| 1 | Supporting Information for |
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| 2 | Skin temperature correction for calculations of air-sea oxygen flux and annual net |
| 3 | community production |
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22 Text S1. The air-sea O₂ flux (F_{A-S}) calculation

The air-sea O_2 flux (F_{A-S}) was calculated using the model described by Liang et al. (2013) and Emerson and Bushinsky (2016), in which both fluxes from diffusion (F_S) and bubble injection (F_B) were considered (Equation 1). A correction factor for bubble flux ($\beta = 0.37$) was also applied (Emerson et al. 2019). We defined the O₂ flux from air to the ocean as positive.

$$F_{A-S} = F_S + \beta \cdot F_B \qquad \text{mol } \mathbf{m}^{-2} \, \mathbf{d}^{-1} \quad (1)$$

The diffusion flux F_s was calculated using Equation 3 (Emerson and Bushinsky, 29 2016), where $[O_2]$ was the measured seawater oxygen concentration in the surface mixed 30 layer, and $[O_2]_{sat}$ was the saturation concentration of oxygen at the given temperature and 31 salinity (Garcia and Gordon, 1992, 1993). When the mixed layer $[O_2]$ is higher than the 32 saturation value, O_2 diffuses out of the ocean and F_s is negative. Because $[O_2]_{sat}$ in 33 Equation 2 and the Schmidt number S_c in Equation 3-4 are both temperature-dependent, 34 the correction of cool skin effect for skin temperature would affect the calculation of F_s .

$$F_s = k_s \cdot ([O_2]_{sat} - [O_2]) \qquad \text{mol } \text{m}^{-2} \text{ d}^{-1} \quad (2)$$

 $\begin{array}{ll} 35 & k_s \text{ is the mass transfer coefficient for air-sea gas diffusion (Emerson and Bushinsky, \\ 36 & 2016). \end{array}$

$$k_s = 1.3 \times 10^{-4} \cdot u_*^a \cdot \left(\frac{S_c}{660}\right)^{-0.5}$$
 m s⁻¹ (3)

37 S_c is the Schmidt number, a function of temperature (Wanninkhof, 1992).

$$S_c = 1953.4 - 128 \cdot t + 3.9918 \cdot t^2 - 0.0005091 \cdot t^3$$
(4)

 u_*^a and u_*^w were water-side and air-side friction velocities, respectively (Emerson and 38

Bushinsky, 2016), where U₁₀ was wind speed at 10 m from the Advanced Scatterometer 39

40 (ASCAT) data product (http://apdrc.soest.hawaii.edu/datadoc/ascat.php).

$$u_*^w = 0.034 \cdot u_*^a$$
 m s⁻¹ (5)

$$u_*^a = \sqrt{C_d} \cdot U_{10} \qquad \qquad \text{m s}^{-1} \qquad (6)$$

 C_d was the drag coefficient, parameterized for different U₁₀ ranges (Liang et al. 2013). 41

$$\begin{array}{ll} 0.0012 & \text{if } U_{10} < = 11 \text{ m s}^{-1} \\ C_d = & (0.49 + 0.065 \cdot U_{10}) \times 10^{-3} & \text{if } 11 \text{ m s}^{-1} < U_{10} < = 20 \text{ m s}^{-1} \\ & 0.0018 & \text{if } U_{10} > 20 \text{ m s}^{-1} \end{array}$$
(7)
The bubble flux F_B included fluxes from small (collapsing) bubble (F_c) and large

43 bubble (F_p).

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mol m⁻² d⁻¹ $F_B = F_c + F_p$ (8)Small bubbles collapsed and completely dissolved in the water, adding O2 into the 44 ocean. The small bubble flux Fc was calculated as the mass transfer coefficient for small 45 bubbles (k_c) multiplied by the mole fraction of oxygen in the air (Liang et al. 2013), where $(X_{O_2} = 0.20946)$.

$$F_c = k_c \cdot X_{O_2} \qquad \text{mol } \text{m}^{-2} \text{ d}^{-1} \quad (9)$$
$$k_c = 5.56 \cdot (u^w_*)^{3.86} \qquad \text{mol } \text{m}^{-2} \text{ s}^{-1} \quad (10)$$

48 On the other hand, large bubbles have gas exchange with the surrounding seawater while ascending in the mixed layer, and they eventually go back to the 49 50 atmosphere. The large bubble flux F_p is calculated using Equation 11.

$$F_p = k_p ((1 + \Delta P) \cdot [O_2]_{sat} - [O_2]) \qquad \text{mol } \text{m}^{-2} \text{ d}^{-1} \quad (11)$$

51 The mass transfer coefficient for large bubbles (k_p), and the bubble produced increment

- 52 of supersaturation (ΔP) were calculated using Equations 12 and 13, respectively
- 53 (Emerson and Bushinsky, 2016).

$$k_p = 5.5 \cdot (u_*^w)^{2.76} \cdot \left(\frac{S_c}{660}\right)^{-0.67}$$
 m s⁻¹ (12)

$$\Delta P = 1.52 \cdot (u_*^W)^{1.06} \tag{13}$$

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57 Figure S1 The difference between the ERA5-derived ΔT and the fixed correction term of 58 -0.17 K.

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