



QC  
880  
.A4  
no. 75/10

DISPERSION OF SULFUR DIOXIDE  
EMISSIONS FROM AREA SOURCES

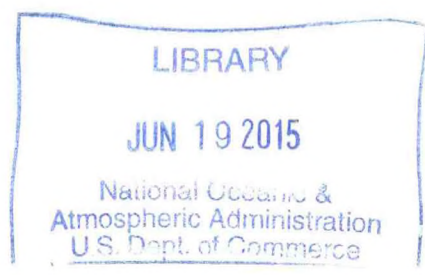
F. A. Gifford

and

S. R. Hanna

Air Resources

Atmospheric Turbulence and Diffusion Laboratory  
National Oceanic and Atmospheric Administration  
Oak Ridge, Tennessee



Published as Chapter 7 of Section II in Power Generation:  
Air Pollution Monitoring and Control, pp. 71-81.

ATDL Contribution File No. 75/10



# POWER GENERATION:

## Air Pollution Monitoring and Control

edited by

**Kenneth E. Noll**

Professor, Environmental Engineering  
Illinois Institute of Technology, Chicago

**Wayne T. Davis**

Assistant Professor, Environmental Engineering  
University of Tennessee, Knoxville

7

### **Dispersion of Sulfur Dioxide Emissions from Area Sources**

**F. A. Gifford and S. R. Hanna**

Atmospheric Turbulence and Diffusion Laboratory,  
National Oceanic and Atmospheric Administration,  
Oak Ridge, Tennessee

#### **INTRODUCTION**

This chapter can be used in evaluating surface concentrations of sulfur dioxide emitted generally over an area. The most common example of an area source is provided by urban domestic and industrial heating, for which it is necessary to consider the sum of a large number of individual sources over an area of some convenient size. Given an area-source inventory, this chapter provides a simple, systematic procedure for calculating the surface concentration at any point, averaged over an hour, a day, or a year. The basic physical model of atmospheric diffusion employed is the same as for Chapter 5 on tall-stack emissions.

Area-source concentration calculations are a recent development compared with calculations of concentrations from isolated sources. There are discussions of some of the methods now available, but these all require the use of a high-speed electronic computer.<sup>1</sup> The method to be described, although very simple, has been shown<sup>2</sup> to provide results of a precision comparable with that of the more elaborate computer calculations and can be used with confidence for area-source calculations in urban air pollution and regional air quality studies. An even simpler area-source calculation<sup>3</sup> suitable for many air pollution control purposes is also described. The model is described here in such a way that all the calculations can be done by hand. For the purpose of making many applications of the model, it has also been programmed in Fortran.<sup>4</sup>

## POWER GENERATION: AIR POLLUTION MONITORING AND CONTROL

### THE AREA-SOURCE GRID

The area source strength data are assumed to be given in the form of a regular "checkerboard" grid pattern. This area-source grid pattern is the usual one in which source information is provided. If the available source strength data are given in some other pattern, for instance by counties or districts, they should be modified to approximate a regular checkerboard pattern by choosing the largest grid-square size that will give an adequate representation of the given data. Squares of 5 x 5 km are fairly standard.

### CALCULATION OF AREA-SOURCE SURFACE CONCENTRATION: ONE-HOUR PERIOD

It is assumed that the concentration is required at the center of a grid square, which is designated square "O." The procedure when the receptor is not centered on a grid square is covered under Correction Factors, below. The calculation requires evaluation of the following simple formula for the area-source concentration,  $\chi_A$ :

$$u_{\chi_A} = c_0 Q_0 + c_1 Q_1 + c_2 Q_2 + c_3 Q_3 + c_4 Q_4 + c_5 Q_5 \quad (1)$$

The Q's are the given area source strength emissions per unit area per second in a line of source-grid squares centered on the square containing the receptor, *i.e.*, square "O" whose strength equals  $Q_0$ , and extending *upwind*. The c's are multipliers that depend on the meteorological conditions and the grid size. For a 5 x 5 km grid the multipliers are given in Table 7.1.

Table 7.1. Grid Multipliers for Meteorological Dispersion Conditions

	<i>Neutral</i>	<i>Stable</i>	<i>Unstable</i>
$c_0$ :	153	331	137
$c_1$ :	48	124	23
$c_2$ :	28	73	12
$c_3$ :	20	54	8.3
$c_4$ :	16	44	6.7
$c_5$ :	14	38	5.3

The area-source calculation, Equation (1), requires combination of these multipliers with upwind source strengths. Since this may have to be done for a number of receptor points and wind directions, it is convenient to introduce the multipliers by means of a multiplier grid, Figures 7.1-7.3, prepared from Table 7.1.

## PREDICTING DISPERSION OF EMISSIONS

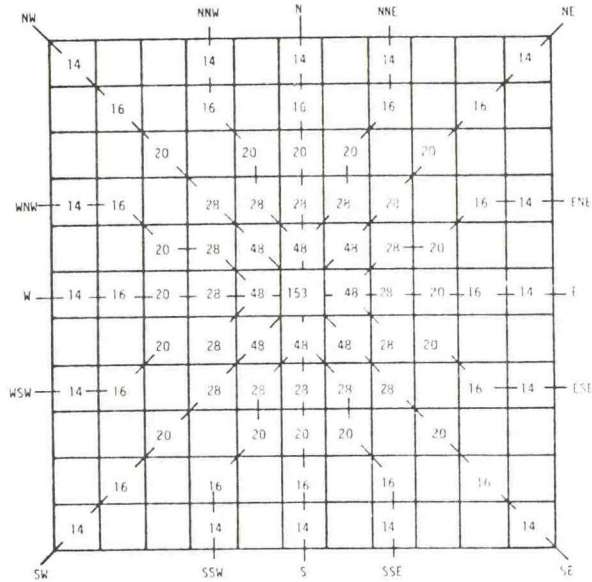


Figure 7.1. Multiplier grid for neutral meteorological conditions.

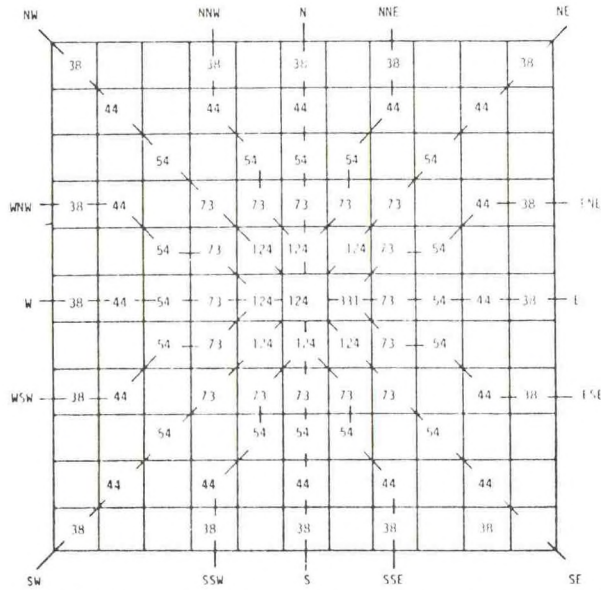


Figure 7.2. Multiplier grid for stable meteorological conditions.



POWER GENERATION: AIR POLLUTION MONITORING AND CONTROL

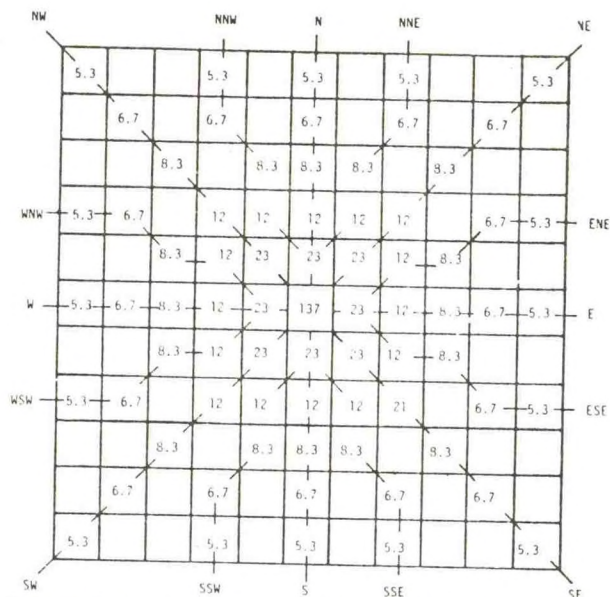


Figure 7.3. Multiplier grid for unstable meteorological conditions.

- Step 1 — Plot the area-source strength data at the centers of 1/2-inch squares. This is the "source grid." It is convenient for the following steps to do this on tracing paper or, better, to make a transparency.
- Step 2 — Select the multiplier grid, Figures 7.1, 7.2, or 7.3, appropriate to the given meteorological conditions. Center the source grid over the multiplier grid so that square "O" corresponds to the source grid square that contains the receptor point.
- Step 3 — Six numbers on the multiplier grid, including the central number at square "O," correspond to each wind direction. Multiply these by the six numbers in the corresponding source-grid squares and sum these products.
- Step 4 — Divide the result of Step 3 by the given mean wind speed,  $u$ . The result is the required hourly average area-source concentration value.
- Step 5 — Relocate the multiplier grid to a new receptor square and repeat Steps 1 through 5.

## PREDICTING DISPERSION OF EMISSIONS

### EQUATIONS FOR AREA SOURCE

The equation for surface concentrations from an area source:

$$\chi_A = \left(\frac{2}{\pi}\right)^{1/2} \frac{(\Delta x/2)^{1-q}}{b(1-q)} \left[ Q_0 + \sum_{i=1}^5 Q_i [(2i+1)^{1-q} - (2i-1)^{1-q}] \right] \quad (2)$$

is based directly, on Equation (2) of Chapter 5;  $\Delta x$  is the size of the source-strength grid, and the rest of the terms are defined in the nomenclature. Equation (2) must be multiplied by the frequency  $f_d$  of wind from the  $d$  direction, to obtain the annual average.

Comparing Equations (1) and (2), it can be seen that the dimensionless multipliers  $c_i$ ,  $i = 0, 1, \dots$  are given by:

$$c_0 = \left(\frac{2}{\pi}\right)^{1/2} \frac{(\Delta x/2)^{1-q}}{b(1-q)} \quad (3)$$

$$c_1 = \left(\frac{2}{\pi}\right)^{1/2} \frac{(\Delta x/2)^{1-q} (3^{1-q} - 1)}{b(1-q)} \quad (4)$$

$$c_2 = \left(\frac{2}{\pi}\right)^{1/2} \frac{(\Delta x/2)^{1-q} (5^{1-q} - 3^{1-q})}{b(1-q)} \quad (5)$$

and so on. The values appearing in Table 7.1 were calculated from these equations.

### CALCULATION OF ANNUAL AVERAGE AREA-SOURCE CONCENTRATION

The procedure is the same as the previous one. The exception is that the annual average wind direction frequency must be included. It is assumed that a standard, 16-point wind direction frequency distribution (wind rose) is available, giving the fraction,  $f_d$ , of the time the wind blows *from* each direction,  $d$ . The average annual wind speed is used and neutral meteorological conditions are assumed to apply. Because the wind rose varies from place to place, it is necessary to calculate a new multiplier grid for each application (each city). The complete procedure is as follows.

**Step 1** — Form an annual average multiplier grid by multiplying each of the values in the hourly average multiplier grid for *neutral meteorological conditions*, Figure 7.1, by the corresponding numbers in the wind direction frequency grid, Figure 7.4, after first summing the  $f_d$ 's as indicated

POWER GENERATION: AIR POLLUTION MONITORING AND CONTROL

in Figure 7.4;  $f_1$  is the relative frequency (fraction) of winds from the NNE,  $f_2$  that from NE, . . . ,  $f_{16}$  that from N.

$f_{14}$			$f_{15}$		$f_{16}$		$f_1$			$f_2$
	$f_{14}$		$f_{15}$		$f_{16}$		$f_1$		$f_2$	
		$f_{14}$		$f_{15}$	$f_{16}$	$f_1$		$f_2$		
$f_{13}$	$f_{13}$		$f_{14}$	$f_{15}$	$f_{16}$	$f_1$	$f_2$		$f_3$	$f_3$
		$f_{13}$	$f_{13}$	$f_{14}$	$f_{15} + f_{16}$ $+ f_1$	$f_2$	$f_3$	$f_3$		
$f_{12}$	$f_{12}$	$f_{12}$	$f_{12}$	$f_{11} + f_{12}$ $+ f_{13}$	1	$f_3 + f_4$ $+ f_5$	$f_4$	$f_4$	$f_4$	$f_4$
		$f_{11}$	$f_{11}$	$f_{10}$	$f_7 + f_8$ $+ f_9$	$f_6$	$f_5$	$f_5$		
$f_{11}$	$f_{11}$		$f_{10}$	$f_9$	$f_8$	$f_7$	$f_6$		$f_5$	$f_5$
		$f_{10}$		$f_9$	$f_8$	$f_7$		$f_6$		
	$f_{10}$		$f_9$		$f_9$		$f_7$		$f_6$	
$f_{10}$			$f_9$		$f_8$		$f_7$			$f_6$

Figure 7.4. Wind direction frequency grid.

Step 2 — Center the source-grid square containing the receptor point over the multiplier grid. It is convenient for this purpose to use a transparent source grid. (If the annual average source strength differs from the short period average value, then of course the annual source strengths must be used.)



## PREDICTING DISPERSION OF EMISSIONS

- Step 3** — Multiply *all* the number pairs of these two grids, and sum. (Where a square of the multiplier overlay falls outside the source grid area, the product is zero.)
- Step 4** — Divide the result of Step 3 by the annual average wind speed to get  $\chi_a$ .
- Step 5** — Relocate the multiplier grid to a new receptor square and repeat Steps 1 through 5.

### Correction Factors

The following procedures should be applied, if required, to the values determined by the foregoing procedure.

#### *One-Hour to 24-Hour or Other Averaging Time*

To calculate average area-source concentrations for 24-hour or other (*e.g.*, monthly) periods, follow the same procedures as for the annual average except that wind direction frequencies appropriate to the period in question must be used.

#### *Grid Size Other Than 5 x 5 km*

Multiply the value obtained at Step 4 by the appropriate correction factor shown in Table 7.2.

**Table 7.2.** Grid Size Correction Factors—Meteorological Conditions.

Grid Size (km)	<i>Neutral</i>	<i>Stable</i>	<i>Unstable</i>
1	.94	.97	.93
2	.97	.98	.96
3	.98	.99	.98
4	.99	1.00	.99
5	1.00	1.00	1.00
10	1.03	1.01	1.03
15	1.04	1.02	1.05
20	1.05	1.02	1.07
25	1.06	1.03	1.08

#### *Receptor Point Not at Center of a Source-Grid Square*

Calculate  $\chi_a$  for the center of the source-grid square containing the receptor point, and for the next nearest square beyond the receptor point. Interpolate linearly between these values.

### Worked Example

#### *Problem*

The source inventory for sulfur dioxide assuming no decay for a (real) city is given in Figure 7.5. The grid spacing is 5 km. (1) Calculate the sulfur dioxide concentration for a receptor located at the

POWER GENERATION: AIR POLLUTION MONITORING AND CONTROL.

center of source square with the heavy outline, for the case of a WNW wind at 10 mph (3.4 m/sec) under neutral meteorological conditions. (2) Given the following annual wind frequency distribution, calculate the annual average concentration for a receptor located at the center of the same source square.

.15	.16	.27	.18	.14	.07
.39	.45	.58	.27	.20	.07
.22	.64	1.42	.36	.24	.14
.10	.34	.50	.14	.05	.05
.08	.31	.13	.05	.05	.05
.05	.12	.26	.08	.10	.11

Figure 7.5. Source inventory grid, annual average particulate emissions ( $\mu\text{g}/\text{m}^3 \text{ sec}$ ).

<i>Direction</i>	$f_d$	<i>Direction</i>	$f_d$
NNE	.02	SSW	.05
NE	.04	SW	.05
ENE	.08	WSW	.05
E	.08	W	.05
ESE	.08	WNW	.12
SE	.05	NW	.14
SSE	.04	NNW	.07
S	.04	N	.02

*Solution*

*Procedure for Hourly Average Concentration.* Select the multiplier grid for neutral conditions, Figure 7.1. Center over this the square of the source inventory overlay (Figure 7.5) containing the receptor point. Corresponding to WNW wind, it is seen that Equation (1) gives:

$$x_0 = \frac{1}{14} (153 \times .05 + 48 \times .05 + 28 \times .50 + 20 \times .34 + 16 \times .22 + 14 \times 0) = 34.4/3.4 = 10. \mu\text{g}/\text{m}^3$$

## PREDICTING DISPERSION OF EMISSIONS

*Procedure for Annual Average Concentration.* Form an annual average multiplier grid by multiplying the corresponding numbers in Figure 7.6 and Figure 7.1. The result is Figure 7.7. Figure 7.6 was obtained by substituting the actual wind direction frequencies in the above table into the annual wind frequency grid, Figure 7.4. The receptor point of Figure 7.5 is now centered over the multiplier grid, Figure 7.7, and all corresponding numbers are multiplied and added; the result equals 24.03. The annual average concentration is:

$$24.03/3.4 = 7.1 \mu\text{g}/\text{m}^3$$

.14			.07		.02		.02			.04
	.14		.07		.02		.02		.04	
		.14		.07	.02	.02		.04		
.12	.12		.14	.07	.02	.02	.04		.08	.08
		.12	.12	.14	.11	.04	.08	.08		
.05	.05	.05	.05	.22	1.0	.24	.08	.08	.08	.08
		.05	.05	.05	.13	.05	.08	.08		
.05	.05		.05	.05	.04	.04	.05		.08	.08
		.05		.05	.04	.04		.05		
	.05		.05		.04		.04		.05	
.05			.05		.04		.04			.05

Figure 7.6. Wind direction frequency grid for example.

*A Simple Approximation to the Area-Source Calculation.* Area-source strength values do not in practice vary much from one grid square to another. Furthermore, the grid multipliers of Table 7.1 show that the contribution to  $\chi_a$  from the zeroth square (strength =



POWER GENERATION: AIR POLLUTION MONITORING AND CONTROL

$Q_0$ ) is weighted most heavily. This suggests the following simple approximation to Equation (1):

$$u\chi_n = CQ_0 \quad (6)$$

where the coefficient C is obtained by summing the values given in Table 7.1, i.e.,

$$C = c_0 + c_1 + c_2 + c_3 + c_4 + c_5 \quad (7)$$

thus C equals 279 for neutral conditions, 664 for stable conditions, and 192 for unstable conditions.

Corresponding to the conditions of the worked example, Equation (6) provides the result,  $\chi_n = 4.1 \mu\text{g}/\text{m}^3$ . This is in reasonably good agreement with the results using Equation (1), especially the annual average value. Hanna<sup>3</sup> has made a number of comparisons and finds Equation (6) to be a valid, useful area-source formula.

2.52			.98		.28		.28			.56
	2.24		1.12		.32		.32		.64	
		2.80		1.40	.40	.40		.80		
1.68	1.92		3.92	1.96	.56	.56	1.12		1.28	1.12
		2.40	3.36	6.72	5.28	1.92	2.24	1.66		
.70	.80	1.00	1.40	10.56	153	11.52	2.24	1.60	1.28	1.12
		1.00	1.40	2.40	6.24	2.40	2.24	1.60		
.70	.80		1.40	1.40	1.12	1.12	1.40		1.28	1.12
		1.00		1.00	.80	.80		1.00		
	.80		.80		.64		.64		.80	
.70			.70		.56		.56			.70

Figure 7.7. Annual average multiplier grid for example.

## PREDICTING DISPERSION OF EMISSIONS

### NOMENCLATURE

- b** = vertical dispersion coefficient corresponding to given atmospheric stability ( $m^{1-q}$ )
- c** = multiplier that depends on the meteorological conditions and the grid size
- $\Delta x$  = size of the source-strength grid (m)
- f<sub>d</sub>** = fraction of the time the wind blows from each direction (dimensionless)
- p** = crosswind dispersion exponent corresponding to a given atmospheric stability (dimensionless)
- q** = vertical dispersion exponent corresponding to a given atmospheric stability (dimensionless)
- Q<sub>N</sub>** = area source strengths of grid square N ( $\mu\text{g}/\text{m}^2 \text{ sec}$ )
- u** = mean wind speed in plume region (m/sec)
- $\chi_A$**  = area source 1-hour average surface sulfur dioxide concentrations for the center of the source-grid square A ( $\mu\text{g}/\text{m}^3$ )

### REFERENCES

1. Stern, A. C., (ed.) "Proceedings of Symposium on Multiple-Source Urban Diffusion Models," USEPA (1970).
2. Gifford, F. A. and S. R. Hanna. "Urban Air Pollution Modeling," *Proceedings of The Second Clean Air Conference*, H. M. England and W. T. Beery, eds. (New York: Academic Press, 1971), pp. 1146-1151.
3. Hanna, S. R. "A Simple Method of Calculating Dispersion from Urban Area Sources," *J. Air Poll. Control Assoc.*, **21**, 774-777 (1971).
4. Hanna, S. R. "Description of ATDL Computer Model for Dispersion from Multiple Sources," *Industrial Air Pollution Control* (Ann Arbor: Ann Arbor Science, 1973), pp. 23-32.