ng 17 mn	a, flow (	liverter	s off			
Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatmeranks: separated non-separated separator: separated non-separated separator: separated non-separated non-separated separated separated separated separated Replicate 21, Treatmeranks: separated	104 25 101 1 ent 4, 10 July, 56 3	Bar spacir 1	ng 17 mn	a, flow (	liverter	s off			

		yearling inook		arling inook	Ste	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatme	ent 4, 14	July, Bar	r spacin	g 17 mm	n, flow	diverter	s off			
Tanks: separated	122	•								
non-separated	15									
Separator: separated non-separated	54									
Replicate 23, Treatme	ent 4, 15	July, Ba	r spacin	g 17 mn	n, flow	diverter	s off			
Tanks: separated	126									
non-separated	5									
Separator: separated	50									
non-separated	1									
Replicate 24, Treatm	ent 4, 20	July, Ba	r spacin	g 17 mm	n, flow	diverter	s off			
Tanks: separated	58									
non-separated	3			1						
Separator: separated non-separated	46									
		Lulu Da		~ 17 mm	n flow	divortor	c off			
Replicate 25, Treatm		July, Ba	r spacin	ig 17 min	n, now	uiverter	SOII			
Tanks: separated	53									
non-separated	12 23									
Separator: separated	23									
non-separated										
Replicate 1, Treatme	nt 5, 29 A	pril, Ba		g 19 mn						17
Tanks: separated			105		4	3	3			17
non-separated			10		5		3			1
Separator: separated										
non-separated										
Replicate 2, Treatme	nt 5, 4 Ma	ay, Bar s		19 mm,	flow div	verters (				1.4
Tanks: separated			63				1			14
non-separated			11				5			
Separator: separated non-separated			19							
Replicate 3, Treatme	nt 5, 7 Ms	av. Bar s	pacing	19 mm.	flow div	verters o	on			
Tanks: separated		.,	16					1		47
non-separated			13			2	4			18
Separator: separated			17					1		15
non-separated										
Replicate 4, Treatme	nt 5, 11 M	Iay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Tanks: separated			18		2	3	6			127
non-separated			3		3	2	18	2		8
Separator: separated			5				4	2		9
non-separated										

		earling inook		arling inook	Stee	elhead	Coho		So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 5, Treatmer	nt 5, 12 M	ay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Tanks: separated			37		1	1	1			324
non-separated			7							4 .
Separator: separated			7			1				3
non-separated					1					
Replicate 6, Treatmer	nt 5, 14 M	ay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Γanks: separated			2							40
non-separated			1		1					6
Separator: separated			7		1		1	1		5
non-separated										
Replicate 7, Treatmer	nt 5, 18 M	ay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Tanks: separated		-	47			6				38
non-separated			14				2			9
Separator: separated			2							2
non-separated										
Replicate 8, Treatmer	nt 5, 20 M	ay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Γanks: separated		•	17			1	2			13
non-separated			3			1	10			
Separator: separated										
non-separated										
Replicate 9, Treatmer	nt 5, 26 M	ay, Bar	spacing	g 19 mm	, flow d	iverters	on			
Tanks: separated	11		13		2		1	2		18
non-separated	4		10		8	4	37	5		6
Separator: separated										
non-separated			2							
Replicate 11, Treatme	ent 5, 24 J	June, Ba	ır spaciı	ng 19 m	m, flow	diverter	s on			
Tanks: separated	149									
non-separated	37									
Separator: separated	20									
non-separated	1									
Replicate 12, Treatme	ent 5, 25 J	June, Ba	ır spaciı	ng 19 m	m, flow	diverter	's on			
Tanks: separated	194									
non-separated	16									
Separator: separated	2									
non-separated	1									
Replicate 12, Treatme	ent 5, 25	June, Ba	ar spacii	ng 19 m	m, flow	diverte	s on			
Tanks: separated			_							
non-separated										
Separator: separated										
non-separated				*						

	yearling inook		arling inook	Stee	elhead	C	oho	So	ckeye
<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
it 5, 26.	June, Ba	r spacii	ng 19 mi	m, flow	diverter	s on			
87									
21									
6									
	June, Ba	r spacii	ng 19 m	m, flow	diverter	s on			
78									
	June, Ba	r spacii	ng 19 mi	m, flow	diverter	son			
32									
	uly, Bar		19 mm	, flow di	verters	on			
		5							
34									
	uly, Bar	spacing	19 mm	, flow di	verters	on			
27									
	uly, Bar	spacing	19 mm	, flow di	verters	on			
53									
	uly, Bar	spacing	19 mm	, flow di	verters	on			
142		1							
		1							
66									
	July, Ba	r spacin	ıg 19 mr	n, flow o	liverters	on			
59									
12									
12									
7									
	<180  it 5, 26, 87 21 6  it 5, 29, 190 56 78  it 5, 30, 1125 21 32  it 5, 2 Ji 134 5 34  it 5, 7 Ji 137 11 27  it 5, 8 Ji 142 17 66  it 5, 10, 59	nt 5, 26 June, Ba 87 21 6 nt 5, 29 June, Ba 190 56 78 nt 5, 30 June, Ba 1125 21 32 nt 5, 2 July, Bar 134 5 34 nt 5, 7 July, Bar 137 11 27 nt 5, 8 July, Bar 110 13 53 nt 5, 9 July, Bar 142 17 66 nt 5, 10 July, Bar 59	<pre>&lt;180 ≥180 &lt;180 nt 5, 26 June, Bar spacin 87 21 6 nt 5, 29 June, Bar spacin 190 56 78 nt 5, 30 June, Bar spacin 1125 21 32 nt 5, 2 July, Bar spacin 134 5 34 nt 5, 7 July, Bar spacin 137 11 27 nt 5, 8 July, Bar spacin 110 13 53 nt 5, 9 July, Bar spacin 142 17 166 nt 5, 10 July, Bar spacin 59</pre>	<180 ≥180 <180 ≥180   ≥180       t 5, 26 June, Bar spacing 19 mm   87   21   6       t 5, 29 June, Bar spacing 19 mm   190   56   78       t 5, 30 June, Bar spacing 19 mm   1125   21   32       t 5, 2 July, Bar spacing 19 mm   134   5       t 5, 7 July, Bar spacing 19 mm   137   11   27       t 5, 8 July, Bar spacing 19 mm   110   13   53       t 5, 9 July, Bar spacing 19 mm   142   1   1   66       t 5, 10 July, Bar spacing 19 mm   59					<180   ≥180   <180   ≥180   <180   ≥180   <180   ≥180   <180   ≥180   <180   ≥180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180   <180

		earling nook		arling nook	Stee	elhead	C	oho	Soc	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 21, Treatme		uly, Bai	r spacin	g 19 mn	n, flow o	liverter	son			
Tanks: separated	65 8									
non-separated	36									
Separator: separated non-separated	30									
Replicate 22, Treatme	ent 5, 14 J	uly, Bai	r spacin	g 19 mn	ı, flow d	liverter	on			
Tanks: separated	118									
non-separated	5									
Separator: separated	91									
non-separated										
Replicate 23, Treatme	ent 5, 16 J	uly, Bar	r spacin	g 19 mn	n, flow o	liverter	on			
Tanks: separated	24									
non-separated	12									
Separator: separated	31									
non-separated										
Replicate 24, Treatme	ent 5, 22 J	uly, Bar	r spacin	g 19 mn	ı, flow d	liverter	on			
Tanks: separated	58									
non-separated	9									
Separator: separated	11									
non-separated										
Replicate 25, Treatme	ent 5, 27 J	uly, Bai	r spacin	g 19 mn	n, flow o	liverter	on			
Tanks: separated	91									
non-separated	12									
Separator: separated	19									
non-separated										
Replicate 1, Treatmen	t 6, 29 Ap	oril, Bar	spacin	g 19 mm	, flow d	liverters	off			
			15			1	2			6
Tanks: separated			45		4	1				
Tanks: separated non-separated			14		4	1	14			2
non-separated Separator: separated										2
non-separated										2
non-separated Separator: separated	at 6, 4 Ma	y, Bar s	14	19 mm,	3	1	14			
non-separated Separator: separated non-separated Replicate 2, Treatmen	at 6, 4 Ma	y, Bar s	pacing 1	19 mm,	3	1	14 <b>ff</b> 6			10
non-separated Separator: separated non-separated Replicate 2, Treatmen	nt 6, 4 Ma	y, Bar s	14  pacing : 95 35	19 mm,	3	1	14 ff			10 3
non-separated Separator: separated non-separated  Replicate 2, Treatmen Tanks: separated non-separated Separator: separated	at 6, 4 Ma	y, Bar s	pacing 1	19 mm,	3 flow div	l verters o	14 <b>ff</b> 6			10
non-separated Separator: separated non-separated  Replicate 2, Treatmen Tanks: separated non-separated	at 6, 4 Ma	y, Bar s	14  pacing : 95 35	19 mm,	3 flow div	l verters o	14 <b>ff</b> 6			10 3
non-separated Separator: separated non-separated  Replicate 2, Treatmen Tanks: separated non-separated Separator: separated non-separated non-separated		ię k	pacing: 95 35 22 1		3 flow div	verters o	14 <b>ff</b> 6 7			10 3
non-separated Separator: separated non-separated  Replicate 2, Treatmen Tanks: separated non-separated Separator: separated		ię k	pacing: 95 35 22 1		3 flow div	verters o	14 <b>ff</b> 6 7			10 3
non-separated Separator: separated non-separated  Replicate 2, Treatmen Tanks: separated non-separated Separator: separated non-separated Replicate 3, Treatmen		ię k	pacing : 95 35 22 1 pacing :		3 flow div	verters of	14  off 6 7			10 3 3
non-separated Separator: separated non-separated Replicate 2, Treatmen Tanks: separated non-separated Separator: separated non-separated Replicate 3, Treatmen Tanks: separated		ię k	pacing 95 35 22 1 pacing 9		3 flow div	verters of	14  off 6 7			10 3 3

		yearling		arling					Coaleana	
	ch	ninook	ch	inook	Stee	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 4, Treatmen	nt 6, 8 M	ay, Bar s	pacing	19 mm,	flow div	erters o				
Tanks: separated			13			1	7			11
non-separated			11		4	2	28			6
Separator: separated										
non-separated										
Replicate 5, Treatmen	nt 6, 12 N	Aay, Bar	spacing	g 19 mm	, flow di	iverters	off			
Tanks: separated			34		1	2	5			68
non-separated			17		3	1	11			
Separator: separated										
non-separated										
Replicate 6, Treatmen	nt 6, 13 N	Aay, Bar	spacing	g 19 mm	, flow di	iverters	off			
Γanks: separated			16				7			20
non-separated			11		1	4	39			5
Separator: separated										
non-separated										
Replicate 7, Treatmen	nt 6, 18 N	Aay, Bar	spacing	g 19 mm	, flow di	iverters	off			
Tanks: separated			27		1	2				45
non-separated			22				5			11
Separator: separated			5							2
non-separated										
Replicate 8, Treatmen	nt 6, 20 N	Iay, Bar	spacing	g 19 mm	, flow di	iverters	off			
Tanks: separated	1		26		1	4				27
non-separated	4		27		2					16
Separator: separated			2			1				
non-separated										
Replicate 9, Treatmen	nt 6. 27 N	lav. Bar	spacing	2 19 mm	. flow di	iverters	off			
Tanks: separated	9	14, 241	17	,	,			7		23
non-separated	6		18		3	6	26	7	7	
Separator: separated		14	1		_	2	1		3	
non-separated										
Replicate 11, Treatme	ent 6, 24	June, Ba	r spacii	ng 19 m	m. flow	diverter	s off			
Γanks: separated	177	,	-1	8	,					
non-separated	38									
Separator: separated	50									
non-separated										
Replicate 12, Treatmo	ent 6. 25	June. Ba	r spacii	ng 19 mi	m. flow	diverter	s off			
Tanks: separated	290	ounc, Da	1	-6 17 111	,		~ ~~			
non-separated	44		1							
Separator: separated	15									
non-separated	15									
non-separated										

## Appendix Table 1. Continued.

		earling		arling	C: "	1		Sala -	0	ale -
	chi	nook	chi	nook	Steell	nead	C	Coho	Soc	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 13, Treatm	ent 6, 26 J	une, Ba	r spacin	g 19 mm	n, flow di	verter	s off			
Γanks: separated	100									
non-separated	22									
Separator: separated	11									
non-separated										
Replicate 14, Treatm	ent 6, 30 J	une, Ba	r spacin	g 19 mn	n, flow di	verter	s off			
Tanks: separated	110		-							
non-separated	38									
Separator: separated	4									
non-separated										
Replicate 15, Treatm	ent 6, 30 J	une, Ba	r spacir	ıg 19 mn	n, flow di	verter	s off			
Tanks: separated	30		-							
non-separated	5									
Separator: separated	1									
non-separated										
Replicate 16, Treatm	ent 6, 2 Ju	lly, Bar	spacing	19 mm,	flow dive	erters	off			
Tanks: separated	111	1								
non-separated	16	2								
Separator: separated	39									
non-separated										
Replicate 17, Treatm	ent 6, 7 Ju	ıly, Bar	spacing	19 mm,	flow dive	erters	off			
Γanks: separated	95									
non-separated	16									
Separator: separated	25									
	1									
non-separated										
		ly, Bar	spacing	19 mm,	flow dive	erters (	off			
Replicate 18, Treatm		ıly, Bar	spacing	19 mm,	flow dive	erters	off			
Replicate 18, Treatm	ent 6, 8 Ju	ıly, Bar	spacing	19 mm,	flow dive	erters	off			
Replicate 18, Treatm Fanks: separated non-separated	nent 6, 8 Ju 116	ıly, Bar	spacing	19 mm,	flow dive	erters	off			
Replicate 18, Treatm Fanks: separated non-separated	116 15	ıly, Bar	spacing	19 mm,	flow dive	erters	off			
Replicate 18, Treatm Fanks: separated non-separated Separator: separated non-separated	116 15 68									
Replicate 18, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Fanks: separated	116 15 68 nent 6, 9 Ju									
Replicate 18, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Fanks: separated non-separated	116 15 68 nent 6, 9 Ju 84 9									
Replicate 18, Treatm Fanks: separated non-separated separator: separated non-separated Replicate 19, Treatm Fanks: separated non-separated Separator: separated	116 15 68 nent 6, 9 Ju									
Replicate 18, Treatm Tanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Tanks: separated non-separated	116 15 68 nent 6, 9 Ju 84 9									
Replicate 18, Treatm Tanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Tanks: separated non-separated Separator: separated non-separated Replicate 20, Treatm	nent 6, 8 Ju 116 15 68 nent 6, 9 Ju 84 9 87	ıly, Bar	spacing	19 mm,	flow dive	erters (	off			
Replicate 18, Treatm Tanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Tanks: separated non-separated Separator: separated non-separated Replicate 20, Treatm Tanks: separated	nent 6, 8 Ju 116 15 68 nent 6, 9 Ju 84 9 87	ıly, Bar	spacing	19 mm,	flow dive	erters (	off			
Replicate 18, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatm Fanks: separated non-separated	nent 6, 8 Ju 116 15 68 nent 6, 9 Ju 84 9 87 nent 6, 10 J 53 6	ıly, Bar	spacing	19 mm,	flow dive	erters (	off			
Replicate 18, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 19, Treatm Fanks: separated non-separated Separator: separated non-separated Replicate 20, Treatm Fanks: separated	nent 6, 8 Ju 116 15 68 nent 6, 9 Ju 84 9 87	ıly, Bar	spacing	19 mm,	flow dive	erters (	off			

		earling nook		arling inook	Ste	elhead	C	Coho	So	ckeye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 21, Treatme	ent 6, 13 J	uly, Ba	r spacin	g 19 mn	n, flow	diverter	off			
Tanks: separated	148									
non-separated	7									
Separator: separated	92	-								
non-separated										
Replicate 22, Treatme	ent 6, 14 J	uly, Ba	r spacin	ıg 19 mn	n, flow o	liverter	s off			
Tanks: separated	108									
non-separated	4									
Separator: separated	139									
non-separated	1									
Replicate 23, Treatme	ent 6, 16 J	uly, Ba	r spacin	ıg 19 mn	n, flow o	diverter	s off			
Tanks: separated	68									
non-separated	17									
Separator: separated non-separated	105									
Replicate 24, Treatme	ent 6, 22 J	luly, Ba	r spacin	ıg 19 mr	n, flow o	diverter	s off			
Tanks: separated	58									
non-separated	10									
Separator: separated	11									
non-separated	2									
Replicate 25, Treatme	ent 6, 28 J	luly, Ba	r spacin	ıg 19 mr	n, flow	diverter	soff			
Γanks: separated	82									
non-separated	18									
Separator: separated	114									
non-separated										

Appendix Table 2. Incidental species captured during separator efficiency studies using a McNary-style wet separator and a high-velocity flume wet separator during biological design criteria studies at McNary Dam, 27 April-30 July, 1998. Species are listed in order of total capture frequency.

Common name	Scientific name	Conventional wet separator	HVF flume wet separator	Total
lamprey	Lampetra tridentata	1,163	3,119	4,282
sucker	Catostomus spp.	25	48	73
shad	Alosa sapidissima	29	42	71
yellow perch	Perca flavescens	6	19	25
chiselmouth	Acrocheilus alutaceus	9	25	34
whitefish	Prosopium williamsoni	10	39	49
peamouth	Mylocheilus caurinus	3	11	14
redside shiner	Richardsonius balteatus	1	3	4
carp	Cyprinus carpio		3	3
sand roller	Columbia transmontanus		3	3
northern pikeminnow	Ptychocheilus oregonensis		3	3
bass	Micropterus spp.	1	1	2
stickleback	Gasterosteus aculeatus	1		1
white sturgeon	Acipenser transmontanus		1	1

Appendix Table 3. Analyses of covariance results among mean separation efficiency values obtained for treatments involving separation-bar spacing (gap) and flow diverter (diverter) condition during biological design criteria studies using a simulated conventional wet separator at McNary Dam, 1998. Sample date (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates. A significant difference ( $\alpha = 0.05$ ) among means is indicated by an asterisk.

0	Length	Analysis	Г	16	D
Species	group	source	F	df	P
Yearling chinook salmon	<180 mm	date	9.64	1	0.004*
Tearing chinook saimon	<100 IIIII		13.10	2	0.000*
		gap diverter	14.35	1	0.000*
		gap vs. diverter	1.53	2	0.230
	total catch	date	6.32	1	0.000*
	total catch		2.91	2	0.066
		gap diverter	3.13	1	0.085
		gap vs. diverter	0.17	2	0.846
Steelhead	≥180 mm	gap	9.10	2	0.002*
Steemead	2100 mm	diverter	0.31	1	0.586
		gap vs. diverter	0.46	2	0.642
	total catch	gap	0.37	2	0.696
		diverter	0.03	1	0.870
		gap vs. diverter	0.10	2	0.905
Sockeye	<180 mm	gap	2.62	2	0.88
Security		diverter	0.21	1	0.648
		gap vs. diverter	4.15	2	0.025*
Total salmonid species	<180 mm	date	13.28	1	0.001*
(spring outmigration)		gap	7.75	2	0.001*
		diverter	5.12	1	0.028*
		gap vs. diverter	2.60	2	0.084
	≥180 mm	gap	23.12	2	0.000*
		diverter	2.20	1	0.152
		gap vs. diverter	0.35	2	0.712

Appendix Table 3. Continued.

	Length	Analysis		
Species	group	source	F	dfP
Total salmonid species	total catch	date	11.82	10.001*
(spring outmigration)		gap	4.70	2
	0.013*			
		diverter	6.72	1
	0.012			
		gap vs. diverter	2.63	2
	0.082			
Subyearling chinook salmon	<180 mm	date	9.45	10.003*
		gap	9.99	2
	0.000*			
		diverter	0.05	1
	0.824			
		gap vs. diverter	1.10	2
	0.338			

Appendix Table 4. Analyses of covariance results among mean separator exit efficiency values obtained for treatments involving separation-bar spacing (gap) and flow diverter (diverter) condition during biological design criteria studies using a simulated conventional wet separator at McNary Dam, 1998. Sample date (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates. A significant difference ( = 0.05) among means is indicated by an asterisk.

Species	Length group	Analysis source	F	df	P
Yearling chinook	<180 mm	date	0.00	1	0.987
salmon		gap	0.73	2	0.487
		diverter	0.09	1	0.760
		gap vs. diverter	1.60	2	0.214
	total catch	date	0.04	1	0.851
		gap	0.63	2	0.537
		diverter	0.09	1	0.763
		gap vs. diverter	1.76	2	0.186
Steelhead	≥180 mm	gap	0.80	2	0.464
		diverter	0.56	1	0.465
		gap vs. diverter	2.06	2	0.160
	total catch	gap	0.25	2	0.784
		diverter	1.53	1	0.231
		gap vs. diverter	1.92	2	0.173
Sockeye	<180 mm	gap	0.07	2	0.933
		diverter	0.04	1	0.851
		gap vs. diverter	2.60	2	0.091
Total salmonid	<180 mm	date	2.13	1	0.150
species (spring		gap	0.99	2	0.380
outmigration)		diverter	0.36	1	0.554
		gap vs. diverter	2.51	2	0.092
	≥ 180 mm	gap	0.31	2	0.736
		diverter	0.02	1	0.892
		gap vs. diverter	1.47	2	0.252
Total salmonid	total catch	date	1.19	1	0.280
species (spring		gap	1.86	2	0.167
outmigration)		diverter	0.02	1	0.886
		gap vs. diverter	4.59	2	$0.015^{\circ}$
Subyearling	<180 mm	date	46.50	1	$0.000^{\circ}$
chinook salmon		gap	5.32	2	0.007
		diverter	0.33	1	0.566
		gap vs. diverter	1.55	2	0.219

Appendix Table 5. Analyses of covariance results among descaling values obtained for treatments involving separation-bar spacing (gap) and flow diverter (diverter) condition using a simulated conventional wet separator during biological design criteria studies at McNary Dam, 1998. Sample date (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates. A significant difference ( $\alpha = 0.05$ ) among means is indicated by an asterisk.

Species	Length group	Analysis source	F	df	P
Yearling chinook salmon	<180 mm	date	0.00	1	0.987
		gap	0.73	2	0.487
		diverter	0.09	1	0.760
		gap vs. diverter	1.60	2	0.214
	total catch	date	0.28	1	0.602
		gap	0.26	2	0.776
		diverter	0.08	1	0.777
		gap vs. diverter	1.25	2	0.296
Steelhead	≥180 mm	gap	0.99	2	0.394
		diverter	3.24	1	0.091
		gap vs. diverter	0.09	2	0.916
	total catch	gap	0.62	2	0.547
		diverter	2.67	1	0.118
		gap vs. diverter	0.18	2	0.840
Sockeye	<180 mm	gap	1.85	2	0.174
		diverter	0.31	1	0.580
		gap vs. diverter	0.22	2	0.800
Total salmonid species	<180 mm	date	2.96	1	0.092
(spring outmigration)		gap	0.43	2	0.651
		diverter	0.01	1	0.916
		gap vs. diverter	0.24	2	0.785
	≥180 mm	gap	3.20	2	0.061
		diverter	0.00	1	0.985
		gap vs. diverter	0.36	2	0.702
Total salmonid species	total catch	date	1.00	1	0.322
(spring outmigration)		gap	0.02	2	0.975
		diverter	0.02	1	0.902
		gap vs. diverter	0.25	2	0.778
Subyearling chinook	<180 mm	date	29.17	1	0.000*
salmon		gap	0.08	2	0.926
		diverter	0.09	1	0.766
		gap vs. diverter	0.04	2	0.958

Appendix Table 6. Total catch, by species and length group (by fork length in millimeters), for individual replicates of separation efficiency tests using a high-velocity flume separator at McNary Dam, 1998.

		Subyearling chinook		Yearling chinook		Steelhead		Coho		keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 1, Treatmen	t 1, 27 Ap	ril, Bar		13 mm	water	velocity	1 m/s, b	ars ang	led	
Tanks: separated non-separated			41 71	5	1	1				
Separator: separated						(10)				
non-separated										
Replicate 2, Treatmen	t 1, 4 May	, Bar sp	oacing 1	3 mm, v	vater ve	locity 1	m/s, bar	s angle	d	
Tanks: separated			31						16	
non-separated			36	2	2	2			12	
Separator: separated			3							
non-separated			5	1	2					
Replicate 3, Treatmen	t 1 7 May	Rarsi	acing 1	3 mm. v	vater ve	locity 1	m/s. bar	s angle	d	
Tanks: separated	it i, / ivia;	, Dai s	1		rater ve	rockey z		o angre	28	
non-separated			28	1	4	6			33	
			3	1	1	O			2	
Separator: separated			2		1	2			2	
non-separated			2			2				
Replicate 4, Treatmen	t 1, 11 Ma	ay, Bar		13 mm,	water v	elocity	l m/s, ba	ars angl	ed	
Tanks: separated			4						21	
non-separated			29	2	1	14				
Separator: separated			1							
non-separated			3		1	9				
Replicate 12, Treatme	nt 1, 22 Ju	une, Bai	spacing	g 13 mm	, water	velocity	1 m/s, l	bars ang	gled	
Tanks: separated	104									
non-separated	8		1							
Separator: separated	2									
non-separated										
Replicate 13, Treatme	ent 1 24 I	ine Rai	r snacin	o 13 mm	. water	velocity	1 m/s. l	bars ang	eled	
Tanks: separated	175	une, Du	spacing	5 10 1111	,	. 010 010	, .		,	
non-separated	50		1	1						
Separator: separated	2		1	1						
non-separated	2									
Replicate 14, Treatme	nt 1, 29 Ju	une, Bai	spacin	g 13 mn	ı, water	velocity	1 m/s, l	bars ang	gled	
Tanks: separated	151		2							
non-separated	31		5							
Separator: separated	9									
	-									

## Appendix Table 6. Continued.

Replicate 15, Treatmen Tanks: separated non-separated separator: separated non-separated Replicate 16, Treatmen Tanks: separated non-separated Separator: separated	54 34 1		spacing	≥180 g <b>13 m</b> m	<180 n, water	≥180 velocity	<180 1 m/s, l	≥180 bars ang	<180	≥180
Tanks: separated non-separated Separator: separated non-separated non-separated Replicate 16, Treatmen Tanks: separated non-separated	54 34 1 nt 1, 6 Jul 98			g 13 mm	ı, water	velocity	1 m/s, l	bars ang	gled	
non-separated Separator: separated non-separated  Replicate 16, Treatmen Tanks: separated non-separated	34 1 at 1, 6 Jul 98	y, Bar s								
Separator: separated non-separated  Replicate 16, Treatmen  Tanks: separated non-separated	1 n <b>t 1, 6 Jul</b> 98	y, Bar s								
non-separated  Replicate 16, Treatmen  Tanks: separated  non-separated	n <b>t 1, 6 Jul</b> 98	y, Bar s								
Replicate 16, Treatmen Tanks: separated non-separated	98	y, Bar s								
Tanks: separated non-separated	98	y, Bar s								
Tanks: separated non-separated	98		pacing 1	13 mm,	water v	elocity 1	m/s, ba	rs angle	ed	
non-separated			1 0	,			,	0		
	14									
	1									
non-separated	•									
Replicate 17, Treatmen	t 1 17 Iv	ılv Rar	snacing	13 mm	water	velocity	1 m/s h	ars and	led	
Tanks: separated	324	ary, Dur	spacing	10 11111	,	relocity	1 1111 09 10	ars ang	icu	
non-separated	7									
Separator: separated	í									
non-separated	1									
non-separated										
Replicate 18, Treatmen		y, Bar s	pacing 1	13 mm,	water v	elocity 1	m/s, ba	rs angle	ed	
Tanks: separated	226									
non-separated	51									
Separator: separated	23									
non-separated										
Replicate 19, Treatmen	t 1, 13 Ju	ıly, Bar	spacing	13 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	113									
non-separated	45		1							
Separator: separated	15									
non-separated										
Replicate 20, Treatmen	t 1, 14 Ju	ıly, Bar	spacing	13 mm	water	velocity	1 m/s, b	ars ang	led	
Γanks: separated	181		. 0				,			
non-separated	50		1							
Separator: separated	37		3							
non-separated										
Replicate 21, Treatmen	t 1, 20 In	ılv. Bar	spacing	13 mm	water	velocity	1 m/s. h	ars ang	led	
Tanks: separated	21	, 2001	Parents		,	·	,			
non-separated	45									
Separator: separated	25									
non-separated	23									

Source	Subyearling chinook		Yearling chinook		Steelhead		Coho		Sockeye	
	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatmen	nt 1, 23 Ju	ıly, Bar	spacing	13 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	22									
non-separated	45									
Separator: separated	17									
non-separated	5									
Replicate 23, Treatmen	nt 1, 27 Ju	ıly, Bar	spacing	13 mm	, water	velocity	1 m/s, b	ars ang	led	
Γanks: separated	24									
non-separated	42									
Separator: separated	2									
non-separated										
Replicate 2, Treatmen	t 2, 4 May	, Bar sı	oacing 1	3 mm, v	vater ve	locity 2	m/s, bar	rs angle	d	
Γanks: separated			8						13	
non-separated			42	5	1	3			. 2	
Separator: separated										
non-separated										
Replicate 3, Treatmen	t 2, 7 May	, Bar s	oacing 1	3 mm, v	vater ve	locity 2	m/s, bai	rs angle	d	
Tanks: separated			6						8	
non-separated			32			5			14	
Separator: separated										
non-separated						1				
Replicate 4, Treatmen	t 2,12 Ma	y, Bar s	pacing 1	13 mm,	water v	elocity 2	m/s, ba	rs angle	ed	
Tanks: separated				7					10	
non-separated			19	3	1	4	3		13	
Separator: separated										
non-separated										
Replicate 12, Treatme	nt 2, 22 Ju	une, Bai	spacin	g 13 mn	ı, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated	91									
non-separated	75		1							
Separator: separated	1									
non-separated										
Replicate 13, Treatme	nt 2, 24 Ju	une, Bai	spacin	g 13 mn	ı, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated	150									
non-separated	71									
Separator: separated										

	Subyearling chinook		Yearling chinook		Steelhead		Coho		Sockeye	
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 14, Treatmen	t 2, 29 Ju	une, Bar	spacing	g 13 mm	, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated	43									
non-separated	24		1	1						
Separator: separated										
non-separated										
Replicate 15, Treatmen	t 2, 30 Ju	une, Bai	r spacing	g 13 mm	, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated	177									
non-separated	164		1							
Separator: separated										
non-separated										
Replicate 16, Treatmen	t 2, 6 Ju	ly, Bar s	spacing :	13 mm,	water v	elocity 2	m/s, ba	ars angle	ed	
Tanks: separated	70									
non-separated	20									
Separator: separated										
non-separated	1									
Replicate 17, Treatmen	t 2, 7 Ju	lv. Bar s	spacing	13 mm.	water v	elocity 2	2 m/s, ba	ars angl	ed	
Tanks: separated	634	.,	Parana	,			,	0		
non-separated	37									
Separator: separated										
non-separated										
Replicate 18, Treatmen	t 2, 9 Ju	lv, Bar s	spacing	13 mm,	water v	elocity 2	2 m/s, ba	ars angl	ed	
Tanks: separated	245		2	7						
non-separated	63		1							
Separator: separated										
non-separated										
Replicate 19, Treatmer	nt 2, 13 J	uly , Ba	r spacin	g 13 mn	ı, water	velocity	2 m/s,	bars an	gled	
Tanks: separated	60									
non-separated	37		1							
Separator: separated	3									
non-separated										
Replicate 20, Treatmen	nt 2, 15 J	uly, Bar	spacing	g 13 mm	, water	velocity	2 m/s, l	bars ang	led	
Tanks: separated	76									
non-separated	61									
Separator: separated	6									

. 27 - 2	Subyearling chinook		Yearling chinook		Steelhead		Coho		Sockeye	
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 21, Treatme	nt 2, 20 Ju	uly, Bar	spacing	13 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	51									
non-separated	20									
Separator: separated	3									
non-separated										
Replicate 22, Treatme	nt 2, 22 Ju	uly, Bar	spacing	13 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	19							1000		
non-separated	47									
Separator: separated										
non-separated										
Replicate 23, Treatme		uly, Bar	spacing	3 13 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	87		1							
non-separated	96									
Separator: separated										
non-separated										
Replicate 1, Treatmen	t 3. 27 An	ril. Bar	spacing	13 mm	water	velocity	1 m/s, b	ars flat		
Tanks: separated	,P	,	24		,				1	
non-separated			30	2	2	5			1	
Separator: separated										
non-separated										
	. 2 . 4 3 4	D		2		1!4 1	/a han	flat		
Replicate 2, Treatmen	t 3, 4 May	y, Bar s	40	3 mm, v	vater ve	2	m/s, bai	Shat	14	
Tanks: separated			27		1	12			5	
non-separated			21			1			3	
Separator: separated			1			1				
non-separated			1							
Replicate 3, Treatmen	t 3, 7 May	v. Bar sı	pacing 1	3 mm, v	vater ve	locity 1	m/s, bar	rs flat		
Tanks: separated	,		12	2					23	
non-separated			38	7	5	35			5	
Separator: separated										
non-separated						1				
Replicate 4, Treatmen	t 3 12 M	av Rar	snacing	13 mm	water v	elocity	1 m/s h	ars flat		
Tanks: separated	5, 12 1718	uj, Dai	22	10 mil,	WALCE V	clocity		MED EIGHT	14	
non-separated			26	4		2	1		2	
Separator: separated			20	7		2			-	
non-separated										

		earling nook		rling look	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 12, Treatmen	nt 3, 22 J	une, Bar	spacing	g 13 mm	, water	velocity	1 m/s,	bars flat		
Γanks: separated	109									
non-separated	13		2							
Separator: separated	3									
non-separated										
Replicate 13, Treatmen	nt 3, 25 ju	ıne, Bar	spacing	13 mm	, water	velocity	1 m/s,	bars flat		
Γanks: separated	146									
non-separated	31									
Separator: separated										
non-separated										
Replicate 14, Treatme	nt 3, 29 J	une, Bar	spacing	g 13 mm	ı, water	velocity	1 m/s,	bars flat	t	
Tanks: separated	182		2							
non-separated	5									
Separator: separated	1									
non-separated										
Replicate 15, Treatme	nt 3, 30 J	une, Bai	r spacing	g 13 mm	ı, water	velocity	1 m/s,	bars flat	t	
Tanks: separated	160	,	•							
non-separated	13									
Separator: separated										
non-separated										
Replicate 16, Treatme	nt 3, 6 Ju	lv. Bar s	spacing	13 mm,	water v	elocity 1	m/s, ba	ars flat		
Tanks: separated	95		2							
non-separated	14		1							
Separator: separated	2									
non-separated										
Replicate 17, Treatme	nt 3, 7 Ju	ly, Bar s	spacing	13 mm,	water v	elocity 1	l m/s, b	ars flat		
Tanks: separated	431									
non-separated	27									
Separator: separated	12									
non-separated										
Replicate 18, Treatme	nt 3, 9 Ju	ly, Bar	spacing	13 mm,	water v	elocity 1	l m/s, b	ars flat		
Tanks: separated	377									
non-separated	72									
	~									
Separator: separated	5									

		earling nook		rling look	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 19, Treatmer	nt 3, 13 J	uly, Bar	spacing	13 mm	, water	velocity	1 m/s, l	bars flat		
Tanks: separated	132									
non-separated	37		1							
Separator: separated										
non-separated										
Replicate 20, Treatmer	nt 3, 14 J	uly, Bar	spacing	13 mm	, water	velocity	1 m/s, l	bars flat		
Tanks: separated	240									
non-separated	35									
Separator: separated										
non-separated	3									
Replicate 21, Treatmer	nt 3, 20 J	ulv. Bar	spacing	13 mm	. water	velocity	1 m/s, l	bars flat		
Tanks: separated	86	,	-1		,					
non-separated	24									
Separator: separated	1									
non-separated	•									
Replicate 22, Treatmer	nt 3, 22 J	ulv. Bar	spacing	13 mm	, water	velocity	1 m/s, l	bars flat		
Tanks: separated	54									
non-separated	20									
Separator: separated										
non-separated										
Replicate 12, Treatmer	nt 3, 22 J	une, Bai	r spacin	g 13 mm	ı, water	velocity	1 m/s,	bars flat		
Tanks: separated	, 0			,						
non-separated										
Separator: separated										
non-separated										
Replicate 23, Treatmen	at 3, 27 J	ulv. Bar	spacing	13 mm	. water	velocity	1 m/s, l	bars flat		
Tanks: separated	38		-1		,					
non-separated	54									
Separator: separated	4									
non-separated										
Replicate 1, Treatment	4, 27 Ar	oril, Bar	spacing	13 mm	, water	velocity	2 m/s, h	oars flat		
Tanks: separated	,	,	59	3		2			2	
non-separated			31	1		1			1	
				_						
Separator: separated										

		earling nook		rling look	Steel	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 2, Treatmen	nt 4, 4 May	, Bar s	pacing 1	3 mm, v	vater ve	locity 2	m/s, bar	rs flat		
Γanks: separated			26						9	
non-separated			55	1		5			20	
Separator: separated										
non-separated										
Replicate 3, Treatmen	nt 4, 7 May	, Bar sı	pacing 1	3 mm, v	vater ve	locity 2	m/s, ba	rs flat		
Tanks: separated			19		1	ĺ			48	
non-separated	1		43	6		8	2		20	
Separator: separated										
non-separated										
Replicate 4, Treatmen	nt 4. 11 Ma	v. Bar	spacing	13 mm.	water v	elocity 2	2 m/s, ba	ars flat		
Tanks: separated	,	.,	8	,	1	1			14	
non-separated			22	2	1	9			3	
Separator: separated			22	_	•					
non-separated										
Replicate 12, Treatme	ent 4, 22 Ju	une, Bai	r spacing	g 13 mm	ı, water	velocity	2 m/s,	bars flat	t	
Tanks: separated	86									
non-separated	41		5							
Separator: separated										
non-separated										
Replicate 13, Treatme	ent 4, 25 Ju	une, Bai	r spacing	g 13 mm	ı, water	velocity	2 m/s,	bars flat	t	
Tanks: separated	190									
non-separated	42									
Separator: separated										
non-separated										
Replicate 14, Treatme	ent 4, 29 Ju	ıne, Baı	r spacing	g 13 mm	ı, water	velocity	2 m/s,	bars flat	t	
Tanks: separated	136		1							
non-separated	23		1							
Separator: separated										
non-separated										
Replicate 15, Treatme	ent 4, 30 Ju	une, Bai	r spacing	g 13 mm	ı, water	velocity	2 m/s,	bars flat		
	181		1							
Tanks: separated										
Tanks: separated non-separated	198									

		earling nook		rling	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 16, Treatme	nt 4, 2 Ju	ly, Bar s	pacing	13 mm,	water v	elocity 2	2 m/s, ba	rs flat		
Tanks: separated	1866									
non-separated	68		2							
Separator: separated non-separated										
Replicate 17, Treatme	nt 4, 7 Ju	ly, Bar s	pacing	13 mm,	water v	elocity 2	2 m/s, ba	ars flat		
Tanks: separated	414									
non-separated	131									
Separator: separated	2									
non-separated										
Replicate 18, Treatme	nt 4, 9 Ju	ly, Bar s	pacing	13 mm,	water v	elocity 2	2 m/s, ba	ars flat		
Tanks: separated	390									
non-separated	28									
Separator: separated	3									
non-separated										
Replicate 19, Treatme	nt 4, 13 J	uly, Bar	spacing	3 13 mm	, water	velocity	2 m/s, t	oars flat		
Tanks: separated	76		1							
non-separated	33									
Separator: separated										
non-separated										
Replicate 20, Treatme	nt 4, 15 J	uly, Bar	spacing	g 13 mm	, water	velocity	2 m/s, h	oars flat		
Tanks: separated	79									
non-separated	60									
Separator: separated										
non-separated										
Replicate 21, Treatme	nt 4, 20 J	uly, Bar	spacing	13 mm	, water	velocity	2 m/s, l	oars flat		
Tanks: separated	30									
non-separated	38									
Separator: separated										
non-separated										
Replicate 22, Treatme	nt 4, 23 J	uly, Bar	spacing	g 13 mm	, water	velocity	2 m/s, l	oars flat		
Tanks: separated	17									
non-separated	47									
Separator: separated										
non-separated										

		earling nook		rling 100k	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 23, Treatmen	nt 4, 24 Ju	ıly, Bar	spacing	13 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated non-separated	55 26									
Separator: separated non-separated										
Replicate 1, Treatment	5. 29 Ap	ril. Bar	spacing	16 mm.	water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	.,		33							
non-separated			26	10	1	14	2		1	
Separator: separated			10							
non-separated			1	3		4				
Replicate 2, Treatment	5, 6 May	, Bar sp	pacing 1	6 mm, v	vater ve	locity 1	m/s, bar	rs angle	d	
Tanks: separated		_	34		2		1		11	
non-separated			6	1		2			14	
Separator: separated			9			1				
non-separated						8				
Replicate 3, Treatment	5, 8 May	, Bar sp	oacing 1	6 mm, v	vater ve	locity 1	m/s, bar	rs angle	d	
Tanks: separated			16				1		44	
non-separated			8	4		12	1		12	
Separator: separated			4		2	1	1		1	
non-separated				1		13				
Replicate 4, Treatment	5, 12 Ma	y, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars angl	ed	
Tanks: separated			22		2				12	
non-separated			33	6	2	43			9	
Separator: separated			2		1	4				
non-separated						6				
Replicate 5, Treatment	5, 14 Ma	y, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars angl		
Tanks: separated			17		3				25	
non-separated			14	7	2	36			5	
Separator: separated						1				
non-separated						1				
Replicate 6, Treatment	5, 18 Ma	y, Bar s	spacing	16 mm,	water v	elocity	1 m/s, ba	ars angl		
Tanks: separated			45		1		2		46	
non-separated			20	2	- 1	1			24	
Separator: separated			24			1	5		3	
non-separated				1						

		earling look		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 7, Treatmen	t 5, 20 Ma	y, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars angle	ed	Pt 1
Γanks: separated	9		45			1			10	
non-separated	1		7	2					4	
Separator: separated	1		21						4	
non-separated			4	1		4				
Replicate 8, Treatmen	t 5, 22 Ma	y, Bar	spacing	16 mm,	water v	elocity 1	l m/s, ba	ars angle	ed	
Tanks: separated	6		25		1				19	
non-separated	3		16	3	3	3	2		12	
Separator: separated			3			2			1	
non-separated						1				
Replicate 9, Treatmen	t 5, 27 Ma	y, Bar	spacing	16 mm,	water v	elocity 1	l m/s, ba	ars angle	ed	
Tanks: separated	42		19				5		23	
non-separated	21		12	7	2	9	2		1	
Separator: separated	2		3		1		1		1	
non-separated						6	1			
Replicate 10, Treatme	nt 5, 1 Jur	ne, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars angl	ed	
Tanks: separated	10		4		1				5	
non-separated	55		22	7	4	23	6	1	16	
Separator: separated			4	1	3	1	9	3		
non-separated				2	3	6	1			
Replicate 11, Treatme	nt 5, 3 Jur	ie, Bar	spacing	16 mm,	water v	elocity	l m/s, ba	ars angle	ed	
Tanks: separated	4		6		1		9		17	
non-separated	10		23	4	4	7	17	2	15	
Separator: separated			1	1			5	1		
non-separated				2	1	6	1			
Replicate 12, Treatmen	nt 5, 22 Ju	ne, Bar	spacing	g 16 mm	, water	velocity	1 m/s, l	bars ang	led	
Tanks: separated	323		1							
non-separated	4			2						
Separator: separated	1									
non-separated										
Replicate 13, Treatmen	nt 5, 26 Ju	ne, Bar	spacing	g 16 mm	, water	velocity	1 m/s, l	oars ang	led	
Tanks: separated	37									
non-separated	27									
Separator: separated	1									
non-separated										

		earling nook		rling 100k	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 14, Treatme	nt 5, 29 Ju	une, Bar	spacing	g 16 mm	, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	150		1							
non-separated	2									
Separator: separated	4									
non-separated										
Replicate 15, Treatme	nt 5, 1 Jul	ly, Bar s	pacing	16 mm,	water v	elocity 1	m/s, ba	ars angle	ed	
Tanks: separated	71									
non-separated	73									
Separator: separated	6									
non-separated										
Replicate 16, Treatme	nt 5, 6 Jul	ly, Bar s	pacing	16 mm,	water v	elocity 1	m/s, ba	ars angle	ed	
Tanks: separated	69		1				,	J		
non-separated	30		1							
Separator: separated	8									
non-separated										
Replicate 17, Treatme	The state of the s	ly, Bar s	pacing 1	16 mm,	water v	elocity 1	m/s, ba	ars angle	ed	
Tanks: separated	547									
non-separated	116									
Separator: separated	11									
non-separated										
Replicate 18, Treatme	nt 5, July,	Bar spa	acing 16	mm, w	ater vel	ocity 1 r	n/s, bar	s angled		
Γanks: separated	180									
non-separated	87									
Separator: separated	8									
non-separated										
Replicate 19, Treatme	nt 5, 13 Ju	ıly, Bar	spacing	16 mm	water	velocity	1 m/s, b	ars ang	led	
Γanks: separated	166									
non-separated	51									
Separator: separated	6									
non-separated										
Replicate 20, Treatme	nt 5, 16 Ju	ıly, Bar	spacing	16 mm	water	velocity	1 m/s, b	ars ang	led	
Γanks: separated	79		,							
non-separated	1									
Separator: separated	6									
non-separated										

		earling nook		rling 100k	Steel	head	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatme	nt 5, 20 Ju	ıly, Bar	spacing	16 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	69									
non-separated	52									
Separator: separated	11									
non-separated										
Replicate 23, Treatme	nt 5, 23 Ju	ıly, Bar	spacing	16 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	30									
non-separated	44									
Separator: separated	34									
non-separated										
Replicate 23, Treatme	nt 5, 28 Ju	ıly, Bar	spacing	16 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	29									
non-separated	35									
Separator: separated non-separated	12									
Replicate 1, Treatmen	+ 6 28 An	ril Ror	cnacina	16 mm	water	olocity	2 m/s h	arc and	lad	
Tanks: separated	t 0, 20 Ap	in, Dai	36	10 111111	water v	clocity	2 1105, 0	ars ang	icu	
non-separated			43	21	1				1	
Separator: separated			1	21					1	
non-separated			1							
Replicate 2, Treatmen	t 6, 5 May	, Bar sp		6 mm, v	vater vel	locity 2	m/s, bar	's angle		
Tanks: separated			36			1			4	
non-separated			32	2		7			7	
Separator: separated										
non-separated										
Replicate 3, Treatmen	t 6, 8 May	, Bar sp	oacing 1	6 mm, v	ater vel	locity 2	m/s, bar	s angle	d	
Tanks: separated			7						13	
non-separated			16	4	1	3			32	
Separator: separated			1							
non-separated										
Replicate 4, Treatmen	t 6, 12 Ma	y, Bar s	pacing	16 mm,	water v	elocity 2	m/s, ba	rs angle	ed	
Tanks: separated		7.	15						8	
non-separated			17	5	2	53	1		5	
Separator: separated										
non-separated						4				

		earling nook		rling 100k	Steel	head	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 5, Treatmen	nt 6, 14 Ma	y, Bar	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars angl		
Tanks: separated			14		1				15	
non-separated			28	1	5	11			38	
Separator: separated non-separated			1							
Replicate 6, Treatmen	nt 6, 18 Ma	v. Bar	spacing	16 mm.	water v	elocity 2	2 m/s, ba	ars angl	ed	
Tanks: separated	5	.,	32	1	1		4		32	
non-separated	1		16	3		6	9		14	
Separator: separated			1	-	1	-	1		1	
non-separated									•	
Replicate 7, Treatmen	nt 6, 20 Ma	v, Bar	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars angl	ed	
Tanks: separated	1		32		1		,	0	21	
non-separated	2		30			4			14	
Separator: separated			1						1	
non-separated										
Replicate 8, Treatmen	nt 6, 22 Ma	y, Bar s	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars angl	ed	
Γanks: separated	2		26		2				19	
non-separated			27	8	3	9			3	
Separator: separated										
non-separated										
Replicate 9, Treatmen	nt 6, 28 Ma	y, Bar s	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars angl	ed	
Γanks: separated	39		17		1		1		3	
non-separated	20		11	7	3	17	4		7	
Separator: separated			1							
non-separated										
Replicate 10, Treatme	ent 6, 1 Jui	ne, Bar	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars angl		
Γanks: separated	15		12	3	4	2	11		2	
non-separated	15		12	4	2	8	9	1		
Separator: separated										
non-separated										
Replicate 11, Treatme	ent 6, 3 Jui	ne, Bar	_	16 mm,	water v	elocity 2	2 m/s, ba	ars angl	ed	
Γanks: separated			5				1			
non-separated			26	3	5	12	27	1	17	
Separator: separated			1		1		1			
non-separated						1				

Subyearling Yearling chinook chinook Steelhead Coho Sockeye <180 ≥180 <180 ≥180 <180 ≥180 Source ≥180 <180 ≥180 Replicate 12, Treatment 6, 23 June, Bar spacing 16 mm, water velocity 2 m/s, bars angled separated non-separated 92 Separator: separated non-separated Replicate 13, Treatment 6, 25 June, Bar spacing 16 mm, water velocity 2 m/s, bars angled Tanks: separated 151 1 non-separated Separator: separated non-separated Replicate 14, Treatment 6, 30 June, Bar spacing 16 mm, water velocity 2 m/s, bars angled 114 Tanks: separated non-separated 52 Separator: separated non-separated Replicate 15, Treatment 6, 1 July, Bar spacing 16 mm, water velocity 2 m/s, bars angled separated 59 Tanks: non-separated 42 2 Separator: separated non-separated Replicate 16, Treatment 6, 6 July, Bar spacing 16 mm, water velocity 2 m/s, bars angled 91 Tanks: separated 4 non-separated Separator: separated 1 non-separated Replicate 17, Treatment 6, 8 July, Bar spacing 16 mm, water velocity 2 m/s, bars angled separated 282 non-separated 196 Separator: separated 2 non-separated Replicate 18, Treatment 6, 10 July, Bar spacing 16 mm, water velocity 2 m/s, bars angled 150 Tanks: separated 3 89 non-separated 3 Separator: separated non-separated

		earling nook		rling 100k	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥18
Replicate 19, Treatme	nt 6, 13 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	318		1							
non-separated	32									
Separator: separated										
non-separated										
Replicate 20, Treatme	nt 6, 15 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	104		4							
non-separated	4									
Separator: separated										
non-separated										
Replicate 21, Treatme	ent 6, 21 Ju	ılv. Bar	spacing	16 mm	. water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	24	,	1 6							
non-separated	36									
Separator: separated										
non-separated										
Replicate 22, Treatme	ent 6, 23 Ju	uly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	27									
non-separated	41									
Separator: separated	1									
non-separated										
Replicate 23, Treatme	ent 6, 28 Ju	uly, Bar	spacing	g 16 mm	, water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	33									
non-separated	57									
Separator: separated	2									
non-separated										
Replicate 1, Treatmen	t 7, 29 Ap	ril, Bar	spacing	16 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated			72						5	
non-separated			14	5	1	5				
Separator: separated										
non-separated										
Replicate 2, Treatmen	t 7, 5 May	, Bar s	pacing 1	6 mm, v	vater ve	locity 1	m/s, ba	rs flat		
Tanks: separated			87	1					15	
non-separated			16	1		6			2	
Separator: separated										
non-separated										

		earling nook		rling 100k	Steel	head	Co	ho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 3, Treatmen	t 7, 7 May	, Bar sp	pacing 1	6 mm, v	vater ve	locity 1	m/s, bar	rs flat		
Tanks: separated			13	7	2	1	1		9	
non-separated			5	6	1	34	3		8	
Separator: separated							1			
non-separated										
Replicate 4, Treatmen	t 7, 12 Ma	ay, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars flat	6 1.	
Tanks: separated			29	1					20	
non-separated			18	2		12			20	
Separator: separated										
non-separated						1				
Replicate 5, Treatmen	t 7, 14 Ma	ay, Bar		16 mm,		elocity	1 m/s, ba	ars flat	15	
Tanks: separated			23	_	1	20			15	
non-separated			14	5	2	28	1		3	
Separator: separated						1				
non-separated						1				
Replicate 6, Treatmen	t 7, 18 Ma	ay, Bar	spacing	16 mm,	water v	elocity	1 m/s, ba	ars flat	25	
Tanks: separated			60	-	2				35	
non-separated			9	1	1	1			6	
Separator: separated										
non-separated										
Replicate 7, Treatmen	t 7, 19 Ma	ay, Bar	spacing	16 mm,		elocity	1 m/s, ba	ars flat	10	
Tanks: separated			16		1	2			12	
non-separated			10	4		3			4	
Separator: separated										
non-separated										
Replicate 8, Treatmen		ay, Bar		16 mm,		elocity	1 m/s, ba	ars flat	42	
Tanks: separated	5		69		2	20			43	
non-separated			14	15	1	20			1	
Separator: separated										
non-separated										
Replicate 9, Treatmen		ay, Bar		16 mm,		elocity	1 m/s, b	ars flat	10	
Tanks: separated	50		24	7	4	10			18	
non-separated	6		5	7	2	10			2	
Separator: separated										
non-separated										

		earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 10, Treatme	nt 7, 2 Ju	ne, Bar	spacing	16 mm,	water v	elocity	1 m/s, b	ars flat		
Tanks: separated	78		20		3		14		2	
non-separated	25		8	7		19	2		2	1
Separator: separated										
non-separated										
Replicate 11, Treatme	nt 7, 4 Ju	ne. Bar	spacing	16 mm,	water v	elocity	1 m/s, b	ars flat		
Tanks: separated	30	,	23	1	1	1	10		7	
non-separated	8		10	7		19	6		1	
Separator: separated						1	-		_	
non-separated						-				
Replicate 12, Treatme	nt 7. 23 Ju	ine. Bai	r spacin	9 16 mm	ı. water	velocity	1 m/s.	bars flat		
Tanks: separated	159	, 2001	1	9	-,		,			
non-separated	20		2	1						
Separator: separated	20		_	•						
non-separated										
Replicate 13, Treatme	nt 7, 26 Ju	une, Bai	r spacin	g 16 mm	ı, water	velocity	1 m/s,	bars flat		
Tanks: separated	59		1							
non-separated	2									
Separator: separated										
non-separated										
Replicate 14, Treatme	nt 7, 29 Ju	une, Bai	r spacin	g 16 mm	ı, water	velocity	1 m/s,	bars flat	:	
Tanks: separated	143		2							
non-separated	5									
Separator: separated										
non-separated										
Replicate 15, Treatme	nt 7, 1 Jul	ly, Bar s	spacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Tanks: separated	77									
non-separated	4									
Separator: separated										
non-separated										
non separated										
Replicate 16, Treatme	nt 7, 6 Jul	ly, Bar s	spacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Replicate 16, Treatme	nt 7, 6 Jul 140	ly, Bar s	spacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Replicate 16, Treatme		ly, Bar s	spacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Replicate 16, Treatme Tanks: separated	140	ly, Bar s	spacing	16 mm,	water v	elocity 1	m/s, ba	irs flat		

	-	earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 17, Treatme	nt 7, 8 Jul	ly, Bar s	pacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Tanks: separated	302									
non-separated	31									
Separator: separated non-separated	4									
Replicate 18, Treatme	nt 7, 9 Jul	ly, Bar s	pacing	16 mm,	water v	elocity 1	m/s, ba	rs flat		
Γanks: separated	190									
non-separated	3									
Separator: separated										
non-separated										
Replicate 19, Treatme	nt 7, 13 Ju	uly, Bar	spacing	16 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated	166									
non-separated	9									
Separator: separated										
non-separated										
Replicate 20, Treatme	nt 7, 16 Ju	uly, Bar	spacing	3 16 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated	96									
non-separated	17									
Separator: separated	1									
non-separated										
Replicate 21, Treatme	nt 7, 21 Ju	uly, Bar	spacing	g 16 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated	48									
non-separated	17									
Separator: separated	1									
non-separated										
Replicate 22, Treatme	nt 7, 23 Ju	uly, Bar	spacing	g 16 mm	, water	velocity	1 m/s, h	ars flat		
Tanks: separated	119									
non-separated	30									
Separator: separated										
non-separated										
Replicate 23, Treatme	nt 7, 27 Ju	uly, Bar	spacing	g 16 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated	31									
non-separated	5									
non-separated Separator: separated	5									

		earling nook		rling nook	Steel	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 1, Treatme	nt 8, 30 Ap	ril, Bar		16 mm	, water	velocity	2 m/s, b	ars flat		3 -
Tanks: separated			46		1		1			
non-separated			35	11		9			2	
Separator: separated non-separated			1							
Replicate 2, Treatme	nt 8, 6 May	, Bar sı	pacing 1	6 mm, v	vater ve	locity 2	m/s, bar	rs flat		
Tanks: separated			20		1		,		31	
non-separated			11	1	2	7			13	
Separator: separated										
non-separated			2							
Replicate 3, Treatme	nt 8, 8 May	. Bar sr	pacing 1	6 mm. v	vater ve	locity 2	m/s, bar	s flat		
Tanks: separated		,1	18			i	1		24	
non-separated			17		1	13	2		19	
Separator: separated							_			
non-separated				1						
Replicate 4, Treatme	nt 8, 13 Ma	av, Bar s	spacing	16 mm,	water v	elocity	2 m/s, ba	ars flat		
Tanks: separated			19		1		,		8	
non-separated			26	2	2	7	1		17	
Separator: separated										
non-separated										
Replicate 5, Treatme	nt 8, 15 Ma	ay, Bar s	spacing	16 mm,	water v	elocity	2 m/s, ba	ars flat		
Tanks: separated			21		1		1		17	
non-separated			16	1	1	5	1		24	
Separator: separated							*			
non-separated										
Replicate 6, Treatme	nt 8, 18 Ma	ay, Bar s	spacing	16 mm,	water v	elocity	2 m/s, ba	ars flat		
Tanks: separated			79				1		45	
non-separated			24	4	3	12			10	
Separator: separated										
non-separated										
Replicate 7, Treatme		ay, Bar		16 mm,	water v	elocity :	2 m/s, ba	ars flat		
Tanks: separated	3		21				1		6	
non-separated	2		14	1	2	5	5		8	
Separator: separated										
non-separated										

		earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 8, Treatmen	t 8, 25 Ma	ay, Bar	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars flat		
Tanks: separated	17		8				6		12	
non-separated	8		21	8	1	13	6		7	
Separator: separated										
non-separated						1				
Replicate 9, Treatmen	t 8, 27 Ma	ay, Bar	spacing	16 mm,	water v	elocity 2	2 m/s, ba	ars flat		
Tanks: separated	24	•	8						8	
non-separated	17		17	8	1	16			8	
Separator: separated										
non-separated										
Replicate 10, Treatme	nt 8 1 Iu	ne. Bar	snacing	16 mm.	water v	elocity :	2 m/s. b	ars flat		
Tanks: separated	7	iic, Dui	5	10,	1				2	
non-separated	15		43	5	6	14	1		4	
Separator: separated	13		45	5	O		1			
non-separated							•			
Replicate 11, Treatme	nt 8. 4 Ju	ne. Bar	spacing	16 mm.	water v	elocity	2 m/s, b	ars flat		
Tanks: separated		,	5	,	3		7		5	
non-separated			27	6	8	41	34	3	24	
Separator: separated										
non-separated										
Replicate 12, Treatme		une, Bai	r spacin	g 16 mm	ı, water	velocity	2 m/s,	bars flat		
Tanks: separated	118									
non-separated	110									
Separator: separated										
non-separated										
Replicate 13, Treatme	nt 8, 25 Ju	une, Bai	r spacin	g 16 mm	ı, water	velocity	2 m/s,	bars flat	-010	
Tanks: separated	236									
non-separated	18		2		1					
Separator: separated										
non-separated										
Replicate 14, Treatme	nt 8, 30 J	une, Bai	r spacin	g 16 mm	ı, water	velocity	2 m/s,	bars flat		
Tanks: separated	139		1							
non-separated	28		1							
			_							
Separator: separated										

## Appendix Table 6. Continued.

		earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 15, Treatmen		ly, Bar s	_		water v	elocity 2	m/s, ba	rs flat		
Tanks: separated	92		2	2						
non-separated	29		1							
Separator: separated non-separated										
Replicate 16, Treatmen	nt 8, 6 Jul	y, Bar s	pacing	16 mm,	water v	elocity 2	m/s, ba	rs flat		
Tanks: separated	123									
non-separated	32									
Separator: separated										
non-separated										
Replicate 17, Treatmen	nt 8, 8 Jul	y, Bar s	pacing	16 mm,	water v	elocity 2	m/s, ba	rs flat		
Tanks: separated	155									
non-separated	70									
Separator: separated										
non-separated										
Replicate 18, Treatmen	nt 8, 10 Ju	ılv, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	115						,			
non-separated	45		1			1				
Separator: separated										
non-separated										
Replicate 19, Treatmen	nt 8, 14 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	123		2							
non-separated	53		2							
Separator: separated	2									
non-separated										
Replicate 20, Treatmen	nt 8, 15 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	78									
non-separated	37									
Separator: separated										
non-separated										
Replicate 21, Treatmen	nt 8, 20 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	71					J	, .			
non-separated	6									
Separator: separated										

		arling look		rling nook	Steel	head	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatmen									-	
Tanks: separated	68	ary, Dur	Spacing	, 10 11111	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	. 010 010				
non-separated	60	*								
Separator: separated	00									
non-separated										
Replicate 23, Treatmen	nt 8, 28 Ju	ıly, Bar	spacing	16 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	27									
non-separated	41									
Separator: separated										
non-separated										
Replicate 1, Treatmen	t 9, 1 May	, Bar sp		9 mm, v	vater ve	locity 1	m/s, bar	rs angle	d	
Γanks: separated			42	3		1			1	
non-separated			8	1					1	
Separator: separated			8							
non-separated						1				
Replicate 2, Treatmen	t 9, 6 May	, Bar sp	oacing 1	9 mm, v	vater ve	locity 1	m/s, bar	rs angle	d	
Tanks: separated			37	1	2	2			54	
non-separated			10	1	2	5			29	
Separator: separated			11	2	2	3			1	
non-separated						2				
Replicate 3, Treatmen	t 9, 11 Ma	ay, Bar	spacing	19 mm,	water v	elocity	1 m/s, ba	ars angl	ed	
Tanks: separated			23	1					15	
non-separated			19	4		1			9	
Separator: separated			8							
non-separated										
Replicate 4, Treatmen	t 9, 13 Ma	ay, Bar	spacing	19 mm,	water v	elocity	1 m/s, ba	ars angle	ed	
Tanks: separated			18	,	3	12	1		19	
non-separated			23		3	35			4	
Separator: separated					1	1				
non-separated						2				
Replicate 5, Treatmen	t 9, 15 Ma	ay, Bar	spacing	19 mm,	water v	elocity	1 m/s, b	ars angl	ed	
Tanks: separated			29		3	9			14	
non-separated			20	3		15			6	
Separator: separated			4	5						

	-	arling look		rling 100k	Steel	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 6, Treatment	9, 19 Ma	y, Bar	spacing	19 mm,	water v	elocity 1	m/s, ba	ars angle		
Tanks: separated			33	1	1	3	1		15	
non-separated			6	1		4			9	
Separator: separated			9						2	
non-separated						3				
Replicate 7, Treatment	9, 20 Ma	y, Bar	spacing	19 mm,	water v	elocity 1	m/s, ba	ars angle	ed	
Tanks: separated	4		23		1	1			11	
non-separated	1	8	3		4				2	
Separator: separated			6			1				
non-separated										
Replicate 8, Treatment	0- 25 Ma	v Ror	nacina	10 mm	water v	alocity 1	m/c h	arc anal	ho	
Tanks: separated	22	iy, Dai s	22	17 11111,	2	3	i iivs, be	ars angi	9	
	10		22	6	1	11			7	
non-separated				0	1				/	
Separator: separated	1		5			2				
non-separated						6				
Replicate 9, Treatment		e, Bar sp						rs angle		
Tanks: separated	126		15	1	6	3	12		13	
non-separated	213		23	4	2	7	9		24	
Separator: separated			3	1	5	6	3			
non-separated				2		9	2			
Replicate 10, Treatmen	t 9, 3 Jui	ne, Bar	spacing	19 mm,	water v	elocity	1 m/s, b	ars angl	ed	
Tanks: separated	23		12		1	2	18		4	
non-separated	225		35	5	4	10	23	2	7	
Separator: separated			8		1	2	7	1		
non-separated			1	1		3		1		
Replicate 11, Treatmen	t 9. 5 .Jui	ne. Bar	spacing	19 mm.	water v	elocity	1 m/s, b	ars angl	ed	
Tanks: separated	12	,	24	1	3	3	19	0	1	
non-separated	8		14	5		10	10		3	
Separator: separated	7		6			1	3			
non-separated	,					•				
non separated										
Replicate 12, Treatmen		ıne, Bar		g 19 mm	, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	124		2							
non-separated	43		1							
Sanarator: sanarated	4									
Separator: separated	-									

		earling nook		rling nook	Stee	lhead	C	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 13, Treatmen	nt 9, 26 J	une, Bar	spacing	g 19 mn	, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	54									
non-separated	14									
Separator: separated	2									
non-separated										
Replicate 14, Treatme		une, Bai	spacin	g 19 mn	ı, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	127		1							
non-separated	39									
Separator: separated										
non-separated										
Replicate 15, Treatme	nt 9, 2 Ju	ly, Bar s	pacing	19 mm,	water v	elocity 1	m/s, b	ars angl	ed	
Tanks: separated	165									
non-separated	44									
Separator: separated										
non-separated										
Replicate 16, Treatme	nt 9, 7 Ju	ly, Bar s	spacing	19 mm,	water v	elocity 1	l m/s, b	ars angl	ed	
Tanks: separated	342		1							
non-separated	134									
Separator: separated	1									
non-separated										
Replicate 17, Treatme	nt 9, 8 Ju	ly, Bar s	spacing	19 mm,	water v	elocity	l m/s, b	ars angl	ed	
Tanks: separated	233									
non-separated	37									
Separator: separated	6									
non-separated										
Replicate 18, Treatme		uly, Bar		g 19 mm	, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	233		3							
non-separated	35		1							
Separator: separated										
non-separated										
Replicate 19, Treatme	nt 9, 14 J	uly, Bar	spacing	g 19 mm	, water	velocity	1 m/s,	bars ang	gled	
Tanks: separated	166									
non-separated	6									
Separator: separated non-separated	43									
1										

		earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 20, Treatme	nt 9, 17 Ju	uly, Bar	spacing	19 mm	, water	velocity	1 m/s, h	ars ang	led	
Tanks: separated	119									
non-separated	38									
Separator: separated non-separated	17									
Replicate 21, Treatme	nt 9, 21 Ju	ulv, Bar	spacing	19 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	34		1 6	,			,			
non-separated	39									
Separator: separated	8									
non-separated										
Replicate 22, Treatme	nt 9, 24 Ju	ıly, Bar	spacing	19 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	82									
non-separated	37									
Separator: separated	29									
non-separated										
Replicate 23, Treatme		ıly, Bar	spacing	19 mm	, water	velocity	1 m/s, b	ars ang	led	
Tanks: separated	82									
non-separated	76									
Separator: separated	36									
non-separated										
Replicate 1, Treatmen	t 10, 1 Ma	y, Bar s			water v	elocity 2	2 m/s, ba	ars angl		
Tanks: separated			19	1					4	
non-separated			34			3			7	
Separator: separated										
non-separated						1				
Replicate 2, Treatmen	t 10, 6 Ma	y, Bar s	_				2 m/s, ba	ars angl		
Γanks: separated			4	1	1	9			17	
non-separated			11	6		15			11	
Separator: separated			2							
non-separated			3							
Replicate 2, Treatmen	t 10, 6 Ma	y, Bar s	_			_	2 m/s, ba	ars angl		
Γanks: separated			4	1	1	9			17	
non-separated			11	6		15			11	
Separator: separated			2							
non-separated			3							

	-	arling look		rling 100k	Steel	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 3, Treatment	t 10, 11 M	ay, Bar	spacing	19 mm	, water	velocity	2 m/s, l	oars ang	led	
Tanks: separated			11	1		10	3		13	
non-separated			19	4		10	3		18	
Separator: separated						2				
non-separated						2	1		1	
Replicate 4, Treatment	t 10, 13 m	av. Bar	spacing	19 mm	water	velocity	2 m/s, b	ars ang	led	
Tanks: separated	,	-5,	21	1	1				4	
non-separated			31	8	3	25	1		15	
Separator: separated				U		1	-			
non-separated						•				
Replicate 5, Treatment	+ 10 15 M	lov Ror	enacino	, 10 mm	water	velocity	2 m/s 1	nars and	led	
	t 10, 15 M	lay, Dar		g 19 mm	, water	3	2 111/5, 1	Jais alig	21	
Tanks: separated			21	2	2	12			13	
non-separated			51	2	2	12	1		13	
Separator: separated			1			,	1			
non-separated						1				
Replicate 6, Treatment	t 10, 19 M	lay, Bar		g 19 mm		velocity		oars ang	led	
Tanks: separated	2		22		1		5		10	
non-separated	5		21	2		2	5		6	
Separator: separated										
non-separated				1		5				
Replicate 7, Treatmen	t 10, 21 M	lay, Bar	spacing	g 19 mm	, water	velocity	2 m/s, l	oars ang	led	
Tanks: separated	3		36	2	2		4		29	
non-separated			35	10		6	11		25	
Separator: separated			2							
non-separated			_							
Replicate 8, Treatmen	+ 10 26 M	lav Rar	enacine	10 mm	water	velocity	2 m/s. l	hars and	led	
	31	lay, Dai	16	2	, water	relocity	<b>2</b> 112 5, .	Jan 5 44116	5	
Tanks: separated	24		25	8		1	2		3	
non-separated	24		23	0		1	2		3	
Separator: separated non-separated										
Replicate 9, Treatmen	+ 10 20 N	lav Bo-	cnooin	n 10 mm	water	velocity	2 m/s 1	nars and	iled	
-	65	lay, Dal	Spacing	4	, water	2	4	Jai Jaile	18	
Tanks: separated			23	11	1	8	6		28	
non-separated	54		23	11	1	0	U		20	
Separator: separated										
non-separated										

		earling nook		rling 100k	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 10, Treatm	ent 10, 2 Ju	une, Bar	spacing	g 19 mm	, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated	194		9	1	4		7	1	1	
non-separated	327		25	4	5	14	18		28	
Separator: separated					1					
non-separated					3					
Replicate 11, Treatm	ent 10, 5 Ju	une, Bar	spacing	g 19 mm	, water	velocity	2 m/s,	bars ang	gled	
Tanks: separated			5		1		8		1	
non-separated			25	2	2	12	24	1	4	
Separator: separated										
non-separated							1			
Replicate 12, Treatm	ent 10, 23	June, Ba	ar spacii	ng 19 mi	n, wate	r veloci	ty 2 m/s	, bars ar	ngled	
Tanks: separated	141									
non-separated	182									
Separator: separated										
non-separated										
Replicate 13, Treatm	ent 10, 26	June, Ba	ar spacii	ng 19 mi	n, wate	r veloci	ty 2 m/s	, bars ar	ngled	
Tanks: separated	75						4			
non-separated	32									
Separator: separated										
non-separated										
Replicate 14, Treatm		June, Ba	ar spacii	ng 19 mi	n, wate	r veloci	ty 2 m/s	, bars ar	ngled	
Tanks: separated	197									
non-separated	5									
Separator: separated										
non-separated										
Replicate 15, Treatm		uly, Bar	_	19 mm,	water	velocity	2 m/s, h	oars ang	led	
Tanks: separated	526 56		2	2						
non-separated Separator: separated	30			2						
non-separated										
Replicate 16, Treatm Tanks: separated	ent 10, 7 Ju 2666	uly, Bar	spacing	19 mm,	water	velocity	2 m/s, k	oars ang	led	
non-separated	106									
Separator: separated	100									
non-separated										
non-separated										

		earling nook		rling nook	Stee	lhead	Co	oho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 17, Treatme	nt 10, 8 Ju	uly, Bar	spacing	19 mm	, water	velocity	2 m/s, l	oars ang	led	
Tanks: separated	186									
non-separated	221									
Separator: separated non-separated	2									
Replicate 18, Treatme	nt 10, 10	July, Ba	r spacir	ıg 19 mı	n, water	r velocit	y 2 m/s,	bars an	gled	
Tanks: separated	127	•	1							
non-separated	9									
Separator: separated										
non-separated										
Replicate 19, Treatme	nt 10, 14	July, Ba	r spacir	ng 19 mi	n, water	r velocit	y 2 m/s,	bars an	gled	
Tanks: separated	128		1							
non-separated	92									
Separator: separated	1									
non-separated										
Replicate 20, Treatme	nt 10, 17	July, Ba	r spacir	ng 19 mi	n, wate	r velocit	y 2 m/s,	bars an	gled	
Tanks: separated	83									
non-separated	111					1				
Separator: separated non-separated	4									
Replicate 21, Treatme	nt 10, 22	July, Ba	r spacii	ng 19 mi	m, wate	r velocit	y 2 m/s,	bars an	gled	
Tanks: separated	11		-							
non-separated	61									
Separator: separated	3									
non-separated										
Replicate 22, Treatme	nt 10, 24	July, Ba	ır spaciı	ng 19 m	m, wate	r velocit	y 2 m/s,	bars an	igled	
Tanks: separated	91		•	0						
non-separated	77			1						
Separator: separated	4									
non-separated										
Replicate 23, Treatme	nt 10, 30	July, Ba	ır spaciı	ng 19 m	m, wate	r velocit	ty 2 m/s,	bars an	ngled	
Tanks: separated	68									
non-separated	90									
Separator: separated	5									
non-separated										

		earling nook		rling nook	Steel	lhead	Co	ho	Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 1, Treatme	ent 11, 1 Ma	y, Bar		19 mm,	water v	elocity	l m/s, ba	ars flat		
Tanks: separated			51		1	1			3	
non-separated			4	1	2	4			2	
Separator: separated			2							
non-separated						1				
Replicate 2, Treatme	ent 11, 6 Ma	y, Bar	spacing	19 mm,	water v	elocity 1	l m/s, ba	ars flat		
Tanks: separated			38						38	
non-separated			3			1			6	
Separator: separated										
non-separated										
Replicate 3, Treatme	ent 11. 8 Ma	av. Bar	spacing	19 mm.	water v	elocity	l m/s, ba	ars flat		
Tanks: separated	11, 0 1.11	.,	49	2	2	11	1		32	
non-separated			9	1	-	12			4	
Separator: separated				-	1					
non-separated					•					
Replicate 4, Treatme Tanks: separated	11, 10 11	,, 2	21 2	2 2	1	4 16	,		3	
non-separated Separator: separated non-separated										
Separator: separated non-separated	ont 11 18 M	lov Roy	enacin	a 10 mm	water	velocity	1 m/s 1	ars flat		
Separator: separated non-separated  Replicate 5, Treatme		Iay, Bai		g 19 mm	ı, water			oars flat		
Separator: separated non-separated  Replicate 5, Treatmet Tanks: separated	ent 11, 18 M 8	Iay, Bar	25		ı, water	5	10	oars flat	50	
Separator: separated non-separated  Replicate 5, Treatmet anks: separated non-separated		Iay, Bai		g <b>19 m</b> m	ı, water			oars flat		
Separator: separated non-separated  Replicate 5, Treatmet anks: separated		Iay, Bar	25		ı, water	5	10	oars flat	50	
Separator: separated non-separated  Replicate 5, Treatme Tanks: separated non-separated Separator: separated non-separated	8		25 4	2		5	10		50 4	
Replicate 5, Treatmet Tanks: separated non-separated ron-separated separated separated separated: separated non-separated non-separated Replicate 6, Treatmet	8		25 4	2		5	10		50 4	
Replicate 5, Treatmet Tanks: separated non-separated ron-separated separated separated separated: separated non-separated non-separated Replicate 6, Treatmet	8	Iay, Baı	25 4	2	a, water	5	10		50 4	
Separator: separated non-separated  Replicate 5, Treatme Tanks: separated non-separated Separator: separated non-separated  Replicate 6, Treatme Tanks: separated non-separated	8	Iay, Bar 51	25 4	2	ı, water	5	10		50 4	
Replicate 5, Treatmet Tanks: separated non-separated ron-separated separator: separated non-separated non-separated Replicate 6, Treatmet Tanks: separated non-separated	8	<b>Iay, Bar</b> 51 12	25 4	2	a, water	5	10		50 4	
Replicate 5, Treatmet Tanks: separated non-separated Tanks: separated non-separated Separator: separated non-separated Tanks: separated non-separated separated separated non-separated separator: separated non-separated non-separated	8 ent 11, 19 N	51 12 1	25 4 spacing	2 g 19 mm	2 4 2	5 1 velocity	10 1 1 m/s, 1	oars flat	50 4 20 1	
Replicate 5, Treatmet Tanks: separated non-separated Tanks: separated non-separated Separator: separated non-separated Replicate 6, Treatmet Tanks: separated non-separated Separator: separated non-separated Replicate 7, Treatmet Replicate 7, Treatmet	8 ent 11, 19 N	51 12 1	25 4 spacing	2 g 19 mm	2 4 2	5 1 velocity	10 1 1 m/s, 1	oars flat	50 4 20 1	
Separator: separated non-separated  Replicate 5, Treatme Tanks: separated non-separated Separator: separated non-separated  Replicate 6, Treatme Tanks: separated non-separated Separator: separated non-separated Replicate 7, Treatme Replicate 7, Treatme	8 ent 11, 19 M ent 11, 21 M	51 12 1	25 4 spacing	2 g 19 mm	a, water 2 4 2	5 1 velocity	10 1 m/s, 1 1 m/s, 1	oars flat	50 4 20 1	

			arling look	Year	rling ook	Stee	lhead	Co	oho	Soc	keye
Source		<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 8, T	reatment	11, 26 M	lay, Bar	spacing	19 mm	, water	velocity	1 m/s,	bars flat		
	rated	33		23	3	2	4	9	1	18	
non-separ	ated	5		3	2		7	1		1	
Separator: sepa								1			
non-separ										1	
Replicate 9, T	reatment	11, 1 Ju	ne, Bar	spacing	19 mm,	water v	elocity 1	l m/s, b	ars flat		
Tanks: sepa	rated	45		31	1	3	4	4		20	
non-separ	ated	20		1	3		11	9		11	
Separator: sepa											
non-separ											
Replicate 10,	reatmen	t 11, 2 Ju	ıne, Bar	spacing	19 mm	, water	velocity	1 m/s,	bars flat		
	rated	513		20	2	3	2	24		23	
non-separ		282		7	1		9	8		20	
Separator: sepa							1				
non-separ											
Replicate 11,	reatmen	t 11, 5 Ju	ıne, Bar	spacing	g 19 mm	, water	velocity	1 m/s,	bars flat		
	rated	2		24			5	5		3	
non-separ	rated			11		1	11	3		5	
Separator: sepa	rated			1	1		1	7		1	
non-separ	rated										
Replicate 12,	<b>Freatmen</b>	t 11, 23	June, Ba	ar spacii	ıg 19 mı	n, wate	r velocit	y 1 m/s	, bars fla	t	
Tanks: sepa	rated	182		2							
non-separ	rated	4									
Separator: sepa	rated	1									
non-separ	rated										
Replicate 13,	Гreatmen	t 11, 26	June, Ba	ar spacii	ng 19 mi	n, wate	r velocit	y 1 m/s	, bars fla	t	
	rated	115									
non-sepa	rated	4									
Separator: sepa											
non-sepa	rated										
Replicate 14,	Гreatmen		June, Ba		ng 19 mi	n, wate	r velocit	y 1 m/s	, bars fla	t	
Tanks: sepa	rated	162		4							
non-sepa		7									
Separator: sepa	rated										
non-sepa	rated										

		earling nook		rling nook	Stee	lhead	Coho		Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 15, Treatme		uly, Bar	spacing	19 mm	, water	velocity	1 m/s, b	ars flat		
Tanks: separated	2093		4							
non-separated	61									
Separator: separated non-separated	3									
Replicate 16, Treatme	nt 11, 7 Ju	ılv. Bar	spacing	19 mm	water	velocity	1 m/s. h	ars flat		
Tanks: separated	491	, ,	1	,	,	, crocky	1 110 0, 0	arb ride		
non-separated	12		_							
Separator: separated	10									
non-separated										
Replicate 17, Treatme	nt 11, 8 Ju	ıly, Bar	spacing	19 mm	water	velocity	1 m/s, b	ars flat		
Γanks: separated	2233									
non-separated	4									
Separator: separated	2									
non-separated										
Replicate 18, Treatme	nt 11, 10 J	July, Ba	r spacin	g 19 mn	n, water	velocit	y 1 m/s,	bars fla	t	
Γanks: separated	211									
non-separated	15									
Separator: separated	2									
non-separated										
Replicate 19, Treatme	nt 11, 14 J	July, Ba	r spacin	g 19 mn	n, water	velocity	y 1 m/s,	bars fla	t	
Γanks: separated	185									
non-separated	24		2							
Separator: separated	4									
non-separated										
Replicate 20, Treatmen	nt 11, 17 J	luly, Ba	r spacin	g 19 mn	n, water	velocity	y 1 m/s,	bars fla	t	
Γanks: separated	151									
non-separated	21									
Separator: separated	2									
non-separated										
Replicate 21, Treatmen		uly, Ba	r spacin	g 19 mn	ı, water	velocity	1 m/s,	bars fla	t i	
Tanks: separated	51									
non-separated	13									
Separator: separated	1									
non-separated										

		earling nook		rling 100k	Steel	lhead	Co	oho	Soci	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 22, Treatmer		July, Ba	r spacin	g 19 mr	n, water	velocit	y 1 m/s,	bars fla	t	
Tanks: separated	107									
non-separated	18									
Separator: separated non-separated	4									
Replicate 23, Treatmen	nt 11, 30	July, Ba	r spacin	g 19 mr	n, water	velocit	y 1 m/s,	bars fla	t	
Tanks: separated	183									
non-separated	74									
Separator: separated										
non-separated										
Replicate 1, Treatment	t 12, 30 A	pril, Ba	r spacin	g 19 mr	n, water	velocit	y 2 m/s,	bars fla	t	
Tanks: separated			16	1		1			2	
non-separated				10		1			2	
Separator: separated										
non-separated										
Replicate 2, Treatment	t 12, 6 Ma	ay, Bar	spacing	19 mm,	water v	elocity 2	2 m/s, b	ars flat		
Tanks: separated			23		2	7			15	
non-separated			10			16		50000	3	
Separator: separated										
non-separated										
Replicate 3, Treatment	t 12, 11 M	Iay, Bar	spacing	g 19 mm	, water	velocity	2 m/s,	bars flat		
Tanks: separated			41			2			35	
non-separated			7	1		3			9	
Separator: separated			1							
non-separated										
Replicate 4, Treatment	t 12, 14 N	Iay, Bar	spacing	g 19 mm	ı, water	velocity	2 m/s,	bars flat		
Tanks: separated			12			1	1		17	
non-separated			10	1		5	3		39	
Separator: separated										
non-separated										
Replicate 5, Treatment	t 12, 15 N	Iay, Bar	spacing	g 19 mm	ı, water	velocity	2 m/s,	bars flat		
Tanks: separated		-	23	1	1	1			14	
non-separated			16	1		1	1		27	
Separator: separated										
non-separated										

			earling look		rling 100k	Stee	lhead	Coho		Soc	keye
Source		<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
	, Treatmen	nt 12, 18 M	lay, Bar	-	19 mm	, water	velocity	2 m/s, l	oars flat		
	eparated eparated			74 31	4	2 3	7 16	1		13	
Separator: s	separated eparated										
Replicate 7	, Treatmen	nt 12, 20 M	lav. Bar	spacing	19 mm	. water	velocity	2 m/s. l	oars flat		
	eparated	,,	,	36	,	,	7	, .	,	23	
	eparated	1		29	3	1	6			9	
Separator: s											
Replicate 8	, Treatmen	t 12. 26 M	av. Bar	spacing	19 mm	. water	velocity	2 m/s. h	ars flat		
	eparated	25	, , ,	22	5	1	2	- 112 5, 1	, ar b riae	22	
	eparated	11		25	10	2	4			6	
Separator: s				20	10	-	-			O	
	eparated										
Replicate 9	, Treatmen	t 12, 29 M	ay, Bar	spacing	19 mm	, water	velocity	2 m/s, t	ars flat		
Γanks: s	eparated	28		3	2	7	4			2	
non-se	eparated	27		19	19	5	12			16	
Separator: s	separated										
non-se	eparated										
Replicate 1	0, Treatme	nt 12, 2 Ju	ine, Bar	spacing	19 mm	, water	velocity	2 m/s, l	oars flat		
	eparated	306		9	2	1	1	16	1	2	
non-se	eparated	291		16	3		7	25	2	1	
Separator: s	separated										
non-se	eparated										
Replicate 1	1, Treatme	nt 12, 4 Ju	ne, Bar	spacing	19 mm	, water	velocity	2 m/s, h	oars flat		
	eparated			13		5	6	16		2	
	eparated			23	3	3	37	30	21		
Separator: s											
	eparated										
Replicate 1	2, Treatme	nt 12, 24 J	une, Ba	r spacin	ıg 19 mı	n, water	r velocit	y 2 m/s,	bars fla	t	
	eparated	145		-	_			,			
non-se	eparated	33									
Separator: s											
	eparated										

		earling nook		rling look	Steel	lhead	Coho		Soc	keye
Source	<180	≥180	<180	≥180	<180	≥180	<180	≥180	<180	≥180
Replicate 13, Treatme	nt 12, 26	July, Ba	r spacin	g 19 mr	n, water	velocit	y 2 m/s,	bars fla	it	
Γanks: separated	113									
non-separated	2									
Separator: separated										
non-separated										
Replicate 14, Treatme	nt 12, 30	June, Ba	ar spacii	ng 19 m	m, wate	r velocit	y 2 m/s	bars fla	at	
Tanks: separated	186		1							
non-separated	2									
Separator: separated										
non-separated										
Replicate 15, Treatme	nt 12, 2 Ju	uly, Bar	spacing	19 mm	, water	velocity	2 m/s, b	ars flat		
Tanks: separated	1170		2							
non-separated	226			1						
Separator: separated										
non-separated										
Replicate 16, Treatme	nt 12, 6 Ju	uly, Bar	spacing	19 mm	, water	velocity	2 m/s, t	ars flat		
Tanks: separated	123									
non-separated	74		1							
Separator: separated										
non-separated										
Replicate 17, Treatme	nt 12, 9 Ju	uly, Bar	spacing	19 mm	, water	velocity	2 m/s, t	ars flat		
Tanks: separated	151		6							
non-separated	32		1							
Separator: separated	1									
non-separated										
Replicate 18, Treatme	nt 12 10	Iuly Ra	r snacin	ισ 19 mr	n water	· velocit	v 2 m/s.	hars fla	ıt	
Tanks: separated	439	, ury, Du	3	9 17	,		,,			
non-separated	104		3							
Separator: separated	104		5							
non-separated										
Replicate 19, Treatme		July, Ba	r spacin	ig 19 mi	n, water	velocit	y 2 m/s,	bars fla	ıt	
Tanks: separated	166									
non-separated	58		1							
Separator: separated			1							
non-separated										

## Appendix Table 6. Continued.

Subyearling Yearling chinook chinook Steelhead Coho Sockeye <180 ≥180 <180 ≥180 Source <180 ≥180 <180 ≥180 <180 ≥180 Replicate 20, Treatment 12, 17 July, Bar spacing 19 mm, water velocity 2 m/s, bars flat Tanks: separated 133 non-separated 17 Separator: separated non-separated Replicate 21, Treatment 12, 22 July, Bar spacing 19 mm, water velocity 2 m/s, bars flat Tanks: 54 separated non-separated 27 Separator: separated non-separated Replicate 22, Treatment 12, 24 July, Bar spacing 19 mm, water velocity 2 m/s, bars flat Tanks: separated 112 47 non-separated Separator: separated non-separated Replicate 23, Treatment 12, 29 July, Bar spacing 19 mm, water velocity 2 m/s, bars flat Tanks: separated 167 non-separated 132 Separator: separated non-separated

Appendix Table 7. Analyses of covariance results among mean separation efficiency values obtained for treatments involving separation-bar spacing (gap), water velocity, and separation-bar array angle during biological design criteria studies using an evaluation high-velocity flume wet separator at McNary Dam, 1998. Sample date (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates.  $\alpha = 0.05$ ,  $\dagger = \text{significant difference}$  among means. Where analysis involved more than two treatments, an association table showing the highest differences between paired treatment means is included. Association tables follow Fishers protected least significant difference, \* = significant differences between paired means.

Species	Length group	Analysis source	F	df	P
Yearling	<180 mm	date	26.73	1	0.000 †
chinook		gap	33.94	2	0.000 †
salmon		velocity	29.48	1	0.000 †
		angle	21.11	1	0.000 †
		gap vs. velocity	3.42	2	0.037 †
		gap vs. angle	3.43	2	0.037 †
		velocity vs. angle	0.84	1	0.361
		gap vs. velocity vs. angle	1.08	2	0.345

Separation-bar gap vs. water velocity

Gap (m), velocity (m/s)	Mean	SE	Association table						
13,1	26.15	5.318		13,1	13,2	16,1	16,2	19,1	
13,2	21.37	2.642	13,2		1				
16,1	67.39	3.037	16,1	*	*				
16,2	47.11	3.117	16,2	*	*	*			
19,1	76.65	3.138	19,1	*	*	*	*		
19,2	49.08	3.418	19,2	*	*	*		*	

Separation-bar gap (mm) vs. separation-bar array angle (0 = flat, a = angled)

Gap (m), angle (0 = flat, a = angled)	Mean	SE		As	ssociation	n table		
13,0	32.22	5.312		13,0	13,a	16,0	16,a	19,0
13,a	15.31	5.647	13,a	*	100			
16,0	60.28	3.039	16,0	*	*			
16,a	54.52	3.115	16,a	*	*			
19,0	73.9	3.414	19,0	*	*	*	*	
19,a	51.82	3.418	19,a	*	*			*

## Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Yearling	total catch	date	24.44	1	0.000 †
chinook salmon		gap	40.08	2	0.000 †
		velocity	31.76	1	0.000 †
		angle	24.72	1	0.000 †
		gap vs. velocity	3.04	2	0.530
		gap vs. angle	3.63	2	0.030 †
		velocity vs. angle	0.69	1	0.410
		gap vs. velocity vs. angle	0.82	2	0.444

Gap (mm), angle ( $0 = \text{flat}$ , $a = \text{angled}$ )	Mean	SE	Association table							
13,0	37.16	4.612		13,0	13,a	16,0	16,a	19,0		
13,a	20.97	4.910	13,a	*						
16,0	64.84	2.656	16,0	*	*					
16,a	59.16	2.654	16,a	*	*					
19,0	74.26	2.671	19,0	*	*	*	*			
19,a	54.53	2.672	19,a	*	*	*	V.V.	*		

Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Steelhead	≥180	gap	77.02	2	0.000 †
		velocity	0.80	1	0.379
		angle	4.10	1	0.053
		gap vs. velocity	2.95	2	0.070
		gap vs. angle	3.61	2	0.041 †
		velocity vs. angle	0.99	1	0.328
		gap vs. velocity vs. angle	4.40	2	0.892

Gap (mm), angle ( 0 = flat, a = angled)	Mean	SE	Association table							
13,0	90.25	4.385		13,0	13,a	16,0	16,a	19,0		
13,a	100	4.385	13,a							
16,0	98.98	2.193	16,0							
16,a	96.39	2.193	16,a	3/2/						
19,0	67.69	2.193	19,0	*	*	*	*			
19,a	75.84	2.08	19,a	*	*	*	*	*		

Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Steelhead	total catch	gap	4.12	2	0.027 †
		velocity	0.10	1	0.756
		angle	1.46	1	0.237
		gap vs. velocity	1.95	2	0.162
		gap vs. angle	0.49	2	0.620
		velocity vs. angle	3.32	1	0.079
		gap vs. velocity vs. angle	2.31	2	0.118

Separation-bar gap (mm)							
Gap (mi	n)	Mean		SE	Association table		
13		28.4		9.846		13	16
16		56.2		4.583	16	*	
19		42.99		4.798	19		

Appendix Table 7. Continued.

Length group		Analysis source	F	df	P
Sockeye	<180 mm	gap	0.27	2	0.767
salmon		velocity	4.63	1	0.037 †
		angle	2.14	1	0.151
		gap vs. velocity	0.91	2	0.409
		gap vs. angle	0.53	2	0.590
		velocity vs. angle	1.62	1	0.210
		gap vs. velocity vs. angle	0.18	2	0.836

# Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Total salmonid species (spring outmigration)	<180	date	10.66	1	0.002 †
		gap	19.28	2	0.000 †
		velocity	31.90	1	0.000 †
		angle	31.05	1	0.000 †
		gap vs. velocity	2.93	2	0.059
		gap vs. angle	1.50	2	0.229
		velocity vs. angle	0.33	1	0.565
		gap vs. velocity vs. angle	3.99	2	0.022 †

### Separation-bar gap vs. water velocity vs. separation-bar array angle

Gap (mm), velocity (m/s), angle (0 = flat, a = angled)	Mean	SE
13,1,0	46.22	6.446
13,1,a	35.59	6.452
13,2,0	44.27	6.446
13,2,a	25.55	7.344
16,1,0	75.14	3.795
16,1,a	52.16	3.795
16,2,0	46.10	3.799
16,2,a	45.77	3.795
19,1,0	84.48	3.810
19,1,a	66.02	3.809
19,2,0	62.76	3.804
19,2,a	39.52	3.807

### Association table

	13,1,0	13,1,a	13,2,0	13,2,a	16,1,0	16,1,a	16,2,0	16,2,a	19,1,0	19,1,a	19,2,0
13,1,a						1000	3500				
13,2,0							1 54.8	1245			
13,2,a	*	7.79			7700				P. T. Back		
16,1,0	*	*	*	*							
16,1,a		*		*	*		23177 37				100
16,2,0				*	*						
16,2,a				*	*						
19,1,0	*	*	*	*	- 17	*	*	*			
19,1,a	*	*	*	*		*	*	*	*		
19,2,0	*	*	*	*	*		*	*	*		
19,2,a					*	*			*	*	*

Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Total salmonid species	≥180	gap	26.79	2	0.000 †
(spring		velocity	1.20	1	0.281
outmigration)		angle	0.80	1	0.377
7		gap vs. velocity	1.57	2	0.223
		gap vs. angle	2.74	2	0.078
		velocity vs. angle	0.34	1	0.564
		gap vs. velocity vs. angle	0.35	2	0.704

	Separa	ation-bar gap				
Gap (mm) Mean SE Association						
13	94.03	5.379		13	16	
16	94.79	2.533	16			
19	71.36	2.344	19	0	0	

# Appendix Table 7. Continued.

	Length				
Species	group	Analysis source	F	df	P
Total	total catch	date	4.06	1	0.047 †
salmonid		gap	14.90	2	0.000 †
species (spring		velocity	29.48	1	0.000 †
outmigrati		angle	26.95	1	0.000 †
on)		gap vs. velocity	1.63	2	0.201
		gap vs. angle	0.29	2	0.746
		velocity vs. angle	0.53	1	0.470
		gap vs. velocity vs. angle	3.69	2	0.029 †

### Separation-bar gap vs. water velocity vs. separation-bar array angle

Gap (mm), veolcity (m/s), angle (0 = flat, a = angled)	Mean	SE
13,1,0	53.33	5.627
13,1,a	44.75	5.633
13,2,0	49.98	5.627
13,2,a	34	6.411
16,1,0	80.88	3.313
16,1,a	59.54	3.314
16,2,0	56.49	3.316
16,2,a	55.29	3.313
19,1,0	80.95	3.326
19,1,a	67.15	3.325
19,2,0	63.2	3.321
19,2,a	47.36	3.324

#### Association table

	13,1,0	13,1,a	13,2,0	13,2,a	16,1,0	16,1,a	16,2,0	16,2,a	19,1,0	19,1,a	19,2,0
13,1,a											
13,2,0											
13,2,a	*										
16,1,0	*	*	*	*	4 4		416	Territoria.	a flagso		A. L. İ
16,1,a		*		*	*						
16,2,0				*	*						
16,2,a				*	*			1751 T-1960			
19,1,0	*	*	*	*		*	*	*			
19,1,a	*	*	*	*	*		*	*	*		
19,2,0		*	*	*	*				*		
19,2,a					*	*		3-	*	*	*

Appendix Table 7. Continued.

Species	Length group	Analysis source	F	df	P
Subyearling chinook salmon	<180	date	37.71	1	0.000 †
		gap	2.31	2	0.104
		velocity	30.40	1	0.000 †
		angle	22.25	1	0.000 †
		gap vs. velocity	0.10	2	0.909
		gap vs. angle	1.10	2	0.338
		velocity vs. angle	0.55	1	0.459
		gap vs. velocity vs. angle	0.52	2	0.597

Appendix Table 8. Analyses of covariance results among mean separator exit efficiency values obtained for treatments involving separation-bar spacing (gap), water velocity, and separation-bar array angle during biological design criteria studies using an evaluation high-velocity flume wet separator at McNary Dam, 1998. Sample date (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates. A significant difference ( $\alpha$  = 0.05) among means is indicated by a cross (†). Where analysis involved more than two treatments, the highest level of interaction is further denoted by a letter referring to an association table clarifying differences between paired treatment means. Association tables follow Fishers Protected Least Significant Difference procedure results, with asteristics indicating differences between paired means.

Species	Length group	Analysis source	F	df	P
Yearling	<180	date	0.17	1	0.685
chinook salmon		gap	0.67	2	0.515
		velocity	27.90	1	0.000 †
		angle	29.70	1	0.000 †
		gap vs. velocity	0.04	2	0.964
		gap vs. angle	0.54	2	0.585
		velocity vs. angle	24.20	1	0.000 †
		gap vs. velocity vs. angle	0.32	2	0.728

Velocity (m/s), angle (0 = flat, a = angled)	Mean	SE	Association table			
1,0	99.66	1.005		1.0	1,a	2,0
1,a	88.98	0.996	1,a	0		
2,0	99.74	1.03	2,0		*	
2,a	99.17	1.099	2,a		*	

Appendix Table 8. Continued.

	Length	Analysis					
Species	group	source	F	df	P		
Yearling	total catch	date	0.08	1	0.771		
chinook salmon		gap	0.97	2	0.385		
		velocity	28.71	1	0.000 †		
		angle	35.61	1	0.000		
		gap vs. velocity	0.12	2	0.884		
		gap vs. angle	0.71	2	0.495		
		velocity vs. angle	27.87	1	0.000		
		gap vs. velocity vs. angle	0.77	2	0.467		

Water velocity	VS.	separation-bar	array ang	le
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Velocity (m/s), angle (0 = flat, a = angled)	Mean	SE	Association table				
1.0	99.6	0.949		1.0	1,a	2,0	
1,a	88.45	0.95	1,a	0			
2,0	99.67	0.949	2,0		*		
2,a	98.99	1.124	2,a		*		

# Appendix Table 8. Continued.

2,a

Length group	Analysis source	F	df	P
≥180	gap	0.43	2	0.653
	velocity	6.00	1	0.021 †
	angle	15.95	1	0.000 †
ì	gap vs. velocity	0.25	2	0.783
	gap vs. angle	0.20	2	0.818
	velocity vs. angle	4.55	1	0.043
	gap vs. velocity vs. angle	0.43	2	0.658
	group	group source  ≥180 gap  velocity  angle  gap vs. velocity  gap vs. angle  velocity vs. angle	group       source       F         ≥180       gap       0.43         velocity       6.00         angle       15.95         gap vs. velocity       0.25         gap vs. angle       0.20         velocity vs. angle       4.55	group       source       F       df         ≥180       gap       0.43       2         velocity       6.00       1         angle       15.95       1         gap vs. velocity       0.25       2         gap vs. angle       0.20       2         velocity vs. angle       4.55       1

Velocity (m/s), angle (0 = flat, a = angled)	Mean SE			Association table					
1.0	96.99	4.848		1.0	1,a	2,0			
1,a	67.42	4.682	1,a	0	All States				
2,0	98.53	4.848	2,0		*				

4.981

2,a

89.54

Appendix Table 8. Continued.

Species	Length group	Analysis source	F	df	P
Steelhead	total catch	gap	0.38	2	0.684
		velocity	6.53	1	0.016 †
		angle	19.32	1	0.000 †
		gap vs. velocity	0.34	2	0.716
		gap vs. angle	0.20	2	0.817
100		velocity vs. angle	4.80	1	0.037 †
		gap vs. velocity vs. angle	0.79	2	0.463

Velocity (m/s), angle $(0 = \text{flat}, a = \text{angled})$	Mean	SE	Association table				
1.0	97.23	4.269		1.0	1,a	2,0	
1,a	69.55	4.075	1,a	*			
2,0	98.76	4.197	2,0		*		
2,a	89.49	4.269	2,a		*		

Appendix Table 8. Continued.

Species	Length group	Analysis source	F	df	P
Sockeye salmon	<180 mm	gap	0.67	2	0.517
		velocity	2.62	1	0.113
		angle	2.78	1	0.103
		gap vs. velocity	0.25	2	0.780
		gap vs. angle	0.56	2	0.575
		velocity vs. angle	0.77	1	0.358
		gap vs. velocity vs.	0.33	2	0.723

Appendix Table 8. Continued.

Specie	es		ength coup	Analys	sis			F	df	F	,	
Total	salmonio	d <	180	date			4	1.75	1	(	0.190	
specie				gap				2.19	2		0.118	
(spring				velocit	V			30.19	1	C	.000 †	
migrai	iioii)			angle				30.01	1		0.000 †	
					velocity	7		3.81	2		.026 †	
				gap vs. velocity				6.55	2		.002 †	
				gap vs. angle velocity vs. angle								
								31.33	1		.000 †	
				gap vs.	velocity	vs. ang	le	3.16	2	0	.047 †	
	S	Separatio	on-bar ga	ap vs. wa	ater velo	city vs.	separatio	on-bar a	rray ang	le		
	Gap (mm), velocity (m/s), angle (0 = flat, a = angled)			Mean				SE				
	13,1,0				99	.16		1.978				
	13.	,1,a			93	.27			1.9	979 .		
	13,2,0				99	.43			1.9	978		
	13,2,a				99	.56			2.2	253		
	16,1,0				99	.53	4.7		1.1	164		
	16,	,1,a			83	.82			1.1	165		
	16,	2,0							1.1	1.166		
	16,	2,a		98.69 1.164								
	19,	1,0		98				1.169				
	19,	1,a		91.13 1.169					69			
	19,	2,0		97.42				1.167				
	19,	2,a			85	5.5		1.168				
					Associat	ion table	9					
	13,1,0	13,1,a	13,2,0	13,2,a	16,1,0	16,1,a	16,2,0	16,2,a	19,1,0	19,1,a	19,2,	
13,1,a	*						55.25					
13,2,0		*							75.			
13,2,a		*	1116-11									
16,1,0	at-	*	y-	st-	<b>V</b> -		200					
16,1,a	*	*	*	*	*	*					A Table Say	
16,2,0		*				*	115					
16,2,a		*		7,7		*	-					
19,1,0 19,1,a	*	1,14	*	*	*	*	*	*	*	(2-14) 1 a		
19,1,a 19,2,0	-					*				*		
19,2,0 19,2,a	*	*	*	*	*		*	*	*	*	*	

# Appendix Table 8. Continued.

Species	Length group	Analysis source	F	df	P
Total salmonid species (spring outmigration)	≥180	gap	0.27	2	0.762
		velocity	7.40	1	0.010 †
		angle	14.93	1	0.000 †
		gap vs. velocity	0.10	2	0.908
		gap vs. angle	0.10	2	0.903
		velocity vs. angle	5.67	1	0.023 †
		gap vs. velocity vs. angle	0.29	2	0.749

velocity (m/s), angle (0 = flat, a = angled)  Mean SE Association table								
1,0	97.48	4.046		1,0	1,a	2,0		
1,a	72.82	3.880	1,a	*				
2,0	98.83	3.975	1,0		*			
2,a	92.97	3.893	2,a		0			

Appendix Table 8. Continued.

			Length			alysis		_			_
Specie			group		SO	urce		F		f	P
	salmonic	l tot	al catch	date				1.68	1		0.199
specie (sprin				gap				1.26	2	(	).289
	gration)			velo	city			37.03	1	(	0.000 †
	B			angle				44.80	1	(	0.000 †
				gap v	s. veloc	ity		3.45	2		0.036 †
				gap v	s. angle			4.58	2	0	0.013 †
				veloc	city vs. a	ngle		36.44	1	0	0.000 †
					s. veloc	_	ngle	3.30	2	C	0.042 †
	S	eparatio	on-bar g				separati		rray ang		·
Ga	p (mm),	_							, ,		
		lat, a = i				Mic	ean			SE	
		13,1,0					.76			2.166	
		13,1,a					.55			2.169	
13,2,0							.14			2.166	
	13,2,a						.23			2.468	
	16,1,0						.45			1.276	
	16,1,a						.92			1.276	
		16,2,0				99.			1.279 1.276		
		16,2,a			98.47						
		19,1,0			97.84 88.36			1.281			
		19,1,a								1.28	
		19,2,0				97. 97.				1.279 1.28	
		19,2,a								1.20	
		7-7-			Associat	ion table	e				
	13,1,0	13,1,a	13,2,0	13,2,a	16,1,0	16,1,a	16,2,0	16,2,a	19,1,0	19,1,a	19,2,0
13,1,a	*	Sec. 3 5 1					200				
13,2,0		*		X 855	f,						
13,2,a		*		一带 1							
16,1,0	*	*	*	*	*						
16,1,a 16,2,0		*			-	*					
16,2,0		*				*					
19,1,0		*	4			*					
19,1,a	*		*	*	*	*	*	*	*		
19,2,0		*				*				*	
19,2,a		*		1		*				*	

# Appendix Table 8. Continued.

Species	Length group	Analysis source	F	df	P
Subyearling chinook	<180	date	24.84	1	0.000 †
salmon		gap	0.46	2	0.630
		velocity	27.49	1	0.000 †
		angle	30.10	1	0.000 †
		gap vs. velocity	0.16	2	0.885
		gap vs. angle	0.03	2	0.973
		velocity vs. angle	18.20	1	0.000 †
		gap vs. velocity vs. angle	0.00	2	0.998

### Water velocity vs. separation-bar array angle

Velocity (m/s), angle (0 = flat, a = angled)	Mean	SE	Association table			
1,0	99.2	0.6867		1,0	1,a	2,0
1,a	92.54	0.6867	1,a	0		
2,0	99.91	0.6867	1,0		*	
2,a	99.07	0.6867	2,a		0	

Appendix Table 9. Analyses of covariance results among mean descaling values obtained for treatments involving separation-bar spacing (gap), water velocity, and separation-bar array angle during biological design criteria studies using an evaluation high-velocity flume wet separator at McNary Dam, 1998. Sample date f (date) was included as a covariate where the analysis was not seriously affected by combining samples from successive replicates. A significant difference (a = 0.05) among means is indicated by a cross (†).

	Length	Analysis			
Species	group	source	F	df	P
Yearling	<180	date	7.03	1	1.010 †
chinook salmon		gap	2.03	2	0.138
		velocity	0.47	1	0.495
		angle	0.54	1	0.466
		gap vs. velocity	0.84	2	0.437
		gap vs. angle	0.35	2	0.708
		velocity vs. angle	0.19	1	0.667
		gap vs. velocity vs. angle	0.37	2	0.693
Yearling	total catch	date	7.97	1	0.006 †
chinook salmon		gap	2.36	2	0.100
		velocity	0.52	1	0.473
		angle	0.28	1	0.599
		gap vs. velocity	0.59	2	0.558
		gap vs. angle	0.40	2	0.673
		velocity vs. angle	0.07	1	0.796
		gap vs. velocity vs. angle	0.47	2	0.627
Steelhead	≥180	gap	0.94	2	0.404
		velocity	0.12	1	0.734
		angle	0.52	1	0.477
		gap vs. velocity	2.30	2	0.120
		gap vs. angle	0.17	2	0.848
		velocity vs. angle	0.63	1	0.434
		gap vs. velocity vs. angle	0.55	2	0.584
Steelhead tota	total catch	gap	0.96	2	0.395
		velocity	0.31	1	0.582
		angle	0.25	1	0.623
		gap vs. velocity	0.58	2	0.564
		gap vs. angle	0.19	2	0.827
		velocity vs. angle	0.05	1	0.831
		gap vs. velocity vs. angle	0.65	2	0.532

Appendix Table 9. Continued.

	Length	Analysis			
Species	group	source	F	df	P
Sockeye salmon	<180 mm	gap	0.49	2	0.616
Sockeye summon (	1200	velocity	0.87	1	0.357
		angle	0.08	1	0.783
		gap vs. velocity	0.06	2	0.938
		gap vs. angle	0.53	2	0.594
		velocity vs. angle	0.83	1	0.366
		gap vs. velocity vs. angle	0.01	2	0.993
Total salmonid	<180	date	1.93	1	0.168
species (spring		gap	1.15	2	0.322
outmigration)		velocity	1.41	1	0.238
		angle	0.03	1	0.872
		gap vs. velocity	0.64	2	0.527
		gap vs. angle	0.21	2	0.812
		velocity vs. angle	1.65	1	0.202
		gap vs. velocity vs. angle	0.04	2	0.964
Total salmonid	≥180	gap	0.41	2	0.668
salmonid		velocity	0.26	1	0.613
pecies		angle	0.00	1	0.987
spring outmigrati	on)	gap vs. velocity	2.26	2	0.065
		gap vs. angle	0.44	2	0.650
		velocity vs. angle	0.68	1	0.416
		gap vs. velocity vs. angle	0.46	2	0.635
Total		date	1.87	1	0.175
almonid		gap	0.86	2	0.427
pecies		velocity	1.72	1	0.193
(spring outmigration)		angle	0.01	1	0.925
		gap vs. velocity	0.43	2	0.652
		gap vs. angle	0.44	2	0.643
		velocity vs. angle	0.57	1	0.453
		gap vs. velocity vs. angle	0.02	2	0.981
ubyearling	<180	date	3.27	1	0.073
chinook		gap	0.83	2	1.438
salmon		velocity	12.27	1	0.001 -
		angle	0.10	1	0.753
		gap vs. velocity	0.06	2	0.937
		gap vs. angle	1.74	2	0.180
		velocity vs. angle	0.44	1	0.510
		gap vs. velocity vs. angle	2.02	2	0.136