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EFFECTS OF CONTROL SYSTEMS ON OPTIMIZATION OF SHIP SIZE **FOR NAVIGATION IN RESTRICTED WATERS OF THE GREAT LAKES**

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EFFECTS OF CONTROL SYSTEMS ON OPTIMIZATION

OF SHIP SIZE FOR NAVIGATION IN RESTRICTED

WATERS OF THE GREAT LAKES

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SUMMARY

The study examined the question of how alteration of traditional channel clearances (i.e., three times ship width for one-way channels, and seven to eight times vessel beam for two-way traffic) would affect the economics of increasing the ship's dimensions. First there was a study of ship dimension optimization, holding draft constant, to meet Great Lakes depth constraints. It was found that the optimum-sized vessel is approximately 1,250' in length, 156' in width, and has a $27.2'$ draft (maximum allowable without dredging).

The second task was to estimate the costs required to modify channels and harbors to accommodate the optimally-sized ship.

It was estimated the dredging costs would be $$6-7 billion (1977 value) if the current channel/ship dimension relationships were maintained.. This investment could be reduced to less than one billion dollars if the channel/ship dimensions were altered so that ships about 50 percent wider were permitted to operate in the same width channel. The savings (in excess of $$5.0$ billion) would be available for investment in advanced ship control systems to maintain the original traffic safety factors. The exact amount of reinvestment into emplacing the control systems would be a function of the safety margin desired.

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INTRODUCTION

The Great Lakes - St. Lawrence Seaway system is the world's largest body of fresh water. The system functions as a major trade route for the midcontinent of North America (Refs. 1, 2). Although a great deal of the system involves open-water navigation, the connecting waterways require transit through constricting channels and locks. These constraints, especially the locks, place a limitation on the number and size of vessels which can effectively use the system, thus establishing the capacity of the system.

Much of the traffic in the Lakes carries dry bulk cargo: iron ore, coal, and rock (Refs. 1, 2, 6, 7, 8, 9). As with all bulk cargo, there is no practicable limit to the vessel size (under ideal conditions) if there is cargo available at the dock. Ship size would only be constrained by the dimensions of the waterways. The economic implications of this constraint become obvious when one considers the fact that any increase in ship size would be directly translatable into cheaper transportation costs per unit.

As a result of the economic benefits available from increasing ship size, there has been continuing interest in developing the waterways so that the largest possible vessels can be used (Refs. 1, 2, 3, 6, 7, 8, 9). Today, the upper limit in wetted-ship dimensions is 1,000' x 105' x 25.5' (Refs. 8, 9).

There have been several studies undertaken for examining the costs and benefits of increasing the waterway dimensions so that larger vessels can make transit (Refs. 1, 2, 3, 6, 7, 8, 9). One study (Ref. 9), for example, examined a series of alternatives that would increase ship size up to dimensions of 1,500' **x** 175' **x** 25.5' and 32'/36'. The estimated costs for widening and deepening the waterways for the larger vessels were staggering, easily exceeding 825 billion.

In all analyses to date, however, traditional navigation and vessel control systems have been assumed. The width of channel, for example, was assumed to be three times the vessel beam for one-way traffic and seven to eight times vessel beam for two-way traffic. These c learance dimensions have been found to be the practicable minimum, given the present methods of vessel control. But the question could be raised as to what extent improved vessel control might alter the channel dimensions requirement. It is plausible that with precision vessel positioning and with fine-tuned vessel steering and response controls the currently-used channel clearance standards could be reduced (Ref. 4). This study evaluates how reduced clearance and headway requirements affect the cost parameters for acquiring and maintaining channel dimensions. The data could be useful in ascertaining the optimum control-system/ship/channel-dimension relationships $(Refs. 4, 5)$.

This study examined the question of how alteration of the traditional channel clearances would affect the economics of increasing the ship's dimensions. It had three specific objectives:

- $-$ determine the costs associated with establishing and maintaining increased channel dimensions for restricted-passage transits in the Upper Great Lakes;
- -- determine the benefits associated with making transits through restricted waters with vessels optimally sized for passage under different control system assumptions; and
- -- relate the determined costs to the resulting benefits so that optimum instrument concepts may be determined.

First, an analysis was made of ship dimensions optimization. The discussion of this portion of the research is in the section on Ship Characteristics

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Determination. The section on Costs for Developing snd Maintaining Channels contains the presentation of the analyses concerning costs associated with channel modification to accommodate passage under different control system assumptions. That section also presents the results of the integration of costs with resulting benefits for different investment profiles.

And, finally, the last section contains the study conclusions and recommendations. The Appendices contain the supporting calculations.

SHIP CHARACTERISTICS DETERMINATION

The first step in the study was to determine the general characteristics of those new ship designs that would be logical contenders for use of the waterways if more elaborate control systems were emplaced. This chapter describes the analysis that was performed in making this determination.

(RFR) criterion. Using the most recent building and operating cost information available, and by varying principal dimensions, the ESP model developed a preliminary ship des ign yielding an economic optimum for ships of this service. There exists an almost infinite number of combinations of length, beam, draft, depth, horsepower, etc., that 'could be used in a new and large ship design. To aid in this preliminary design process, the University of Michigan's Extended Season Program (ESP), a computer ship design and operation model for the Great Lakes coal, iron ore, and taconite colliers, was used. This computer model has yielded accurate economic results for Great Lakes bulk carriers.¹ The measure of merit for the design of the large ship was the Required Freight Rate

 $^{\text{1}}$ It is pointed out, however, that the model has never been used to analyz the economics of ships in the size range under consideration, and no ship of these dimensions have ever been built for Great Lakes service. Hence, i has not been possible to validate the results of the model output agains actual ships.

In making the analysis, consideration was given to the factors of:

- $-$ principal dimension
- $--$ cargo
- -- propulsion plant
- -- superstructure
- investment and financial criteria.

Ship Factors Considered

Principal Dimensions

In determining the new vessel, the principal dimensions must be consistent with the rules of sound naval architecture. Additionally, the dimensions must be compatible with the Great Lakes environment. In this context, draft of the vessel is the primary design-limiting dimension in the design process. The maximum draft presently operating in the Great Lakes is 25.5 feet. However, the maximum possible draft fluctuates with the rise and fall of the lakes' water level. Recent conditions, for example, have allowed safe drafts of 27.2 feet. It was decided to use the temporary draft level of 29.2 feet as the design criterion on the assumption that high lake levels will continue to occur in the future. The benefits from slight over-design for draft will offset the costs for the extra weight during those periods when lake level is such that lesser draft is required.

Except for draft, all other ship dimensions were allowed to vary during the optimization analyses. The parameters that were manipulated were length, beam, and block co-efficient (C_b) . ² The specific numbers were:

 $\overline{2}$ Block coefficient is the percentage of a ship's sectional area that would fill a rectangle of the same beam and depth dimensions.

```
length: ly000 y ly100 p ly200 y ly300 y Iy400 y lg500'
beam: 105', 135 y 150 y 200'
block coefficients (C_b): 84, 86, 88, 90, 94, 96, 98.
```
Cargo

Bulk commodities would be the cargo that could effectively utilize the size of vessels under consideration. And of these, coal has the least density. With a density of 4-5 cubic feet per ton, coal would require a higher hold volumetric capacity for the same cargo deadweight. For that reason, the vessel designs were based on coal as the carried cargo. The vessel was also equipped with self-unloading equipment with an unloading rate of 10,000 long tons per hour.

Propulsion Plant

Because of the unique environment found in the Great Lakes, the propulsion plant must be capable of operating within a wide range of speeds typically encountered in both restricted waterways and open lakes, and in high maneuvering conditions. The ship will have controllable pitch propellers. In addition to the controllable-pitch propeller, the vessel shall be outfitted with a bow thruster to aid in maneuverability in restricted waters.

By comparison to the vessel size, large Great Lakes bulk carriers operate in a shallow draft condition. Because of the shallow draft operation, difficulties arise if the shaft horsepower is allowed to become too large. Such difficulties are seen in hydrodynamic and vibrational areas, and are **a** result of close propeller tip clearances, rake angle of the after-hull section, and propeller diameter restrictions coupled with the high applied horsepowers. All of the previously enumerated conditions are critical in shallow draft

operations, even if propeller tunnels are used. Past experience on the Great Lakes under these conditions has indicated that a 10,000-horsepower per screw limit be observed to minimize the effects of shallow draft operation.

In order to observe these horsepower restrictions and still maintain the required speed for the ship, usually in the range of 12-14 knots, a twin screw operation is mandatory. With this type of required speed, **a** total shaft horsepower of 14,000 to 20,000 would be required. Twin screw configuration would allow 7,000 to 10,000 horsepower per screw, which would be within the allowable range.

Superstructure

The historical ship arrangement for Great Lakes vessels has typically been a fore and after superstructure. Newer vessels such **as** the thousand-footers have satisfactorily adopted the ocean going arrangement of an all-aft superstructure. Use of an all-aft superstructure saves both lightship weight and initial cost. Even though ship maneuvering in the Great Lakes is often in restricted channels, rivers, and locks, the all-aft superstructure has shown not to be detrimental to ship operations, and has been used in this evaluation.

Economic Criteria

Not only will the optimum vessel design depend on ship particulars, but it will also be affected by economic considerations. Such considerations include the owner's required rate-of-return-on-investment, ship life, and income tax rate.

With interest rates at unprecedented levels and long-term inflation generally predicted, a 15 percent after-tax rate-of-return-on-investment was selected as a reasonable investment criterion.

Ship life on the Great Lakes is much longer than on the oceans. Salt water is much harsher on steel ships and their components than is fresh water. The average vessel age of many Great Lakes fleets is over 50 years. As a result, a 35-year life expectancy seemed a reasonable and conservative vessel life factor to use in the calculations.

A corporate income tax-rate of 46 percent was used. This rate is approximately that currently applied today (1980) in the United States.

Optimum Design Selection

By using the University of Michigan computer program to optimize ship design parameters, the investigators were able to evaluate the economies of over 250 different design concepts. First, for each design, an estimate was developed for the delivered cost of the ship. Then operating costs were estimated over a variety of trade routes within the upper Great **Lakes.** Both the capital investment calculations and the annual operating cost calculations were performed on a specially structured computer $program, 3$ These calculations were then used as input into the required freight rate computations.

Early analyses indicated that the optimum ship Length would be from L,OOO to l,300 feet long; the optimum beam would be at a ratio of about one-eighth of the length; the optimum horsepower would be in the 7,000 to 20,000 horsepower range; and the block coefficient (C_b) would be in the .88 to .94 range. A series of required freight rates on a coal service between Duluth and Buffalo for five typical configurations is shown in Table l. As seen, the major design parameters all fall in the ranges just enumerated.

³ A sub-program of the University of Michigan Department of Naval Architecture and Marine Engineering Extended Season Program.

TABLE l. Required freight rates for selection of coal colliers in Duluth/ Buffalo service.

Source: Calculated.

It should be noted that the first ship in Table 1 the 1,000 ft **x** 105 ft **x** 56 ft) is capable of operating in the Great Lakes today. There would need to be channel and/or harbor modifications to accommodate any of the remaining four.

After iterating through the cases, an optimum ship design was selected, and is identified in Table 2. Also in the table, for comparison, is the largest ship (called "parent") capable of operating in the upper Great Lakes today.

Table 3 compares the optimum ship against the existing parent for **a** variety of transits in the Great Lakes. As seen, the reduction in unit transportation costs ranges from less than two percent to over ten percent. The most likely transits for the coal carriers (from the port of Duluth) average about ten percent savings.

In examining Table 2 and Table 3 it should be remembered that the costs only considered investment and operation of the ships. Channel preparation and maintenance costs are not considered in these calculations.

The data clearly indicated that there is an optimum ship size for upper Great Lakes service. And while it is not readily apparent in the data, the optimum point is strongly influenced by the draft limitation. (In ocean

TABLE 2. Comparison of optimum ship design with largest ship presently capable of operating in upper Great Lakes.

Source: Calculated

service, where operators have no draft limitation, the economic optimum-sizedship is essentially infinite, or at least significantly greater than found in the Great Lakes.)

Finally, the analyses also clearly indicated that freight rate reductions are possible if ship size can be increased beyond the presently existing maximum

TABLE 3. Required freight rates for two ships in coal service in upper Great Lakes (\$/ton of coal).

*** Assume Soo Locks are able to allow transit of optimum ship.**

size. It now remains to be determined whether this benefit potential would be more than offset by costs associated with either increasing channel size or by emplacing control systems that would permit larger ships to safely operate in the current channels. The next section will examine the capital costs and operating costs associated with developing and maintaining channels to accommodate the larger ships.

COSTS FOR DEVELOPING AND MAINTAINING CHANNELS

While the Great Lakes **have a large number of ports, only a small number are involved in most of the cargo movement. The first task in investigating the development and maintenance of channels was to decide upon which ports should be included in the analysis. The second task was** to **develop costs for enlarging and maintaining the channels. In conjunction with this activity, cost analyses** were developed on the basis of emplacing an advanced control system (i.e., only

deepening the channel to accommodate ships of the dimensions under consideration; widening the channel was omitted). The final activity was to compare the different costs, and their assumptions, and to isolate those costs that would be eliminated with the use of advanced control systems.

Port Selection

There was first an extensive screening of all ports in the upper Great Lakes that are capable of handling any ship that can transit the Welland Canal 30' **x** 76' **x** 26'!. The ports were then categorized according to annual cargo tonnage, and availability of Corps of Engineer Lake Survey charts. The final selection included:

Channels

St. Marys River Straits of Mackinac St. Clair River Detroit River Toledo Harbor to Detroit **River** Pelee Passage

Fortunately, the Corps of Engineers, Chicago District, recently (1977) performed extensive analyses on the same ports. The investigation, therefore, concentrated on extending the Corps' effort to specific questions raised in this study.

In their analysis, the Corps of Engineers examined project maps, dredging surveys, Lake Survey Center charts, and harbor modifications. Information was **also obtained from the Corps' Rivers and Harbors Port Series,** Greenwood's Guide to Great Lakes Shipping, and the Great Lakes Pilot.

The Corps' analyses "assumed that generally: (1) a no-passing channel should be three times the beam of the vessel, (2) a two-way channel should be 7.6 times vessel width, and (3) turning basins should be 1.5 times vessel length."⁴

The Corps of Engineers next prepared detailed estimates of costs that would occur in sizing the channels to accommodate vessels of different sizes. Appendix A contains a description of the procedures that were followed in making these estimates.

⁴ "Methodology for Cost Estimating," undated memorandum, Corps of Engineers, Chicago District. The memo cites the following documents as the basis for dimensions: Engineering Manual EM111021607 (2 August 1965) Tida Hydraulics, Page 13, and the Gross Isthmus Canal Study, Panama, Appendix 6, Navigation in Confined Channels, Page F-2.

As noted, the improvements were calculated on the basis of increasing a channel dimension to accommodate a ship of a particular size using a ratio of channel width to ship beam as one reference point, snd a ratio of turning basin diameter to ship length as a second reference point. Ship depth was a third factor in establishing the channel size. Appendix 8 presents the costs that resulted from the analyses for several vessel sizes, each with a variety of drafts..Also included are the projected operating and maintenance costs for keeping the channels at the prescribed dimensions after the initial expansion has been completed.

Table 4 is a presentation of calculations derived from the Corps of Engineers costs. It shows the differences in costs (1977 dollars) that would occur in expanding the ports and channel facilities to accommodate various sizes of vessels under two different sets of assumptions:

- 1) expanding the channel clearances per the traditional ratio; 3 times ship beam for one-way traffic; 7.6 times ship beam for two-way traffic; 1 1/2 times ship length for turning basin diameter.
- 2) not altering the channel widths, but dredging to meet turning-basin requirements as per 1.5 times ship's length. This option would be considered typical of the expense required to accommodate larger vessels if they were also equipped with advanced control systems.

Table 4 shows the cost estimates for channel preparation for different sizes of ships under the two sets of assumptions described above. (The details for the federal capital cost are shown in Appendix C .) The data show quite clearly that significant increases occur as ship's beam expands, especially when the traditional allowances for ship beam/channel width are followed. Of particular interest is the difference in capital costs between the two

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Cj 4

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TABLE 4. (Continued).

Vessel Size:

 $\hat{\boldsymbol{\beta}}$

Source: Calculated from data developed by Corps of Engineers

approaches. These differences have been plotted in Figure 1. The range is caused by costs associated with increasing the length (with the beam remaining constant), the lower estimate being the cost for $1,100$ -foot ships. The upper range is for 1,300-foot ships.

As seen in Table 4, the (1977 dollar) cost for enlarging channels and increasing turning basin diameter to accommodate $1,100$ -ft x 105 -ft ships would be \$370 million if the traditional channel/ship relationships are followed. If the channels and ports were to be expanded only to meet the length requirements, and the locks were to be increased only to meet minimum pass-through requirements, the cost would only be \$215 million (1977 dollars). Theoretically, then, the difference in the two costs $(\frac{155}{10})$ million) is the amount that could be spent to emplace control systems that would provide the same margin of safety, and still not exceed the costa for the traditional system.

It is possible, by interpolation, to estimate the cost for improving channels and ports to accommodate the optimum design described in the preceding chapter, a ship with dimensions of $1,250$ ft (length) by 156 ft (width). The cost (1977 dollars) would be approximately \$5.99 billion if channel and port enlargement is based on the traditional ship/channel width relationships. The cost (1977 dollars) would be about \$720 million if channel improvements were confined to only those improvements necessary to complement-an advanced control system, i.e., turning basins and locks. If a control system could be emplaced that would provide the same traffic flow attributes as a conventional channel system for \$5.2 billion $($5.99 - .72$ billion) or less, then it would make economic sense to choose that alternative.

Finally, Figure 2 shows the difference in capital costs between the two systems i.e., conventional channel clearance and a control system-oriented

FIG. 1. Differences in capital costs between two systems for accommodating larger ships in upper Great Lakes channels and ports. Source: Table 4.

FIG. 2. Capital available for installation of advanced control systems as the relationship between ship's beam and channel clearance is reduced (for ships with length of 1,100 to 1,300 feet).

clearance) as functions of the ratio between ship beam and one-way channel clearance distance. (The ratio for the conventional system is $3:1.$) As seen, the more the ratio of channel dimension to ship's beam can be reduced, the greater the fund availability for control system emplacement.

CONCLUSIONS AND RECOMMENDATIONS

There were two major conclusions of the study. First, the optimum size bulk carrier for upper Great Lakes services was determined to be 1,250 ft by 156 ft, assuming a maximum draft constraint of 27.2 feet. The shallow draft is the major factor in forcing the length and width limitations. Vessels of the optim~ size would produce **a** savings in excess of 10 percent on the longest transits (Duluth to Buffalo) when compared with the largest (and most efficient) ships in service today.

There would be major capital investments required to modify the water system so that the larger vessels could be accommodated. It is estimated that an initial investment of \$6 billion (1977 value) would be required to complete the channel and turning basin expansions, and lock enlargements. On the basis of current traffic flows, and assuming a 50-year capital investment write-off period, all bulk cargo would be confronted with a surcharge of $$1-2$ per ton.⁵

The second conclusion of the study was that it is possible to save up to \$5.0 billion (1977 value) in channel, turning basin, and lock improvement costs by emplacing advanced concept ship maneuvering control systems. The exact amount of savings would be a function of a control system's ability to precisely regulate the movement of the vessel. The greater the control, the less clearance is required between ship and channel bank.

⁵ Based on annual total tonnage of about 120,000,000 tons.

It was beyond the scope of the study to investigate the economics of emplacing advanced concept control systems only within specific channel networks, (e.g., St. Marys River). Such analysis would be logical next steps in further analyses. The analyses would be compared with research which is presently underway on the effectiveness and adaptability to a specific channel location of various control systems.

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Volume III: Parametric Studies, by H. Nowacki, Report No. 153, 1974.

Annex: Methods of Evaluation and Computer Program, by Peter Swift et al., Report No. 156, 1975.

2. Transport Analysis - Great Lakes and Seaway. Department of Naval Architecture & Marine Engineering, The University of Michigan, 5 Volumes.

Volume I: Summary and Miscellaneous, by Harry Benford, Report 158, 1975.

Volume IV: Environmental Considerations, by John B. Woodward, Report No. 161, 1974.

Volume V: Dimensional Enlargement of Great Lakes Bulk Carriers -Weights and Costs, by Peter Swift et al., Report No. 162, 1975.

- 3. Maneuvering Characteristics of Great Lakes Vessels, by Steven C. Fisher, Report No. 205, Department of Naval Architecture & Marine Engineering, The University of Michigan, 1978.
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- 7. Cost-Benefits Analysis Model for Great Lakes Bulk Carriers Operatin During an Extended Season, by Harry Benford et al., Report No. 114, Department of Naval Architecture 6 Marine Engineering, The University of Mich igan, 1971,
- 8. Plan of Study for Great Lakes Connecting Channels and Harbors Study, U.S. Army Corps of Engineers, Detroit, Michigan, 1978.
- 9. Feasibility Study for Additional Locks and Other Navigation Improvements, \overline{St} . Lawrence Seaway Plan of Study, U.S. Army Corps of Engineers, Buffalo, New York, 1978.

APPENDIX A

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DESCRIPTION OF PROCEDURES USED BY THE CORPS OF ENGINEERS IN DETERMINING COSTS OF CHANNEL IMPROVEMENTS TO ACCOMMODATE LARGER VESSELS

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PLANS AND COST ESTIMATES

Channels: The work to establish channel cost estimates consisted of the development of criteria to size the channels relative to the considered vessel sizes. This was followed by the development of a computer program to efficiently translate the criteria into channel dimensions for the 79 reaches, both up and down bound conditions, times 28 vessel's cases for a total of 4,424 distinct solutions. Next came a plan layout of these cases, the estimation of dredging quantities of rock and other material for the cases from cross sectioning the 79 reaches, and finally applying cost figures which include the disposal price to obtain the dredging estimate first costs.

The criteria established are based upon current literature and practice. References for this are:

- l. Interoceanic Canal studies, Appendix 6, Navigation in Confined Channels. Corps of Engineers 1970.
- 2. Journal of the Waterways, Harbors, and Coastal Engineering Division, American Society of Civil Engineers. Volume 97, August 1971, containing water depths required for ship navigation (R.G. Waugh), and vessel controllability in restricted waters (E.W. Edrin), Volume 99, February 1973, containing design of ship channels and maneuvering areas $(C.K. Kray).$
- 3. EM 1100-2-1607, 2 August 1965, Corps of Engineers.
- 4. Squat Study St. Lawrence ship channel, L. Simard, March 1969.
- 5. Report No. 3, Committee on Tidal Hydraulics, Corps of Engineers, May 1965.

In addition, discussions were had with the University of Michigan Naval Architecture and Marine Engineering Department to confirm the approach and **criteria'**

Squat criteria are based upon the empirical equation

$$
S = \frac{V_{1}^{2}}{2g} \qquad 1.01 \qquad \frac{A_{1}}{A_{w}} \qquad ^{2} - 0.84
$$

from the St. Lawrence study.

 V_s = Ship velocity relative to water A_1 = Cross sectional area of channel A_{α} = Channel cross section area - vessel cross section area $g = 32.2 \text{ ft/sec}^2$

In addition, the channel type, either confined or open, is recognized through a modification to the effective width of the channel. This recognizes that squat appears to be less in channels cut in wider shallow bodies of water as opposed to channels immediately bounded by banks or placed in narrow rivers where the ship channel constitutes a significant portion of the river.

Required channel widths are a function of the controllability of the vessels using the channel. It is a function of the vessel distance from the bank, passing or no passing conditions, vessel velocity relative to the water, channel shape, and amount of water under the vessel keel. Channel width appears to be a trade-off with channel depth. The wider a channel, the less can be the depth of water under the keel to maintain the same degree of controllability. This situation of controllability is discussed more fully in the reference documents. The mathematical procedures outlined in the Interoceanic Canal

studies were utilized in the computer model of this study. This was done through curve fitting techniques that reduce the family of curves graphed on the next two pages to equation form for efficient computer programming.

The resulting equations are:

First graph upper portion

Ratio_x = (240.12 F_Y \cdot ³⁶²)² - Ratio_v - 37.18)² - 55.8

First graph lower portion

Ratio_x = (93.92 F₀ \cdot 1079) /Ratio_y 12.7226

Second graph

Ratio_y = (115.99 R 2.0371) ($_{\text{Fv}}$ **)** 4.351

F being a Froude Number

R being (ship cross section) / (channel cross section)

These graphs are shown as exhibits on the following pages.

The limits of 3 times vessel beam for one way traffic and 7.6 times vessel beam for two way traffic were utilized as lower and upper bounds, respectively to constrain the empirical equation of tbe computer model.

Trim and bottom clearance are handled in the model by the addition of a 2 foot clearance to the calculated squat regardless of bottom material type.

Harbors: Two types of work had to be performed at each of the harbors investigated. First, entrance and inner harbor criteria had to be estimated, plans prepared, and cost estimates made. Second, similar work had to be accomplished to provide for berthing spots and turning basins. Work was essentially **confined to the non-river sections of the harbors, as inspection** indicated facility improvements necessary to allow the transiting of the rivers would for the most part be exceedingly non-economical.

Legend .07 Contour **of indicated Froude number along** vhich **ship navigability is approximately constant.** The **nearly** horizontal part **oi** the contour represents **conditions at which the ship** just clears the channel bottom.

CHANNEL DESIGN CVRVES

Harbor entrance criteria considered vessel roll, pitch, heave, squat, and trim. Vessel roll response was estimated from charts on pp. 434-437 in Section 2, Ocean Navigation, Report of Proceedings XXIInd Congress of Permanent International Association of Navigation Congresses, 1969; extrapolation from the charts was necessary. Pitch-heave response was estimated according to (pitch $+$ heave - amplitude) at bow = $0.2x$ (wave height as recommended by E.O. Tuck (University of Michigan). Dr. Tuck's recommendation was based on extrapolation of charts in the paper, Beck, R., and Tuck, E., Computation of Shallow Water Ship Motions, Proc. Ninth Symposium on Naval Hydrodynamics, 1970. Waves used in the roll, pitch, and heave calculations were 10-year recurrence summer July-August-September) waves for Lakes Erie, Huron, and Michigan from WES TR H-76-1, Reports, $1, 3$, and 4 , Design Wave Information for the Great Lakes by D. Resio and C. Vincent. For Lake Superior, as Report 5 of TR H-76-1 has not yet been published, it was arbitrarily assumed that the summertime climates of the Lake Superior ports would resemble that of Milwaukee. Squat was computed from an equation on page F-11 of Annex V, Appendix B, of the Study of Engineering Feasibility of a sea-level Panama Canal. An additional 2-foot clearance was allowed, regardless of whether the lake bed was rocky or soft material. Recommended harbor entrance widths vary from three times the vessel beam (2 June 1977 letter from President, Lakes Carriers' Association, to Division Engineer, NC) to 7.6 times the vessel beam. (CERC special report $#2$, Small Craft Harbors: Design, Construction and Operation.)

Width of harbor entrance should be as follows:

Squats were calculated for vessel speeds of 5 mph and 10 mph, except where existing channels are so narrow that squat would exceed 6 to 8 feet. Also calculated were channel widths for which 1 ft and 2 ft squat would be experienced at those two speeds. Outer harbors protected by permeable breakwater were assumed to be infinitely-wide channels due to the permeable walls; consequently, zero squat was predicted for such areas. The 1,300 and 1,500-foot vessels were found to have very small ro11 and pitch-heave responses to summertime storm waves.

APPENDIX B

CORPS OF ENGINEERS SUMMARY 'OF COSTS ASSOCIATED WITH INCREASING CHANNEL CLEARANCES FOR LARGER GREAT LAKES VESSELS

(All figures in 1977 dollars)

Vessel Size: 940' x 105'

 \$000!

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Vessel Size: 940' **x** 105'

(\$000) (Operating & Maintenance)

Vessel Size: $\frac{1,100' \times 105'}{1,100' \times 105'}$

 (5000)

September 1977 Costs

Vessel Size: $\frac{1,100' \times 105'}{1,000}$

(\$000) (Operating & Maintenance)

 \sim

 (5000)

Vessel Size: $\frac{1,200' \times 130'}{1,200'}$

(\$000) (Operating & Maintenance)

 \mathcal{A}

Vessel Size: $1,300' \times 130'$

 $($ \$000 $)$

Vessel Size: 1,300' x 130'

(\$000) (Operating & Maintenance)

 (8000)

Vessel Size: $\frac{1,300' \times 175'}{1}$

(\$000) (Operating & Maintenance)

APPENDIX C

DETAILS OF COMPARISON OF FEDERAL CONSTRUCTION COSTS FOR DIFFERENT METHODS OF INCREASING VESSEL SIZE IN UPPER GREAT LAKES SERVICE

(Based on Costs Shown in Appendix B) (All figures are in thousands of 1977 value dollars)

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COMPARISON OF FEDERAL CONSTRUCTION COSTS

