A Comparative Analysis of the Effects on Technical Efficiency and Harvest of Sea Scallops (*Placopecten magellanicus*) By Otter Trawls of Various Mesh Sizes

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East Coast Fisheries Association

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EAST COAST FISHERIES ASSOCIATION*

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INTRODUCTION

Since 1983, the sea scallop, <u>Placopecten magellani-</u> <u>CUS</u> (Gmelin), fishery has been regulated by the Fishery Management Plan for Sea Scallops (FMPSS) under the authority of the New England Fisheries Management Council (NEFMC, 1982). The regulations restrict vessels which land shucked meats to a maximum number of meats per pound; vessels which land shell-stock are subject to minimum shell size restriction. The current meat count and shell stock regulations are 30 meats per pound (MPP) with a 10% tolerance between February 1 and September 30 and 33 MPP with a 10% tolerance between October 1 and January 31, and a minimum shell size of 3.5-inches (88.9 mm) in which no more than 40 out of 400 scallops can be less than 3.5-inches.

The regulations have posed several problems. First, there is a possible problem of inequity between firms which shuck at sea and firms which shell stock or land whole scallops in the shell; the existence of the inequity has not been substantiated, but it likely occurs within both fleets. Second, it has been demonstrated that there is considerable variation in the meat count for scallops of given shell heights; this is believed to be related to spatial and temporal differences and the reproductive cycle (DuPaul and Kirkley, 1987, 1988; Shumway and Schick, 1988; DuPaul et al., 1988). Third, the meat count for landed product may be different than the meat count for harvested

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product due to shucking and at-sea handling practices.

As a result of these sources of variations and problems, the current regulations may be inadequate. Alternative forms of regulations need to be considered. This study analyzes the harvesting efficiency and size, selectivity of various mesh sizes on vessels which trawl for scallops; these vessels typically land shell stock. If changes in mesh and ring size increase escapement of small scallops and have minimal effects on the harvesting efficiency, gear restrictions may offer a feasible alternative to the current set of regulations. However, it is stressed that the analysis of harvesting efficiency and size selectivity in this study is predicated on the resource conditions prevailing for the time and resource areas examined. Different resource conditions could yield different results; for example, size selectivity for an area comprised of mostly large scallops would be different than the size selectivity of an area comprised of mostly small scallops.

MATERIALS AND METHODS

Data collection

A nine-day sea scallop conservation engineering project was conducted aboard the F/V <u>Miss Quality</u> from the port of Wanchese, North Carolina. The vessel, a commercial sea scallop shell-stocker, departed at 0800 on 20 April and returned on 28 April, 1988. Fishing gear trials with sea

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scallop trawl nets were conducted in the mid-Atlantic area, adjacent to the New Jersey coast (NEFC Statistical Areas 614, 621, and 622, Figure 1). The trawl trials were conducted for the purpose of obtaining catch and lengthfrequency data necessary for analyzing harvesting efficiency and size selectivity of trawls.

A second vessel, the F/V Lady Cheryl, a commercial dredge vessel from New Bedford, Massachusetts, conducted dredge hauls in the same area as the shell-stocking vessel. The dredge vessel fished concurrently an eight foot experimental survey dredge (2-inch rings) with a one and onehalf inch (38 mm) liner and a standard 15-foot commercial scallop dredge (3-inch rings). These tows were made to compare size selectivity and catch rates of various gear configurations in the same resource area at the same time.

Experimental hauls for both vessels were made at depths ranging from 23 to 35.5 fathoms (41 to 64 meters). Average depth fished by the F/V <u>Miss Quality</u> was 33 fathoms (59 meters); average depth fished by the F/V <u>Lady Cheryl</u> was 26 fathoms (47 meters). Typically, 2 baskets of scallops from each net-mesh combination per tow were sampled for a total of four baskets of scallops per tow on the net boat; sample size for the dredge vessel was one basket per tow from each dredge for a total of two baskets per tow.

Scallops were measured by 5 mm intervals using measuring devices available from the National Marine Fisheries Service. Length of tow, time of day, depth, and baskets of

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FIGURE 1. NATIONAL MARINE FISHERIES SERVICE (NNES)

THREE- DIGIT STATISTICAL AREAS



scallops, fish, and trash were recorded for all tows. A total of 43 trawl tows were used to analyze size selectivity and harvesting efficiency; scallops from 15 tows by the dredge were used for analysis.

Vessel description

F/V Miss Ouality

The F/V <u>Miss Quality</u> is a 78-foot (23.8 meters), 24-foot beam (7.3 meters), 9-foot (2.7 meters) draft, steel-hulled combination western (stern ramp and dual net reel) and southern rigged (port and starboard 50-foot outriggers) sea scallop trawler. The main engine is a Caterpillar 5.88 reduction turning-a 7046 four blade propeller; gross-registered-tonnage is 159 tons with a fishhold capacity of 40 tons. The vessel can accommodate a crew of six.

Electronics for the F/V <u>Hiss Quality</u> included: Furuno Echo Sounder Type FE-D813AF; EPSCO Chromascope Fish Finder, CVS-886; Northstar 7000, Remote Control equipped with Wood Freeman Automatic Pilot; EPSCO, C-Plot 2; Furuno-Radar Type FR-711 (72 mile range); Furuno-Radar Type FR-240, Mark-II (24 mile range); EPSCO C-Nav XL Plotter; and Sea Water Temperature, Dytek Laboratories, Model 703200.

Radio communications equipment included: Patterson Mfg. Co. Sideband, FCC Data-310-A (Call WYK4056); Regency Polaris VHS; three citizen band radios--Cobra 148GTL-OX CB,

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Horizon Maxi CB, and Realistic TRC-415.

F/V Lady Chervl

The F/V Lady Chervl is a 100-foot (30.5 meter), 12-foot draft (3.65 meter) steel-hulled western rigged sea scallop dredge vessel. The gross-registered-tonnage is 194 tons and the vessel can accommodate a crew of 14.

Fishing gear

Two sea scallop shell-stocking trawl nets, two modified trawl nets, and one typical calico scallop trawl net were evaluated during the fishing experiment. Simultaneous trawl hauls were conducted to test differences between The trawl boards were attached directly to trawl nets. wings, thereby maintaining the spread and "mouth" opening of the trawl net. Two identical sets of otter boards were used off the starboard and port outriggers. Board dimensions were 11-feet (3.35 meters) by 3.4-feet (1.12 meters). Fifty fathom (19.4 meters) bridle cables of 5/8-inches (16 mm) wire cable extended from both the 5/8-inch starboard and port main cable. The ratio of wire to water depth was maintained at 3 to 1; however, each main cable was alternately decreased by 25 fathoms (45.7 meters) to prevent the two nets from tangling during fishing operations.

Sea scallop shell-stocking trawl nets

The trawl configuration consisted of a two-seam,

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narrow 9:1 tapered trawl body with codend. Two similar sized shell-stocking trawl nets were tested: a 98 foot (29.9 meter) headrope and footrope, 5-inch mesh body (four mm polyethylene twine) with a 4 1/2-inch mesh codend; and a 100 foot (30.5 meter) headrope and footrope, 4-inch mesh body (three mm polyethylene twine) with a 4 1/2-inch mesh codend. The wing construction of the five-inch mesh trawl consisted of 90 dog wings with a 90 mesh belly; the wing construction of the 4-inch mesh trawl net consisted of 113 dog mesh with a 234 mesh belly. Headropes and footropes were 3/4-inch diameter (19 mm) with 1/2-inch diameter (13 mm) chain attached 12 links every 16-inches. The 100 foot, 4-inch mesh trawl net was constructed to minimize the difference of surface area between that of the five-inch net.

The codend of each of the above nets consisted of Number 120 nylon braided twine, 60 meshes in length. During the codend experiment, a 5-inch codend, 120 nylon braided twine, 50 meshes in length, was used.

Sea scallop shell-stocking nets were heavily equipped with chaffing gear to avoid wear. An approximate one-meter length of 3/16-inch (5 mm) diameter or Number 20 braided nylon was doubled and attached around the entire codend. From the terminus of the codend, working forward, a chaffing strand was attached to each mesh row for about half the length of the codend; thereafter, a strand was attached every other row for approximately 20 knots above the codend.

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Calico scallop trawl net

A typical, two-seam, semi-bailon design, calico trawl net was tested with a sea scallop trawl net. The calico trawl net was constructed entirely of 3-inch mesh, No. 84 braided nylon. The 36 foot long (11 meters), 5/8-inch (16 mm) diameter combination rope/wire headrope and footrope, with identical top and bottom sections, was rigged with a "Texas drop chain". This consisted of 1/2-inch (13 mm) cable running the length of the footrope and fastened at regular intervals by 3-link chain drops. Both the codend and the trawl net body were protected with polyethylene chaffing gear, similar to the arrangement described above.

Fishing operations

Fishing operations were conducted in coastal waters, east of Virginia, Maryland, and New Jersey from approximately 39 24' N, 74 01' W to 37 04' N, 74 55' W in depths ranging from 27 to 35 fm. Fishing was conducted between April 21 and 27, 1988; 43 tows were completed. Two nets were simultaneously towed with towing times ranging from 10 to 182 minutes; towing speed was 2.8 knots. Net mesh size of the paired tows are presented in Table 1. Tows 1 through 5 were conducted to examine whether or not there were any port or starboard related differences.

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| Tow # | Net | • | lesh Size (inche | a) |
|--------|-----|-----------|------------------|--------|
| | | Top Panel | Bottom Panel | Codend |
| 1-5 | 1 | 5 | 5 | 4 1/2 |
| | 2 | 5 | 5 | 4 1/2 |
| 6-12 | 1 | 5 | 5 | 4 1/2 |
| | 2 | 4 | 4 | 4 1/2 |
| 13-24 | 1 | 5 | 5 | 5 |
| | 2 | 4 | 4 | 4 1/2 |
| 25-31Þ | 1 | 3 | 3 | 3 |
| | 2 | 4 | 4 | 4 1/2 |
| 32-33 | 1 | 5 | 4 | 4 1/2 |
| | 2 | 4 | 4 | 4 1/2 |

TABLE 1

Paired tows and corresponding mesh sizes of trawl nets*

"Side-by-side gear configurations were examined.

bCalico scallop trawl net.

The dredge vessel, <u>Lady Cheryl</u>, made corresponding tows on the same bearings as F/V <u>Miss Quality</u> a few hours after <u>Miss Quality</u> had fished. Table 2 provides the tow numbers for the dredge vessel comparable to the tows made by the trawl vessel.

Catch and length-frequency data

Catch data were collected for each tow and net (Table 1 of Appendix I). Catch and scallop size distribution for each grouping of tows for which data were obtained are presented and discussed in the results section of this study. The catch of scallops was recorded in baskets; the two handled plastic baskets often used on commercial fishing vessels measured 17-inches across the top, 13-inches at the bottom, and 15-inches high. Length-frequency data for 2 baskets per net per tow were obtained. The two baskets were a sub-sample from the total catch after debris and by-catch were separated from the scallops. The shell height of scallops was measured in 5 mm intervals.

Purposes of the study were to examine harvesting efficiency and size selectivity. Harvesting efficiency was examined by comparing seemingly unrelated regression estimates of catch-effort models for four of the mesh combinations; a conventional F-test was used to examine the efficiency of tows 32 and 33. Size selectivity was examined by graphical interpretation. Selection curves based on the methods of Beverton and Holt (1957), Pope et al. (1975),

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TABLE 2

| | F/V Lady | <u>Chervl</u> | | P / | P/V <u>Miss Quality</u> | | | |
|---------|-------------------------|-----------------------|-------|------------|-------------------------|--------------------|--|--|
| Tow # | Dredge Size (ft.) | Ring Size (in.) | Tow # | Mes Top | h Size Bottom | (inches) Codend | | |
| 61-65 | 8 15 | 2ª 3 | 6-12 | 5 4 | 5 4 | 4 1/2 4 1/2 | | |
| 84-88 | 8 15 | 2 3 | 13-24 | 5 4 | 5 4 | 5 4 1/2 | | |
| 106-110 | 8 15 | 2 - 3 | 25-31 | 3 4 | 3 4 | 3 4 1/2 | | |

Matched tows involving F/V <u>Lady Chervl</u> using scallop dredges and F/V <u>Hiss Quality</u> using scallop trawl nets.

All tows made with 8-foot dredge, 2-inch (50.8 mm) rings, and a 1.5-inch (38 mm) liner. and Serchuk and Smolowitz (1980) were not used to examine selectivity for several reasons. First, grouping of data into 5 mm intervals caused heteroscedasticity. Second, truncation at 0 and 1 posed special estimation problems. Third, estimates of number of scallops that escaped harvest relative to the number of scallops actually retained in the net were imprecise. In essence, estimates of percent retention were inaccurate.

The statistical problems of heteroscedasticity and double truncation can be easily remedied. Procedures to correct for heteroscedasticity caused by grouping of data are summarized in Maddala(1977) and Bewley (1989). The problem of double truncation may be corrected by using a 'two limit probit' or 'two limit tobit' model (Rosett and Nelson 1975). These procedures, however, were not further pursued because it was not thought that estimates of size selectivity based on the data available were meaningful. That is, estimates of percent retention for closely similar mesh sizes are not indicative of actual size selectivity. Nevertheless, data for estimating relative size selectivity are presented in this report.

Size selectivity was inferred from the lengthfrequency and cumulative distribution graphs. However, the analysis of size selection is conditional on the prevailing resource conditions and areas fished. Different stock distributions, densities, and size compositions could yield different results (Bourne 1965). For example, selectivity

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would be different for an area characterized by a large concentration of small scallops vs. large scallops.

RESULTS

Harvesting efficiency

Although the experiment was primarily concerned with determining size selectivity of different mesh sizes, it was also important to determine the relative efficiency of different mesh sizes. That is, what was the difference between catch for a given level of fishing effort by one mesh size and catch for the same level of effort for a different mesh size. The possible difference between catches is important to know if mesh restrictions are to be implemented. It also was necessary to quantify differences in harvest levels to validate the trawl experiment. For example, if the same mesh trawl was towed on both sides of the vessel and there were differences in the catch levels, the analyses of harvesting efficiency and size selectivity would have to be modified to reflect port-starboard differences.

In this section, an analysis of the relative efficiency of different mesh sizes is presented. Analyses are based on the assumption that the traditional catch-effort model characterizes the relationship between catch and effort:

(1) $C_{it} = \beta_i$ Effort_{it}

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where C is catch per tow, effort is time per tow measured in minutes, i is the ith mesh size, and β is the coefficient to be estimated.

Model (1) is estimated for each combination of mesh size by seemingly unrelated regression or Zellner estimation. The relative efficiency is examined by imposing the restriction that β for one mesh size equals β for another mesh size; a likelihood ratio test is used to test for statistical differences. If the two estimated β coefficients are equal, there is no statistical difference in catch between the various gear combinations for a given level of effort.

The statistical results of the tests for differences between mesh size are presented in table 3. The first test was a test to determine if the 5-inch body, 4.5-inch codend mesh towed on one side of the vessel had the same effect on catch as the same mesh towed on the other side of the vessel. This was used as a 'ground truth' comparative test.

As indicated in table 3, catch for a given level of effort by the 5-inch body, 4.5-inch codend mesh towed on one side of the vessel was not statistically different than catch obtained by the same mesh towed on the other side of the vessel. However, there were substantial differences in between the catch and effort relationships for the other three mesh combinations.

A limited number of observations prevented testing the equality between the efficiency of a 4-inch body,

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| TABLE | 3 |
|-------|---|
|-------|---|

Results for equality tests of coefficients

| Structur | e testede | Chi-sguared ^b | Critical-value |
|------------------------------|---------------|--------------------------|----------------|
| (βι | = βj) | | 1-percent |
| 5 inch body, | 4.5 inch code | nd 4.88 | 6.64 |
| 5 inch body, | 4.5 inch code | nd | |
| 4 inch body, | 4.5 inch code | nd 12.77° | 6.64 |
| 5 inch body, | 4.5 inch code | nd | |
| 4 inch body, | 4.5 inch code | nd 13.97° | 6.64 |
| 5 inch body, | 5.0 inch code | nd | |
| calico trawl 4 inch body, | 4.5 inch code | 15.18° nd | 6.64 |

"Null hypothesis is that $\beta_1 = \beta_2$ or that the effort coefficient is equal for the two catch-effort equations.

bChi-squared is for one degree of freedom.

•Effort coefficients between pair of mesh sizes examined were statistically different.

`

4.5-inch codend vs. a 5-inch top panel, 4-inch bottom panel, and a 4 1/2-inch codend (tows 32 and 33). However, a regression of catch on effort of the two yielded coefficients of .194 and .1984, respectively. The correlation between catches for the two mesh sizes was .98; thus, indicating little difference between the two mesh combinations.

Additional tests were performed on the equivalency of the relationship between catch and effort with one mesh held constant and towed in conjuction with different mesh sizes. The 4-inch body, 4.5-inch codend towed with a 5-inch body, 4.5-inch codend was compared to the 4-inch body, 4.5-inch codend towed with a 5-inch body, 5-inch codend. Similarly, the 5-inch body, 4.5-inch codend was tested against the 4-inch body, 4.5-inch codend. Standard F-tests failed to reject any differences. The 4-inch body, 4.5-inch codend harvested the same regardless of the other two meshes towed; the same results were found for the 5-inch body, 4.5-inch codend mesh.

Table 4 presents the estimated coefficients of the catch-effort equations for the different mesh sizes (i.e., final form estimates). As indicated by the coefficient estimates, the 4-inch body with a 4.5-inch codend is considerably more efficient than the other mesh sizes. That is, a unit effort with this mesh yields a larger catch response than any other mesh size.

Relative harvesting efficiency was examined in terms of the technical relationship between catch and effort.

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|] | Mesh combination examined/tested | | | combination Coefficient ^a mined/tested (β _i) | | | |
|---|-------------------------------------|-------|-----|--|--------|--------|-------|
| | | | | | | | |
| 5 | inch | body. | 4.5 | inch | codend | .018 | 3.06 |
| 5 | inch | body, | 4.5 | inch | codend | i .018 | 3.06 |
| 4 | inch | body, | 4.5 | inch | codend | I.228 | 5.59 |
| 5 | inch | body, | 4.5 | inch | codend | . 103 | 4.97 |
| 4 | inch | body, | 4.5 | inch | cođend | 1.192 | 6.90 |
| 5 | inch | body, | 5.0 | inch | codend | . 090 | 6.16 |
| C | alico | trawl | | | | .027 | 6.65 |
| 4 | inch | body, | 4.5 | inch | codend | 1.181 | 24.55 |

Estimated coefficients of catch-effort equations

TABLE 4

^aFinal form coefficient estimates reflect results of statistical tests of the equality of coefficients (See Table 3 for explanation of structures tested).

bAll parameters were statistically different than zero $(p \le 0.05)$.

The estimated β coefficients in Table 4 are indicative of the relative efficiency of the various meshes (e.g., the coefficient for the calico trawl is .027 and that for the 4-inch body, 4 1/2 codend is .181; thus, the standard 4-inch body, 4 1/2-inch codend is more than six times as efficient as the calico trawl (.181/.027)). Overall, the 4-inch body, 4.5-inch codend was considerably more efficient in terms of total catch for given levels of effort. Harvest levels for the 4-inch body, 4.5-inch codend were approximately double the harvest levels of the 5-inch body, 4.5-inch codend and 5-inch body, 5-inch codend.

In conclusion, the 4-inch body, 4.5-inch codend mesh was considerably more efficient than the other mesh size combinations. Furthermore, of the mesh sizes tested, the 4-inch body, 4.5 inch codend yielded equivalent results regardless of the other gear with which it was towed.

Size selection

A primary purpose of the study was to examine whether or not an increase in the mesh size would result in reduced catches of small scallops. Additional purposes were to determine (1) if changes in mesh would result in escapement of smaller scallops with no appreciable change in the catch of larger scallops, and (2) size selectivity. Several methods were used to estimate size selection curves for the 3" rings on the dredge and the various mesh sizes.

Using the alternate haul method of Serchuk and

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Smolowitz (1980), the calculated the mean (50%) size selection was 75 to 85 mm for the dredge. The 25 to 75% range was between 70 and 90 mm. However, the estimated size selection was found to be extremely sensitive to the method used to calculate an adjustment factor. The closely similar mesh method of Davis (1934) and Beverton and Holt(1957) failed to yield adequate estimates of size selectivity for the various mesh sizes.

Although the various methods yielded conflicting results, they all appeared to suggest approximately 100% retention of scallops larger than 95 mm. (3.7-inches) for the 3" rings. The Beverton and Holt method indicated 100% retention of scallops between 115 (4.5-inches) and 120 mm. (4.7-inches) for the 5" body-4.5" codend and 4" body-4.5" codend. However, the estimated retention factors for the mesh combination appeared to be very unstable.

Additional problems prevented accurate estimation of size selection curves. First, grouping of the data into 5 mm intervals posed a problem of heteroscedasticity and masked the size selection. Second, retention rates of 0 and 100% resulted in double censored values; a two-limit probit or two-limit tobit model is necessary to estimate size selection. This approach was used to estimate size selection without correcting for heteroscedasticity, but the results appeared to be inadequate. Moreover, Beverton and Holt (1957) have demonstrated that estimates of size selectivity using the alternate haul method applied to data

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obtained from closely similar meshes are incorrect. Simply, they do not yield accurate and unbiased estimates of true retention.

It was concluded that while estimates of relative size selectivity were possible, these estimates would not be meaningful or useful for assessing size selectivity. As a result of the various problems, the analysis of size selection was restricted to analyzing the corresponding length-frequency and cumulative distribution information. The analyses, however, were primarily in terms of graphical interpretation. These are subsequently described with respect to the grouped net tows and matched dredge tows.

Tows 1-5 (5" body-4.5" codend: -identical nets)

As previously indicated, the purpose of tows 1-5 was to examine possible port-starboard differences. The nets were identical in configuration and mesh sizes, but one of the net was new. Harvesting efficiency appeared to be nearly equal (Table 4). The size distributions, though, displayed minor differences (Figure 2). The starboard net had more scallops in the 85-90 mm and 50-55 mm size ranges. Since these were the first 5 tows, during which time the scientific and commercial fishing crew were becoming familiar with operations, the length frequency data may be subject to measurement error. Catch and tow data for tows 1-5 are presented in Appendix I. There were no matched tows by the scallop dredge vessel.

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FIGURE 2

5-NCH BODY, 45-NCH CODEND

SHELL HEIGHT (MM)

PERCENTAGE OF SCALLOPS

Tows 6-12 (5" body-4.5" codend vs. 4" body-4.5" codend)

Tows 6-12 were conducted to examine whether or not an increase in the size of the mesh of the body would reduce catch and allow greater escapement of smaller scallops. Corresponding matched tows by the dredge vessel were 61-65. The number of scallops per 5 mm size interval are presented in Table 5; the catch per tow information is presented in Appendix 1.

As indicated by the numbers of scallops by size in Table 5, there does not appear to be any size selection for scallops less than 80 mm in size. This is further illustrated in Figure 3; comparisons of size distributions for individual tows appear in Appendix II. Minor size selection may occur between 80 and 90 mm; the 4° body-4.5° codend had proportionately more scallops between 80 and 90 mm (51.7 vs. 46.6%). Beyond 90 mm, the 5° body-4.5° codend harvested proportionately more scallops.

In comparison, the dredges with 3" and 2" rings indicated considerable differences in size selectivity. As expected, the 2" ring had proportionately more small scallops. If the size distribution of the 2" ring is indicative of the size distribution of the resource available, the 3" ring and the two meshes allow considerable escapement of smaller scallops.

A comparison of the size distribution and mean catch per hour of the four gear combinations indicates that the 4"

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TABLE 5

| | | Hesh S | Bizes | | Ring Sizes | | | | |
|-----------------|------------|--------|--------|------------|------------|--------|--------|--------|--|
| Shell Height | 4/4.5 inch | | 5/4.5 | 5/4.5 inch | | 3 inch | | 2 inch | |
| | Number | \$ | Number | \$ | Number | \$ | Number | ł | |
| 20~25 | 0 | | 0 | | 0 | | 0 | | |
| 25-30 | 0 | | 0 | | 0 | | Ø | | |
| 30-35 | 0 | | 0 | | 0 | | 3 | . 14 | |
| 35-40 | 1 | . 02 | 0 | | 0 | | 16 | . 74 | |
| 40-45 | 9 | . 18 | 9 | .19 | 0 | | 58 | 2.67 | |
| 45-50 | 29 | . 58 | 26 | . 55 | 5 | . 28 | 123 | 5.66 | |
| 50-55 | 63 | 1.26 | 52 | 1.10 | 23 | 1.28 | 165 | 7.59 | |
| 55-60 | 101 | 2.03 | 116 | 2.45 | 21 | 1.17 | 153 | 7.04 | |
| 60-65 | 73 | 1.47 | 123 | 2.59 | 19 | 1.06 | 172 | 7.91 | |
| 65-70 | 92 | 1.85 | 81 | 1.71 | 31 | 1.72 | 105 | 4.83 | |
| 70-75 | 281 | 5.64 | 228 | 4.81 | 24 | 1.33 | 217 | 9.98 | |
| 75-80 | 701 | 14.07 | 605 | 12.76 | 114 | 6.34 | 285 | 13.11 | |
| 80-85 | 1406 | 28.22 | 1099 | 23.19 | 347 | 19.29 | 323 | 14.86 | |
| 85-90 | 1170 | 23.48 | 1110 | 23.42 | 409 | 22.73 | 258 | 11.87 | |
| 90-95 | 595 | 11.94 | 663 | 13.99 | 305 | 16.95 | 150 | 6.90 | |
| 95-100 | 278 | 5.58 | 348 | 7.34 | 210 | 11.67 | 82 | 3.77 | |
| 100-105 | 129 | 2.59 | 215 | 4.54 | 180 | 10.01 | 46 | 2.12 | |
| 105-110 | 43 | .86 | 58 | 1.22 | 69 | 3.84 | 13 | . 60 | |
| 110-115 | 9 | .18 | 5 | 1.10 | 31 | 1.72 | 4 | .18 | |
| 115-120 | 1 | .02 | 2 | . 04 | 10 | . 56 | 1 | . 05 | |
| 120-125 | 0 | | 0 | | 1 | .06 | 0 | | |
| 125-130 | 1 | .02 | 0 | | ` Ø | | 0 | | |
| 130-135 | 0 | | 0 | | 0 | | 0 | | |
| 135-140 | 0 | | 0 | | 0 | | 0 | | |
| 140-145 | 0 | | 0 | | 0 | | 0 | | |
| 145-150 | 0 | | 0 | | 0 | | 0 | | |
| 150-155 | 0 | | 0 | | 0 | | 0 | | |
| 155-160 | 0 | | 0 | | 0 | | 0 | | |
| Total | 4982 | | 4740 | | 1799 | | 2174 | | |

Length-frequency distribution of sea scallops captured by tow two different mesh combinations (tows 6-12) and ring diameters (tows 61-65)



CHELL HEIGHT (MM)

SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS MESH SIZES

FIGURE 3

PERCENTAGE OF SCALLOPS

body-4.5" codend harvested more scallops between 80 and 85 mm (Figure 4). At the 85-90 mm range, all gear except the 2" ring harvested nearly equal proportions of sea scallops. Beyond 90 mm, the dredge with the 3" rings harvested proportionately more large scallops. The relative efficiency of the 4" body-4.5" codend, however, may result in higher total catches of scallops larger than 90 mm.

Scallops of 70 mm in size are considered to be recruited into the commercial dredge fishery which shucks scallops. Scallops smaller than 70 mm (approximately 2.75 inches) are typically not shucked. In comparison, 90 mm scallops represent the recruitment size in the shell-stock fishery; the regulation restrictions shell stock to a minimum shell size of 3.5 inches (88.9 mm). Scallops less than 70 mm accounted for approximately 7.4, 8.6, and 5.5% of the total catch by the 4" body-4.5" codend, 5" body-4.5" codend, and the dredge with the 3" rings (Figure 5). In comparison, scallops less than or equal to 90 mm accounted for 78.8. 72.8, and 55.2% of the respective gear harvests. Alternatively, nearly 45% of the scallops caught by the dredge using a 3" ring were greater than 90 mm; 21 to 27% of the scallops caught, respectively, by the 4" body-4.5" codend and 5" body-4.5" codend were greater than 90 mm.

Information on the cumulative size distribution and mean catch per hour fishing indicates that although the 4" body-4.5" codend had a higher total mean catch per hour, it had a lower catch per hour of scallops > 90 mm than did the

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FIGURE 4

SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS GEAR





6 THROUGH #2 = TRAML NET 61 THROUGH 65 = DREDGE

DEMCENTAGE OF SCALLOPS

FIGURE 5

SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS GEAR





6 THROUGH I2 = TRAM. NET 61 THROUGH 65 = DREDGE

COMOUNTE PERCENTAGE

dredge using the 3" rings (Table 6). Equivalent catches per hour between the 4" body-4.5" codend and the 3" ring appear to occur for a cull size range of 80-85 mm. It is important to realize, however, these comparisons may be biased because size distribution does not equate to volume (i.e., number of baskets).

Tows 13-24 (4" body-4.5" codend vs. 5" body-5" codend)

Tows 13-24 were made to obtain information about changes in catch and size distribution with a larger body Specifically, these twos were made to mesh and codend. obtain information for the purpose of testing the standard shell-stocking net with a 4" body and 4.5" codend against a 5" body and 5" codend. Twelve tows were completed; length and frequency data were obtained for 7 tows (13,15,16,17,18,19, and 24). Total catch ranged from 8.3 to 61 baskets per tow (Appendix I). Length frequency data are summarized in Table 7 and depicted in Figures 6-7. Corresponding matched tows by the dredge vessel were 84-88 (Table 7 and Figure 7). Percent length-frequency data per tow are depicted in Appendix II.

In comparison to tows (6-12), relative size selectivity was more pronounced for the 4" body-4.5" codend evaluated against the 5" body-5.0" codend. The smaller mesh took considerably more scallops between 20 and 80 mm. Horeover, the size distribution from tows 13-24 for the 4" body-4.5" codend was comparable to the distribution for tows 6-12.

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TABLE 6

| Gear | Mean catch | Estimated mean baskets per hour for cull sizes | | | | |
|---------------------|------------|--|--------|--------|--------------|--|
| | per hour | : Sel : : 70mm | ected | cull s | izes 90mm | |
| A" body_A 5" godood | | Baskets | per ho | ur | | |
| 4" Dody-4.5" codena | 10.49 | 9.71 | 7.65 | 4.69 | 2.22 | |
| 5" body-4.5" codend | 4.19 | 3.83 | 3.09 | 2.12 | 1.14 | |

Comparison of mean catch per hour by selected cull sizes (tows 6-12 and 61-65)

.

| | | Me s h : | Sizes | | | Ring | Sizes | |
|-----------------|------------|-----------------|----------|-------|------------|-------|--------|-------|
| Shell Height | 4/4.5 inch | | 5/5 inch | | 3 inch | | 2 inch | |
| | Numbe | r % | Numbe | er % | Numbe | r t | Numbe | er % |
| 20-25 | 1 | . 02 | 0 | | 0 | | 1 | .05 |
| 25-30 | 3 | . 05 | 0 | | 1 | .06 | 2 | . 10 |
| 30-35 | 3 | .05 | 0 | | 0 | | 13 | . 66 |
| 35- 40 | 1 | . 02 | 0 | | 1 | .06 | 37 | 1.89 |
| 40-45 | 5 | . 09 | 0 | | 2 | .11 | 103 | 5.26 |
| 45-50 | 8 | . 14 | 2 | . 04 | 11 | .62 | 173 | 8.84 |
| 50-55 | 45 | . 77 | 8 | .15 | 17 | .95 | 236 | 12.05 |
| 55-60 | 96 | 1.63 | 21 | . 40 | 13 | .73 | 217 | 11.08 |
| 60-65 | 151 | 2.57 | 56 | 1.07 | 29 | 1.62 | 177 | 9.04 |
| 65-70 | 102 | 1.74 | 56 | 1.07 | 21 | 1.18 | 84 | 4.29 |
| 70-75 | 307 | 5.23 | 194 | 3.70 | 42 | 2.35 | 117 | 5.98 |
| 7 5-80 | 850 | 14.47 | 690 | 13.15 | 112 | 6.27 | 164 | 8.38 |
| 80-85 | 1779 | 30.28 | 1794 | 34.18 | 301 | 16.86 | 188 | 9.60 |
| 85-90 | 1492 | 24.40 | 1456 | 27.74 | 391 | 21.90 | 185 | 9.45 |
| 90-95 | 566 | 9.63 | 508 | 9.68 | 355 | 19.89 | 136 | 6.95 |
| 95-100 | 211 | 3.59 | 222 | 4.23 | 227 | 12.72 | 55 | 2.81 |
| 100-105 | 133 | 2.26 | 152 | 2.90 | 129 | 7.23 | 29 | 1.48 |
| 105-110 | 75 | 1.28 | 61 | 1.16 | 81 | 4.54 | 26 | 1.33 |
| 110-115 | 26 | . 44 | 8 | .15 | 37 | 2.07 | 10 | . 51 |
| 115-120 | 12 | . 20 | 10 | . 19 | 12 | .67 | 5 | .26 |
| 120-125 | 4 | .07 | 2 | . 04 | 2 | . 11 | 0 | |
| 125-130 | 1 | .02 | 3 | .06 | ` 1 | .06 | 0 | |
| 130-135 | 0 | | 2 | .04 | 0 | | 0 | |
| 135-140 | 2 | .03 | 1 | .02 | 0 | | 0 | |
| 140-145 | 2 | .03 | 0 | | 0 | | 0 | |
| 145-150 | 0 | | 1 | .02 | 0 | | 0 | |
| 150-155 | 0 | | 1 | .02 | 0 | | 0 | |
| 155-160 | 0 | | 0 | | 0 | | 0 | |
| Total | 5875 | | 5248 | | 1785 | | 1958 | |

Length-frequency distribution of sea scallops captured by tow two different mesh combinations (tows 13-24) and ring diameters (tows 84-88)

TABLE 7


SHELL HEIGHT (MM)

SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS MESH SIZES

FIGURE 6

DEBCENTAGE OF SCALLOPS



FIGURE 7

13 THROUGH 24 - TRAM. NET 64 THROUGH 36 - DNEDGE

DEMCENTAGE OF SCALLOPS

Relative size selectivity between the two nets appeared to be complete at 80 mm. Beyond 80 mm, the 5" body-5" codend caught proportionately more scallops than did the 4" body-4.5" codend. Relative size selection between the 3" and 2" rings also appeared to be complete by 80 mm. The 3" ring caught proportionately more scallops larger than 80 mm than did the 2" ring; the 3" ring also caught proportionately more scallops larger than 90 mm than did all the other gear combinations.

A comparison of the average number of baskets per hour indicates that the 4" body-4.5" codend was the most technically efficient gear in terms of baskets per hour (Table 8). However, the dredge using 3" rings was more efficient for cull sizes greater than 80 mm. The 5" body-5" codend was half as efficient as the 4" body-4.5" codend for scallops greater than 90 mm. Figure 8 indicates that the two meshes harvested nearly equal proportions of scallops smaller than 85 mm and scallops greater than 85 mm; however, the smaller mesh harvested more than double the number of scallops smaller or larger than 85 mm.

Tows 25-31 (4" body-4.5" codend vs. 3" body-3" codend)

Tow 25-31 were made to obtain information on catch and size selectivity for a calico trawl (3" body-3" codend) relative to the typical trawl (4" body-4.5" codend) used by shell-stockers or net vessels. Seven tows were made, but excessive clogging of the calico trawl with mud, sand, and

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| Gear | Mean catch | Average number o: | f | Cu | ll siz | ê B |
|----------------------------|---------------------|----------------------|--------------|------|--------|------|
| | por nour | per basket | 70 | 80 | 85 | 90 |
| t" body- | | | | | | |
| 4.5" codend | 10.16 | 420 | | | | |
| Size distri Number of s | bution-% callops | | 92 .9 | 73.2 | 43.0 | 17. |
| per basket Number of s | callons | | 390 | 307 | 181 | 74 |
| per hour | 0411050 | | 3962 | 3119 | 1839 | 752 |
| 5* body- | | | | | | |
| 5" cođend | 5.24 | 375 | | | | |
| Size distri Number of s | bution-% callops | | 97.3 | 80.4 | 46.2 | 18. |
| per basket Number of s | callons | | 365 | 302 | 173 | 69 |
| per hour | CUITOPD | | 191 3 | 1582 | 907 | 362 |
| 3" ring | 9.63 | 357 | | | | |
| Size distri Number of s | bution-% callops | | 94.7 | 86.1 | 69.2 | 47. |
| per basket Number of s | callops | | 338 | 307 | 247 | 169 |
| per hour | | | 3255 | 2956 | 2379 | 1627 |
| " ring | 2.55 | 435 | | | | |
| Size distri | bution-% | | 46.7 | 32.4 | 22.8 | 13. |
| per basket | Cattobe | | 103 | 141 | 99 | 58 |
| Number of s | callops | | | | | |

Catch and distribution at various cull sizes by selected gear (tows 13-24 and 84-88)

TABLE 8



SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS GEAR





CUMULATIVE PERCENTABE

other debris permitted only three successful tows; matching dredge tows were 106-110. Shorter tow times failed to alleviate the clogging problem. Catch data are presented in Appendix I. Length frequency data are presented in Table 9 and depicted in Figure 9.

Size selectivity for the 4" body-4.5" codend and the calico trawl appeared to be complete by the 80-85 mm size range. As would be expected, the smaller mesh calico trawl harvested proportionately more small scallops (Figure 10). Scallops less than 85 mm accounted for 75.8% of the calico catch and 58.6% of the 4" body-4.5" codend catch. In terms of relative harvesting efficiency, the 4" body-4.5" codend was approximately 8.2 times as efficient as the calico trawl (10.95 vs. 1.33 baskets per hour of fishing).

In comparison, size selectivity for the 3" ring appeared to be complete for scallops between 80 and 90 mm. Scallops smaller than 85 mm accounted for only 29.5% of the 3" ring catch (Figure 10). The same size scallops (< 85 mm) accounted for 47.7% of the 2" ring catch. Interestingly, the calico trawl harvested a larger proportion of small scallops than did the 2" ring dredge with a liner.

A comparison of the relative technical efficiency indicates that the 3" ring used by the dredge vessel was the most technically efficient in terms of baskets per hour (13.23 baskets per hour). The 3" ring was also the most technically efficient gear for various cull sizes (Table 10). Scallops larger than 90 mm accounted for 13 and 41.2% of the

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| | | Mesh : | Sizes | | | Ring 1 | Sizes | |
|-----------------|--------|--------|--------|-------|--------|--------|--------------|-------|
| Shell Height | 4/4.5 | inch | Calico | 0 | 3 : | lnch | 2 i 1 | nch |
| | Number | | Numbei | r 1 | Number | r ¥ | Number | r % |
| 15-20 | 0 | | 2 | .13 | 0 | | Ø | |
| 20-25 | 0 | | 34 | 2.20 | 0 | | 2 | . 11 |
| 25-30 | 0 | | 84 | 5.46 | 1 | .05 | 1 | .05 |
| 30-35 | 0 | | 28 | 1.82 | 0 | | 3 | .16 |
| 35-40 | 0 | | 11 | .71 | 1 | .05 | 1 | .05 |
| 40-45 | 0 | | 15 | . 97 | 0 | | 1 | .05 |
| 45-50 | 0 | | 23 | 1.49 | 0 | | 5 | . 26 |
| 50-55 | 0 | | 58 | 3.77 | 2 | . 11 | 19 | . 98 |
| 55-60 | 7 | . 60 | 103 | 6.69 | 2 | . 11 | 29 | 1.50 |
| 60-65 | 14 | 1.20 | 79 | 5.13 | 6 | .33 | 62 | 3.21 |
| 65-70 | 13 | 1.12 | 23 | 1.49 | 2 | . 11 | 31 | 1.60 |
| 70-75 | 41 | 3.52 | 73 | 4.74 | 14 | .77 | 51 | 2.64 |
| 75-8 0 | 172 | 14.78 | 202 | 13.13 | 126 | 6.92 | 186 | 9.62 |
| 80-85 | 435 | 37.37 | 431 | 28.00 | 383 | 21.04 | 531 | 27.47 |
| 85-90 | 331 | 28.44 | 265 | 17.22 | 533 | 29.29 | 575 | 29.75 |
| 90-95 | 86 | 7.39 | 63 | 4.09 | 292 | 16.04 | 254 | 13.14 |
| 95-100 | 34 | 2.92 | 14 | .91 | 92 | 5.05 | 54 | 2.79 |
| 100-105 | 15 | 1.29 | 15 | . 97 | 93 | 5.11 | 45 | 2.33 |
| 105-110 | 8 | .69 | 10 | .65 | 102 | 5.60 | 42 | 2.17 |
| 110-115 | 2 | .17 | 0 | | 52 | 2.86 | 18 | . 93 |
| 115-120 | 3 | .26 | 3 | .19 | 73 | 4.01 | 8 | . 41 |
| 120-125 | 2 | .17 | 0 | | 37 | 2.03 | 8 | .41 |
| 125-130 | 0 | | 2 | .13 | 4 | . 22 | 2 | . 11 |
| 130-135 | 0 | | 0 | | 2 | .11 | 4 | . 21 |
| 135-140 | 1 | | 0 | | 2 | .11 | 1 | .05 |
| 140-145 | 0 | | 0 | | 0 | | 0 | |
| 145-150 | 0 | | 1 | .06 | 0 | | 0 | |
| 150-155 | 0 | | 0 | .02 | 0 | | 0 | |
| 155-160 | 0 | | 0 | | 1 | .05 | 0 | |
| Total | 1164 | | 1539 | | 1820 | | 1933 | |

Length-frequency distribution of sea scallops captured by tow two different mesh combinations (tows 25-31) and ring diameters (tows 106-110)

TABLE 9

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SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS GEAR

FIGURE 9

29 THROUGH SI - CALCO NET 106 THROUGH TIO - EMEDBE

SHELL HEGHT (M

PERCENTAGE OF SCALLOPS



29 THROUGH 31 = CALICO NET 106 THROUGH TID = DREDGE

CONTRACTIVE PERCENTAGE

FIGURE 10

| 600 P | Mean catch | Average number of | <u>ـــــ</u> | Cu | ll size | 6 6 |
|------------------------------|---------------------|---------------------------|--------------|------|---------|------------|
| Gear | per nour | scallops per basket | 70 | 80 | 85 | 90 |
| 4" body- | 10.05 | | | | | |
| 4.5" codend | 10.95 | 388 | | | | |
| Size distrib Number of so | bution-% callops | | 97.1 | 79.4 | 41.4 | 13.0 |
| per basket | | | 377 | 308 | 167 | 50 |
| per hour | Callops | | 4128 | 3373 | 1763 | 548 |
| 3" calico | | | | | | |
| | 1.33 | 661 | | | | |
| Size distrib | bution-% | | 70.1 | 52.2 | 24.2 | 7.0 |
| per basket | | | 463 | 345 | 160 | 46 |
| number of so per hour | callops | | 616 | 459 | 213 | 61 |
| 3" ring | 13.23 | 364 | | | | |
| Size distrib Number of so | oution-% callops | | 99.2 | 91.5 | 70.5 | 41.2 |
| per basket Number of so | | | 361 | 333 | 257 | 150 |
| per hour | | | 4776 | 4406 | 3400 | 1985 |
| 2" ring | 3.95 | 407 | | | | |
| (With liner) Size distrib |) pution-% | | 92.0 | 79.8 | 52.3 | 22.6 |
| per basket | allong | | 374 | 325 | 213 | 92 |
| per hour | attobs | | 1477 | 1284 | 841 | 363 |

TABLE 10 Catch and distribution at various cull sizes

by selected gear (tows 29-31 and 106-110)

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total catch by the 4" body-4.5" codend and 3" ring dredge; 93% of the scallops by the calico trawl were less than 90 mm.

Tows 32-33 (4" top panel, 4" bottom panel, 4.5" codend vs. 5" top panel, 4" bottom panel, 4.5" codend).

Tows 32-33 were made to determine whether or not size selection and technical efficiency would vary depending on the size of the top panel. For these two tows, only the size of the top panel was different. No matching tows by the dredge vessel were made. The number of baskets per tow displayed little variation between sides or over tows (23-25 baskets per tow) (Appendix I). Baskets per hour were nearly equal. The length frequency data are summarized in Table 11 and depicted in Figure 11.

As indicated in Table 11 and Figure 11, size selectivity was approximately the same for both gear configurations. Scallops between 75 and 90 mm accounted for nearly equal proportions of the total catches by the two gear configurations (75.2 vs. 75.6% for the 4" bottom and 5" bottom, respectively). A comparison of the cumulative percentage of the total catch by the two configurations also indicates nearly identical proportions (Figure 12). Scallops larger than 90 mm accounted for 12.8 and 11.8% of the total catch by the 4" top panel, 4" bottom panel, 4.5" codend and 5" top panel, 4" bottom panel, 4.5" codend gear configurations, respectively.

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| | Hesh Sizes | |
|-----------------|--------------|----------------------|
| Shell Height | 4/4/4.5 inch | 5/4/4.5 inch |
| <u></u> | Number % | Number % |
| 20-25 | 0 | 1.06 |
| 25-30 | 2.14 | 2.12 |
| 30-35 | 0 | 0 |
| 35-40 | 0 | 0 |
| 40-45 | 0 | 2.12 |
| 45-50 | 1.07 | 6.36 |
| 50-55 | 17 1.15 | 21 1.26 |
| 55-60 | 30 2.03 | 40 2.40 |
| 60-65 | 37 2.51 | 51 3.06 |
| 65-70 | 22 1.49 | 27 1.62 |
| 70-75 | 68 4.61 | [~] 60 3.60 |
| 75-80 | 249 16.88 | 294 17.65 |
| 80-85 | 472 32.00 | 556 33.37 |
| 85-90 | 388 26.31 | 409 24.55 |
| 90-95 | 90 6.10 | 114 6.84 |
| 95-100 | 36 2.44 | 34 2.04 |
| 100-105 | 30 2.03 | 27 1.62 |
| 105-110 | 13 .88 | 12 .72 |
| 110-115 | 6.41 | 5.30 |
| 115-120 | 5.34 | 1.06 |
| 120-125 | 1.07 | 1.06 |
| 125-130 | 4.27 | 0 |
| 130-135 | 1.07 | 1 .06 |
| 135-1 40 | 2.14 | 1.06 |
| 140-145 | 1.07 | 0 |
| 145-150 | 0 | 0 |
| 150-155 | 0 | 1.06 |
| 155-160 | 0 | 0 |
| Total | 1475 | 1666 |

Length-frequency distribution of sea scallops captured by tow two different mesh combinations (tows 32-33)

TABLE 11



LENCENTAGE OF SCALLOPS

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SIZE DISTRIBUTION OF SEA SCALLOPS CAPTURED BY VARIOUS GEAR



CUMULATIVE PERCENTAGE

CONCLUSIONS

A major objective of the study was to examine size selectivity. The purpose of examining size selectivity was to determine the feasibility of imposing mesh regulations on trawlers to reduce mortality of small scallops. If larger meshes or other changes in the gear reduce the harvest of small scallops without affecting the harvest of large scallops, gear restrictions would likely be feasible and acceptable to industry.

Although size selection curves could be estimated with the available data, they were not used to examine size selection. This was because estimates were for relative size selectivity between two similar mesh sizes and statistically blased. Thus, the accuracy and usefulness of the estimates to assess size selectivity are questionable. Instead, size selectivity was inferred via other data analyses.

Analyses of the data indicated that larger meshes resulted in reduced catches of smaller scallops. Larger meshes generally caused reduced catches of all scallops. The major effect of increasing mesh size appeared to be on harvesting efficiency rather than on size selection (Table 12). For example, scallops smaller than 90 mm accounted for approximately 81.5% of the total catch by both the 4" body-4.5" codend and 5" body-4.5" codend for tows 13-24. However, the harvest rate of the 4" body-4.5" codend was approximately double the rate of the 5" body-5" codend. The

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| Tows/ Gear | Baskets per hour | | Selec | ted shell | . size ra | anges |
|---------------|---------------------|---|-------|-----------|-----------|-------|
| configuration | | | < 75 | 75-95 | > 90 | > 95 |
| | | | P | ercent of | sample- | |
| 6-12 | | | | | | |
| 4/4.5 | 10.49 | | 13.03 | 77.10 | 21.81 | 9.87 |
| 5/4.5 | 4.19 | | 13.40 | 73.36 | 27.23 | 13.24 |
| 3" ring | 8.00 | | 6.84 | 65.31 | 44.80 | 27.85 |
| 2" ring | 3.00 | | 46.56 | 46.74 | 13.60 | 6.70 |
| 3-24 | | | | | | |
| 4/4.5 | 10.16 | * | 12.31 | 78.78 | 18.54 | 8,91 |
| 5/5.0 | 5.24 | | 6.43 | 84.75 | 18.50 | 8.82 |
| 3" ring | 9.63 | | 7.68 | 64.92 | 47.29 | 27.40 |
| 2° ring | 2.55 | | 59.24 | 34.38 | 13.33 | 6.38 |
| 29-31 | | | | | | |
| 4/4.5 | 10.95 | | 6.44 | 87.98 | 12.97 | 5.58 |
| Calico | 1.33 | | 34.60 | 62.45 | 7.04 | 2.95 |
| 3" ring | 13.23 | | 1.53 | 73.29 | 41.22 | 25.18 |
| 2" ring | 3.95 | | 10.60 | 79.98 | 22.56 | 9.42 |

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TABLE 12

smaller mesh did harvest proportionately more small (< 75 mm) scallops.

It is important to realize that all results presented in this study reflect specific resource conditions. In terms of numbers of scallops available for harvest, the resource appeared to be dominated by scallops between 75 and 95 mm (Table 12). Scallops larger than 95 mm appeared to account for a relatively small proportion of the resource available for harvest.

An analysis of equity between trawl vessels and dredge vessels was not an objective of this study, but available data permit a preliminary examination of the equity of the regulations. In terms of numbers of scallops and baskets per hour, the standard 4" body-4.5" codend, trawl generally had a relative advantage. However, the 3" ring generally harvested more scallops larger than 90 mm. These results suggest that minimum shell size restrictions on shell stock more adversely affect shell-stockers than would an equivalent minimum shell size on scallops which are shucked at sea. These conclusions, however, only apply to resource conditions prevailing during this particular experiment.

In conclusion, the major effect on catches of small scallops of increased mesh sizes appears to be a reduction in harvesting efficiency. Escapement of smaller scallops because of larger meshes appears to be minimal. However, larger meshes compared to the 3" calico trawl appear to suggest considerable escapement. In terms of implementing

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mesh restrictions, larger meshes do not appear to be feasible if industry support is a concern to management authorities. Increasing the mesh to a 5° body with a 4.5° codend or a 5° body with a 5° codend would reduce catch, given prevailing conditions during this experiment, by 40 and 52%, respectively. Alternatively, restricting the size of top body panel to 5° would not be feasible since there was no difference in catch between a 4° body with 4.5° codend and 4° bottom panel with a 5° top body panel and 4.5° codend. In essence, restrictions on the top panel would not appear to adequately control mortality. However, if management is only concerned with reducing the catch of smaller scallops, increasing the mesh size offers an alternative to accomplish this objective.

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APPENDIX I

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| DESCRILOPS TRASH | 00.8 | 00.8 03.5 | 00.8 03.2 | 00.8 04.8 | 04.0 00.5 | 03.5 02.3 | 05.8 00.8 | 05.5 02.5 | 04.4 01.1 | 04.1 03.0 | 07.0 06.7 | 02.1 06.0 | 16.0 05.5 | 05.5 06.0 | 14.0 05.5 | 05.2 05.0 | 10.2 07.1 | 03.5 05.0 | 09.8 05.6 | 03.5 04.0 | 15.5 09.7 | 07.7 07.5 | 63.0 12.5 | 30.0 | 41.0 07.0 | 20.0 10.0 | 21.0 | 26.0 | 23.0 13.0 | 11.0 08.2 | 10.0 09.0 | 03.3 04.0 |
|-------------------------|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|---------|-----------|-----------|---------|---------|-------------|-----------|-----------|-----------|
| MESH SIZE (") | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/4.5 | 4/4.5 | 5/5 | 4/4.5 | 5/5 | 4/4.5 | 5/5 | 4/4.5 | 5/5 |
| SHI P SIDE | р. | S | ቤ | S | 64 | S | ρ, | ŝ | <u>р</u> , | \$ | P4 | S | Ρ4 | S | ы | ŝ | Ē4 | S | ы | S | ይ | S | <u>с</u> , | S | ይ | S | ሲ | S | р ., | S | С, | ŝ |
| ENDING LORAN(Y) | 42418.0 | 42418.0 | 42412.9 | 42412.9 | 42381.0 | 42381.0 | 42389.8 | 42389.8 | 42412.8 | 42412.7 | 42980.4 | 42980.4 | 43021.4 | 43021.4 | 43049.5 | 43049.5 | 43071.6 | 43071.6 | 43071.4 | 43071.4 | 43048.3 | 43048.3 | 42988.2 | 42988.2 | 42998.2 | 42998.2 | 43001.4 | 43001.4 | 43052.6 | 43052.6 | 43084.8 | 43084.8 |
| STARTING LORAN(T) | 42411.3 | 42411.3 | 42419.5 | 42419.5 | 42408.5 | 42408.5 | 42379.5 | 42379.5 | 42382.1 | 42382.1 | 42963.2 | 42963.2 | 42984.6 | 42984.6 | 43023.9 | 43023.9' | 43053.0 | 43053.0 | 43079.6 | 43079.6 | 43077.2 | 43077.2 | 43043.0 | 43043.0 | 42985.3 | 42985.3 | 42988.1 | 42988.1 | 42986.6 | 42986.6 | 43059.9 | 43059.9 |
| ENDING LORAN (X) | 26746.5 | 26746.5 | 26764.1 | 26764.1 | 26778.5 | 26778.5 | 26783.3 | 26783.3 | 26776.5 | 26776.5 | 26520.6 | 26520.6 | 26499.4 | 26499.4 | 26476.0 | 26476.0 | 26454.6 | 26454.6 | 26449.7 | 26449.7 | 26473.2 | 26473.2 | 26498.2 | 26498.2 | 26499.9 | 26473.2 | 26500.2 | 26500.2 | 26498.2 | 26498.2 | 26448.8 | 26448.8 |
| STARTING LORAN(X) | 26745.2 | 26745.2 | 26745.1 | 26745.1 | 26775.1 | 26775.1 | 26779.9 | 26779.9 | 26793.2 | 26793.2 | 26488.8 | 26488.8 | 26502.8 | 26502.8 | 26495.8 | 26495.8 | 26473.9 | 26473.9 | 26445.4 | 26445.4 | 26449.7 | 26449.7 | 26484.0 | 26484.0 | 26497.7 | 26497.7 | 26502.3 | 26502.3 | 26500.5 | 26500.5 | 26467.6 | 26467.6 |
| TOW LENGTH (MIN.) | 064 | 064 | 065 | 065 | 063 | 063 | 079 | 079 | 124 | 124 | 068 | 068 | 083 | 083 | 076 | 076 | 066 | 066 | 086 | 086 | 120 | 120 | 182 | 182 | 141 | 141 | 154 | 154 | 160 | 160 | 073 | 073 |
| TIME | 1036 | 1036 | 1157 | 1157 | 1334 | 1334 | 1503 | 1503 | 1638 | 1638 | 0620 | 0620 | 0807 | 0807 | 1011 | 1011 | 1155 | 1155 | 1419 | 1419 | 1600 | 1600 | 2010 | 2010 | 2349 | 2349 | 0238 | 0238 | 0545 | 0545 | 0939 | 0939 |
| DATE | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/21 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/22 | 4/23 | 4/23 | 4/23 | 4/23 | 4/23 | 4/23 |
| MOT. | 1 | 1 | 7 | 7 | ന | ŝ | 4 | 4 | ŝ | ŝ | 9 | 9 | 7 | 7 | ω | 8 | σ | σ | 10 | 10 | 11 | 11 | 12 | 12 | 13 | 13 | 14 | 14 | 15 | 15 | 16 | 16 |

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| | | | TOW | STARTING | ENDING | STARTING | ENDING | SHT P | MESH | BASKETS | BASKETS |
|--|--|--|------------|----------|------------------|----------|----------|--------------|---------|----------------|-----------------|
| DATE TIME (MIN.) LORAN(X) | ME (MIN.) LORAN(X) | (MIN.) LORAN(X) | LORAN(X) | | LORAN(X) | LORAN(Y) | LORAN(Y) | SIDE | | OF SCALLOPS | OF TRASH |
| 4/23 1110 060 26444.8 | 10 060 26444.8 | 060 26444.8 | 26444.8 | | 26464.0 | 43087.2 | 43866.0 | <u>م</u> | | | |
| 4/23 1110 060 26444.8 | 10 060 26444.8 | 060 26444.8 | 26444.8 | | 26464.0 | 43087.2 | 43866.0 | - V3 |) - u/u | | |
| 4/23 1355 060 26491.4 | 55 060 26491.4 | 060 26491.4 | 26491.4 | •• | 26500.0 | 43051.0 | 43030.4 | . <u>р</u> . | 4/4.5 | 12.0 | 2 |
| 4/23 1355 060 26491.4 | 55 060 26491.4 | 060 26491.4 | 26491.4 | | 26500.0 | 43051.0 | 43030.4 | . 03 | 5/5 | 0.5.4 | |
| 4/23 1519 091 26499.6 | 19 091 26499.6 | 091 26499.6 | 26499.6 | | 26504.2 | 43023.2 | 43036.8 | <u>م</u> ا | 4/4.5 | 16.2 | 2. 2. |
| 4/23 1519 091 26499.6 | 19 091 26499.6 | 091 26499.6 | 26499.6 | | 26504.2 | 43023.2 | 43036.8 | 0 | 5/5 | 07.0 | |
| 4/23 1815 135 26504.6 | 15 135 26504.6 | 135 26504.6 | 26504.6 | •• | 26505.0 | 43035.3 | 43031.6 | <u>م</u> ו | 4/4.5 | | 0.00 |
| 4/23 1815 135 26504.6 2 | 15 135 26504.6 2 | 135 26504.6 2 | 26504.6 2 | | \$6505.0 | 43035.3 | 43031.6 | 1 62 | 5/5 | | |
| 4/23 2100 150 26500.0 2 | | 150 26500.0 2 | 26500.0 | • 4 | 26498.7 | 43027.6 | 43998.6 | р. | 4/4.5 | | |
| 4/23 2100 150 26500.0 2 | 00 150 26500.0 2 | 150 26500.0 2 | 26500.0 2 | N | 6498.7 | 43027.6 | 43998.6 | . 02 | 5/5 | | |
| 4/24 0050 220 26499.8 2 | 50 220 26499.8 2 | 220 26499.8 2 | 26499.8 2 | 2 | 1.6499.I | 43031.5 | 43191.9 | ի թե | 4/4.5 | 010 | |
| 4/24 0050 220 26499.8 2 | 50 220 26499.8 2 | 220 26499.8 2 | 26499.8 2 | 54 | 6499.1 | 43031.5 | 43191.9 | . 03 | 5/5 | | |
| 4/24 0405 155 26502.8 2 | 05 155 26502.8 2 | 155 26502.8 2 | 26502.8 2 | ~ | 6497.8 | 43000.8 | 43011.6 | і д . | 4/4 5 | | |
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| 4/24 0/12 146 26504.4 2 | 12 146 26504.4 2 | 146 26504.4 2 | 26504.4 2 | 3 | 6502.4 | 43019.1 | 43028.5 | і А ч | 5/5 | 09.5 | 0 70 |
| 4/24 U/12 146 26504.4 2 | | | 26504.4 | | 36502.4 | 43019.1 | 43028.5 | S | 4/4.5 | 21.0 | 08.0 |
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| 4/24 1327 010 26498.3 | 0/ 010 26498.3 | 010 26498.3 | 26498.3 | | 26498.9 | 43019.6 | 43009.3 | ሲ | CALICO | | |
| 1 24 122/ 0TO 20498.3 | 010 26498.3 | 010 26498.3 | Z0498.3 | | 26498.9 | 43019.6 | 43009.3 | ŝ | 4/4.5 | 02.0 | 01.0 |
| 1.24 IDDU U32 26494.8 | | 032 26494.8 | 26494.8 | | 26499.0 | 42024.9 | 43035.8 | 4 | CALICO | 00.3 | 01.5 |
| 1/24 1744 052 20494.8 | 14 007 20494.0 | 0075 20494.0 | 20434°0 | | 20499.0 | 42024.9 | 43035.8 | ŝ | 4/4.5 | 0.00 | 04.0 |
| 1,04 1744 069 204901/ | 1 06407 200 VI | 1 007 7 700 1 007 7 000 7 0000 7 000 7 000 7 000 7 000 7 000 7 000 7 000 7 000 7 000 | 1.04704 J | | 1017700 | 43036.4 | 43019.6 | ዋ | CALI CO | 02.0 | 02.5 |
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| */24 IYIU UGU 26498.] 2(| U UOU 26498.1 20 | 050 26498.1 20 | 26498.1 20 | 5 | 5500.7 | 43012.9 | 43016.9 | S | 4/4.5 | 10.0 | |
| +/ 23 1823 122 26501.4 2 | | 122 26501.4 2 | 26501.4 2 | 2 | 6499.3 | 42990.9 | 42997.7 | գ | 5/4/4.5 | 25.0 | 25.50 |
| +/ Z) 18Z5 122 26501.4 2 | 2 122 26501.4 2 | 122 26501.4 2 | 26501.4 2 | 2 | :6499.3 | 42990.9 | 42997.7 | ι W | 4/4.5 | 24.0 | |
| 1/25 2050 125 26497.8 2 | | 125 26497.8 2 | 26497.8 2 | 2 | 6500.3 | 42984.0 | 43000.5 | ዉ | 5/4/4.5 | 23.0 | |
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| ENDING LORAN(Y) | 43015.5 43015.5 43015.5 43015.5 43015.5 43020.1 43020.1 43020.1 43022.1 42022. | 41567.4 41567.4 | 41471.3 41471.3 |
| STARTING LORAN(Y) | 43009.6 43009.6 420990.9 42990.9 42002.5 43002.5 43002.5 43006.4 43006.4 43006.4 43006.4 42006.4 42395.1 42395.1 42395.1 42395.1 | 41597.8 41597.8 | 41504.2 41504.2 |
| ENDING Loran(X) | 26499.6 26499.6 26498.8 26498.8 26500.5 26500.5 26500.5 26498.8 26498.8 26498.8 26498.8 26498.8 26783.2 26783.2 26844.9 26844.9 | 26911.9 26911.9 | 26890.7 26890.7 |
| STARTING LORAN(X) | 26503.9 26503.9 26500.2 26500.2 26497.2 26496.7 26496.7 26496.7 26496.7 26496.7 26496.7 26501.2 26501.2 26501.2 26501.2 26576.8 26776.8 26843.2 26843.2 26843.2 | 26911.2 26911.2 | 26892.3 26892.3 |
| TOW LENGTH (MIN.) | 125 125 132 132 120 120 120 097 097 097 097 097 097 065 097 | 060 060 | 067 067 |
| TIME | 1120 1120 1405 1405 1655 1655 1655 1930 1930 1930 1930 1930 1930 1930 1930 | 0105 0105 | 0330 0330 |
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|---|---|------|---------------|-----------|-----------|-----------|-----------|--------|----------|---------|
| 0500 015 26455 26461 43069 43064 3-inch 1.50 8.00 0525 015 26445 33064 3-inch 1.50 6.00 0525 015 26445 43065 43065 43065 5-inch 1.50 6.00 0551 015 26472 26476 43065 43067 2-inch 1.50 6.00 0551 015 26472 26476 43055 2-inch 0.75 3.10 0551 016 2647 26470 43047 2-inch 0.75 3.10 0539 016 2647 26470 43048 43055 2-inch 0.75 3.13 0539 016 26467 26450 43055 2-inch 0.75 3.16 0534 016 26451 26455 43095 3-inch 0.75 2.81 0534 016 26454 26455 43095 3-inch 1.75 2.86 <td>ļ</td> <td>TIME</td> <td>(MIN.)</td> <td>LORAN (X)</td> <td>LORAN (X)</td> <td>LORAN (Y)</td> <td>LORAN (Y)</td> <td>*(u)</td> <td>SCALLOPS</td> <td>HOUR</td> | ļ | TIME | (MIN.) | LORAN (X) | LORAN (X) | LORAN (Y) | LORAN (Y) | *(u) | SCALLOPS | HOUR |
| 0500 015 26455 26461 43063 43057 2-inch 1.50 6.00 0552 015 26463 26469 43053 43057 2-inch 1.50 6.00 0551 015 26475 26476 43053 43057 2-inch 0.75 3100 0551 015 26472 26476 43054 43047 3-inch 1.50 6.00 0551 015 26474 23054 43047 3-inch 0.75 3100 0553 016 26476 43054 43047 3-inch 0.75 3100 0539 016 26477 23058 43055 3-inch 0.75 2.81 0639 016 26451 26450 43063 31065 3-inch 0.75 2.81 0639 016 26451 26452 43091 43093 3-inch 0.75 2.81 0103 016 26454 26450 43093 | | 0200 | 015 | 26455 | 26461 | 43069 | 43064 | 3-inch | 2.00 | 8.00 |
| (5255 015 26463 25646 43053 43057 3-inch 1.50 6.00 0551 015 26472 26476 43053 43057 3-inch 0.33 111.00 0551 015 26472 26476 43054 43057 3-inch 0.75 31.00 0551 015 26472 26476 43054 43057 3-inch 0.75 31.00 06515 016 26477 26470 43048 43055 3-inch 0.75 31.00 06539 016 26457 26450 43058 43055 3-inch 0.75 3.00 0639 016 26457 26450 43058 43055 3-inch 0.75 2.81 1034 016 26451 26452 43065 3-inch 0.75 2.81 1034 016 26451 26450 43065 3-inch 0.75 2.81 1034 016 26454 < | | 0500 | 015 | 26455 | 26461 | 43069 | 43064 | 2-inch | 1.50 | 6.00 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 0525 | 015 | 26463 | 26469 | 43063 | 43057 | 3-inch | 1.50 | 6.00 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 0525 | 015 | 26463 | 26469 | 43063 | 43057 | 2-inch | 0.33 | 1.32 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 0551 | 015 | 26472 | 26476 | 43054 | 43047 | 3-inch | 2.75 | 11.00 |
| 0615 016 26474 26470 43048 43055 3-inch 2.50 9.38 0633 016 26467 26462 43058 43055 2-inch 0.75 2.81 0633 016 26467 26462 43058 43055 2-inch 0.50 1.88 1034 016 26457 23058 43065 2-inch 0.50 1.88 1034 016 26457 23054 43090 3-inch 1.50 2.81 1059 019 26454 26455 43091 43083 3-inch 1.50 2.81 1059 019 26453 26448 43085 43093 3-inch 1.75 2.81 1128 015 26448 43085 43093 2-inch 1.75 2.14 1128 015 26448 43085 43093 3-inch 1.75 2.14 1128 015 26448 43085 43093 2-inc | | 0551 | 015 | 26472 | 26476 | 43054 | 43047 | 2-inch | 0.75 | 3.00 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 0615 | 016 | 26474 | 26470 | 43048 | 43055 | 3-inch | 2.50 | 9.38 |
| 0639 016 26467 26462 43058 43065 3-inch 1.50 5.63 1034 016 26457 26452 43058 43065 2-inch 0.50 1.88 1034 016 26454 26450 43084 43090 3-inch 1.50 5.63 1059 019 26450 26453 26450 43081 43093 3-inch 1.20 3.16 1059 019 26450 26453 26448 43093 3-inch 1.25 2.0 1128 015 26453 26448 43093 3-inch 1.25 2.14 0.0 1154 014 26448 43093 3-inch 1.25 2.14 0.0 1154 014 26448 43093 3-inch 1.26 2.14 0.50 2.14 1154 014 26444 43093 2-inch 1.25 2.14 0.0 2.6 2.14 11218 | | 0615 | 016 | 26474 | 26470 | 43048 | 43055 | 2-inch | 0.75 | 2.81 |
| 0639 016 26467 25462 43058 43065 2-inch 0.50 1.88 1034 016 26454 26450 43084 43090 3-inch 3.50 13.13 1034 016 26454 26450 43084 43090 3-inch 3.50 13.13 1059 019 26450 26453 26445 43083 3-inch 1.00 9.47 1128 015 26453 26448 43091 43083 2-inch 1.25 14,00 1128 015 26453 26442 43094 43103 3-inch 1.75 2.16 1154 014 26448 43094 43103 3-inch 1.75 2.14 1154 014 26442 43094 43103 3-inch 1.75 2.14 1154 017 26448 43004 43103 3-inch 1.75 2.14 1154 017 26448 43017 43 | | 0639 | 016 | 26467 | 26462 | 43 05 8 | 43065 | 3-inch | 1.50 | 5.63 |
| 1034016 26454 26450 43084 43090 $3-inch$ 3.50 13.13 1034016 26454 26450 43084 43090 $2-inch$ 0.75 2.81 1059019 26450 26455 43091 43083 $3-inch$ 1.00 9.47 1059019 26450 26455 43091 43083 $2-inch$ 1.00 3.16 1128015 26453 26448 43093 $3-inch$ 1.25 $14,00$ 1154014 26444 43094 43103 $3-inch$ 1.75 2.14 1154014 26444 43094 43103 $3-inch$ 1.75 2.66 1154014 26444 43094 43103 $3-inch$ 1.75 2.16 1154014 26444 43094 43103 $2-inch$ 1.75 2.60 1154017 26449 43003 43103 $2-inch$ 1.75 5.36 1158017 26499 43017 43025 $3-inch$ 1.75 5.00 1218017 26499 43017 43022 $3-inch$ 1.00 2.65 1036016 26499 43017 43022 $3-inch$ 1.00 2.65 1036016 26499 43017 43029 $2-inch$ 1.00 2.65 1036016 26499 43017 43029 $2-inch$ 1.00 2.66 1036016 26 | | 0639 | 016 | 26467 | 26462 | 43058 | 43065 | 2-inch | 0.50 | 1.88 |
| 1034016 26454 26450 43084 43090 $2-inch$ 0.75 2.81 1059019 26450 26455 43091 43083 $3-inch$ 3.00 9.47 1059019 26450 26455 43091 43083 $3-inch$ 1.00 3.16 1128015 26453 26443 43085 43093 $3-inch$ 1.25 $14,00$ 1128015 26453 26444 43085 43093 $2-inch$ 1.75 5.36 1154014 26448 26444 43094 43103 $2-inch$ 1.75 5.36 1154017 26444 26444 43003 $2-inch$ 1.75 5.36 1154017 26444 26446 43101 43032 $2-inch$ 1.75 5.36 1218017 26444 26449 43101 43022 $3-inch$ 1.75 5.36 1218017 26449 26499 43017 43022 $3-inch$ 1.75 5.16 1036016 26499 43017 43022 $2-inch$ 1.00 2.65 1059015 26499 26499 43030 43029 $3-inch$ 1.25 5.00 1122015 26499 26499 43030 43029 $2-inch$ 1.00 2.65 1059015 26499 26499 43030 43029 $2-inch$ 1.00 $14,00$ 1122015 264 | | 1034 | 016 | 26454 | 26450 | 43084 | 43 090 | 3-inch | 3.50 | 13.13 |
| 1059019 26450 26455 43091 43083 $3-inch$ 3.00 9.47 1059019 26450 26455 43091 43083 $2-inch$ 1.00 3.16 1128015 26453 26443 43085 43093 $2-inch$ 1.25 $14,00$ 1128015 26443 264448 43085 43093 $2-inch$ 1.75 5.36 1154014 26448 264442 43103 $2-inch$ 1.75 5.36 1154017 264448 264442 43103 $2-inch$ 1.75 5.36 1218017 264444 264446 43101 43092 $3-inch$ 1.75 5.36 1218017 264444 264446 43101 43092 $3-inch$ 1.00 2.65 1036016 26499 43017 43026 $2-inch$ 1.00 2.65 1036015 26499 43017 43026 $2-inch$ 1.00 2.75 1059015 26499 43017 43026 $2-inch$ 1.00 2.75 1059015 26499 43017 43029 $2-inch$ 1.00 3.75 1059015 26499 43021 43029 $2-inch$ 1.00 2.65 1122015 26499 43021 43029 $2-inch$ 1.00 4.00 1122015 26499 43021 43029 $2-inch$ 1.00 4.00 </td <td></td> <td>1034</td> <td>016</td> <td>26454</td> <td>26450</td> <td>43084</td> <td>43090</td> <td>2-inch</td> <td>0.75</td> <td>2.81</td> | | 1034 | 016 | 26454 | 26450 | 43084 | 43090 | 2-inch | 0.75 | 2.81 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1059 | 019 | 26450 | 26455 | 43 09 1 | 43083 | 3-inch | 3.00 | 9.47 |
| 1128015 26453 264448 43085 43093 $3-inch$ 1.25 $14,00$ 1128015 26453 264448 43085 43093 $2-inch$ 1.50 2.00 1154014 26444 43093 $2-inch$ 1.75 5.36 1154014 26444 43094 43103 $3-inch$ 1.75 5.36 1154014 26444 264446 43101 43092 $2-inch$ 1.75 5.36 1218017 26444 26446 43101 43092 $3-inch$ 1.75 5.16 1218017 26449 264496 43101 43092 $2-inch$ 1.00 2.65 1036016 26499 26499 43017 43026 $2-inch$ 1.00 2.65 1059015 26499 26499 43023 $2-inch$ 1.00 3.75 15.00 1059015 26499 26499 43023 $2-inch$ 1.00 3.75 15.00 1059015 26499 26499 43023 $2-inch$ 1.00 3.75 15.00 1122015 26499 26499 43023 $2-inch$ 1.00 4.00 1122015 26499 26499 43023 $2-inch$ 1.00 4.00 1122015 26499 26499 43021 43029 $2-inch$ 1.00 4.00 1152015 26499 26499 43021 | | 1059 | 019 | 26450 | 26455 | 43091 | 43083 | 2-inch | 1.00 | 3.16 |
| 1128015 26453 26448 43085 43093 $2-inch$ 1.50 2.00 1154014 26448 26442 43094 43103 $3-inch$ 1.75 5.36 1154014 26448 26442 43094 43103 $3-inch$ 1.75 5.36 1218017 26444 26446 43101 43092 $3-inch$ 1.00 2.65 1218017 26449 26449 43101 43092 $3-inch$ 1.00 2.65 1036016 26499 43017 43026 $3-inch$ 1.00 2.75 5.00 1036015 26499 43017 43026 $3-inch$ 1.00 2.75 5.00 1059015 26499 43017 43026 $2-inch$ 1.25 5.00 1059015 26499 43017 43026 $2-inch$ 1.25 5.00 1059015 26499 43017 43029 $2-inch$ 1.25 5.00 1059015 26499 43017 43029 $2-inch$ 1.25 5.00 1122015 26499 43023 43029 $2-inch$ 1.25 5.00 1122015 26499 43023 $2-inch$ 1.25 5.00 1122015 26499 43023 43029 $2-inch$ 1.00 $4,00$ 1152015 26499 43023 43029 $2-inch$ 1.00 $4,00$ | | 1128 | 015 | 26453 | 26448 | 43085 | 43093 | 3-inch | 1.25 | 14.00 |
| 1154 014 26448 26442 43094 43103 $3-inch$ 1.75 5.36 1154 017 26444 26446 43101 43092 $2-inch$ 0.75 2.14 1218 017 26444 26446 43101 43092 $3-inch$ 3.50 6.18 1218 017 26444 26446 43101 43092 $2-inch$ 1.00 2.65 1036 016 26499 43017 43026 $3-inch$ 1.00 2.65 1036 016 26499 43017 43026 $2-inch$ 1.00 3.75 1036 015 26499 43017 43026 $2-inch$ 1.00 3.75 1059 015 26499 26499 43017 43029 $2-inch$ 1.00 3.75 1059 015 26499 26499 43017 43029 $2-inch$ 1.00 3.75 1059 015 26499 26499 43023 $2-inch$ 1.200 3.75 $16,00$ 1122 015 26499 26499 43023 43029 $2-inch$ 1.00 $4,00$ 1122 015 26499 26499 43023 $3-inch$ 3.75 $16,00$ 1122 015 26499 26499 43023 $2-inch$ 1.00 $4,00$ 1122 015 26499 26499 43023 $2-inch$ 1.00 $14,00$ 1152 015 26499 26499 4302 | | 1128 | 015 | 26453 | 26448 | 43085 | 43093 | 2-inch | 1.50 | 2.00 |
| 1154014 26448 26442 43094 43103 $2-inch$ 0.75 2.14 1218017 26444 26446 43101 43092 $3-inch$ 3.50 6.18 1218017 26444 26446 43101 43092 $3-inch$ 3.50 6.18 1218017 26444 26449 43017 43092 $2-inch$ 1.00 2.65 1036016 26499 43017 43026 $3-inch$ 3.50 13.13 1036015 26499 43017 43026 $2-inch$ 1.00 3.75 1059015 26499 43030 43039 $2-inch$ 1.00 3.75 1059015 26499 26499 43030 43029 $2-inch$ 1.00 3.75 1059015 26499 26499 43030 43029 $2-inch$ 1.00 4.00 1122015 26499 43021 43013 $3-inch$ 3.50 $14,00$ 1122015 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 4.00 1122015 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 4.00 | | 1154 | 014 | 26448 | 26442 | 43094 | 43103 | 3-inch | 1.75 | 5.36 |
| 1218017 26444 26446 43101 43092 $3-inch$ 3.50 6.18 1218017 26444 26446 43101 43092 $2-inch$ 1.00 2.65 1036016 26498 26499 43017 43026 $3-inch$ 3.50 13.13 1036016 26499 43017 43026 $2-inch$ 1.00 2.65 1059015 26499 43017 43026 $2-inch$ 1.00 3.75 1059015 26499 43030 43039 $3-inch$ 3.75 15.00 1059015 26499 26499 43030 43039 $3-inch$ 3.75 15.00 1122015 26499 26499 43030 43029 $2-inch$ 1.00 4.00 1122015 26499 26499 43023 43029 $2-inch$ 1.00 4.00 1122015 26499 43021 43013 $3-inch$ 3.50 $14,00$ 1122015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 4 | | 1154 | 014 | 26448 | 26442 | 43094 | 43103 | 2-inch | 0.75 | 2.14 |
| 1218017 26444 26446 43101 43092 $2-inch$ 1.00 2.65 1036016 26498 26499 43017 43026 $3-inch$ 3.50 13.13 1036016 26498 26499 43017 43026 $3-inch$ 3.50 13.13 1059015 26499 26499 43017 43026 $2-inch$ 1.00 3.75 1059015 26499 26499 43030 43039 $3-inch$ 3.75 15.00 1059015 26499 26498 43030 43039 $2-inch$ 1.25 5.00 1122015 26499 26498 43038 43029 $2-inch$ 1.26 4.00 1122015 26499 26498 43038 43029 $2-inch$ 1.00 4.00 1122015 26499 26499 43021 43013 $3-inch$ 3.50 $14,00$ 1122015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 26499 43021 43013 $2-inch$ 1.00 4.00 1152 <t< td=""><td></td><td>1218</td><td>017</td><td>26444</td><td>26446</td><td>43101</td><td>43 09 2</td><td>3-inch</td><td>3.50</td><td>6.18</td></t<> | | 1218 | 017 | 26444 | 26446 | 43101 | 43 09 2 | 3-inch | 3.50 | 6.18 |
| 1036016 26498 26499 43017 43026 $3-inch$ 3.50 13.13 1036016 26499 26499 43017 43026 $2-inch$ 1.00 3.75 1059015 26499 26499 43030 43039 $3-inch$ 3.75 15.00 1059015 26499 26499 43030 43039 $2-inch$ 1.25 5.00 1122015 26499 26498 43038 43029 $2-inch$ 1.25 5.00 1122015 26499 26498 43038 43029 $2-inch$ 1.00 4.00 1122015 26499 26498 43021 43013 $3-inch$ 3.50 $14,00$ 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26499 43021 43013 $2-inch$ 1.00 12.00 1216015 2 | | 1218 | 017 | 26444 | 26446 | 43101 | 43 09 2 | 2-inch | 1.00 | 2.65 |
| 1036016 26498 26499 43017 43026 $2-inch$ 1.00 3.75 1059015 26499 26499 43030 43039 $3-inch$ 3.75 15.00 1059015 26499 26499 43030 43039 $3-inch$ 3.75 15.00 1122015 26499 26498 43033 43029 $3-inch$ 3.50 14.00 1122015 26499 26498 43038 43029 $3-inch$ 1.25 5.00 1122015 26499 26498 43038 43029 $2-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $3-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 43021 43013 $2-inch$ 1.00 4.00 1152015 26498 26499 43012 $2-inch$ 1.00 4.00 1216015 26498 26499 43012 43022 $3-inch$ 3.00 12.00 1216015 26498 26499 43012 43022 $2-inch$ 0.75 3.00 1216015 26499 43012 43022 $2-inch$ 0.75 3.00 1216015 2 | | 1036 | 016 | 26498 | 26499 | 43017 | 43026 | 3-inch | 3.50 | 13.13 |
| 1059 015 26499 26499 43030 43039 3-inch 3.75 15.00 1059 015 26499 26499 43030 43039 3-inch 3.75 15.00 1122 015 26499 26498 43030 43029 2-inch 1.25 5.00 1122 015 26499 26498 43038 43029 2-inch 1.00 4.00 1122 015 26499 26498 43038 43029 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 3-inch 3.00 12.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26499 43021 43013 2-inch 1.00 4.00 1152 015 26499 43012 43022 2-inch 3.00 12.00 1216 | | 1036 | 016 | 26498 | 26499 | 43017 | 43026 | 2-inch | 1.00 | 3.75 |
| 1059 015 26499 26499 43030 43039 2-inch 1.25 5.00 1122 015 26499 26498 43038 43029 3-inch 3.50 14,00 1122 015 26499 26498 43038 43029 3-inch 3.50 14,00 1122 015 26499 26498 43038 43029 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 3-inch 3.00 12.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 0.75 3.00 1216 015 26499 43012 43022 2-inch 0.75 3.00 12.00 | | 1059 | 015 | 26499 | 26499 | 43030 | 43 039 | 3-inch | 3.75 | 15.00 |
| 1122 015 26499 26498 43038 43029 3-inch 3.50 14,00 1122 015 26499 26498 43038 43029 2-inch 1.00 4.00 1122 015 26499 26499 43021 43013 3-inch 3.00 12.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 0.75 3.00 1216 015 26499 43012 43022 2-inch 0.75 3.00 | | 1059 | 015 | 26499 | 26499 | 43030 | 43039 | 2-inch | 1.25 | 5.00 |
| 1122 015 26499 26498 43038 43029 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 3-inch 3.00 12.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43012 43013 2-inch 1.00 4.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 0.75 3.00 1216 015 26498 26499 43012 43022 2-inch 0.75 3.00 | | 1122 | 015 | 26499 | 26498 | 43038 | 43029 | 3-inch | 3.50 | 14.00 |
| 1152 015 26498 26499 43021 43013 3-inch 3.00 12.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 2-inch 0.75 3.00 | | 1122 | 015 | 26499 | 26498 | 43038 | 43029 | 2-inch | 1.00 | 4.00 |
| 1152 015 26498 26499 43021 43013 2-inch 1.00 4.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 3-inch 0.75 3.00 | | 1152 | 015 | 26498 | 26499 | 43021 | 43013 | 3-inch | 3.00 | 12.00 |
| 1216 015 26498 26499 43012 43022 3-inch 3.00 12.00 1216 015 26498 26499 43012 43022 2-inch 0.75 3.00 | | 1152 | 015 | 26498 | 26499 | 43021 | 43013 | 2-inch | 1.00 | 4.00 |
| 1216 015 26498 26499 43012 43022 2-inch 0.75 3.00 | | 1216 | 015 | 26498 | 26499 | 43012 | 43022 | 3-inch | 3.00 | 12.00 |
| | | 1216 | 015 | 26498 | 26499 | 43012 | 43022 | 2-inch | 0.75 | 3.00 |

* 3-inch = 15-foot dredge, 2-inch = 8-foot dredge

APPENDIX -II

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LENCENTAGE OF SCALLOPS



DEDCENTAGE OF SCALLOPS



PERCENTAGE OF SCALLOPS



DEPICENTAGE OF SCALLOPS



PERCENTAGE OF SCALLOPS



LENCENTAGE OF SCALLOPS



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