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Final Report

SIMULATION STUDIES FOR NOAA STABILIZED COMPENSATION PROGRAM

Prepared under Contract No. 2-35369

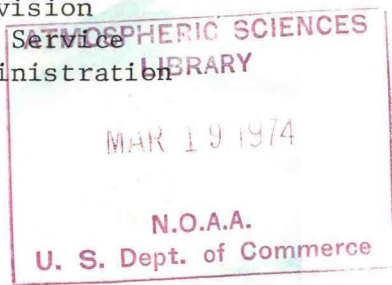
by

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National Oceanic and Atmospheric Administration
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FOREWORD

This report was prepared by the Research Triangle Institute, Research Triangle Park, North Carolina, under Contract 2-35369. The work has been administered by the Data Processing and Analysis Division, National Environmental Satellite Service, National Oceanic and Atmospheric Administration. Dr. John A. Leese is the NESS Technical Representative for the contract.

The program studies began on 21 April, 1972, and were completed on 20 May 1973. Participating RTI staff members were as follows:

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- G. S. Brown, Member of the Technical Staff
- J. H. White, Member of the Technical Staff

ABSTRACT

This report describes the participation of the Research Triangle Institute in the NOAA/NESS program to achieve data quality assurance. Long-term observation of the quality of the data from the scanning radiometer systems aboard the ITOS type spacecraft has indicated that a requirement exists for a systematic means of maintaining data quality.. Previous studies have further indicated that the alignment of the equipment used to compensate for spacecraft tape recorder flutter effects was particularly sensitive in affecting data quality. This equipment was selected as the subject of a pilot program to assure data quality by stabilized control. RTI has contributed to the overall objective of this pilot program by conducting analyses of the z-axis* compensation technique as it interacts with the data and by recommending diagnostic logic to survey data quality as the data are ingested from the Command and Data Acquisition Station (CDA).

*NOAA nomenclature referring to the flutter components introduced at the spacecraft tape recorder.

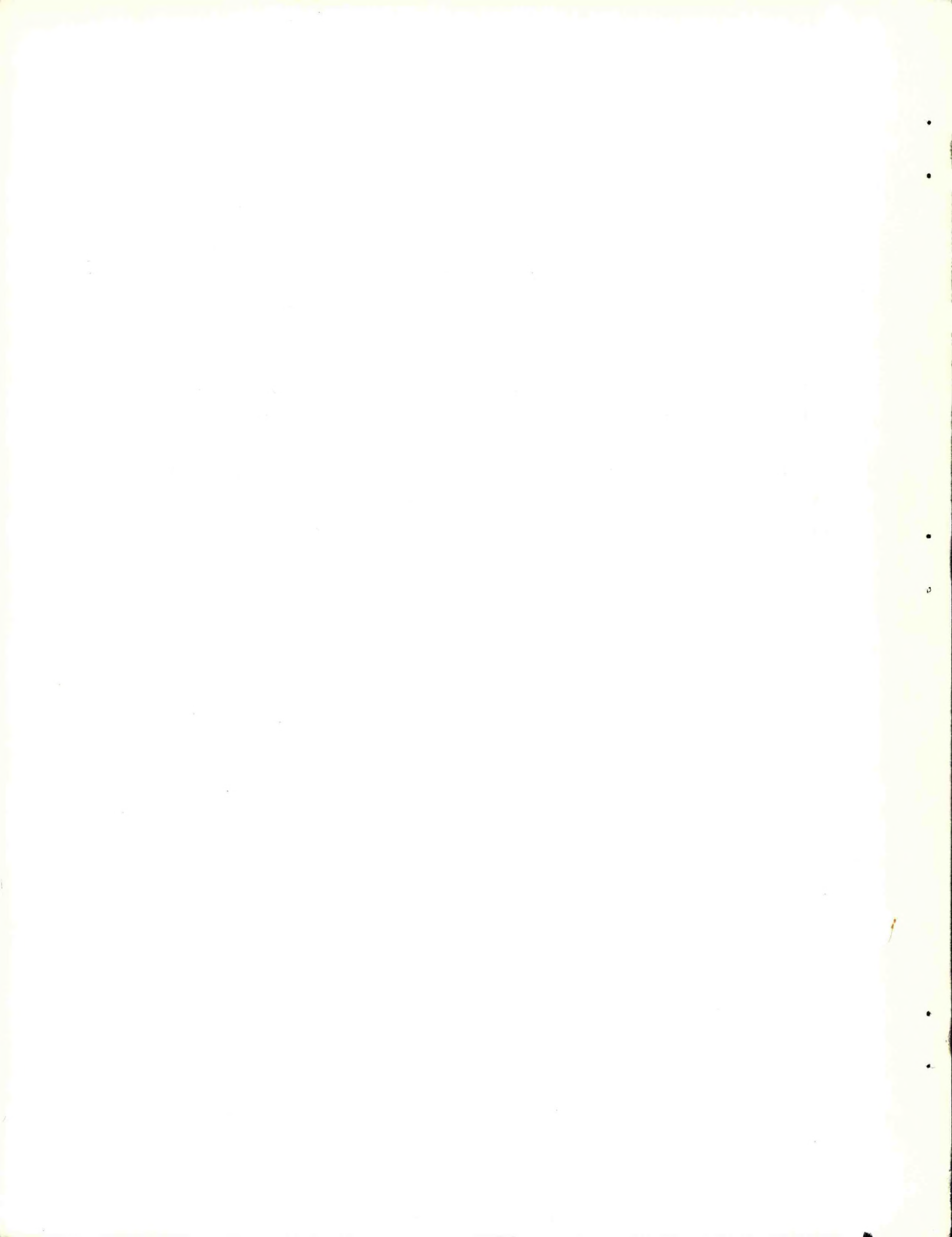


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1.0 INTRODUCTION

This report describes the participation of the Research Triangle Institute in the NOAA/NESS program to achieve data quality assurance. Long-term observation of the quality of the data from the scanning radiometer systems aboard the ITOS type spacecraft has indicated that a requirement exists for a systematic means of maintaining data quality. Previous studies have further indicated that the alignment of the equipment used to compensate for spacecraft tape recorder flutter effects was particularly sensitive in affecting data quality. This equipment was selected as the subject of a pilot program to assure data quality by stabilized control. RTI has contributed to the overall objective of this pilot program by conducting analyses of the z-axis compensation technique as it interacts with the data and by recommending diagnostic logic to survey data quality as the data are ingested from the Command and Data Acquisition Station.

Figure 1-1 shows the overall flow of ITOS scanning radiometer data. During real time operation, the data are recorded on the spacecraft tape recorder for subsequent readout. During acquisition the tape recorder is played back at an increased speed, the data is frequency division multiplexed, and then transmitted to the ground station via an S-Band telemetry link. At the ground station the data is received, demultiplexed and recorded. During recorder playback, the data is z-axis corrected and fed to the long lines for transmittal to DAPAD where it is digitized and input to the data processing equipment.

Figure 1-2 indicates the overall philosophy of the program to stabilize data quality. The concept consists of monitoring specific parameters in the data as they are ingested into the Digital Data Handling System (DDHS), conducting analyses in real-time, evaluating these analyses and communicating informative diagnostics to the CDA if data quality is not being maintained. In the event a fault does exist at the CDA, it is anticipated that these diagnostics will be of assistance in localizing and correcting this condition. This program represents an on-going effort at NESS. As a result, this report documents only those areas in which RTI was directly involved. This involvement consisted of an investigation of the compensation technique, the development of a digital model of the hardware, and the use of this model to derive sensitivities to be used as guidelines in the development of the required diagnostic logic.

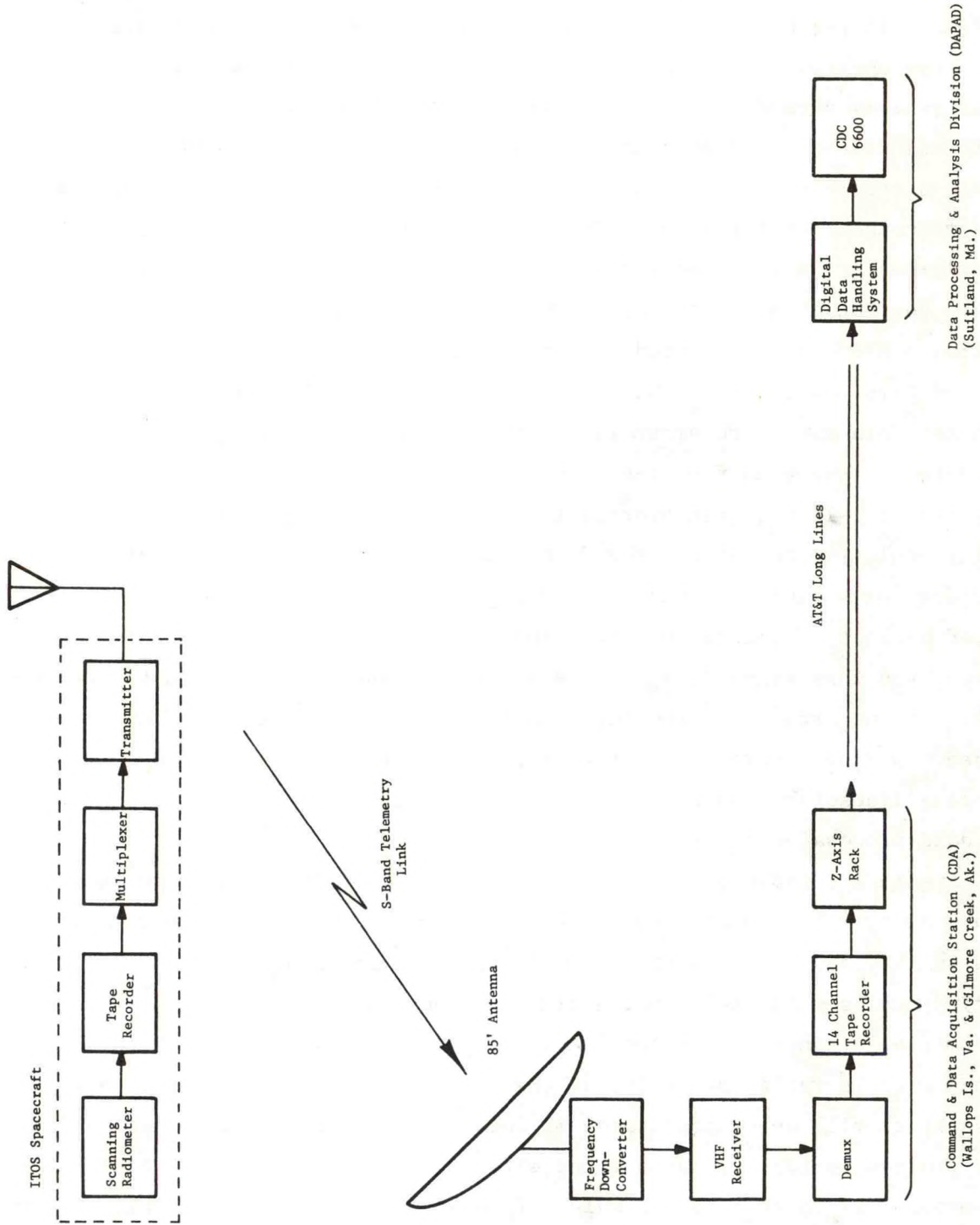


Figure 1-1. ITOS Scanning Radiometer Data Flow.

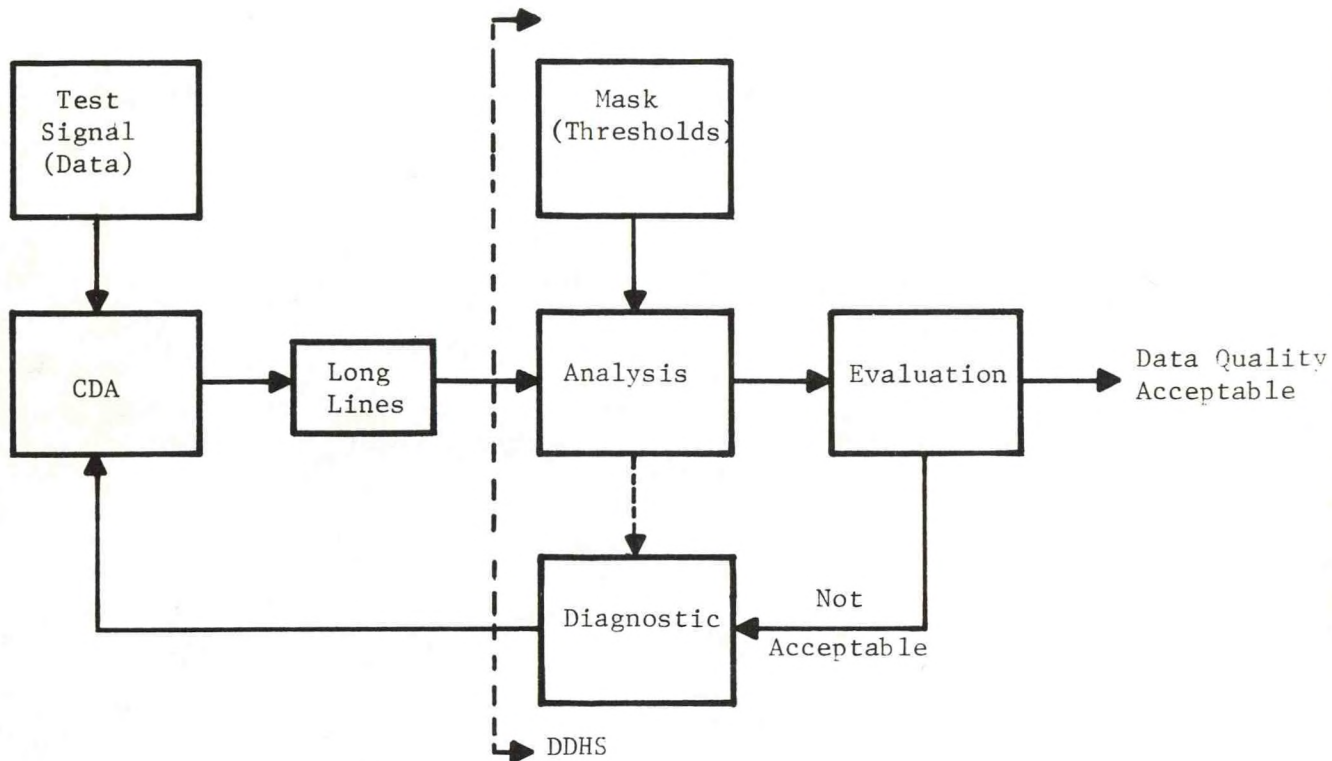


Figure 1-2. Overall Data Quality Assurance Philosophy.

The report has three main features. The initial sections present a tutorial discussion of frequency modulation theory to serve as background and also a tutorial discussion of the theory of operation of the z-axis compensation technique. Subsequent sections describe the model, pertinent analyses conducted with the model, and preliminary diagnostic logic recommendations based on these analyses. The computer algorithm is then documented in detail in the appendices. It is hoped that this approach will result in the report being a working document for NESS and RTI personnel as well as documenting the effort expended during the study.



The following table shows the results of the experiment. The data indicates that the reaction rate is significantly higher at higher temperatures. This is consistent with the Arrhenius equation, which predicts that the rate constant increases exponentially with temperature. The observed increase in rate with temperature supports the proposed mechanism for the reaction.

2.0 FREQUENCY MODULATION CONSIDERATIONS

This section presents a tutorial introduction to the mathematical aspects of frequency modulation. The intent here is to indicate the effects of the modulation technique being non-linear. Of prime concern is the spectral representation of an FM modulated waveform, especially the facts that spectral superposition does not apply and that tone modulation has a distributed spectral representation which is tone amplitude dependent.

2.1 Theoretical Considerations

The "frequency" of a waveform is defined as the time-rate-of-change of phase and as such usually suggests a periodic phenomenon (i.e. in the spectral sense). On the other hand "frequency modulation" implies a time varying frequency which is contrary to the usual notion. It therefore becomes important in the context of frequency modulation to distinguish between "spectral" and "instantaneous" frequencies.

In general, a frequency modulated wave $x_c(t)$ can be written as

$$x_c(t) = A_c \cos \theta_c(t) \quad (2-1)$$

where A_c is constant and $\theta_c(t)$ is a function of the carrier frequency and some baseband signal $x(t)$. In order to distinguish between the two types of frequency mentioned in the preceding paragraph, $\theta_c(t)$ can be written as

$$\theta_c(t) = 2\pi f_c t + \phi(t)$$

where f_c is the carrier (spectral) frequency and $\phi(t)$ contains the baseband signal $x(t)$. Returning to the concept that frequency is the time-rate-of-change of phase, one can define "instantaneous" frequency as

$$\xi(t) = \frac{1}{2\pi} \frac{d}{dt} \theta_c(t) = f_c + \frac{1}{2\pi} \frac{d\phi(t)}{dt}$$

If the baseband signal is now taken to be the change in instantaneous frequency as a function of time,

$$\xi(t) = f_c + f_D x(t)$$

(where f_D is called the "deviation" constant and is a system parameter), one can identify

$$\frac{d\phi(t)}{dt} = 2\pi f_D x(t)$$

or

$$\phi(t) = 2\pi f_D \int_0^t x(\tau) d\tau .$$

Now the modulated wave given in eq. 2-1 can be written as

$$x_c(t) = A_c \cos[\omega_c t + 2\pi f_D \int_0^t x(\tau) d\tau] \quad (2-2)$$

indicating the relation between a baseband signal and the modulated carrier.

The point of this discussion is to demonstrate that an intuitive notion of the relationship of the spectral distribution of signal information at baseband and its distribution after modulation is not available. This will be pursued in greater detail in the following section which deals with the spectrum of a frequency modulated wave.

2.2 Spectral Analysis of Modulated Carrier

The spectral analysis of a frequency modulated carrier is pertinent to the study in that data processing equipment bandwidths are continually of interest. For this reason a discussion of the behavior of the spectral distribution of the modulated carrier is included. The approach will be to initially examine the behavior of a carrier modulated by a single tone as a function of tone amplitude and frequency and to then extend this to a two tone situation. Multiple tone situations will not be discussed as they are simply mathematically complicated extensions of the two tone case and offer no additional insight.

Consider the baseband tone,

$$x(t) = A_m \cos \omega_m t .$$

Equation 2-2, the modulated carrier takes on the form,

$$\begin{aligned}
 x_c(t) &= A_c \cos(\omega_c t + 2\pi f_D \int_0^t A_m \cos \omega_m \tau d\tau) \\
 &= A_c \cos(\omega_c t + \frac{f_D A_m}{f_m} \sin \omega_m t) \quad .
 \end{aligned}$$

Define,

$$\beta = \frac{f_D A_m}{f_m}$$

and obtain

$$x_c(t) = A_c \cos(\omega_c t + \beta \sin \omega_m t) \quad . \quad (2-3)$$

The parameter β is termed the modulation index and represents the maximum phase deviation produced by the tone. Rewriting equation 2-3 as

$$x_c(t) = A_c [\cos \omega_c t \cos(\beta \sin \omega_m t) - \sin \omega_c t \sin(\beta \sin \omega_m t)]$$

and writing $\cos(\beta \sin \omega_m t)$ and $\sin(\beta \sin \omega_m t)$ in terms of Bessel functions of the first kind, one can achieve a Fourier series type representation for $x_c(t)$.

In particular,

$$\begin{aligned}
 x_c(t) &= A_c J_0(\beta) \cos \omega_c t \\
 &+ \sum_{n \text{ odd}}^{\infty} A_c J_n(\beta) [\cos(\omega_c + n\omega_m)t - \cos(\omega_c - n\omega_m)t] \\
 &+ \sum_{n \text{ even}}^{\infty} A_c J_n(\beta) [\cos(\omega_c + n\omega_m)t + \cos(\omega_c - n\omega_m)t] \quad .
 \end{aligned}$$

Notice that the spectrum of the modulated carrier consists of an infinite number of lines spaced at intervals of ω_m about the carrier with amplitudes that vary as Bessel functions of the modulation index. An illustrative line

spectrum for a frequency modulated tone is shown as Figure 2-1.

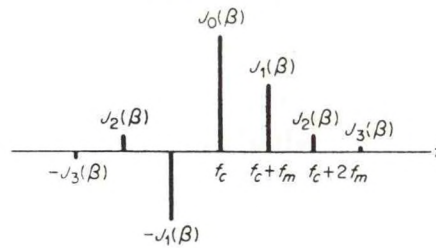


Figure 2-1. An FM line spectrum, single tone modulation.

Further, notice that for a given tone frequency, the modulation index β changes as the amplitude of the tone varies which produces a different spectral distribution. Figure 2-2 shows the behavior of Bessel functions versus their argument.

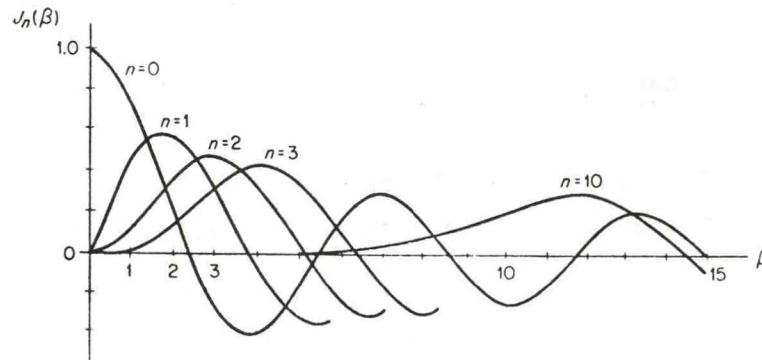


Figure 2-2. Bessel functions of fixed order plotted versus the argument β .

One may view the variation in spectral distribution as a function of amplitude and frequency by noting that the harmonics generated by $\beta=2$ are quite different from harmonics generated by $\beta=4$. This differential in β could be simply the result of a two-to-one increase in tone amplitude. Notice that for $\beta=12$ (which incidentally represents an unlikely situation), the maximum spectral line occurs at $n=10$ which represents a frequency ten times the tone frequency and would require an extremely wide channel bandwidth. Figure 2-3

indicates the effect of changing tone amplitude and frequency. The effect of amplitude only and frequency only changes are indicated (recall that

$$\beta \sim \frac{A_m}{f_m}).$$

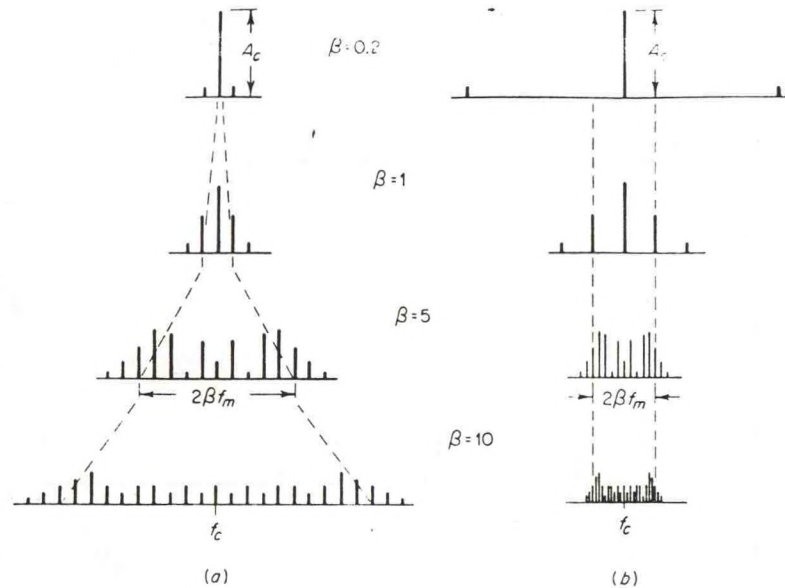


Figure 2-3. Tone-modulated FM line spectra showing the effects of tone amplitude and frequency. (a) frequency fixed, increasing amplitude; (b) amplitude fixed, decreasing frequency.

The preceding discussion has treated the behavior of the spectrum for only a single tone. It is of interest to consider the additional influence of a multiple tone signal as this represents a more realistic situation. The mathematics of investigating the general multitone situation is extremely cumbersome and, as a result, only the two tone case will be discussed here. This is adequate as all the pertinent effects will be revealed.

Following the mathematical procedure introduced for a single tone and omitting the intermediate details, for a signal of the form

$$x(t) = A_1 \cos \omega_1 t + A_2 \cos \omega_2 t$$

where f_1 and f_2 are not harmonically related, one can write the modulated carrier as,

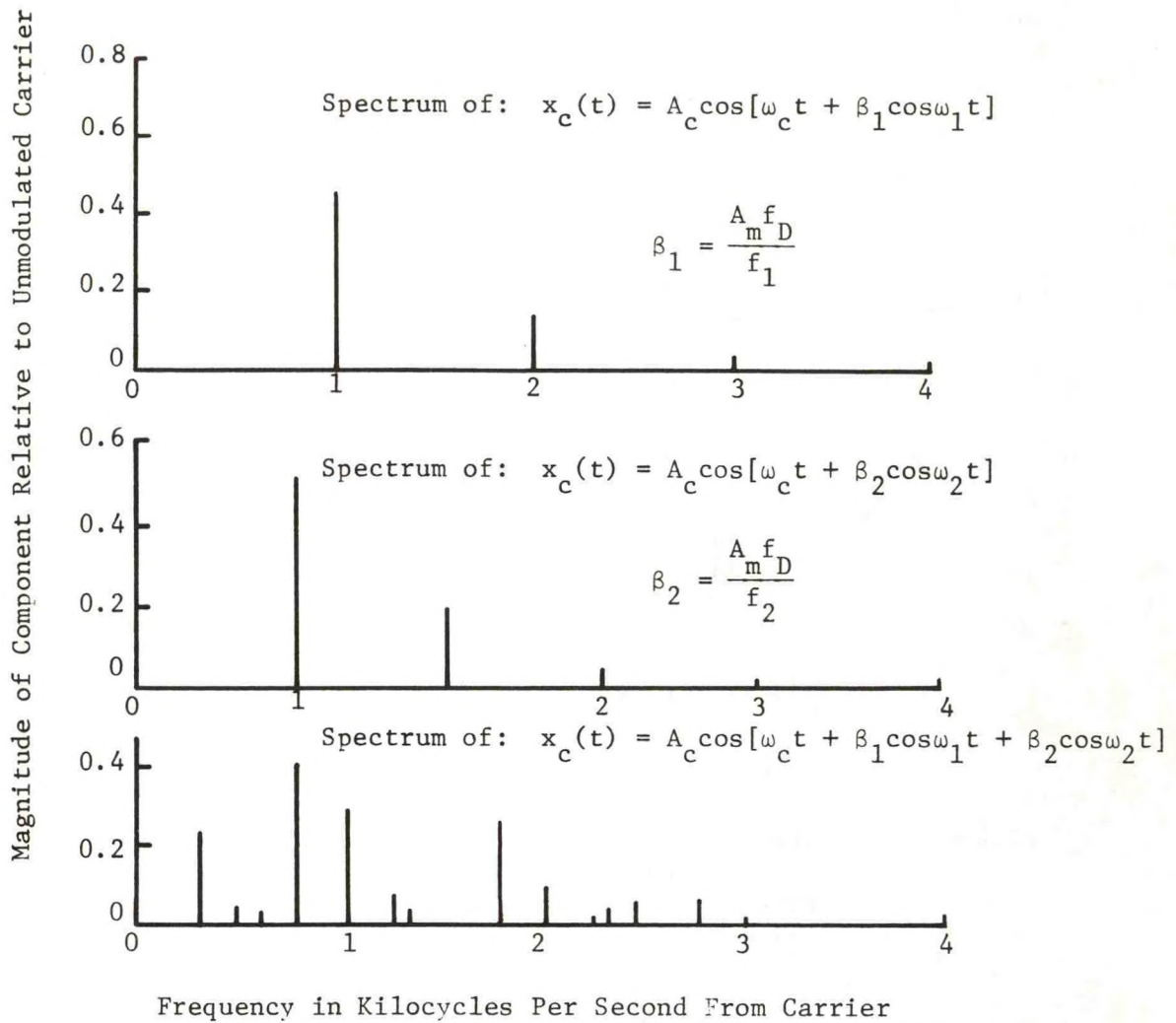


Figure 2-4. Spectra Showing the Failure of Superposition in Frequency Modulation.

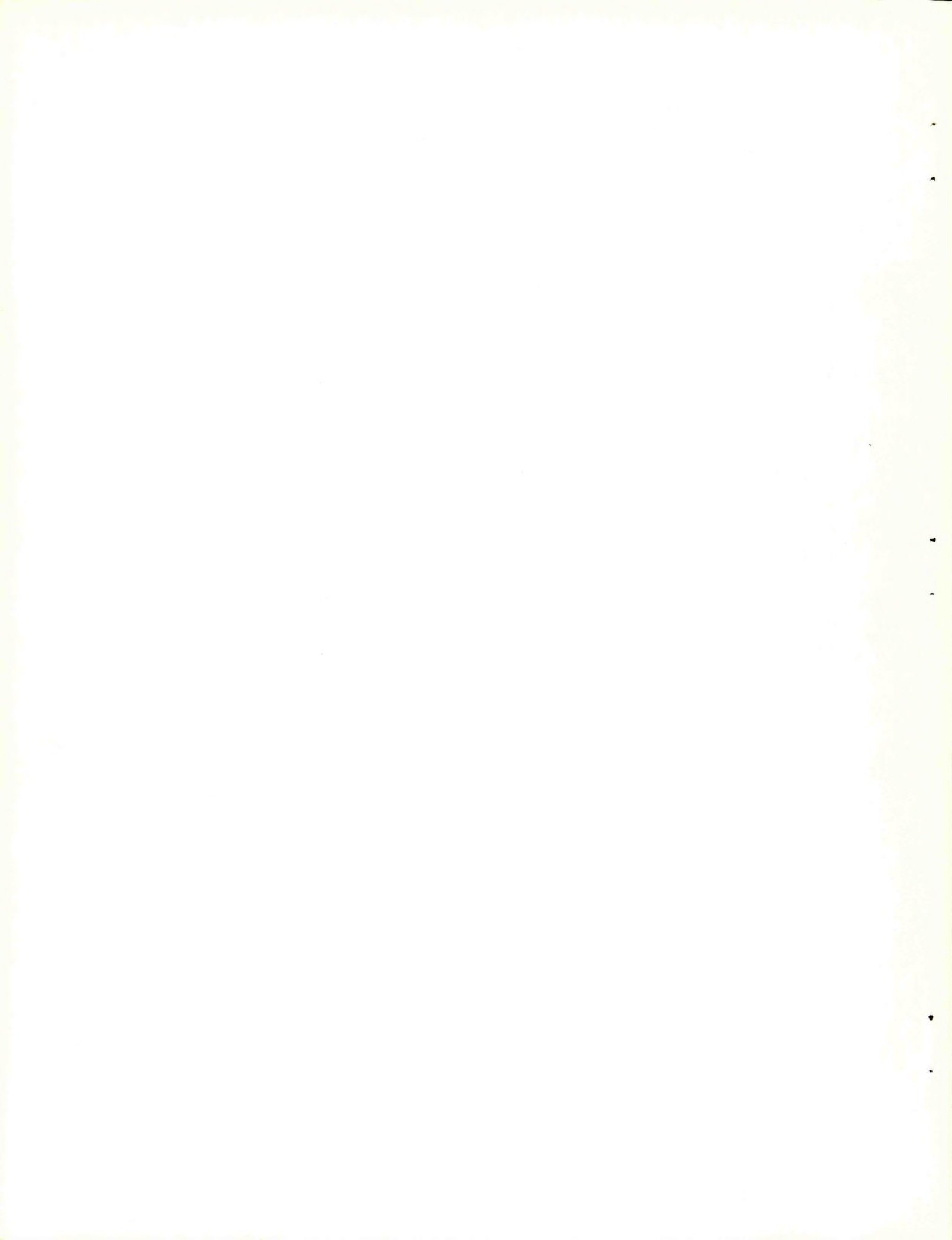
$$x_c(t) = A_c \sum_n^{\infty} \sum_m^{\infty} J_n(\beta_1) J_m(\beta_2) \cos(\omega_c + n\omega_1 + m\omega_2)t .$$

Again, without including the details, this may be interpreted in the spectral domain as being divided into four categories:

1. the carrier alone at f_c
 2. sidebands at $f_c \pm nf_1$ due to f_1 alone
 3. sidebands at $f_c \pm mf_2$ due to f_2 alone
- and 4. sidebands at $f_c \pm nf_1 \pm mf_2$ due to the beat-frequency modulation between the two tones.

This last category is the result of the modulation process being non-linear and, as would be expected, gives rise to the feature of FM that spectral superposition does not hold and as such data interaction can occur if the modulated carrier is bandlimited to any extent. Figure 2-4 demonstrates this effect by presenting the single and sum spectra of two tones.

The preceding discussion has been brief, but has demonstrated the data dependence of the modulated subcarrier spectrum. The basic reason for including this discussion is to admit that bandpass filtering the modulated carrier may cause distortion of the baseband signal and interaction of spectral harmonics. Standard rules of thumb are common in selecting bandwidth requirements and are conditioned on the data characteristics. For example "Carson's Rule" provides that for most applications, a bandwidth of $\pm (f_D + f_m)$ about the carrier frequency is adequate (f_D is the previously mentioned deviation constant and f_m is the highest frequency in the baseband signal). These topics are explored in greater detail in references 2-1 and 2-2.



3.0 Z-AXIS RACK OPERATION

This section presents a qualitative discussion of the operation of the z-axis rack. Included is an introduction to pulse-averaging discriminator operation and utilization of the output of the reference discriminator in order to compensate for tape recorder speed error.

3.1 Discriminator Operation

A block diagram of the basic pulse-averaging discriminator (see ref. 3-1) used in the z-axis rack is shown in Figure 3-1. The input bandpass filter shown is not necessary for the discussion but is included for completeness.

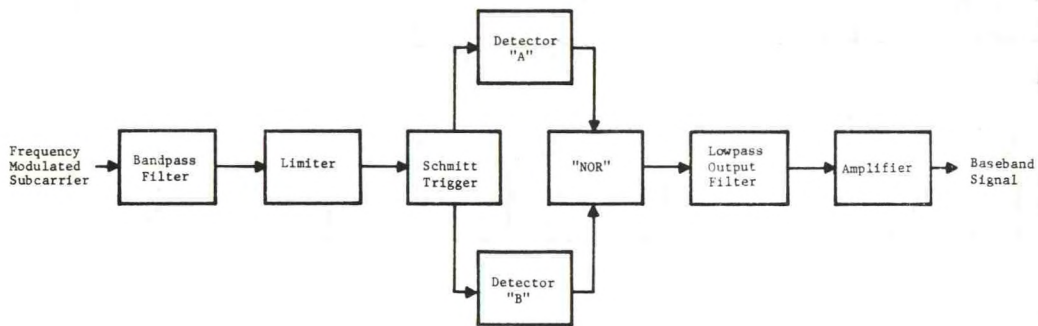


Figure 3-1. Basic Discriminator Block Diagram.

Figure 3-2 indicates waveforms encountered at various locations in the discriminator and may be used to describe the functional operation of this type of FM demodulator. Figure 3-2-a indicates a simple 290 Hz base-band tone which will be used to modulate a 5000 Hz sub-carrier. (It should be noted that the waveform parameters such as subcarrier frequency, etc., were chosen for ease of graphic presentation rather than as representative of the actual hardware configuration.) A portion of the modulated subcarrier is shown in Figure 3-2-b. This represents the input to the discriminator.

This frequency modulated subcarrier is first "hard limited" at the input in order to remove any residual amplitude modulation that may have been introduced in the satellite modulator, multiplexer and transmitter or in the ground station receiver and demultiplexer. The resultant waveform is shown in Figure 3-2-c. It should be remarked that limiting does not theoretically introduce base-band distortion in that all base-band information

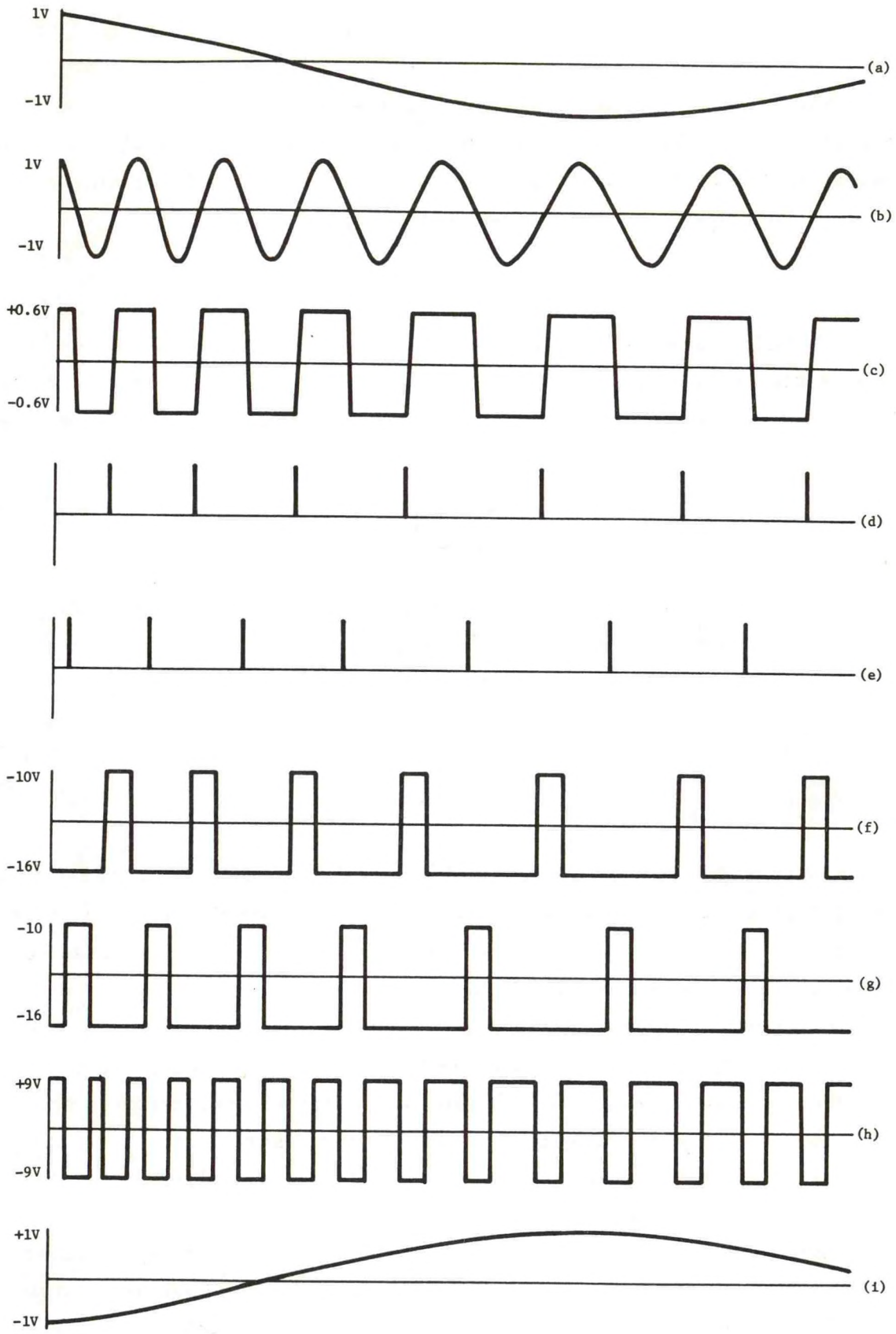
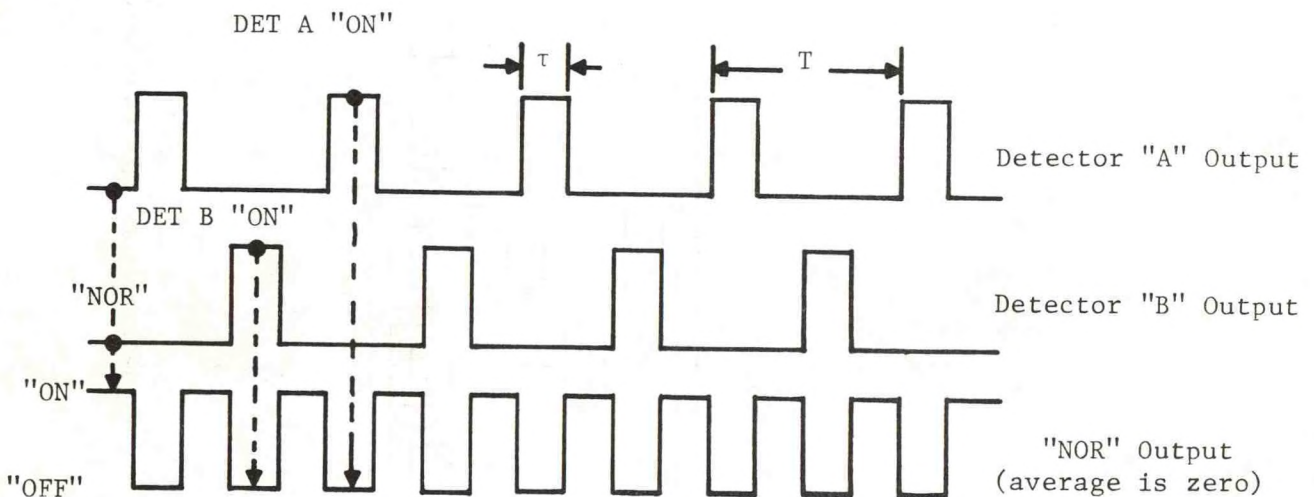


Figure 3-2. Basic Discriminator Operation - Waveforms.

is contained in the zero-crossings of the frequency modulated subcarrier. These crossings are accurately preserved in the process of limiting.

The limited subcarrier is then fed to a Schmitt Trigger for purposes of detecting the aforementioned zero crossings. The Schmitt Trigger outputs a pulse each time the limited waveform passes through zero. A separate pulse is output depending on whether the zero crossing was positive going or negative going. The upcrossings are indicated in Figure 3-2-d and the downcrossings in Figure 3-2-e. The upcrossings are fed to detector "A" and the downcrossings to detector "B" where the pulses are "stretched" to have a width which is one-fourth the period of the unmodulated subcarrier. This choice of pulse width is not arbitrary. It results from the constraints that an unmodulated subcarrier will provide zero at the output of the demodulator and that one of the effects of the "NOR" is to act as a frequency doubler. Figure 3-3 indicates the relationship between the subcarrier period and pulse width in the unmodulated situation. (This figure will be more informative if referred to again following the discussion of the "NOR" circuit and low pass output filter.)



T is period of the subcarrier

τ is the detector pulse width ($= T/4$)

Figure 3-3. Constraints on Detector Pulse Width.

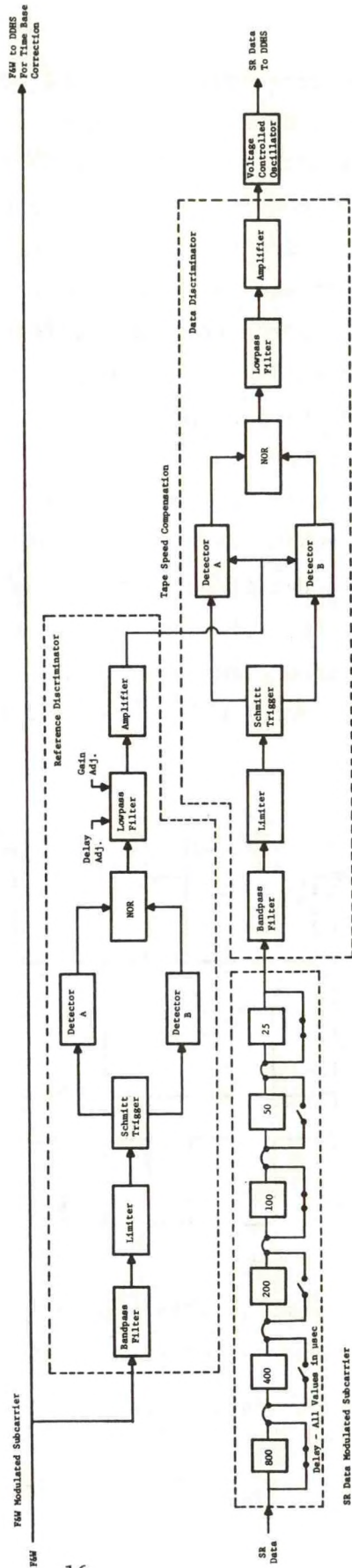


Figure 3-4. Z-Axis Rack Compensation Technique.

The outputs of detectors "A" and "B" are shown in Figures 3-2-f and 3-2-g, respectively.

The stretched pulses are fed to the "NOR" circuit. This circuit produces an "ON" condition if there is a pulse from neither detector "A" nor detector "B" as shown in Figure 3-2-h. Notice that the time the waveform spends in the "ON" condition varies with time while the time spent in the "OFF" condition does not. This waveform when low-pass filtered (i.e. averaged) will produce the waveform shown in Figure 3-2-i. Notice that the original base-band signal is recovered exactly except for a change in polarity. The polarity is reversed in the output amplifier.

3.2 Flutter Compensation Technique

The effect of tape speed error on the spacecraft tape recorder is to shift the data sub-carrier frequency to a higher frequency when the recorder is running faster than nominal and to a lower frequency when the tape recorder is running slower than nominal. Since flutter is a time varying error in recorder speed, its effect is to deviate the carrier from nominal in some time varying fashion. This is equivalent to frequency modulating the sub-carrier with the flutter variations. By recording an unmodulated sub-carrier on a separate track on the tape recorder, a flutter only signal may be recovered upon playback for use in correcting the flutter corrupted data subcarrier.

A detailed block diagram of the correction scheme is shown in Figure 3-4. Further design details may be found in ref. 3, but have been omitted here as they do not substantially contribute to the theory of operation of the compensation technique. The basic theory behind the technique is to translate the flutter only signal to baseband (demodulate the subcarrier) by means of a "reference" discriminator. This signal is then used to vary the pulse width in the data discriminator detectors. When the "NOR" output is subsequently integrated (in the low-pass output filter), the result is as if no flutter had been present.

Figure 3-5 indicates the "NOR" output waveforms for the uncompensated and compensated situations. Figure 3-5-a shows the uncompensated case as was also seen in Figure 3-2. Notice that in the "OFF" state (-9v), the duration per cycle is constant due to a pulse being present with nominal width.

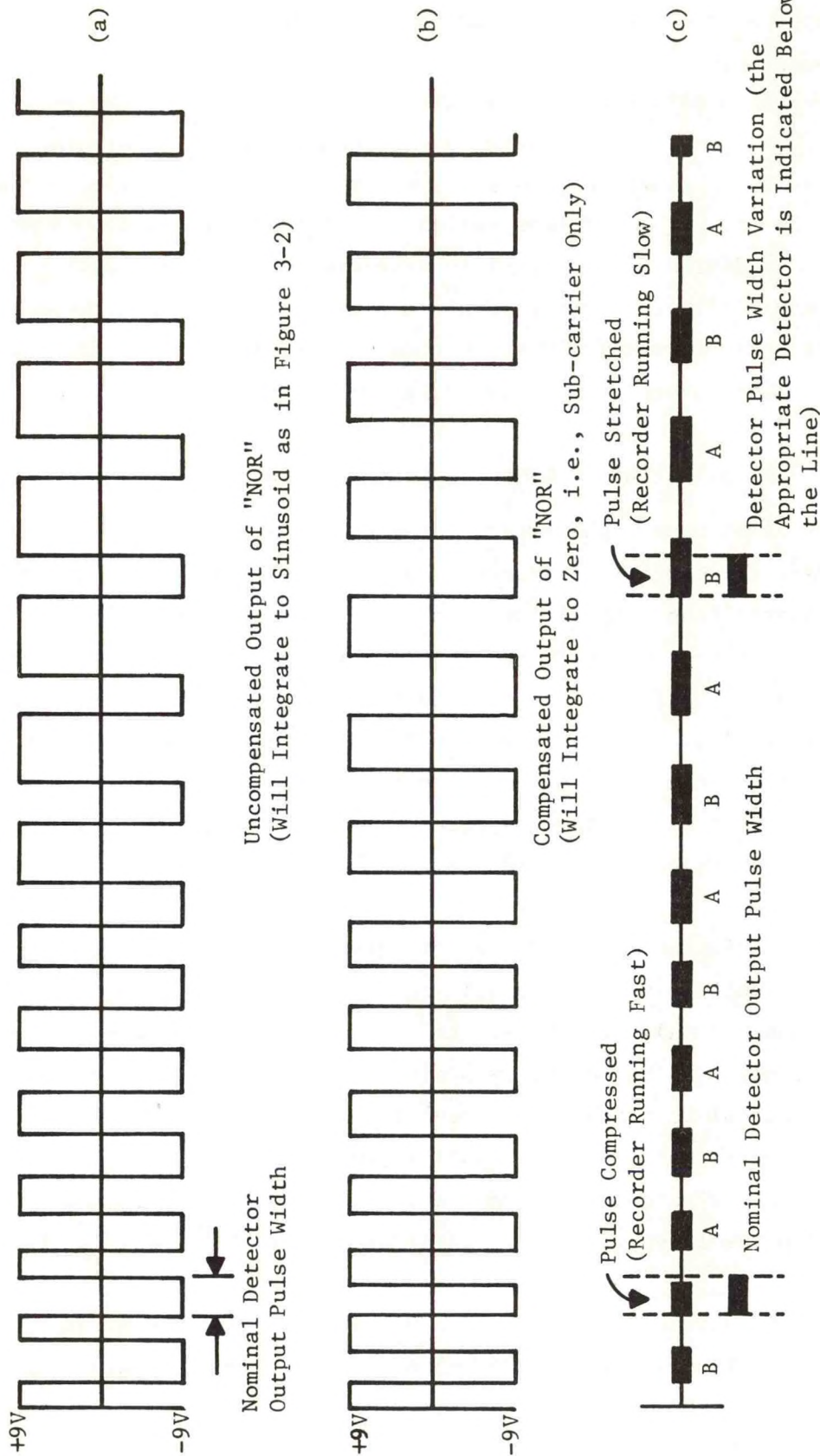


Figure 3-5. Compensation of Flutter only Condition.

In Figure 3-5-b is shown the output of the "NOR" after the detector pulse widths have been modified. For the case where the recorder is running faster than nominal, the pulse width is compressed while when the recorder is running slower than nominal, the pulse width is expanded. Note that although the frequency of the resultant waveform varies as a function of the flutter, the output of the low-pass filter (an integrator) will be zero indicating that the flutter effect has been removed. It should be emphasized that the present discussion is concerned with a flutter only situation. In the presence of joint flutter and data information, only the flutter components are (theoretically) affected; the data are preserved intact.

At this point it is logical to discuss the prominent features of rack alignment as they relate to overall performance. The salient features of interest here are, 1) the scaling between the reference discriminator output and the extent of detector pulse width modification, and 2) the phase (or time) synchronization between the reference discriminator output and the detector outputs in the data discriminator.

With regard to the reference discriminator output scaling, consider the compensated data channel detector output pulse width to be represented by

$$T_{\text{nominal}} + K \cdot V_{\text{flutter}}(t)$$

where T_{nominal} is (as has been previously discussed) constrained to be one-fourth the sub-carrier period and $V_{\text{flutter}}(t)$ is the output voltage of the low-pass filter in the reference channel. The parameter "K" is then the scaling required to match this voltage to the correct percentage expansion and compression of the detector output pulses in the data channel to effectively remove the flutter. If "K" is zero, no compensation has taken place. On the other hand if "K" is less than the correct value, insufficient compensation will occur. Further, if "K" is greater than the correct value, the data channel will be overcompensated and the flutter components enhanced. This behavior can be viewed as linear up to a saturation point where the stretched pulses begin to overlap or the compressed pulses begin to vanish. (This saturation effect was not considered during the study as this situation is considered non-normal.)

Temporal synchronization is required as a result of two features in the ITOS SR data processing channel. First, the flutter and data signals are

modulated on different subcarrier frequencies in the multiplex scheme and thus have different transport times through the MUX/DEMUX electronics. Second, the flutter baseband signal is obtained after the low-pass filter and amplifier in the reference channel discriminator and used to modify the data channel discriminator at the detector circuits. Thus the transport delay(s) of the "NOR", low-pass filter, and output amplifier of the reference discriminator must be incorporated. The majority of the synchronization is achieved by delaying the data channel prior to demodulation. A secondary adjustment is available in the reference discriminator. However, it appears to be a phase adjustment only and thus does not possess the range of the main delay. In order to effect proper cancellation, the time delay is adjusted to synchronize the reference channel and the data channel. In the event that the two channels become phased 180° with respect to each other, a flutter enhancement occurs instead of cancellation. The extent of misalignment to cause enhancement is not considered likely at the ITOS identified flutter frequencies but could be significant if higher flutter frequencies were encountered.

4.0 MODEL DESCRIPTION

The basic approach to the model is that of a time domain simulation rather than development of a numerical treatment of theoretical transfer functions. This is largely the result of the non-linear functions encountered in the limiter, Schmitt Trigger, detectors, and the "NOR" circuits. The only exceptions to this design philosophy are the input band-pass filters and the lowpass output filters, where the frequency domain transfer functions were analytically specified and Fourier-transform, multiplication, inverse transform techniques were employed to avoid time-consuming numerical convolutions. Figure 4-1 shows an overall block diagram of the model implementation. The various approaches to each of the functional blocks are described in the following paragraphs. Table 4-1 indicates the parameter options incorporated into the model.

4.1 Reference Channel

The reference channel subcarrier frequency (f_0) is set at 6.25 Hz in order to be compatible with ITOS-D at 4:1 playback. The deviation index was selected to be $\pm 15\%$ about this. The input band-pass filter was modeled about these parameters. Initially a theoretical complex frequency plane description for the filter transfer function was attempted but was rejected due to design complexity, and an ideal (rectangular amplitude and linear phase response) filter substituted. This has the effect of producing better transmission characteristics within the band-pass but introduces possible distortion as the base-band information contained in the higher order sidebands of the modulated subcarrier is rejected. This is considered to be negligible for the tone modulation used in the analysis.

The input amplifier, limiter, and cascade amplifier parameters were selected to be compatible with the EMR discriminator described in ref. 3-1.

The Schmitt Trigger (zero crossing detector) was forced to trigger on a threshold of +1 mv for upcrossings and -1 mv for downcrossings to account for quantization noise contained in the (model) digitized frequency modulated subcarrier. A distinct deviation from the EMR discriminator design was the substitution of +9 volt level for an "on" condition and a -9 volt level for an "off" condition in the pulse stretching detectors (normal levels are -10 volts for "on" and -16 volts for "off"). This deviation resulted from a requirement to change pulse height instead of width in the compensation scheme in order to achieve

Z-Axis Rack Model Configuration

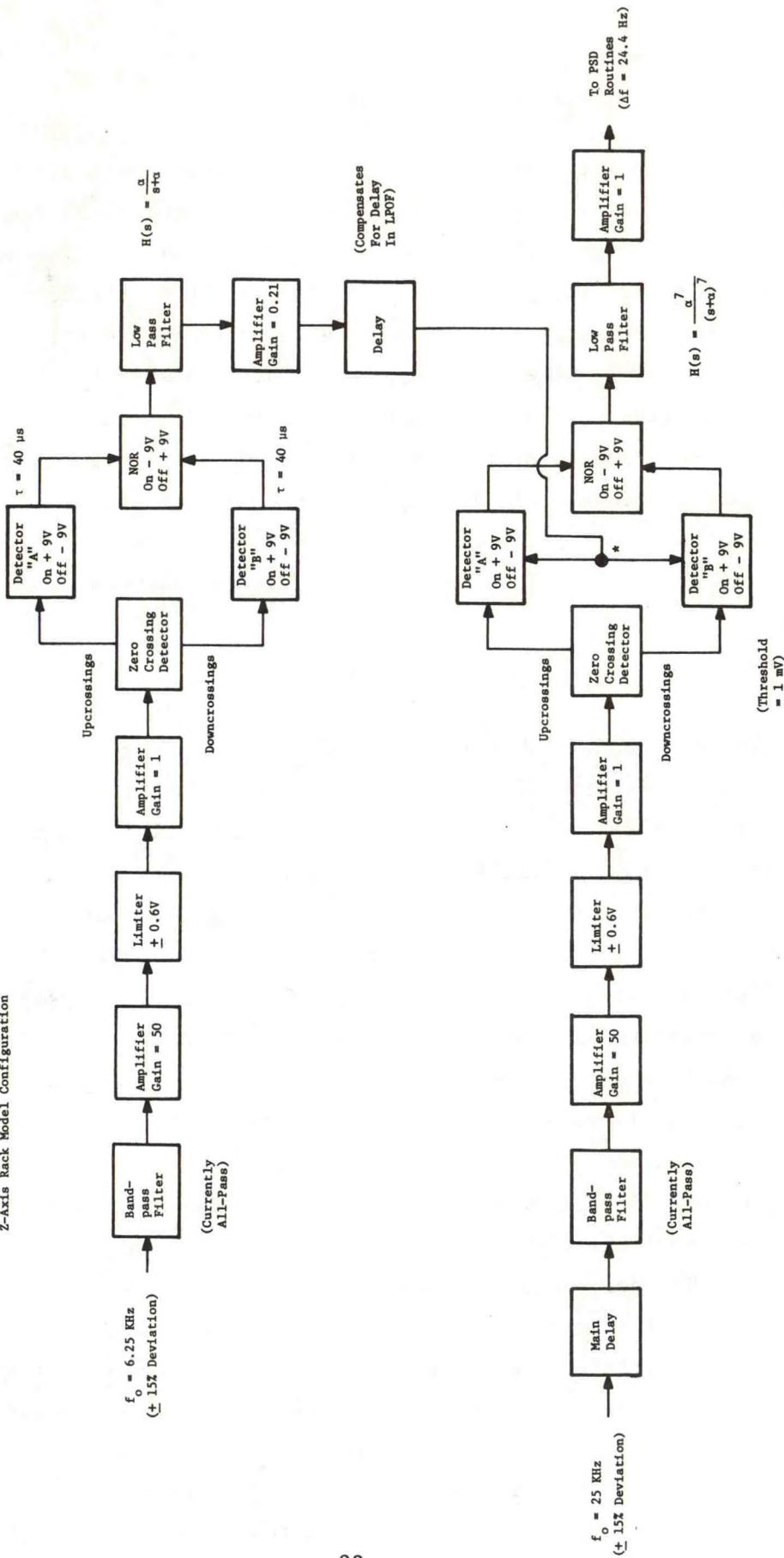


Figure 4-1. Overall Block Diagram of Model Implementation.

TABLE 4-1. PARAMETER OPTIONS

1. Transfer function of band-pass filter(s)
2. Input gain of limiter(s)
3. Clipping level
4. Output gain of limiter(s)
5. Inherent delay of limiter
6. Threshold of Schmitt Trigger(s)
7. Inherent delay of Schmitt Trigger
8. Pulse width scaling of detector (data only)
9. Pulse width of detectors
10. Output amplitude of detectors for "ON" condition ("ON" is pulse)
11. Output amplitude of detectors for "OFF" condition ("OFF" is no pulse)
12. Inherent delay of detectors
13. Output amplitude of "NOR" for "ON" condition
14. Output amplitude of "NOR" for "OFF" condition
15. Inherent delay of "NOR"
16. Transition voltage of "NOR"
17. Transfer function of low-pass filter(s)
18. Gain of output amplifier(s)
19. Main delay (error)

finer resolution (i.e., each pulse width represents a small finite number of words in the algorithm, thus a small amount of width compensation would be absorbed in time base quantization effects). The "NOR" circuit was modeled as a logical equivalent of the EMR circuitry with the specified levels of ± 9 volts. Notice that the utilization of a "NOR" has the effect of doubling the subcarrier frequency and phase inverting the output signal (see section 3.0).

The output low-pass filter was modeled in the complex frequency domain and transform-inverse transform techniques employed. The filter has a 6 db/octave roll-off and serves to integrate the output of the "NOR" circuit and to attenuate the contribution of the doubled subcarrier frequency.

The gain of the output amplifier was determined empirically for a single tone (see Section 5.0) and the polarity chosen to compensate for the phase inversion of the "NOR" circuit. Insofar as the amplifier is linear over its operating region the use of a single tone to determine the gain is justified.

An additional "delay" was incorporated into the model at the output of the reference discriminator to advance the reference signal with respect to the data subcarrier due to the delays encountered in the reference channel input bandpass filter and lowpass output filter. This would normally be achieved in the main delay in the data channel; however, in order to preserve the latter delay as a main delay "error", it was introduced at this point in the model.

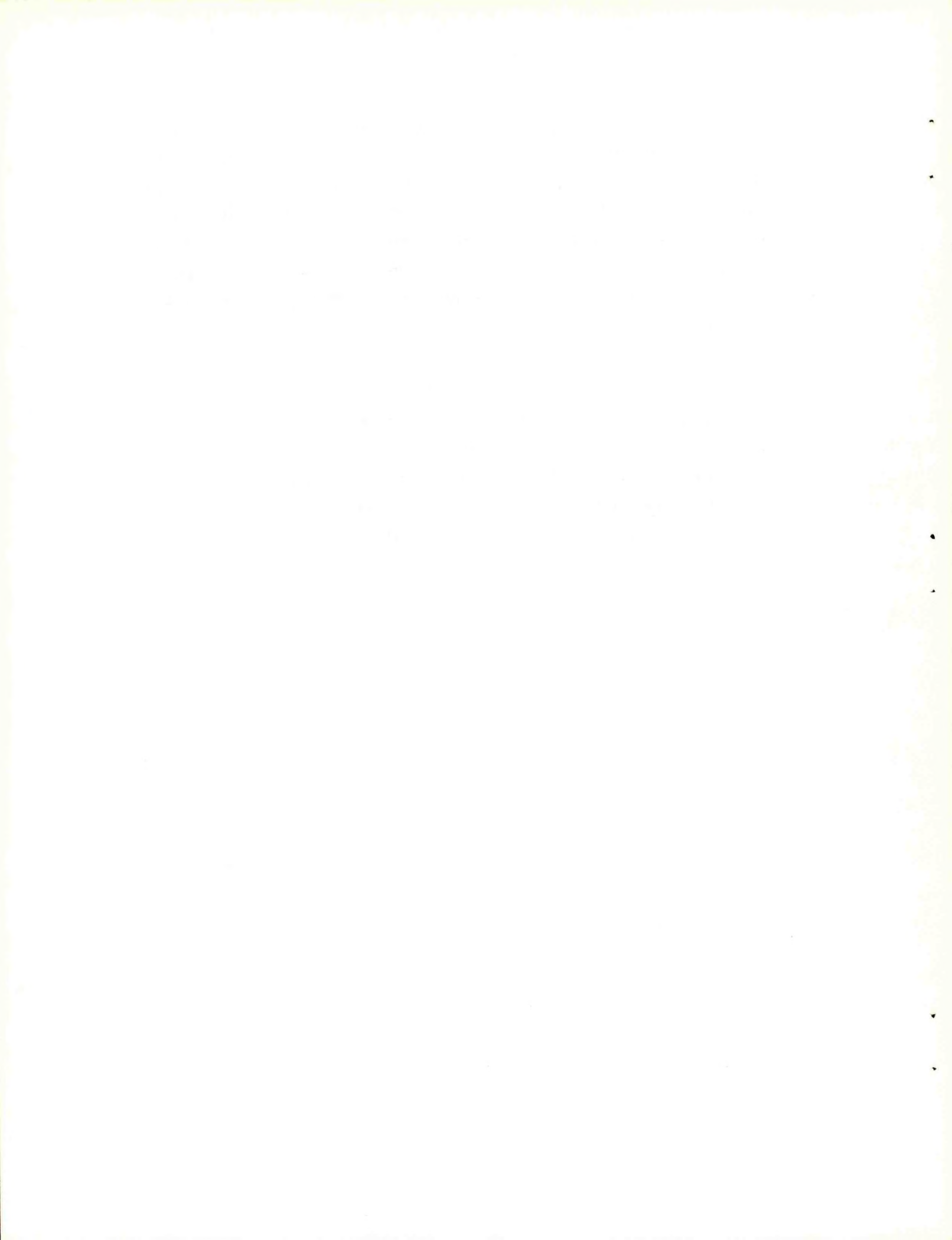
4.2 Data Channel

The data discriminator is modeled essentially in the same manner as the reference discriminator with the following exceptions. First, the data channel subcarrier was shifted to 25 KHz instead of 22 KHz utilized in the hardware. This was necessitated by the requirement that the detector output pulse width be one-fourth the period of the subcarrier frequency and the requirement that this time span occupy an integer number of words in the computer algorithm. Since the percentage deviation remained at $\pm 15\%$, this does not reflect any significant restriction on the model capability. Second, since the base-band signals and subsequently modulated subcarriers are generated within the algorithm, they are initially in phase and the requirement for a main delay per se does not exist. The main delay actually incorporated into the model

represents a delay "error" and is more meaningful in terms of overall rack operation. Third, the low-pass output filter was modeled (again in the complex frequency domain) as a seven pole passive filter with a roll-off of 42 dB per octave. This closely approximates the 40 dB/octave EMR specification. Fourth, the gain of the output amplifier was taken to be unity for convenience. This does not represent any compromise on model performance insofar as the areas of interest are represented by relative rather than absolute results.

4.3 Analysis Technique

The technique used for analysis of the results obtained from the model consisted primarily of the examination of flutter residuals and the sporadic harmonic behavior due to modulation non-linearities in the spectral domain. A sample output is shown in Appendix C. Additional comments regarding the specific analyses conducted are contained in the following section.



5.0 SENSITIVITIES DERIVED FROM MODEL

The model was exercised parametrically to determine sensitivity to significant parameters. While the capability exists to analyse each of the parameters listed in Table 4-1, this study concentrated on the main delay and reference discriminator output gain settings. The reasoning behind this choice is twofold: one, the other parameters are considered to provide second order effects and, two, these two parameters represent critical adjustments in the z-axis rack alignment. These two parameters were initially tested by observing the degree of cancellation of a single tone imposed on both the data and flutter channels. Subsequently, analyses were conducted with multiple tones and random noise backgrounds.

Figure 5-1 shows the flutter residual after cancellation of a 1.2 count* tone at 196 Hz as a function of delay error in micro-seconds. A change in delay of 12.5 μ sec would produce a change in flutter residual of approximately 0.02 counts at this frequency, representing a change slightly in excess of 1.5%. Since 25 μ sec is the resolution of the delay line, it would appear that the ability to achieve the proper delay is available (i.e., $\pm 12.5 \mu$ sec) providing the required total delay is within the range of the delay line (1575 μ sec). Notice that since what is being affected in the compensation is a cancellation effect, as the tone frequency increases, the apparent total phase change due to 12.5 μ sec error also increases. At 800 Hz (approximately the highest flutter frequency identified on ITOS-D), 12.5 μ sec would produce a phase change equivalent to 50 μ sec at 200 Hz. From Figure 5-1, one can roughly anticipate a flutter residual of 0.08 counts or about 6% of peak. Thus based on pure tone cancellation, the delay line adjustment resolution is adequate for z-axis operation. It will be seen later that the non-linearities associated with the modulation technique make the establishment of the proper delay setting difficult in an operational environment.

*The term "count" represents the output of an eight-bit digitizer at DDHS which encodes the dynamic range of the sensor into a range of 256 levels. Strict details of this encoding are omitted here. It is sufficient to remark that low count values represent high temperatures while high count values represent low temperatures. Two counts are roughly equivalent to one degree Kelvin at the warm end and this scale factor is fairly linear over the temperature range of interest.

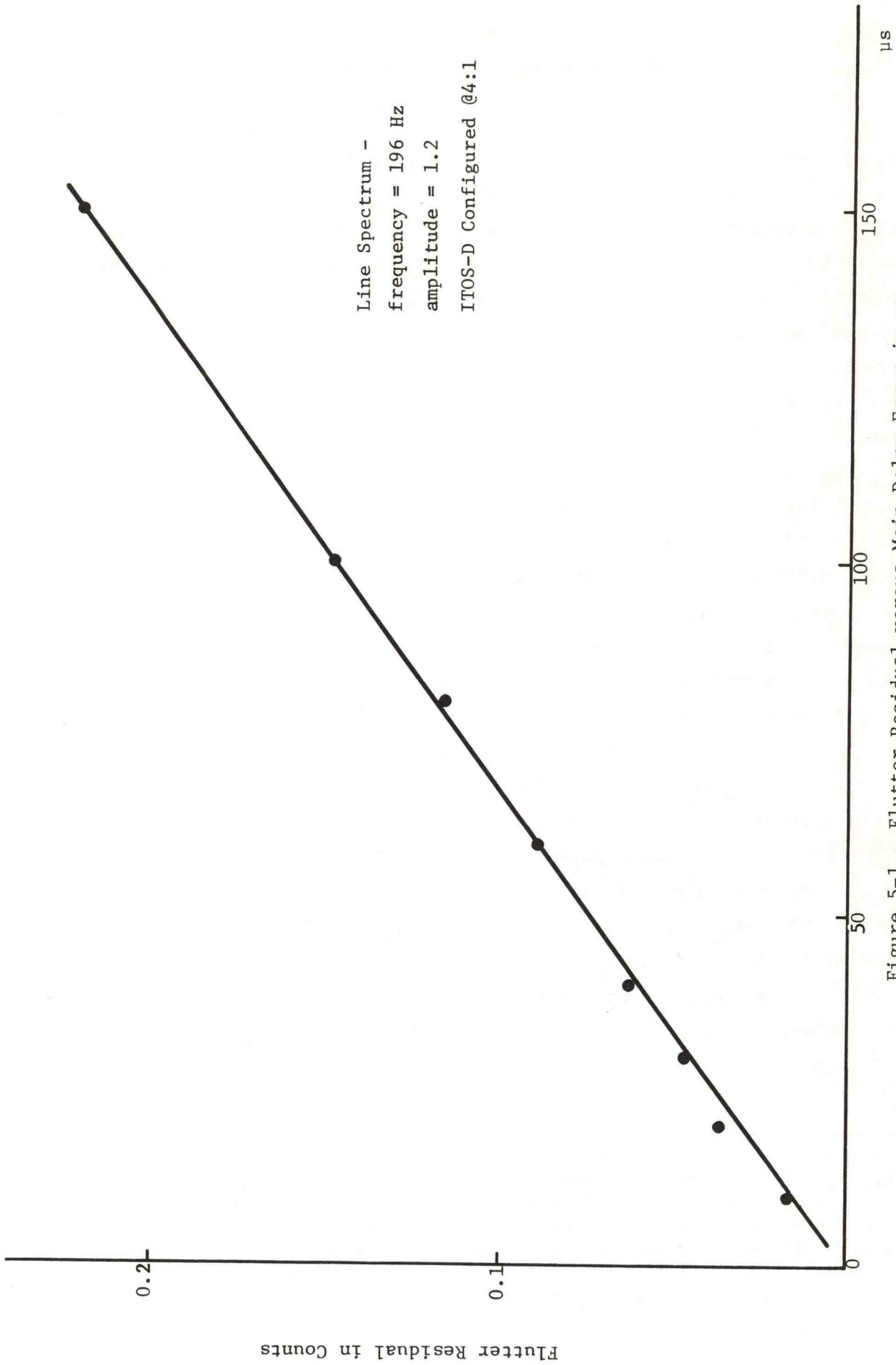


Figure 5-1. Flutter Residual versus Main Delay Error in μs .

Figure 5-2 indicates the sensitivity of flutter residual as a function of reference discriminator output gain. Notice that zero gain represents no compensation and the original tone amplitude of 1.2 counts is preserved. In the range of zero to -0.21 the data channel is undercompensated while in the range of -0.21 to -0.6 overcompensation occurs. The gain is negative in sign to account for the inversion which occurs in the "NOR" circuit as described in Section 3.0. In the actual hardware this is achieved in the output amplifier while in the model it is achieved mathematically as the sign on the value input for the gain parameter. It should be noted that the absolute value of gain was derived empirically in order to effect model performance and may not reflect the actual hardware gain of the output amplifier. The value is indicative of relative behavior. No attempt was made to examine the saturation effect described in Section 3.0. As in the case of the delay setting, it will be shown later that an optimum gain setting will be difficult to achieve in an operational situation.

Table 5-1 shows the effect of modulating the data and flutter channels with four tones nominally identified to have the same frequency and amplitude as ITOS-D flutter components, and subsequently observing rack operation as the main delay is perturbed from its nominal setting. Notice the tone at 782 Hz deteriorates back to the no compensation condition more rapidly than lower frequencies. This is caused by a given delay representing a larger phase error at the higher frequencies. As a result, the no-compensation and flutter enhancement situations are reached sooner at the higher frequency tones. Notice that this behavior is similarly observed for tones at 102 Hz and 417 Hz. Note that a contrary effect is observed for the tone at 156 Hz where a delay error actually improves the rack performance until an error of 100 μ s is reached. This is considered to be due to the fact that due to the significant difference in tone amplitude, the tone is spectrally distributed differently and that in effect the non-linearity of the modulation technique has produced a phenomenon wherein the rack would appear to be exceeding the theoretical single tone performance. It should be commented that this type of data interaction was found to be prevalent in all multiple tone analyses. It is this type of behavior which causes the actual hardware to be difficult to align operationally.

Table 5-2 indicates the effect of varying the reference discriminator gain on the rack performance with the four tones described in the previous paragraph. Notice that the phenomenon of data interdependence is much more

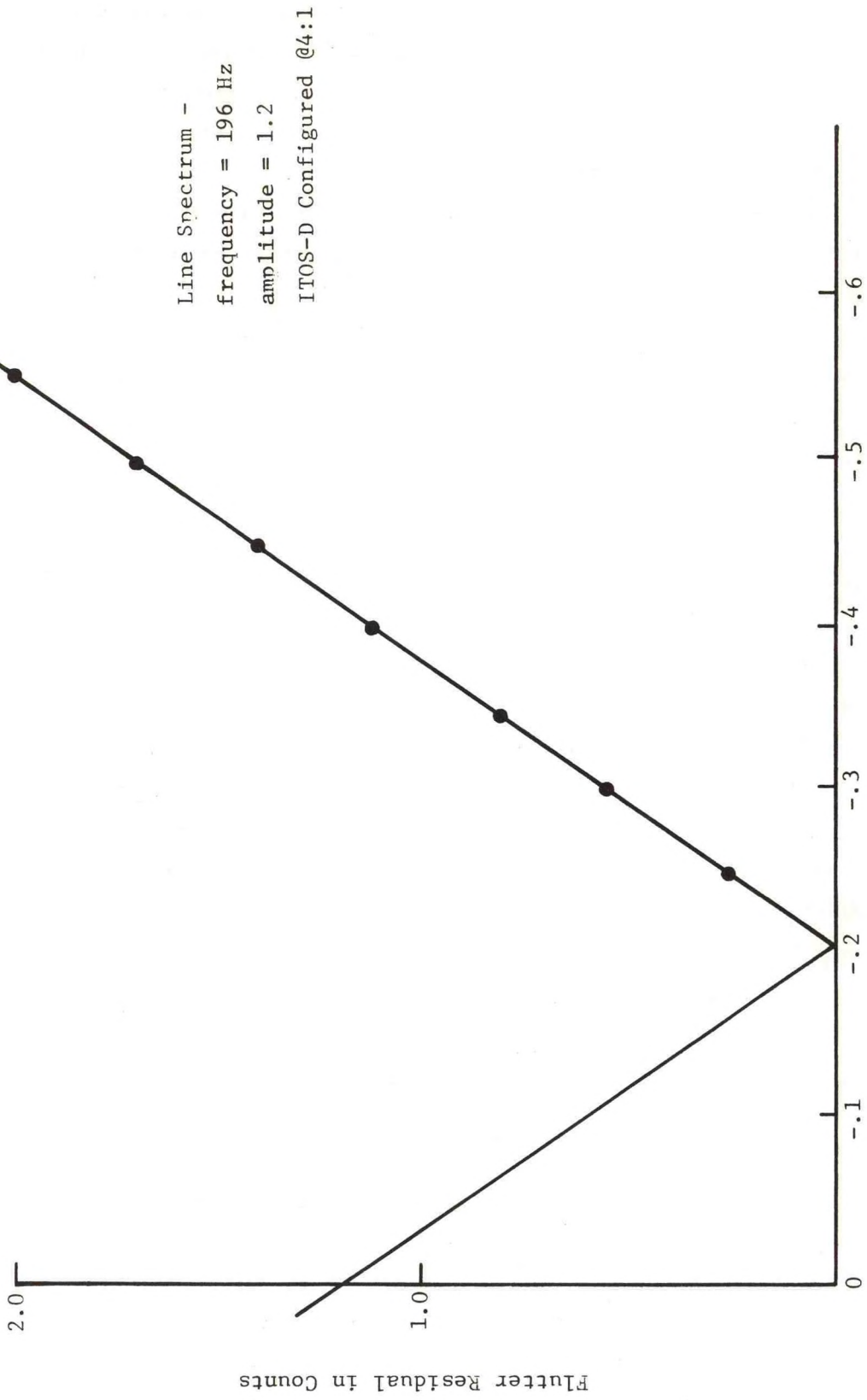


Figure 5-2. Flutter Residual versus (Model) Ref. Disc. Output Gain.

TABLE 5-1. TONES ON DATA AND FLUTTER CHANNELS - DELAY ERROR EFFECT
ITOS-D CONFIGURED AT 4:1

<u>Delay Error μs</u>	<u>102 Hz</u>	<u>156 Hz</u>	<u>417 Hz</u>	<u>782 Hz</u>
No Compensation	0.439	0.109	0.763	0.370
0	0.020	0.011	0.017	0.081
10	0.021	0.018	0.028	0.086
20	0.022	0.018	0.041	0.087
30	0.024	0.009	0.055	0.082
40	0.026	0.007	0.075	0.089
60	0.031	0.004	0.115	0.110
80	0.036	0.002	0.153	0.135
100	0.041	0.001	0.192	0.162
150	0.052	0.009	0.290	0.234
200	0.070	0.007	0.388	0.308

Values for no-compensation represent flutter tone amplitude in counts. The other values represent flutter residual in counts.

TABLE 5-2. TONES ON DATA AND FLUTTER CHANNELS - GAIN ADJUSTMENT EFFECT

<u>Gain*</u>	<u>102 Hz</u>	<u>156 Hz</u>	<u>417 Hz</u>	<u>782 Hz</u>
No compensation	0.476	.112	.780	.379
-0.17	.070	.011	.191	.133
-0.18	.047	<u>.010</u>	.157	.119
-0.19	.024	.012	.122	.105
-0.20	<u>.014</u>	.017	.088	.091
-0.21	.030	.022	.053	.078
-0.22	.053	.028	.021	.065
-0.23	.076	.034	<u>.020</u>	.054
-0.24	.100	.040	.053	.044
-0.25	.124	.047	.087	.038
-0.26	.147	.053	.121	<u>.037</u>

Values for no compensation represent flutter tone amplitude in counts. The other values represent flutter residual in counts.

*The values of gain are model dependent and should be interpreted only in a relative sense.

radical here as evidenced by the (underlined) gain at which each tone is most effectively cancelled. In this case it is virtually impossible to define an optimum setting. Note that the various values tend to cluster around the -0.21 value obtained for the single tone at 196 Hz shown in Figure 5-2.

In view of the fact that the delay and gain adjustments are set simultaneously in an operational situation, the difficulty in identifying an optimum setting for delay and gain is further emphasized. In the model case, the situation is somewhat simplified in that the frequency modulated signals are initially in time synchronization. The only differential delay up to the point of compensation is due to the input band-pass filters of the reference and data discriminators. Since these have been modeled as ideal filters with linear phase response, the transit delay may be calculated exactly (the delay is given by the slope of the phase response). Thus in the model, lack of knowledge about the delay setting does not influence the gain setting analysis. However, in the hardware situation, the alignment resorts to an iterative process. It has been observed in actual testing that the main delay setting is the better initial parameter to adjust in achieving the final alignment.

Table 5-3 indicates an analysis where no tone modulation was applied to either the flutter or data sub-carriers and noise alone imposed on the flutter sub-carrier only. The intent here was to demonstrate the fact that noise on the flutter channel would result in increased noise level on the data channel output via the flutter compensation technique. The notation is defined as follows:

σ_{NC}^2 = the noise variance of the data channel output with no compensation

σ_C^2 = the noise variance of the data channel output with compensation

σ_n^2 = the contribution of noise in the data channel output due to noise on the flutter channel.

The data channel output has an apparent noise output due to quantization effects in the digital model. The important parameter to view here is σ_n^2 as a function of the bandwidth of the low-pass output filter on the reference discriminator. As would be expected, as the bandwidth is reduced, the noise variance reduces nearly proportionately.

Table 5-3. Noise on Flutter Channel - White, Uniform Dist., $\sigma^2 = 0.11$.

Bandwidth of low-pass output filter	σ_{NC}^2	σ_C^2	σ_n^2
2 kHz	0.012	0.097	0.085
1 kHz	0.012	0.053	0.041
500 Hz	0.012	0.032	0.020
250 Hz	0.012	0.021	0.009
100 Hz	0.012	0.017	0.005

$$\sigma_n^2 = \sigma_{NC}^2 - \sigma_C^2 \quad (\text{since the noise samples are uncorrelated}).$$

Table 5-4. Noise and Four Tones on Flutter Channel, Four Tones on Data Channel
dB Improvement

Bandwidth of low-pass output filter	102 Hz	156 Hz	417 Hz	782 Hz	σ_C^2
2 kHz	24.0	13.0	49.9	34.0	0.244
1 kHz	22.7	13.2	23.8	14.4	0.197
500 Hz	23.5	20.1	13.4	6.2	0.216
250 Hz	22.0	23.9	5.5	0.3	0.447
100 Hz	12.6	5.8	-1.0	0.0	1.055

$$\sigma_{NC}^2 = 1.119$$

Values represent "dB Improvement" as defined in Appendix C.

Table 5-4 shows the effect of re-instituting the four tones on the data and flutter channels in the presence of a noise background. The values presented here represent "dB improvement" as described in Appendix C. The intent is to show the trade-off of low-pass output filter bandwidth reducing the total noise on the data channel versus flutter cancellation effectiveness. Notice that as the bandwidth is reduced the cancellation ability degrades beginning at the higher tone frequencies as would be expected. The -1.0 "dB improvement" at the 417 Hz tone for a 100 Hz filter is in reality a flutter enhancement and is likely due to the odd spectral distribution of the modulated carrier which gives rise to the data interaction described previously. The 2 KHz filter provides superior cancellation performance to the lower bandwidth filters in all cases. However a reduction to 1 KHz reduces the overall noise variance and still provides acceptable cancellation. This kind of optimization of bandwidth versus performance would be more emphatic if the flutter noise was not white noise but was concentrated about certain flutter harmonics. Figure 5-3 shows the spectral distribution for the first 100 lines (≈ 2440 Hz) of the data channel output for the first three cases in Table 5-4. The flutter tones are indicated by the small diamonds below each plot. Of particular interest here is the behavior of the lines above the filter cut-off. For example, in Figure 5-3-c, wave numbers 90 and 93 have been significantly enhanced even when they are well in excess of the range of compensation. This again points out the strong data interaction due to the spectral distribution of the modulated carrier.

Finally, the effect of changing the roll-off rate of the low-pass output filter was investigated. Figure 5-4 shows the spectrum of Figure 5-3-b as compared with a similar situation where the order of the filter was increased from a single pole (roll-off rate of 6 dB/octave) to a two pole configuration (roll-off rate of 12 dB/octave). As would be expected, the total noise variance of the data channel was reduced from 0.197 to 0.170. This can be seen visually by inspecting Figure 5-4 in the region above the cutoff frequency (1000 Hz). However, notice that the cancellation effectiveness has decreased for the higher roll-off rate (note the increase in amplitude at those wave numbers marked with a diamond below each figure). This would lead one to the conclusion that significant information relative to effective cancellation is contained in wavenumbers greater than the cut-off frequency

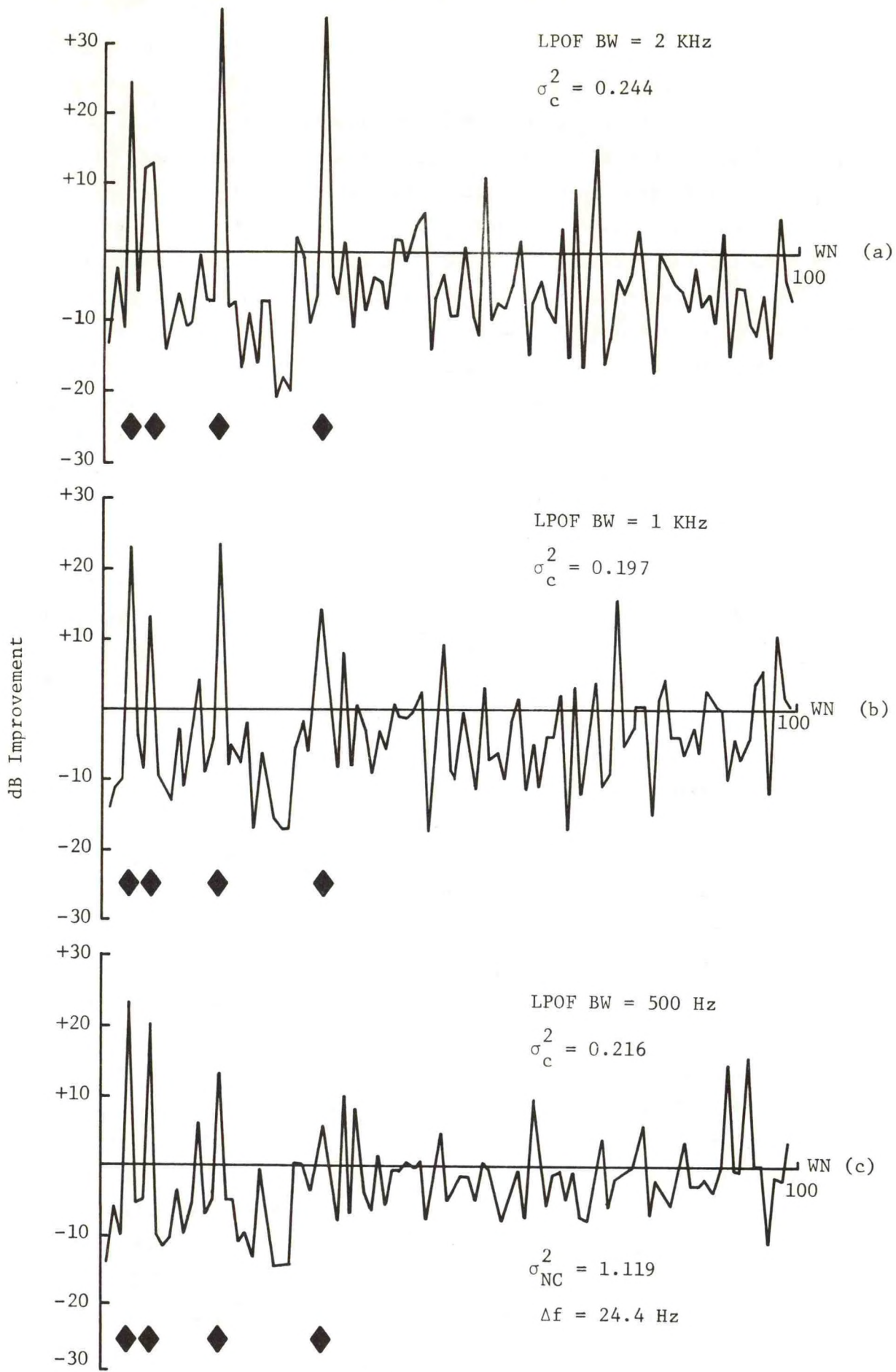


Figure 5-3. Data Channel Output Spectra for First Three Cases Shown in Table 5-4.

and that the lack of this information due to a higher rate of attenuation above cut-off noticeably affects performance.

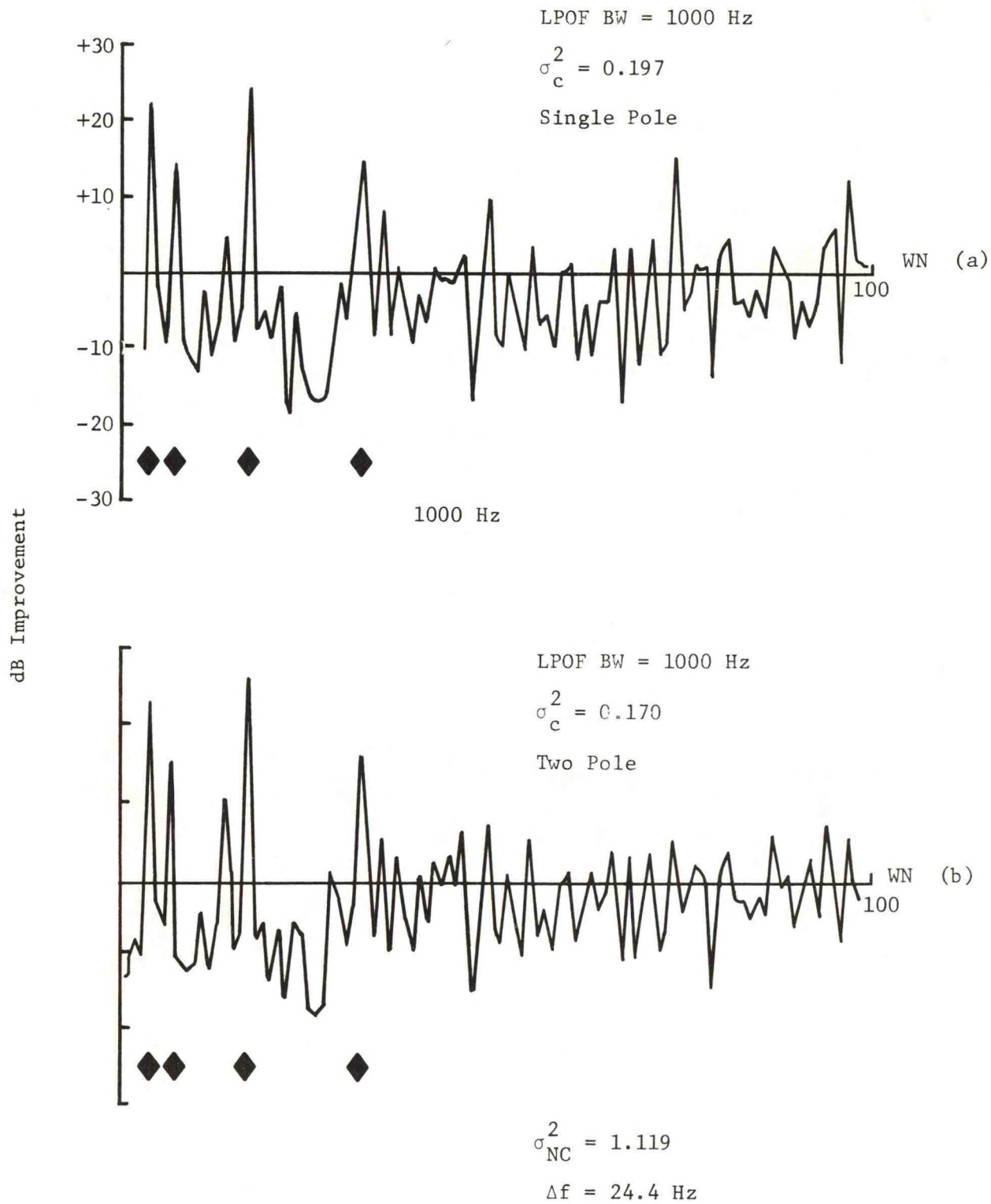
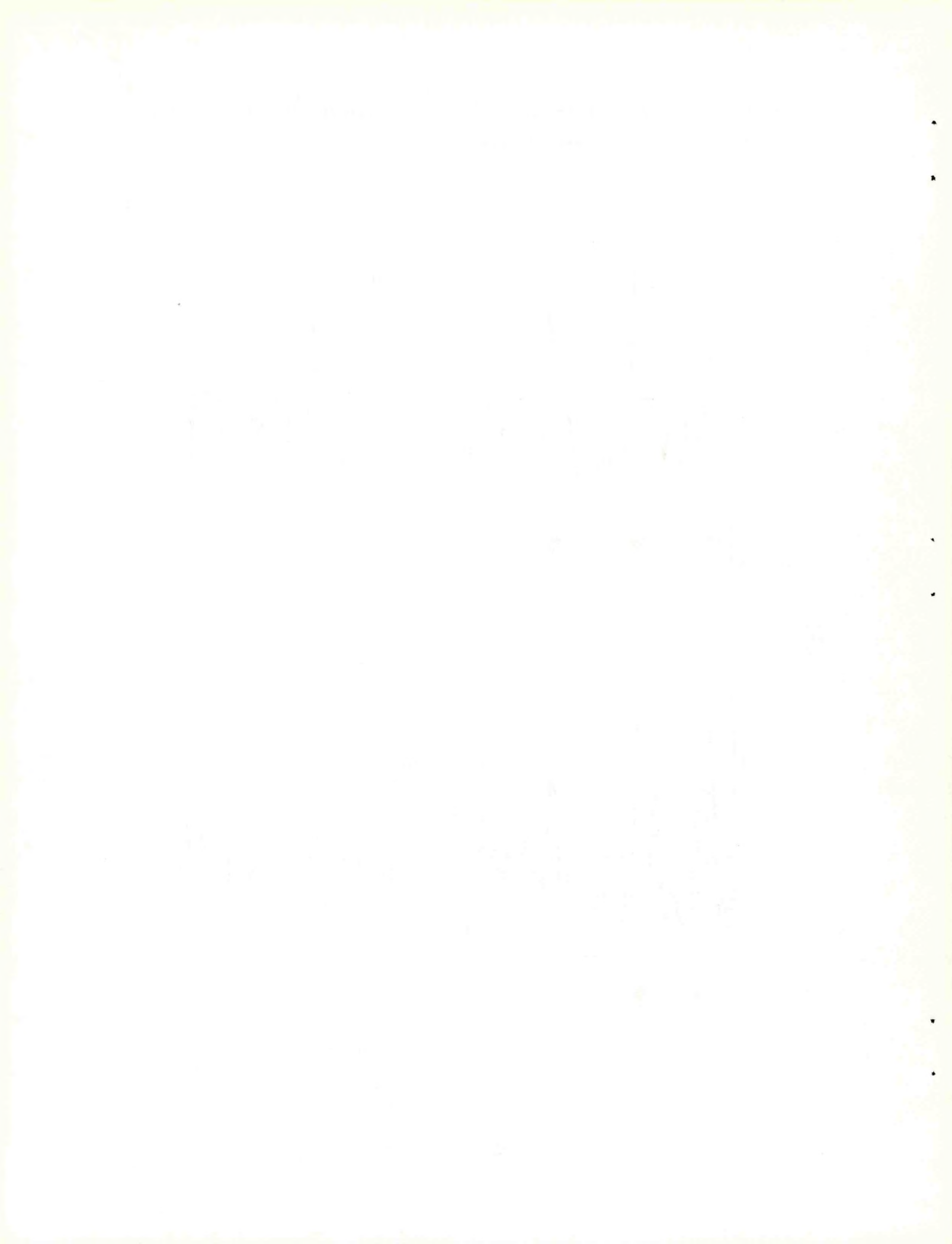


Figure 5-4. Effect of Changing Filter Roll-off.



6.0 PRELIMINARY RECOMMENDATIONS FOR DIAGNOSTIC IMPLEMENTATION

The philosophy of diagnostic implementation on-line at the DDHS is constrained to be a minimum interference technique. On a routine basis it must be rapid, repetitive, and not impose on computer storage requirements. Also, during those ingests where abnormal conditions are suspected, it must be of sufficient detail to be useful in correcting any system fault which may be present. These operational and performance constraints are best met here with an approach to the diagnostic implementation which is adaptive in the degree of detail as a function of the data quality observed.

Figure 6-1 shows a flow diagram of a recommended diagnostic procedure which would accommodate the above philosophy. As a simple measure of performance, an RMS would be computed on the space view each frame during ingest. This value would then be compared with a preset threshold. The threshold would represent the maximum noise level for which average or above average data quality could be assured. In the event the RMS was lower than the threshold, the ingest would continue and the operator advised of a normal condition at the termination of the ingest. In the event the RMS is greater than this threshold, it would be compared to a second (higher) threshold which would represent the maximum RMS noise which would assure the minimum acceptable data quality. If the RMS was lower than this threshold, a 64 sample power spectrum would be computed on the space view. The spectrum would be compared to a stored reference mask to see which flutter harmonics had changed and the result output for analysis. The ingest would continue and the operator advised of marginal data quality at the termination of the ingest. If, on the other hand, the RMS exceeded the maximum acceptable noise level, more detailed spectral analysis would be pursued. It would be ascertained whether nighttime visible data could be obtained within the remaining data to be ingested. If so, then a 1024 sample power spectrum would be computed and output for analysis and the ingest terminated. If not, the ingest would be terminated. The operator would be advised of the status at the termination of the ingest. A decision to reingest would then be made on the status observed and available spectral data.

During the course of the study, the complete diagnostic philosophy was not incorporated for on-line evaluation during ingest. However, an initial diagnostic configuration was developed and provided to NESS personnel for

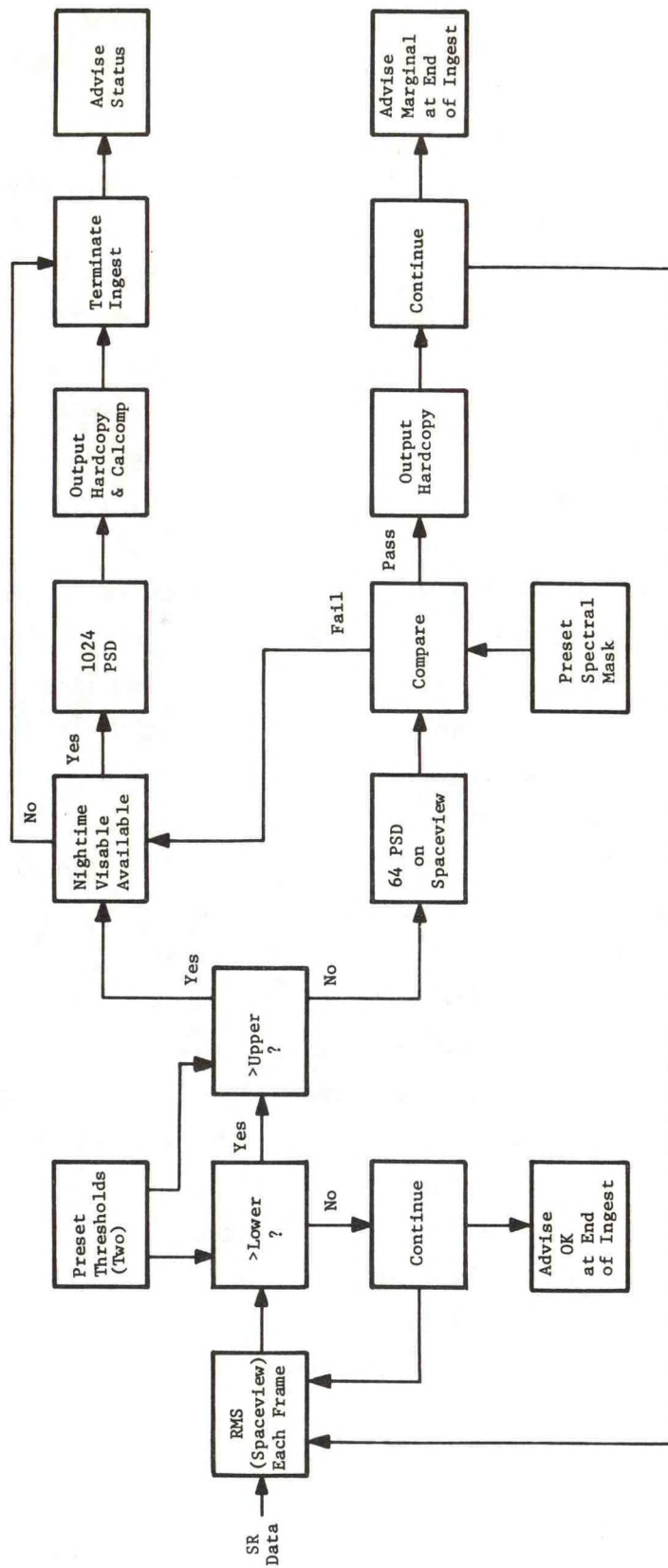
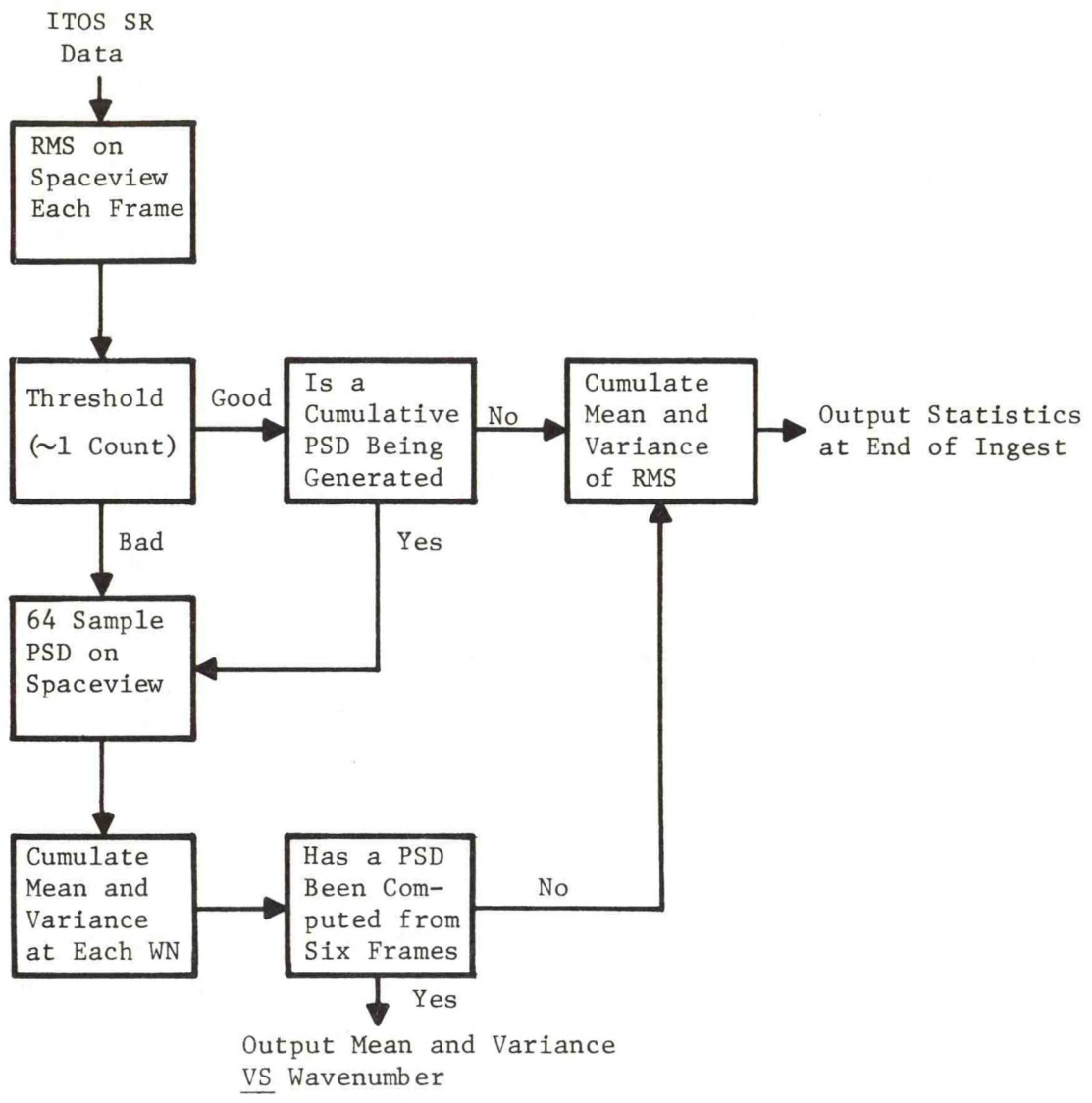


Figure 6-1. Preliminary Diagnostic Logic Flow Diagram.

preliminary simulation testing on the CDC 6600 at Suitland. The key elements of this configuration are shown in Figure 6-2. It is the intent of this type of approach to structure the final diagnostic configuration dynamically in order to maintain compatibility with system changes at NESS. In particular, it was not clear at the time of the conception of this configuration whether night-time visible data would be available, thus it has been deleted from the structure in such a way as to be included later if available.

The concept of performing a 64 sample power spectrum was given special attention in deriving the configuration shown. An analysis was performed to indicate the improvement in spectral stability which could be achieved by averaging. A vector of 1024 random samples with a flat spectrum was generated and its spectrum computed. This spectrum was then condensed to an equivalent 64 sample spectrum by summing the energy over groups of 16 wavenumbers. This result indicated a very flat spectrum as would be expected. The original 1024 sample data vector was then segmented into 16 independent 64-sample data sets and a spectrum computed for each. The results indicated these small sample spectra to be statistically unstable (i.e., flatness was not achieved). A cumulative average was then performed for the small sample spectra to determine the minimum number of spectra which could be averaged in order to reach a stable statistic. The average value at each wavenumber was computed with the number of spectra incorporated varying from 2 to 16. An apparently stable statistic was achieved at a minimum of six individual spectra. This cumulative average was then incorporated into the diagnostic logic.

The configuration shown in Figure 6-2 thus represents the basic cornerstone of the logic to achieve the final goal of stable compensation. It can be expanded and revised in accordance with ground system and satellite changes.

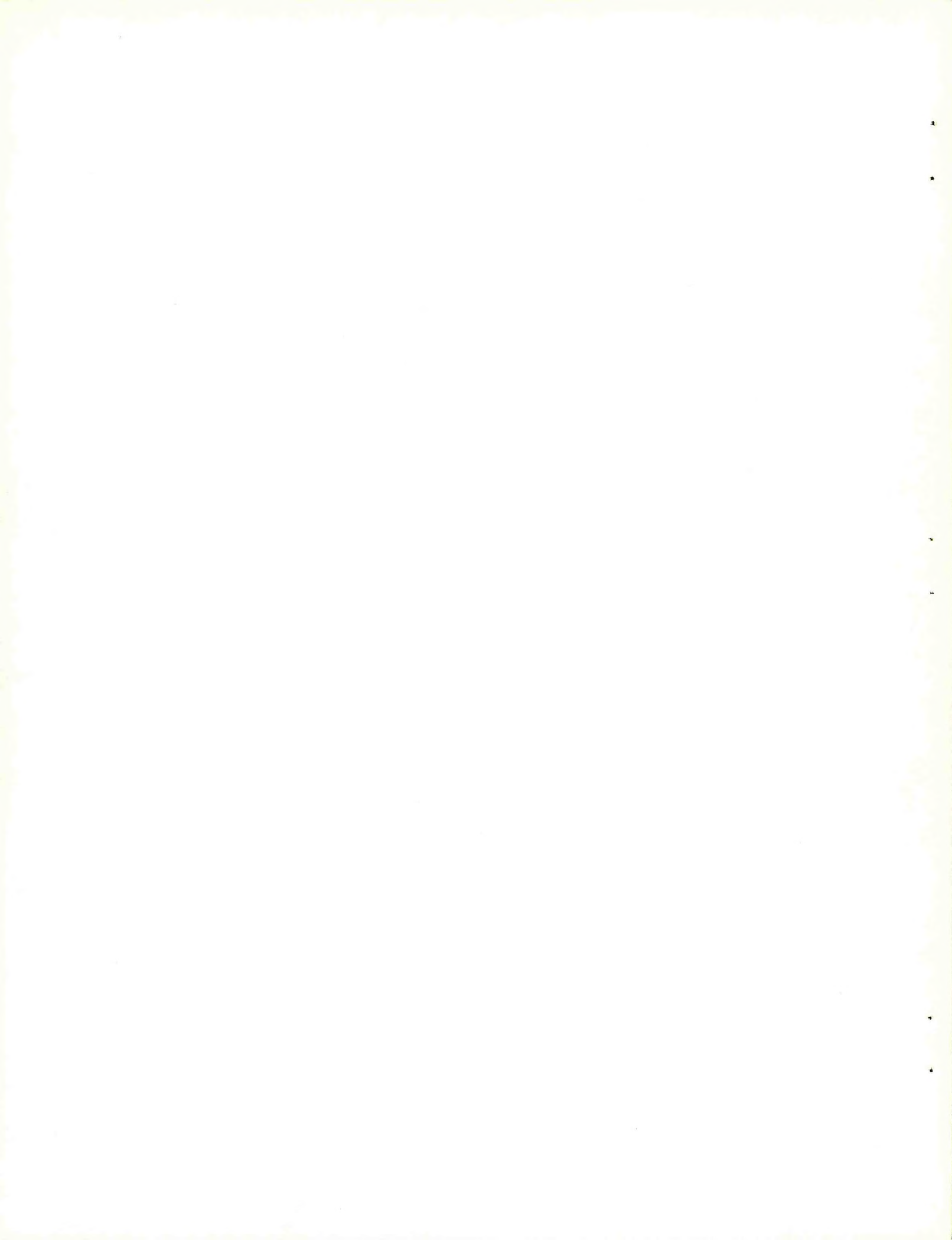


Note: Need to be sure not to compute PSD on all frames (i.e., upper threshold has not been incorporated) in the case of bad data.

Figure 6-2. Initial Diagnostic Configuration.

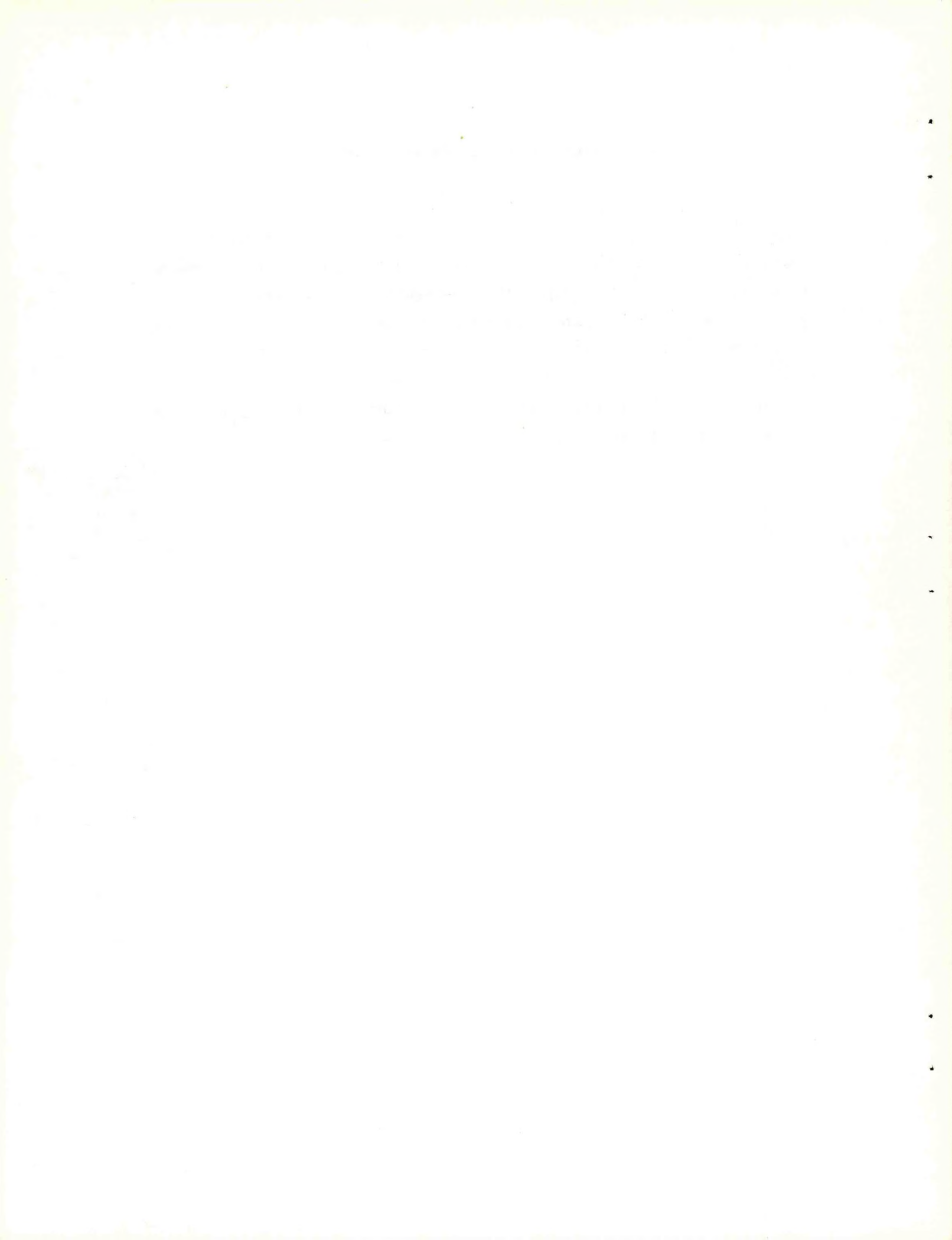
7.0 RECOMMENDED STANDARD OPERATING PROCEDURES

In order to provide a base for achieving stable overall system operation, a portion of the study was directed at preparing (in cooperation with Wallops CDA personnel) a "standardized operating procedure" for periodic alignment of the z-axis rack hardware. This effort resulted in an over detailed procedure which proved not to be viable on a day-to-day operational basis and was subsequently not formally adopted. It does represent a fairly complete technique for alignment and is included as Appendix E.

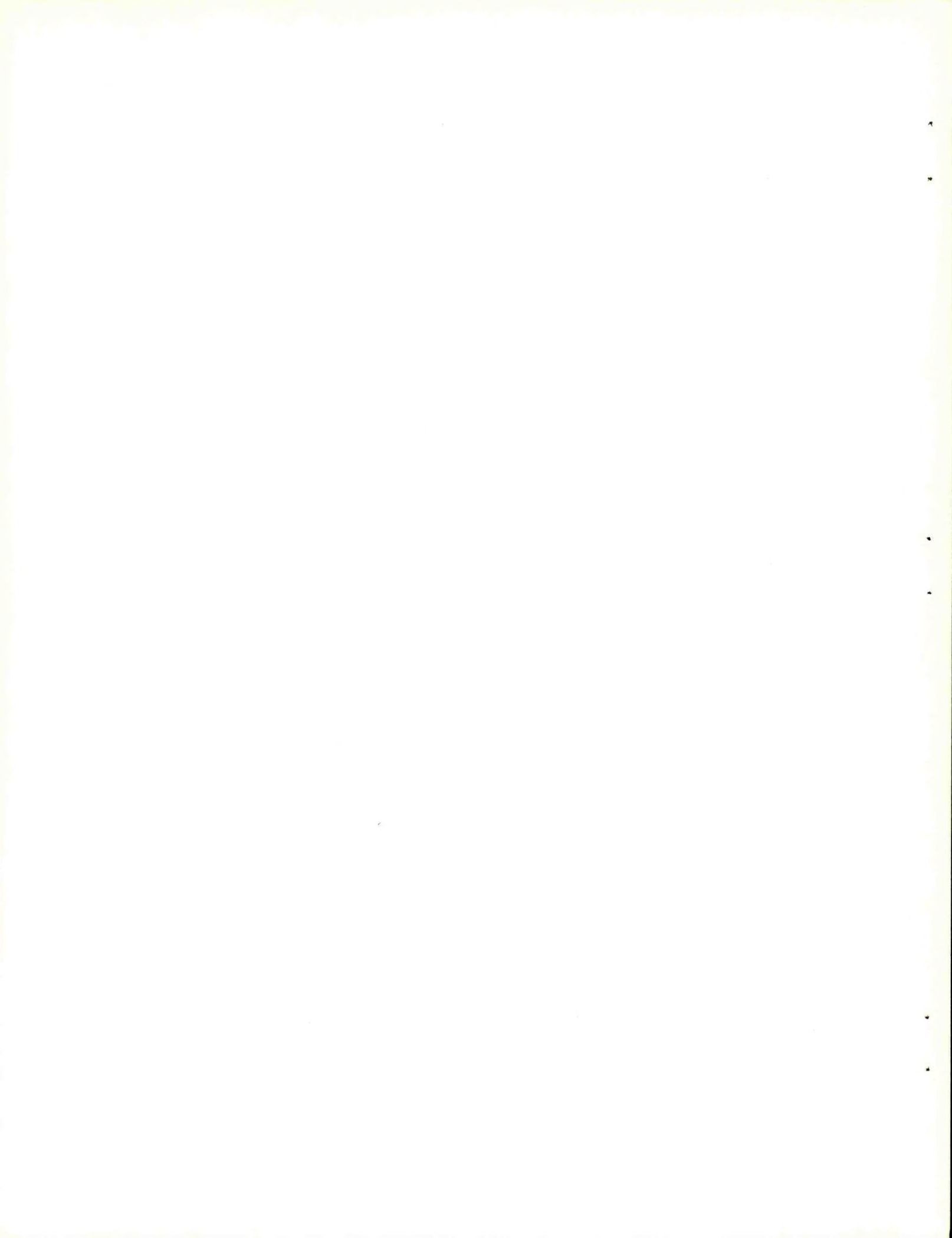


8.0 RECOMMENDATIONS FOR FUTURE EFFORT

It is recommended that the effort described in this report be continued toward the overall goal of achieving stable data quality assurance in an operational sense. Additional studies directed toward this end would include analytical investigations to quantitatively predict the effect of system changes (i.e. for future satellite configurations) on data quality and feasibility investigations to expand the scope of the diagnostic logic implementation. Additionally, close co-ordination and support is recommended during the actual operational implementation of this diagnostic logic at NESS.



9.0 APPENDICES



APPENDIX A

MODEL IMPLEMENTATION

This appendix presents a detailed block diagram of the digital computer algorithm which comprises the model developed during the study. A description of the model inputs follows as Appendix B, a sample output description as Appendix C, and a sample listing as Appendix D.

The block diagram indicates program control with the exception of the dotted line showing data flow for the flutter channel output. The subroutine call names are shown in parentheses. Power spectra are available as output at intermediate points in the program and are so indicated on the block diagram.

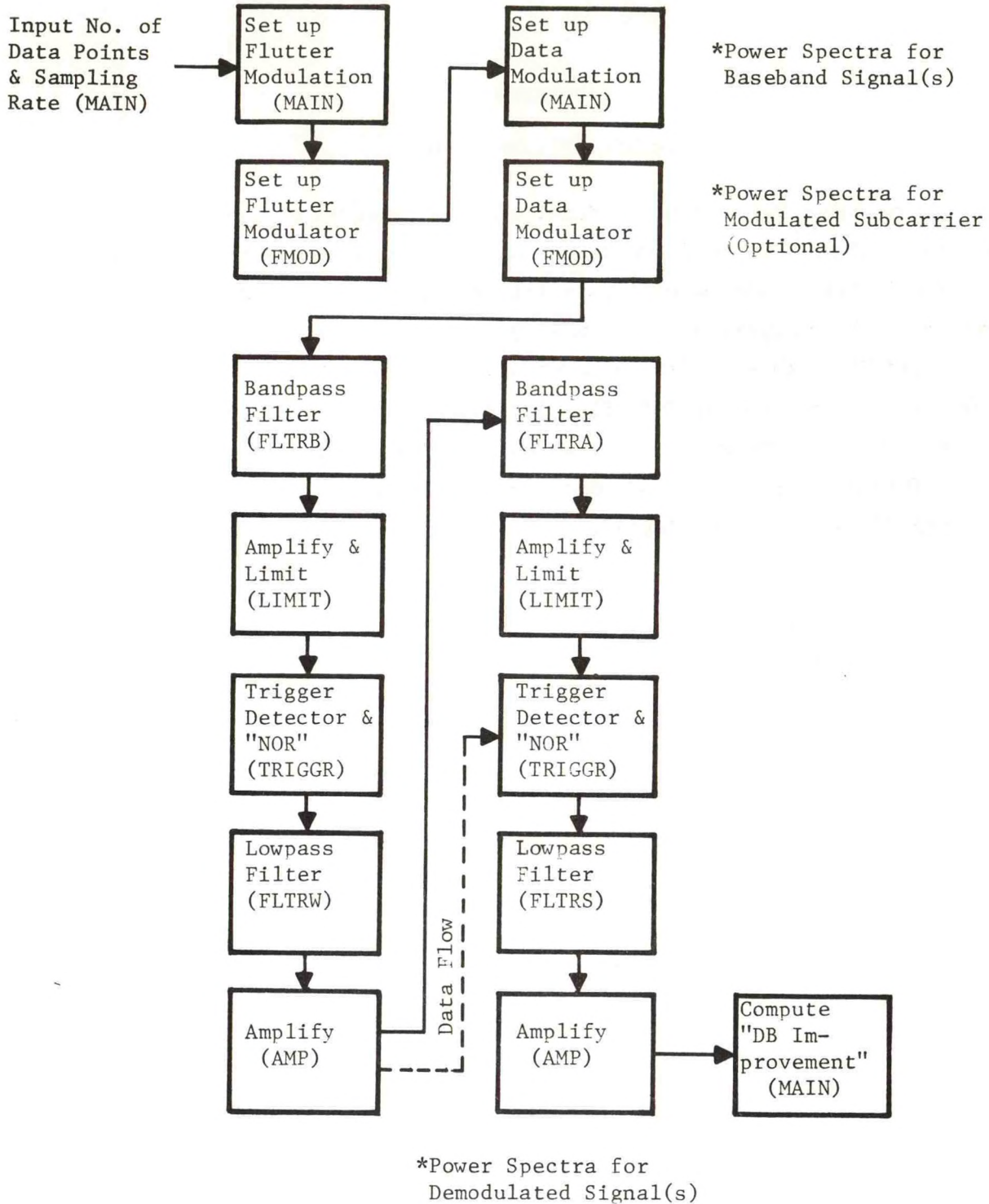


Figure A-1. Block Diagram of Model Implementation.

APPENDIX B

MODEL INPUT DESCRIPTION

This appendix presents the configuration of the data cards used with the model. A separate data deck must be supplied for each pass through the algorithm. The data deck must be complete within itself, and no data cards are common to multiple passes. With proper care this provides maximum program flexibility in terms of conducting analyses. For the first two passes the input bandpass filters are bypassed, and cards No. 3 and 4 as well as 22 and 23 must be removed. The parentheses following the card number indicate the calling routine. The cards are numbered sequentially but with gaps in the numbering system due to data deck modification during development. The deck was not renumbered in order to avoid confusion over the span of the study. The numbers to the left of the description indicate card column.

Data Deck Configuration

Flutter Channel

Card Number 1 (MAIN)

- 1-5 Number of data points to be analyzed (Integer Format)
- 6-25 Period of time between data points in seconds ("F" Format)

Card Number 2 (MAIN) - Integer Format - Diagnostic

- 1 Enter 1 if output is to be written on paper after program has executed (the reference and data channel output signals)

Card Number 3 (FLTRB) - Integer Format - Diagnostic

- 1 Enter 1 if array is to be written as it appears initially in the program.
- 2 Enter 1 if array is to be written after it is rearranged suitably for use by the Fourier transform subroutine.
- 3 Enter 1 if the Fourier spectrum is to be printed.
- 4 Enter 1 if the filtered Fourier spectrum is to be printed.
- 5 Enter 1 if the inverse Fourier transform output is to be printed.
- 6 Enter 1 if the array is to be printed after it is rearranged to be used by other subroutines.

Card Number 4 (FLTRB) - 3F10.3

- 1-10 Number of poles in filter
- 11-20 Maximum deviation frequency
- 21-30 Subcarrier frequency

Card Number 7 (LIMIT) - Integer Format - Diagnostic

- 1 Enter 1 if it is desired to write the data out after the flutter channel has been limited.

Card Number 8 (LIMIT) - "F" Format

- 1-10 The gain of the limiter stage before the flutter signal is limited. Must include decimal.
- 11-20 The gain of the limiter stage after the limiter must include decimal.
- 21-30 The amount of delay inherent in the limiter. Must include decimal.
- 31-40 The absolute value at which the signal is clipped. Must include decimal.

Card Number 9 (TRIGGR) - Integer Format - Diagnostic

- 1 Enter 1 if it is desired to output the data after the flutter channel has been examined for positive going and negative going zero crossings.
- 2 Enter 1 if it is desired to output the data which consists of the outputs of the A and B detectors.
- 3 Enter 1 if it is desired to output the data after the "NOR" circuit has "NORED" the outputs of the two detectors.

Card Number 10 (TRIGGR) - "F" Format

- 1-10 The triggering level of the Schmitt Trigger for increasing voltages.
- 11-20 The triggering level of the Schmitt Trigger for decreasing voltages.
- 21-30 The delay associated with the Schmitt Trigger circuit.

Card Number 11 (TRIGGR) - "F" Format

- 1-10 Enter 0.0
- 11-20 Pulse width of detector A in seconds.
- 21-30 The delay in seconds associated with the A detector.
- 31-40 The amplitude of the detector A pulse output.
- 41-50 The amplitude of the detector A output when no pulse is being output.

Card Number 12 (TRIGGR) - "F" Format

- 1-10 Enter 0.0.
- 11-20 Pulse width of detector B in seconds.
- 21-30 The delay in seconds associated with the detector.
- 31-40 The amplitude of the detector B pulse output.
- 41-50 The amplitude of the detector B output when no pulse is being output.

Card Number 13 (TRIGGR) - "F" Format

- 1-10 The amplitude of the "NOR" circuit output voltage when it is in the high state.
- 11-20 The amplitude of the "NOR" circuit output voltage when it is in the low state.
- 21-30 The delay in seconds associated with the "NOR" circuit.
- 31-40 The input level which differentiates the low level from the high level.

Card Number 14 (FLTRW) - Integer Format - Diagnostic

- 1 Enter 1 if flutter array is to be output as it appears upon entry to the filter subroutine.
- 2 Enter 1 if flutter array is to be output after it is rearranged (put in complex form) suitably for use by the Fourier transform subroutine.

- 3 Enter 1 if Fourier spectrum of input data is desired.
- 4 Enter 1 if the spectrum of the filtered data is desired.
- 5 Enter 1 if the inverse Fourier transform output is desired.
- 6 Enter 1 if the flutter array is to be output after the filtering operations have ended.

Card Number 15 (FLTRW) - Integer Format

- 1-3 The degree of the transfer polynomial numerator for the output flutter channel filter.
- 4-6 The degree of the transfer polynomial denominator for the output filter in the flutter channel.

Card Number 16 (FLTRW) - 5E16.8

- 1-80 The coefficients of the numerator polynomial of the output flutter channel filter, power increasing except for the constant term which is last. Additional cards may be used for high order polynomials.

Card Number 17 (FLTRW) - 5E16.8

- 1-80 The coefficients of the denominator polynomial of the output flutter channel filter, power increasing except for the constant term which is last. Additional cards may be used for high order polynomials.

Card Number 18 (AMPL) - Integer Format - Diagnostic

- 1 Enter 1 if the arrays are to be output after the flutter array is amplified.

Card Number 19 (AMPL) - "F" Format

- 1-10 Enter the gain of the amplification stage.

Card Number 20 (DELAY) - Integer Format - Diagnostic

- 1 Enter 1 if the arrays are to be output after the flutter array is delayed (advanced, see Card No. 21).

Card Number 21 (DELAY) - "F" Format

- 1-10 The time in seconds by which the flutter channel signal is advanced with respect to the signal (effectively a positive error in main delay setting).

Card Number 21A (DELAY) - Integer Format - Diagnostic

- 1 Enter 1 if the arrays are to be output after the signal array is delayed (advanced, see Card No. 21B).

Card Number 21B (DELAY) - "F" Format

- 1-10 The time in seconds by which the signal channel is advanced with respect to the flutter (effectively a negative error in main delay setting).

Data Channel

Card Number 22 (FLTRA) - Integer Format - Diagnostic

- 1 Enter 1 if signal and "A" array are to be written as they appear initially in the program. Useful only for debugging program.
- 2 Enter 1 if signal array is to be written after it is rearranged suitably for use by the Fourier transform subroutine.
- 3 Enter 1 if the Fourier spectrum of the signal data is to be printed.
- 4 Enter 1 if the filtered Fourier spectrum is to be printed.
- 5 Enter 1 if the inverse Fourier transform output is to be printed.
- 6 Enter 1 if the array is to be printed after it is rearranged to be used by other subroutines.

Card Number 23 (FLTRA) - 3F10.3

- 1-10 Number of poles in filter.
11-20 Maximum deviation frequency.
21-30 Subcarrier frequency.

Card Number 26 (LIMIT) - Integer Format - Diagnostic

- 1 Enter 1 if it is desired to write the signal data out after it has been limited.

Card Number 27 (LIMIT) - "F" Format

- 1-10 The gain of the limiter stage before the signal channel is limited. Must include decimal.
11-20 The gain of the limiter stage after the limiter. Must include decimal.
21-30 The amount of delay inherent in the limiter. Must include decimal.
31-40 The absolute value at which the signal is clipped. Must include decimal.

Card Number 28 (TRIGGR) - Integer Format - Diagnostic

- 1 Enter 1 if it is desired to output the data after the signal channel has been examined for positive going and negative going zero crossings.
- 2 Enter 1 if it is desired to output the data which consists of the outputs of the A and B detectors.
- 3 Enter 1 if it is desired to output the data after the "NOR" circuit has "NORED" the outputs of the two detectors.

Card Number 29 (TRIGGR) - "F" Format

- 1-10 The triggering level of the Schmitt Trigger for increasing voltages.

- 11-20 The triggering level of the Schmitt Trigger for decreasing voltages.
- 21-30 The delay associated with the Schmitt Trigger circuit.

Card Number 30 (TRIGGR) - "F" Format

- 1-10 The ratio of the detector A pulse width output to the magnitude of the wow and flutter channel, i.e., the "coefficient" determined by

$$\text{detector pulse width} = \text{"coefficient"} \times \text{flutter magnitude} \\ + \text{nominal detector pulse width.}$$

- 11-20 The nominal pulse width detector A (see expression above).
- 21-30 The delay in seconds associated with the A detector.
- 31-40 The amplitude of the detector A pulse output.
- 41-50 The amplitude of the detector A output when no pulse is being output.

Card Number 31 (TRIGGR) - "F" Format

- 1-10 Ratio of the detector B pulse width to the magnitude of the wow and flutter signal. See corresponding entry in card number 30.
- 11-20 The nominal pulse width of detector B. See corresponding entry in card number 30.
- 21-30 The delay in seconds associated with the B detector.
- 31-40 The amplitude of the detector B pulse output.
- 41-50 The amplitude of the detector B output when no pulse is being output.

Card Number 32 (TRIGGR) - "F" Format

- 1-10 The amplitude of the "NOR" circuit output voltage when it is in the high state.
- 11-20 The amplitude of the "NOR" circuit output voltage when it is in the low state.
- 21-30 The delay in seconds associated with the "NOR" circuit.
- 31-40 The input level which differentiates the low level from the high level.

Card Number 33 (FLTRS) - Integer Format - Diagnostic

- 1 Enter 1 if signal array is to be output as it appears upon entry to the output filter subroutine. Useful for debugging only.
- 2 Enter 1 if flutter array is to be output after it is rearranged (put in complex form) suitably for use by the Fourier transform subroutine.
- 3 Enter 1 if the spectrum of data is desired.

- 4 Enter 1 if the spectrum of the filtered data is desired.
- 5 Enter 1 if the Fourier transform output is desired.
- 6 Enter 1 if the flutter array is to be output after the filtering operations have ended.

Card Number 34 (FLTRS) - Integer Format

- 1-3 The degree of the transfer polynomial numerator for the output signal channel filter.
- 4-6 The degree of the transfer polynomial denominator for the output filter in the signal channel.

Card Number 35 (FLTRS) - 5E16.8

- 1-80 The coefficients of the numerator polynomial of the output signal channel filter, power increasing except for the constant term which is last. Additional cards may be used for high order polynomials.

Card Number 36 (FLTRS) - 5E16.8

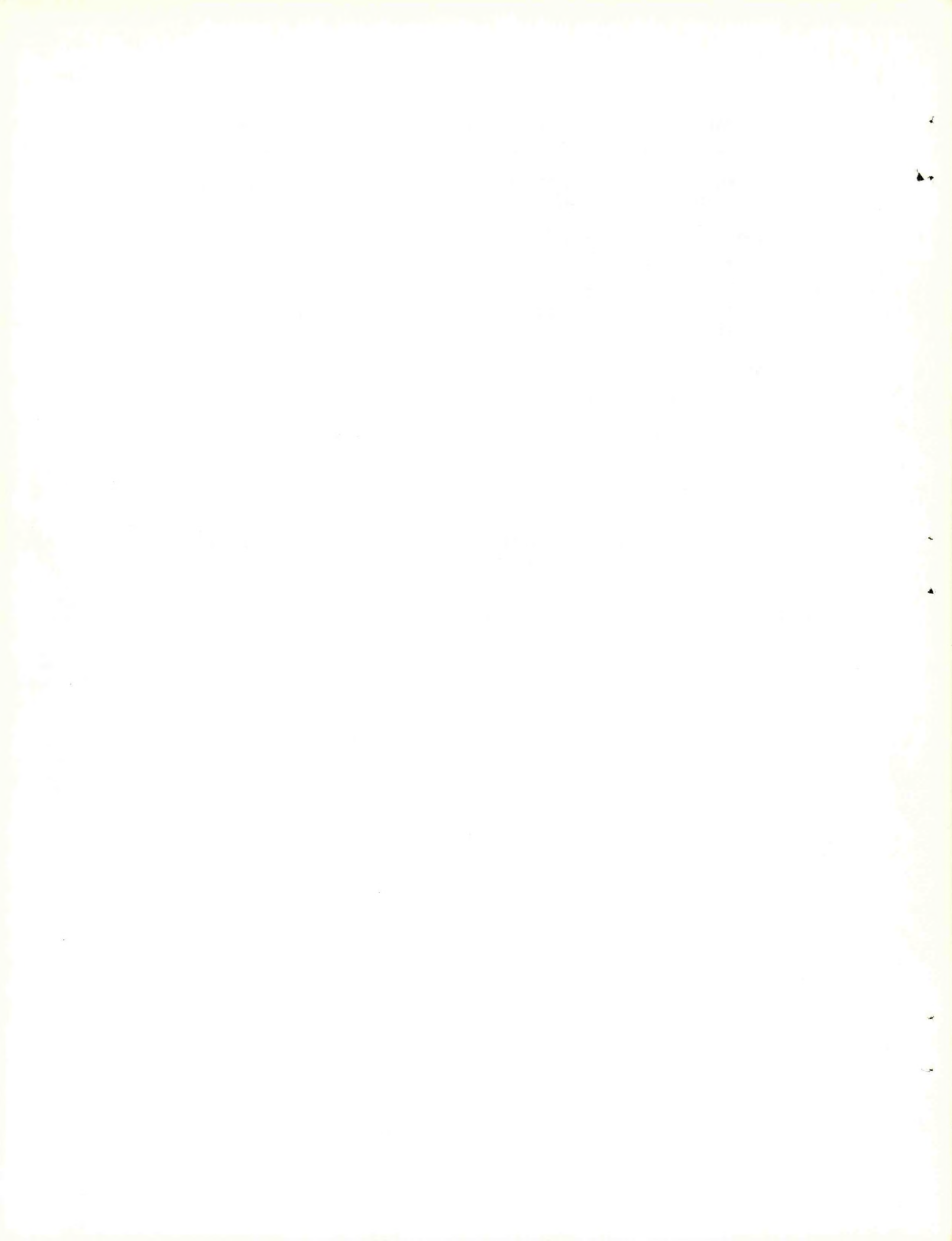
- 1-80 The coefficients of the denominator polynomial of the output signal channel filter, power increasing except for the constant term which is last. Additional cards may be used for high order polynomials.

Card Number 37 (AMPL) - Integer Format - Diagnostic

- 1 Enter 1 if the arrays are to be output after the signal array is amplified.

Card Number 38 (AMPL) - "F" Format

- 1-10 Enter the gain of the amplification stage.



APPENDIX C

STANDARD OUTPUT FORMAT

This appendix indicates the data output format from the model. Also available is a description of the input parameters (which has not been included here). As described in Appendix B, intermediate diagnostic output is also available as an option.

The basic parameter of interest in model performance is "dB Improvement" across the spectral band. This is defined as

$$20 \log_{10} \frac{A_n \text{ (without compensation)}}{A_n \text{ (with compensation)}}$$

where A_n is the amplitude of the "n"th harmonic in a spectral analysis of the data channel output. The spectrum for no compensation is generated during the first pass through the algorithm and stored. The above computation is provided for each subsequent pass desired.

Figure C-1 indicates the output format. The first column represents the wavenumber with wavenumber 1 being the "DC" term. The spectrum is computed using the Fast-Fourier transform method and incorporates 4096 data points at a sampling rate of 10 μ sec which corresponds to a Δf of 24.4 Hz at the DDHS. The second column represents the frequency in hertz at the spacecraft during record (i.e., real time), while the third column represents the frequency in hertz as seen at the DDHS during 4:1 playback from the CDA. (Recall that there is a 20.833:1 recorder speed increase during satellite readout.) The fourth column represents the spectral amplitude in counts for the no-compensation case and the fifth column the spectral amplitude in counts for the compensated case. Note that the flutter tones referred to in Section 5.0 appear at wavenumbers 5, 8, 18, and 33. The sixth column represents the "dB Improvement" mentioned above. In order to provide a feeling for what the magnitude of these numbers means, a 20 "dB Improvement" would indicate that the flutter harmonic has been reduced to one-tenth its original amplitude. Correspondingly, a 40 "dB Improvement" would indicate a reduction of the flutter harmonic amplitude to 1% of its original amplitude. Negative values indicate flutter enhancement. It should be noted that for the case presented,

	S/C	4/1	NO-Z	Z-COR	DB-IMP	4/1	S/C	4/1	NO-Z	Z-COR	DB-IMP
1	0.0	0.0	0.000	0.038	-146.753	61	281.3	1464.8	0.023	0.013	4.818
2	9.4	24.4	0.000	0.039	-69.889	62	285.9	1489.3	0.008	0.019	-7.807
3	9.4	48.8	0.001	0.040	-37.930	63	290.6	1513.7	0.007	0.011	-4.375
4	14.1	73.2	0.000	0.031	-38.040	64	295.3	1538.1	0.005	0.011	-7.124
5	18.8	97.7	0.000	0.015	-30.176	65	300.0	1562.5	0.014	0.025	-5.188
6	23.4	122.1	0.001	0.041	-33.951	66	304.7	1586.9	0.016	0.026	-4.098
7	28.1	146.5	0.001	0.040	-30.674	67	309.4	1611.3	0.022	0.013	4.506
8	32.8	170.9	0.121	0.030	-12.032	68	314.1	1635.7	0.007	0.019	-8.382
9	37.5	195.3	0.001	0.029	-33.030	69	318.8	1660.2	0.006	0.015	-7.157
10	42.2	219.7	0.002	0.035	-25.375	70	323.4	1684.6	0.014	0.018	-2.003
11	46.5	244.1	0.002	0.030	-25.342	71	328.1	1709.0	0.000	0.014	-33.305
12	51.6	268.6	0.003	0.029	-19.199	72	332.8	1733.4	0.027	0.014	5.356
13	56.3	293.0	0.001	0.038	-30.521	73	337.5	1757.8	0.006	0.007	-2.070
14	60.9	317.4	0.000	0.008	-26.555	74	342.2	1782.2	0.010	0.021	-6.614
15	65.6	341.8	0.001	0.034	-27.743	75	346.9	1806.6	0.009	0.012	-1.944
16	70.3	366.2	0.004	0.005	-2.632	76	351.6	1831.1	0.017	0.008	6.065
17	75.0	390.6	0.003	0.035	-21.237	77	356.3	1855.5	0.003	0.016	-14.304
18	79.7	415.0	0.788	0.020	-31.856	78	360.9	1879.9	0.018	0.011	-3.992
19	84.4	439.5	0.001	0.026	-33.242	79	365.6	1904.3	0.004	0.005	-1.152
20	89.1	463.9	0.003	0.045	-22.528	80	370.3	1928.7	0.009	0.024	-8.595
21	93.8	488.3	0.004	0.035	-18.316	81	375.0	1953.1	0.025	0.030	-1.627
22	98.4	512.7	0.011	0.009	-15.502	82	379.7	1977.5	0.008	0.014	-5.176
23	103.1	537.1	0.011	0.042	-11.884	83	384.4	2002.0	0.011	0.013	-1.712
24	107.8	561.5	0.002	0.035	-25.449	84	389.1	2026.4	0.009	0.017	-5.269
25	112.5	585.9	0.003	0.026	-18.051	85	393.8	2050.8	0.020	0.031	-3.889
26	117.2	610.4	0.009	0.044	-13.846	86	398.4	2075.2	0.023	0.021	0.434
27	121.9	634.8	0.008	0.042	-14.270	87	403.1	2099.6	0.016	0.021	-2.079
28	126.6	659.2	0.011	0.050	-12.825	88	407.8	2124.0	0.006	0.009	-2.894
29	131.3	683.6	0.005	0.019	-12.257	89	412.5	2148.4	0.011	0.017	-4.034
30	135.9	708.0	0.003	0.038	-21.526	90	417.2	2172.9	0.023	0.025	-0.853
31	140.6	732.4	0.006	0.018	-9.953	91	421.9	2197.3	0.012	0.016	-2.987
32	145.3	756.8	0.009	0.029	-9.967	92	426.6	2221.7	0.018	0.023	-2.077
33	150.0	781.3	0.387	0.075	-14.289	93	431.3	2246.1	0.010	0.020	-5.841
34	154.7	805.7	0.004	0.026	-15.722	94	435.9	2270.5	0.011	0.009	2.093
35	159.4	830.1	0.012	0.011	-1.231	95	440.6	2294.9	0.008	0.013	-3.735
36	164.1	854.5	0.008	0.017	-6.474	96	445.3	2319.3	0.026	0.021	1.699
37	168.8	878.9	0.012	0.006	6.387	97	450.0	2343.8	0.010	0.025	-7.557
38	173.4	903.3	0.005	0.022	-13.384	98	454.7	2368.2	0.031	0.029	0.710
39	178.1	927.7	0.015	0.023	-3.551	99	459.4	2392.6	0.010	0.008	1.980
40	182.8	952.1	0.003	0.018	-15.054	100	464.1	2417.0	0.016	0.015	-0.873
41	187.5	976.6	0.017	0.015	0.929	101	468.8	2441.4	0.028	0.031	-1.018
42	192.2	1001.0	0.006	0.030	-14.072	102	473.4	2465.8	0.016	0.014	0.922
43	196.9	1025.4	0.016	0.015	0.996	103	478.1	2490.2	0.032	0.035	-0.873
44	201.6	1049.8	0.006	0.039	-16.687	104	482.8	2514.6	0.014	0.015	-0.747
45	206.3	1074.2	0.013	0.039	-9.367	105	487.5	2539.1	0.001	0.002	-7.928
46	210.9	1098.6	0.004	0.013	-9.961	106	492.2	2563.5	0.015	0.019	-1.963
47	215.6	1123.0	0.007	0.020	-8.919	107	496.9	2587.9	0.015	0.008	5.643
48	220.3	1147.5	0.008	0.032	-12.600	108	501.6	2612.3	0.002	0.011	-15.666
49	225.0	1171.9	0.011	0.025	-6.957	109	506.3	2636.7	0.014	0.015	-0.819
50	229.7	1196.3	0.010	0.010	0.748	110	510.9	2661.1	0.034	0.034	-0.074
51	234.4	1220.7	0.008	0.026	-9.951	111	515.6	2685.5	0.007	0.012	-4.105
52	239.1	1245.1	0.006	0.021	-10.841	112	520.3	2710.0	0.015	0.017	-4.027
53	243.8	1269.5	0.005	0.028	-15.906	113	525.0	2734.4	0.010	0.017	-4.500
54	248.4	1293.9	0.018	0.028	-3.824	114	529.7	2758.8	0.027	0.029	-0.441
55	253.1	1318.4	0.006	0.023	-12.314	115	534.4	2783.2	0.015	0.013	1.143
56	257.8	1342.8	0.029	0.045	-3.735	116	539.1	2807.6	0.005	0.003	4.263
57	262.5	1367.2	0.012	0.028	-7.704	117	543.8	2832.0	0.017	0.015	1.345
58	267.2	1391.6	0.013	0.016	-1.809	118	548.4	2856.4	0.022	0.024	-0.629
59	271.9	1416.0	0.003	0.027	-20.195	119	553.1	2880.9	0.011	0.007	3.671
60	276.6	1440.4	0.017	0.011	-3.684	120	557.8	2905.3	0.019	0.022	-1.064

Figure C-1. Sample Model Output Format.

the reference discriminator output gain was slightly misaligned resulting in a small "DC" component to be introduced into the data channel during the compensation process. For this reason the -146.753 "dB Improvement" of wavenumber 1 should be ignored. Columns 7 through 12 represent a continuation of the data presented in 1 through 6. Since 4096 samples were used in the spectral analysis, 2048 harmonics were generated with a Nyquist frequency of 50,000 Hz. This is well beyond the data channel bandwidth and only frequencies out to approximately 3000 Hz (wavenumber 120) at the DDHS were output. This adequately covers the band of interest for analysis of the z-axis rack operation.

APPENDIX D

SAMPLE PROGRAM LISTING

This appendix includes a sample listing of the digital algorithm used during this study. The model was programmed in Fortran IV - G level for an IBM Systems 370/65 located at the Triangle Universities Computation Center in the Research Triangle Park, N. C. The system log and source module map have been retained in the listing for completeness.


```

1 //MODEL JOB RTI.C43.P01217, RUEDGER, H, MSGLEVEL=1, REGION=375K, 1
2 //
3 // T=3,P=150,PTY=0
4 // EXEC FTGCLG
5
6 ***
7 FORTRAN WG* LEVEL COMPILER, LINKEDIT, AND EXECUTE
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IEP237I 562 ALLOCATED TO FT03F001
IEP237I 504 ALLOCATED TO FT01F001
IEP142I - STEP WAS EXECUTED - COND CODE 0000
IEP285I SYS73331.T234925.RV000.MODEL.LOADSET PASSED
IEP285I VOL SER NOS= SPARE9.
CORE=376K TIME--1:53.5 CPU---1:38.8 I/O---0:14.7 RC-----0
USED=350K UR--3380 DISK---59 SEEK---19 MO---204 TAPE-----0

IEP285I SYS73331.T234925.RV000.MODEL.LOADSET DELETED
IEP285I VOL SER NOS= SPARE9.
IEP285I SYS73331.T234925.RV000.MODEL.LOADSET KEPT
IEP285I VOL SER NOS= SPARE9.
TIME---2:31.6
MODEL

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1 0001 C***** MAIN PROGRAM *****
2 0002 COMMON SIGNAL(4096),A(4096),WAF(4096),SPEC(120),DUFF,DUHD
3 0003 DIMENSION FIRST(120)
4 0004 DIMENSION INV(1024),S(1024)
5 1 FORMAT(IH1)
6 50 FORMAT(3ZE15.8)
7 51 FORMAT(IX,10F12.7)
8 C***** PROGRAM TO GENERATE TEST DATA *****
9 C****
10 C MODEL CURRENTLY CONFIGURED FOR ITOS-D AT FOUR TO ONE
11 C PLAYBACK
12 C LET SAMPLE TIME BE 10 MICROSECONDS
13 C****
14 DO 5000 KKK=1,11
15 PI = 3.1415926
16 TPI=2.0*PI
17 READ(1,48) NUMBER,PERIOD
18 48 FORMAT(I5,F20.4)
19 READ(1,49) IWRIT
20 49 FORMAT(40I1)
21 NA = NUMBER / 32
22 NE = 0
23 C DO 60 ND = 1, NA
24 C NB = NE + 1, NA
25 C NE = NE + 32
26 C 60 READ(8,50) (SIGNAL(MI), MI = NB,NE)
27 C NE = 0
28 C DO 61 ND = 1,NA
29 C NB = NE + 1
30 C NE = NE + 32
31 C 61 READ(8,50) (WAF(NI),NI = NB,NE)
32 IX = NUMBER
33 I = 0
34 62 IX = IX / 2
35 I = I + 1
36 IF(IX.LE.1) GO TO 63
37 GO TO 62
38 63 NUNA = IX
39 NNUB=NUMBER/4
40 NUMBER=4096
41 NUNA=12
42 NNUB=1024
43 HEIGHT=NUMBER/8
44 C ZERO ALL DATA ARRAYS
45 DO 1000 KZ=1,NUMBER
46 SIGNAL(KZ)=0.0
47 A(KZ)=0.0
48 WAF(KZ)=0.0
49 1000 CONTINUE
50 C
51 C SET UP FLUTTER MODULATION
52 PHM=0.0
53 PHIN=0.0
54 IX=7
55 DO 10 JA=1,NUMBER
56 CONSA=(FLOAT(JA)/512.0)*PI
57

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0038 CONSA=AMOD(CONSA,TEI)
0039 CONSB=(FLOAT(JA)/292.571)*PI
0040 CONSB=AMOD(CONSB,TEI)
0041 CONSC=(FLOAT(JA)/120.471)*PI
0042 CONSC=AMOD(CONSC,TEI)
0043 CONSD=(FLOAT(JA)/64.0)*PI
0044 CONSD=AMOD(CONSD,TEI)
0045 A(JA)=0.4*COS(CONSA)+0.1*COS(CONSB)+0.65*COS(CONSC)
      1+0.32*COS(CONSD)
0046 CALL RANDU(IY,FLY)
0047 ARND=2.0*(FLY-0.5)
      REMOVES RANDOM NOISE FIELD
0048 ARND=0.0

C****
0049 A(JA)=A(JA)+ARND
0050 IX=IY
0051 PHAX=AHAX1(PHAX,A(JA))
0052 PHIN=AHIN1(PHIN,A(JA))
0053 10 CONTINUE
C**** GENERATE APPENDAGE FOR TRIGGER
0054 NP1=NUMBER+1
0055 CALL RANDU(IY,FLY)
0056 ARND=2.0*(FLY-0.5)
      REMOVES RANDOM NOISE FIELD
0057 ARND=0.0

C****
0058 CONSA=(FLOAT(NP1)/512.0)*PI
0059 CONSA=AMOD(CONSA,TEI)
0060 CONSB=(FLOAT(NP1)/292.571)*PI
0061 CONSB=AMOD(CONSB,TEI)
0062 CONSC=(FLOAT(NP1)/120.471)*PI
0063 CONSC=AMOD(CONSC,TEI)
0064 CONSD=(FLOAT(NP1)/64.0)*PI
0065 CONSD=AMOD(CONSD,TEI)
0066 DUMF=0.4*COS(CONSA)+0.1*COS(CONSB)+0.65*COS(CONSC)
      1+0.32*COS(CONSD)
      DUMF=DUMF+ARND
0067 IP(KKK-GT-1) GO TO 400
0068 WRITE(3,110)
0069 110 FORMAT('AMPLITUDE SPECTRA FOR FLUTTER INPUT')
0070 CALL PSD(A,NUMBER,NUMA)
0071 WRITE(3,210) PHAX
0072 210 FORMAT(' MAXIMUM FLUTTER AMPLITUDE IS',F10.3)
0073 PHIN=0.0
0074 220 FORMAT(' MINIMUM FLUTTER AMPLITUDE IS',F10.3)
0075 400 CONTINUE
C
0076 SET UP FLUTTER MODULATOR
0077 FO=6250.0
0078 DEVI=937.5
0079 CALL FMOD(FO,DEVI,1,NUMBER)
      SET UP DATA CHANNEL MODULATION
C
0080 SMAY=0.0
0081 SHIN=0.0
0082 DO 30 JA=1,NUMBER
0083 CONSA=(FLOAT(JA)/512.0)*PI
0084 CONSA=AMOD(CONSA,TEI)

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0085 CONSB=(FLOAT(JA)/292.571)*PI
0086 CONSB=AHOD(CONSB,TEI)
0087 CONSC=(FLOAT(JA)/120.471)*PI
0088 CONSC=AHOD(CONSC,TEI)
0089 CONSD=(FLOAT(JA)/64.0)*PI
0090 CONSD=AHOD(CONSD,TEI)
0091 CONSE=(FLOAT(JA)/256.0)*PI
0092 CONSE=AHOD(CONSE,TEI)
0093 CONSP=(FLOAT(JA)/49.951)*PI
0094 CONSP=AHOD(CONSP,TEI)
0095 A(JA)=0.4*COS(CONSA)+0.1*COS(CONSB)+0.65*COS(CONSC)
      1+0.32*COS(CONSD)
      2+0.75*COS(CONSE)+0.25*COS(CONSF)
C
0096 SHAX=AHAX1(SHAX,A(JA))
0097 SHIN=AHIN1(SHIN,A(JA))
0098      30 CONTINUE
C**** GENERATE APPENDAGE FOR TRIGGER
0099 CONSA=(FLOAT(NP1)/512.0)*PI
0100 CONSA=AHOD(CONSA,TEI)
0101 CONSB=(FLOAT(NP1)/292.571)*PI
0102 CONSB=AHOD(CONSB,TEI)
0103 CONSC=(FLOAT(NP1)/120.471)*PI
0104 CONSC=AHOD(CONSC,TEI)
0105 CONSD=(FLOAT(NP1)/64.0)*PI
0106 CONSD=AHOD(CONSD,TEI)
0107 DUHD=0.4*COS(CONSA)+0.1*COS(CONSB)+0.65*COS(CONSC)
      1+0.32*COS(CONSD)
C****
0108 IF(KKK.GT.1) GO TO 500
0109 WRITE(3,120)
0110      120 FORMAT('AMPLITUDE SPECTRA FOR SIGNAL INPUT')
0111 CALL PSD(A,NUMBER,NUMA)
0112 WRITE(3,230) SHAX
0113      230 FORMAT(' MAXIMUM SIGNAL AMPLITUDE IS',F10.3)
0114 WRITE(3,240) SHIN
0115      240 FORMAT(' MINIMUM SIGNAL AMPLITUDE IS',F10.3)
0116      500 CONTINUE
C
0117 SET UP DATA MODULATOR
0118 FO=25000.0
0119 DEVIA=3375.0
0120 CALL FMOD(FO,DEVIA,0,NUMBER)
C
0121 IF(KKK.GT.1) GO TO 525
C
0122 WRITE(3,125)
C
0123 C 125 FORMAT('AMPLITUDE SPECTRA FOR MODULATED CARRIER')
0124 CALL PSD(SIGNAL,NUMBER,NUMA)
C
0125      525 CONTINUE
C
0126 CALL WRITE(WEIGHT)
0127 IF(KKK.LE.2) GO TO 535
0128 CALL FLTRB(PERIOD,NUMBER,NUMA,NUMB,INVS)
0129      535 CONTINUE
0130 WRITE(3,1)
0131 CALL LIMIT(PERIOD,1,NUMBER)
0132 CALL TRIGGR(PERIOD,1,NUMBER)
0133 CALL FLTRM(PERIOD,NUMBER,NUMA,NUMB,INVS)
0134      545 CONTINUE
0135 CALL APPL(1,NUMBER)
0136      555 CONTINUE
0137      565 CONTINUE
0138      575 CONTINUE

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1 0129 WRITE(3,130)
2 0130 130 FORMAT('AMPLITUDE SPECTRA FOR FLUTTER OUTPUT')
3 0131 CALL PSD(WAF,NUMBER,NUMA)
4 0132 WRITE(3,1)
5 0133 IF(KKK.GT.1) GO TO 600
6 0134 DO 550 I=1,NUMBER
7 0135 WAF(I)=0.0
8 0136 550 CONTINUE
9 0137 600 CONTINUE
10 0138 CALL DELAYP(PERIOD,0,NUMBER)
11 0139 CALL DELAYP(PERIOD,1,NUMBER)
12 0140 IF(KKK.LE.2) GO TO 635
13 0141 CALL FLTRA(PERIOD,NUMBER,NUMA,NUMB,INVS)
14 0142 635 CONTINUE
15 0143 CALL LIMIT(PERIOD,0,NUMBER)
16 0144 CALL TRIGGE(PERIOD,0,NUMBER)
17 0145 CALL FLTRS(PERIOD,NUMBER,NUMA,NUMB,INVS)
18 0146 CALL AMPL(0,NUMBER)
19 0147 IF(IWRIT.EQ.0) GO TO 66
20 0148 NE = 0
21 0149 DO 65 ND = 1, MA
22 0150 NB = NE + 1
23 0151 NE = NE + 32
24 0152 65 WRITE(6,50) (SIGNAL(I),I=NB,NE)
25 0153 66 CONTINUE
26 0154 WRITE(3,140)
27 0155 140 FORMAT('AMPLITUDE SPECTRA FOR SIGNAL OUTPUT')
28 0156 CALL PSD(SIGNAL,NUMBER,NUMA)
29 0157 IF(KKK.GT.1) GO TO 700
30 0158 DO 750 I=1,120
31 0159 FIRST(I)=SPEC(I)
32 0160 750 CONTINUE
33 0161 GO TO 800
34 0162 700 CONTINUE
35 0163 WRITE(3,720)
36 0164 720 FORMAT('1 S/C 4/1 NO-Z Z-COR DB-IMP
37 0165 DF=1/(NUMBER*PERIOD)
38 0166 DO 850 I=1,60
39 0167 FGD1=(I-1)*DF
40 0168 FGD2=FGD1+60.0*DF
41 0169 FSC1=FGD1*(4.0/20.833)
42 0170 FSC2=FGD2*(4.0/20.833)
43 0171 I2=I+60.0
44 0172 DB1=20.*ALOG10(FIRST(I)/SPEC(I))
45 0173 DB2=20.0*ALOG10(FIRST(I2)/SPEC(I2))
46 0174 WRITE(3,730) I,FSC1,FGD1,FIRST(I),SPEC(I),DB1,
47 0175 1I2,FSC2,FGD2,FIRST(I2),SPEC(I2),DB2
48 0176 730 FORMAT(I4,2F8.1,3F10.3,10X,I4,2F8.1,3F10.3)
49 0177 850 CONTINUE
50 0178 800 CONTINUE
51 0179 5000 CONTINUE
52 0180 CALL EXIT
53 0181 END
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SYMBOL	LOCATION	COMMON BLOCK / SYMBOL LOCATION	MAP SIZE SYMBOL LOCATION	C1E8 SYMBOL LOCATION	SYMBOL LOCATION	SYMBOL LOCATION	SYMBOL LOCATION
SIGNAL	0	A	4000	8000	C000	C1E0	
DUMD	C1E4						
SUBPROGRAMS CALLED							
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IBCOM#	13C	RANDU	140	PSD	144	FMCD	148
LIMIT	150	TRIGGR	154	FLTRW	158	AHPL	15C
FLTRA	164	FLTRS	168	EXIT	16C	COS	170
AMIN1	178	ALOG10	17C				
SCALAR MAP							
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
KKK	3E0	PI	3E4	TPI	3E8	NUMBER	3FC
IWRIT	408	NA	3F8	NE	3FC	IY	404
NUMA	41C	NNUMB	40C	WEIGHT	410	KZ	414
PHIN	430	JA	420	CONSA	424	CONSB	42C
CONSD	444	IY	434	FLY	438	ARND	43C
FO	458	DEVIA	448	SRAX	44C	SMIN	450
CONSP	46C	ND	45C	NB	460	II	464
PGD1	480	PGD2	470	PSC1	474	PSC2	478
DB1		DB2	484				
ARRAY MAP							
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
FIRST	488	INV	668	S	1668		
FORMAT STATEMENT MAP							
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
1	2688	50	266D	51	2674	48	267D
110	268A	210	2682	220	26D6	120	26FA
240	2744	130	2767	140	2790	720	2788
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,NOLIST,DECK,LOAD,MAP							
OPTIONS IN EFFECT NAME = MAIN LINECNT = 58							
STATISTICS SOURCE STATEMENTS = 180, PROGRAM SIZE = 14296							
STATISTICS NO DIAGNOSTICS GENERATED							

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C
C
C
0001 SUBROUTINE PHOD(C,E,MODE,NUMBER)
0002 COMMON SIGNAL(4096),Z(4096),WAF(4096),SPEC(120),DUMP,DDUMD
0003 REAL*8 A(4096),FO,DEVIA,SUN,TEMP,CONS
0004 REAL*8 PI,TPI
0005 REAL*8 DDUMF,DDUMD,NDP1
0006 PI=3.141592653589793D0
0007 TPI=2.D0*PI
0008 FO=C
0009 DEVIA=B
0010 DDUMF=DUMP
0011 DDUMD=DDUMD
0012 C NDP1=NUMBER+1
0013 C NDP1=MP1
0014 C**** *FIX* FOR APPENDAGE
0015 C**** NDP1=NUMBER
0016 DO 60 J=1,NUMBER
0017 60 A(J)=Z(J)
0018 SUM=0.D0
0019 DO 40 JE=1,NUMBER
0020 SUN=SUM+A(JE)*0.00001D0
0021 TEMP=SUM
0022 C**** *FIX* TO LET UNMODULATED CARRIER HAVE ZERO CROSSING IN FIRST
0023 C ELEMENT OF ARRAY
0024 JH=JE-1
0025 CONS=(FO*PI*0.00002D0*JH)+DEVIA*TEMP*TPI
0026 C****
0027 CONS=DMOD(CONS,TPI)
0028 IF(MODE.EQ.1) GO TO 45
0029 SIGNAL(JE)=DSIN(CONS)
0030 GO TO 40
0031 45 WAF(JE)=DSIN(CONS)
0032 C**** TRIGGER APPENDAGE
0033 IF(MODE.EQ.1) GO TO 55
0034 CONS=(FO*PI*0.00002D0*NDP1)+DEVIA*(TEMP+DDUMD)*TPI
0035 DDUMD=DSIN(CONS)
0036 GO TO 50
0037 55 CONS=(FO*PI*0.00002D0*NDP1)+DEVIA*(TEMP+DDUMF)*TPI
0038 DUMF=DSIN(CONS)
0039 50 CONTINUE
0040 C****
0041 RETURN
0042 END

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SYMBOL	LOCATION	SYMBOL	LOCATION	COMMON BLOCK / MAP	HAP SIZE	C1E8 LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	
SIGNAL	0	Z	4000		8000								
DUMD	C1E4										DUMF	C1E0	
SUBPROGRAMS CALLED													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
DSIM	D4												
SCALAR MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
PI	F0	TEI	F8	PO	100	DEVIA	108	DDUMF	110				
DDUMD	118	MDF1	120	SUM	128	TEPP	130	CONS	138				
C	140	B	144	NUMBER	148	J	14C	JE	150				
JM	154	MODE	158										
ARRAY MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
A	160												
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,MOLIST,DECK,LOAD,MAP													
OPTICNS IN EFFECT NAME = FNOD													
STATISTICS SOURCE STATEMENTS = 35,PROGRAM SIZE = 33918													
STATISTICS NO DIAGNOSTICS GENERATED													

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0001 SUBROUTINE FLTRB(PERIOD,NUMBER,NUMA,NUMB,INVS,S)
0002 THIS SUBROUTINE CONVERTS THE HOW AND FLUTTER DATA CHANNEL FROM
0003 THE TIME DOMAIN TO THE FREQUENCY DOMAIN. IT THEN MULTIPLIES
0004 THE RESULT BY A TRANSFER FUNCTION WHICH IS INPUT AS A QUOTIENT
0005 OF TWO POLYNOMIALS. THEN THE CHANNEL IS CONVERTED BACK TO THE
0006 TIME DOMAIN
0007 COMMON SIGNAL(4096),WAF(4096)
0008 COMPLEX WAF,INUM,XDENOM,QUOTNT
0009 DIMENSION N(3),INV(NUMB),S(NUMB),COFN(10),COFD(10)
0010 DIMENSION QUOTNT(2048)
0011 DIMENSION ANP(4096),PHASE(4096)
0012 DIMENSION CO(4096),QA(4096)
0013 200 FORMAT(1X,10P12.7)
0014 201 FORMAT(' BANDPASS FILTER ROUTINE')
0015 210 FORMAT(' ARRAY BEFORE DATA IS REARRANGED PROPERLY')
0016 222 FORMAT('1 DATA HAS NOW BEEN REARRANGED IN PROPER CELLS OF ARRAY RE
0017 223 FORMAT('1 OUTPUT OF FOURIER TRANSFORM')
0018 224 FORMAT('1DATA AFTER MULTIPLICATION BY TRANSFER FUNCTION')
0019 225 FORMAT('1DATA AFTER INVERSE TRANSFORMATION')
0020 226 FORMAT('1DATA AFTER REPACKING TO OBTAIN 3 REAL ARRAYS')
0021 230 FORMAT(2I3)
0022 231 FORMAT(5E16.8)
0023 232 FORMAT(1H1,2I3)
0024 233 FORMAT(1H,5F16.8)
0025 WRITE(3,210) IWR1,IWR2,IWR3,IWR4,IWR5,IWR6
0026 IF(IWR11.EQ.1) WRITE(3,221)
0027 IF(IWR11.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
0028 M(1) = NNUNA
0029 M(2) = 0
0030 M(3) = 0
0031 NOTE:: WAF ARRAY IS DECLARED COMPLEX, SO THERE ARE ONLY TWO
0032 ARRAYS INSTEAD OF THREE IN THE COMMON SINCE THE COMPLEX ARRAY
0033 IS THE SAME SIZE AS TWO STANDARD REAL ARRAYS. HOWEVER, THE DATA
0034 (ALL REAL DATA) IN THE COMPLEX ARRAY IS ONLY STORED IN THE LAST
0035 HALF OF THE ARRAY (IN BLTH REAL AND COMPLEX CELLS). THEREFORE
0036 THE DATA MUST BE SPREAD OUT AMONG THE REAL CELLS THROUGHOUT THE
0037 ARRAY
0038 AN ATTEMPT HAS BE MADE TO ACCOMPLISH THAT HERE.
0039 L = NUMBER / 2
0040 LL = L + 1
0041 DO 250 IIA = 1, L
0042 IIB = IIA + L
0043 IIC = IIA * 2
0044 IID = IIC - 1
0045 G = REAL(WAF(IIB))
0046 G = AIMAG(WAF(IIC))
0047 WAF(IID) = CMPLX(G,0.0)
0048 G = AIMAG(WAF(IIE))
0049 WAF(IIC) = CMPLX(G,0.0)
0050 IF(IWR12.EQ.1) WRITE(3,222)
0051 IF(IWR12.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
0052 IPSET = 1
0053 CALL HARR(WAF,M,INV,S,IPSET,IFERR)
0054
0055
0056
0057

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0042 WRITE(3,17) IFERR
0043 17 FORMAT(' IFERR = ',I3)
0044 IF(IHRI3.EQ.1) WRITE(3,223)
0045 IF(IHRI3.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
C****
0046 READ(1,234) POL,DEV,FO
0047 234 FORMAT(3F10.3)
0048 WRITE(3,235) DEV,PC
0049 235 FORMAT(' DEV=',F10.3,' FO=',F10.3)
0050 DELF=1.0/(PERIOD*NUMBER)
C****
C
C *1* IN 1-5 ACCOUNTS FOR WN 1 BEING DC
C****
0051 NI=(1.0-DEV)*FO/DELF+1.5
0052 NH=(1.0+DEV)*FO/DELF+1.5
0053 NLP1=NL+1
0054 MHP1=MH+1
0055 BW=(NH-NL)/2
C****
0056 NHALF=NUMBER/2
0057 DO 400 J=1,NL
0058 AMAG=0.0
0059 AFAZE=(POL/4.0)*3.14159
0060 CO(J)=AMAG*COS(AFAZE)
0061 QA(J)=AMAG*SIN(AFAZE)
0062 QUOTNT(J)=CHEPLX(CO(J),QA(J))
0063 400 CONTINUE
0064 DO 410 J=NLP1,MH
0065 AMAG=1.0
0066 AFAZE=(POL/4.0)*3.14159*(FO/DELF+1-J)/BW
0067 CO(J)=AMAG*COS(AFAZE)
0068 QA(J)=AMAG*SIN(AFAZE)
0069 QUOTNT(J)=CHEPLX(CO(J),QA(J))
0070 410 CONTINUE
0071 DO 420 J=NHP1,MHALF
0072 AMAG=0.0
0073 AFAZE=(POL/4.0)*3.14159
0074 AFAZE=-AFAZE
0075 CO(J)=AMAG*COS(AFAZE)
0076 QA(J)=AMAG*SIN(AFAZE)
0077 QUOTNT(J)=CHEPLX(CO(J),QA(J))
0078 420 CONTINUE
C****
C
C WRITE(3,233)
C
C WRITE(3,240) (QUOTNT(J),J=1,512)
C 240 FORMAT(1X,8F15.8)
C****
DO 425 J=1,MHALF
0079 WAF(J)=WAF(J)*QUOTNT(J)
0080 425 CONTINUE
DO 430 J=2,MHALF
0081 430 CONTINUE
WNO=NUMBER-J+2
0082 WAF(NNO)=CORJG(WAF(J))
0083 MHP1=NHALF+1
0084 WAF(NNO)=CORJG(WAF(J))
0085 MHP1=NHALF+1
0086 WAF(MHP1)=CHEPLX(0.0,0.0)
C****

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0087 ZERO=0.0
0088 DO 500 J=1,NHALF
0089 X=CO(J)
0090 Y=QA(J)
0091 AMP(J)=SQRT(X**2+Y**2)
0092 IF(X.EQ.ZERO.AND.Y.GT.ZERO) GO TO 550
0093 IF(X.EQ.ZERO.AND.Y.LT.ZERO) GO TO 545
0094 IF(X.EQ.ZERO.AND.Y.LT.ZERO) GO TO 540
0095 GO TO 560
0096 540 PHASE(J)=270.0
0097 GO TO 500
0098 545 PHASE(J)=0.0
0099 GO TO 500
0100 550 PHASE(J)=90.0
0101 GO TO 500
0102 560 PHASE(J)=ATAN(Y/X)
0103 PHASE(J)=57.296*PHASE(J)
0104 IF(X.LT.ZERO) GO TO 520
0105 IF(X.GT.ZERO.AND.Y.LT.ZERO) GO TO 530
0106 GO TO 500
0107 520 PHASE(J)=PHASE(J)+180.0
0108 GO TO 500
0109 530 PHASE(J)=PHASE(J)+360.0
0110 GO TO 500
0111 500 CONTINUE
C WRITE(3,610) (AMP(J),J=1,512)
C WRITE(3,233)
C WRITE(3,610) (PHASE(J),J=1,512)
0112 610 FORMAT(10F10.3)
C***
0113 IF(IWR14.EQ.1) WRITE(3,224)
0114 IF(IWR14.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
C TAKE THE INVERSE TRANSFORM.
IPSET = -1
0115 CALL HARM(WAF,M,INV,S,IPSET,IPERR)
0116 WRITE(3,17) IPERR
0117 IF(IWR15.EQ.1) WRITE(3,225)
0118 IF(IWR15.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
C COMPRESS THE DATA BACK INTO ONE HALF THE ARRAY SO IT WILL BE IN
C THE PROPER FORM FOR A THREE ARRAY COMMON.
DO 271 I1H = 1,L
0120 I1J = L - I1H + 1
0121 I1I = L + I1J
0122 I1K = I1J * 2
0123 I1L = I1K - 1
0124 A = REAL(WAF(I1K))
0125 B = REAL(WAF(I1L))
0126 271 WAF(I1H) = CMLPX(B,A)
0127 IF(IWR16.EQ.1) WRITE(3,226)
LIST=L+1
0129 IF(IWR16.EQ.1) WRITE(3,201) (WAF(IST),IST=LIST,NUMBER)
0130 RETURN
0131 END
0132

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SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
SIGNAL	0	COMMON BLOCK / MAP	4000	MAP SIZE	C000				
SUBPROGRAMS CALLED									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IBCOM#	160	HARM	164	CMPI#	168	COS	16C	SIN	170
SQRT	174	ATAN	178						
SCALAR MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
NNUMB	220	IWR11	224	IWR12	228	IWR13	22C	IWR14	230
IWR15	234	IWR16	238	IST	23C	HUBBR	240	NNUMA	244
L	248	LL	24C	IIA	250	IIB	254	IIC	258
IID	25C	G	260	IFSET	264	IFERR	268	POL	26C
DEV	270	FO	274	DELF	278	PERIOD	27C	ML	280
WH	284	NLP1	288	WHP1	28C	BW	290	NHALF	294
J	298	AMAG	29C	APAZE	2A0	NMC	2A4	MHP1	2A8
ZERO	2AC	X	2E0	Y	2E4	IIN	288	IIJ	28C
IIM	2C0	IIK	2C4	IIL	2C8	A	2CC	B	2D0
LIST	2D4								
ARRAY MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
R	2D8	INV	2E4	S	2E8	COFN	2EC	COFD	314
QUOTNT	340	AMP	4340	PHASE	8340	CO	C340	QA	10340
FORMAT STATEMENT MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
200	14340	201	14346	210	1434P	221	1436B	222	14398
223	143F6	224	14417	225	1444A	226	14470	230	144A1
231	144A7	232	144AE	233	144E7	17	144C1	234	144D5
235	144DC	610	144F1						
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,NOLIST,DECK,LOAD,MAP									
OPTIONS IN EFFECT NAME = FLTRB , LIMBCNT = 58									
STATISTICS SOURCE STATEMENTS = 132,PROGRAM SIZE = 86516									
STATISTICS NO DIAGNOSTICS GENERATED									


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0001 SUBROUTINE FLTRA(PERIOD,NUMBER,MNUMA,MNUMB,INV,S)
0002 C THIS SUBROUTINE DOES THE SAME AS THE FLTRB SUBROUTINE ONLY IT
0003 C OPERATES ON THE SIGNAL ARRAY INSTEAD OF THE WAF.
0004 COMMON SIGNAL(4096),WAF(4096)
0005 COMPLEX SIGNAL,XNUM,XDENOM,QUOTINT
0006 DIMENSION M(3),INV(MNUMB),S(MNUMB),COFW(10)
0007 DIMENSION COFD(10)
0008 DIMENSION QUOTINT(2048)
0009 DIMENSION ANP(4096),PHASE(4096)
0010 DIMENSION CO(4096),QA(4096)
0011 200 FORMAT(6I1)
0012 201 FORMAT(1X,10P12.7)
0013 210 FORMAT(' BANDPASS FILTER ROUTINE')
0014 221 FORMAT(' ARRAY BEFORE DATA IS REARRANGED PROPERLY')
0015 222 FORMAT(' DATA HAS NOW BEEN REARRANGED IN PROPER CELLS OF ARRAY RE
0016 223 ADY FOR TAKING FOURIER TRANSFORM')
0017 223 FORMAT(' OUTPUT OF FOURIER TRANSFORM')
0018 224 FORMAT(' DATA AFTER MULTIPLICATION BY TRANSFER FUNCTION')
0019 225 FORMAT(' DATA AFTER INVERSE TRANSFORMATION')
0020 230 FORMAT(2I3)
0021 231 FORMAT(5E16.8)
0022 232 FORMAT(1H,2I3)
0023 233 FORMAT(1H,3F16.8)
0024 WRITE(3,210)
0025 READ(1,200) IWR1,IWR2,IWR3,IWR4,IWR5,IWR6
0026 IP(IWR1.EQ.1) WRITE(3,221)
0027 IP(IWR1.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
0028 M(1) = MNUMA
0029 M(2) = 0
0030 M(3) = 0
0031 C NOTE: HERE AS IN THE FLTRB SUBROUTINE THE DATA MUST BE
0032 C REDISTRIBUTED AMONG THE REAL AND COMPLEX CELLS OF THE SIGNAL
0033 C ARRAY. THE ONLY DIFFERENCE IS THAT THE DATA MUST BE SHIPPED FROM
0034 C THE LOWER HALF OF THE ARRAY UPWARD INSTEAD OF DOWNWARD.
0035 L = NUMBER / 2
0036 LL = L + 1
0037 DO 250 IIA = 1, L
0038 IIB = L - IIA + 1
0039 IIC = IIB * 2
0040 IID = IIC - 1
0041 G = REAL(SIGNAL(IIE))
0042 H = AIMAG(SIGNAL(IIB))
0043 SIGNAL(IID) = CMPLX(G,0.0)
0044 250 SIGNAL(IIC) = CMPLX(H,0.0)
0045 IP(IWR2.EQ.1) WRITE(3,222)
0046 IP(IWR2.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
0047 C TAKE THE FOURIER TRANSFORM
0048 IFSET = 1
0049 CALL HARR(SIGNAL,M,INV,S,IFSET,IFERR)
0050 WRITE(3,17) IFERR
0051 17 FORMAT(' IFERR = ',I3)
0052 IP(IWR3.EQ.1) WRITE(3,223)
0053 IP(IWR3.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
0054 C****
0055 READ(1,234) POL,DEV,PO
0056
0057

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PORTRAM IV G LEVEL 21 FLTRA DATE = 73332 00/31/53 PAGE 0002

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0048 234 FORMAT(3F10.3)
0049 WRITE(3,235) DEV
0050 235 FORMAT(' DEVIATION EQUALS',F10.3)
0051 DELF=1.0/(PERIOD*NUMBER)
C****
C
C****
      *1* IN 1-5 ACCOUNTS FOR WN 1 BEING DC
0052 NL=(1.0-DEV)*FO/DELF+1.5
0053 NH=(1.0+DEV)*FO/DELF+1.5
0054 NLP1=NL+1
0055 NHP1=NH+1
0056 BW=(NH-NL)/2
C****
0057 NHALF=NUMBER/2
0058 DO 400 J=1,NL
0059 AHAG=0.0
0060 AFAZE=(POL/4.0)*3.14159
0061 CO(J)=AHAG*COS(AFAZE)
0062 QA(J)=AHAG*SIN(AFAZE)
0063 QUOTNT(J)=CHPLX(CO(J),QA(J))
0064 400 CONTINUE
0065 DO 410 J=NLP1,NH
0066 AHAG=1.0
0067 AFAZE=(POL/4.0)*3.14159*(FO/DELF+1-J)/BW
0068 CO(J)=AHAG*COS(AFAZE)
0069 QA(J)=AHAG*SIN(AFAZE)
0070 QUOTNT(J)=CHPLX(CO(J),QA(J))
0071 410 CONTINUE
0072 DO 420 J=NHP1,NHALF
0073 AHAG=0.0
0074 AFAZE=(POL/4.0)*3.14159
0075 AFAZE=-AFAZE
0076 CO(J)=AHAG*COS(AFAZE)
0077 QA(J)=AHAG*SIN(AFAZE)
0078 QUOTNT(J)=CHPLX(CO(J),QA(J))
0079 420 CONTINUE
C****
C
C 240 WRITE(3,233)
C 240 WRITE(3,240) (QUOTNT(J),J=1,512)
C 240 FORMAT('X,8F15.8)
C****
      DO 425 J=1,NHALF
0080 SIGNAL(J)=SIGNAL(J)*QUOTNT(J)
0081 425 CONTINUE
      DO 430 J=2,NHALF
0082 430 CONTINUE
      NMO=NUMBER-J+2
0083 SIGNAL(NMO)=CONJG(SIGNAL(J))
0084 NHP1=NHALF+1
0085 SIGNAL(NHP1)=CHPLX(0.0,0.0)
0086 430 CONTINUE
C****
0088 ZERO=0.0
0089 DO 500 J=1,NHALF
0090 X=CO(J)
0091 Y=QA(J)
0092 AMP(J)=SQRT(X**2+Y**2)
0093 IF(X.EQ.ZERO.AND.Y.GT.ZERO) GO TO 550
  
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0094 IF(X.EQ.ZERO.AND.Y.EQ.ZERO) GO TO 545
0095 IF(X.EQ.ZERO.AND.Y.LT.ZERO) GO TO 540
0096 GO TO 560
0097 540 PHASE(J)=270.0
0098 GO TO 500
0099 545 PHASE(J)=0.0
0100 GO TO 500
0101 550 PHASE(J)=90.0
0102 GO TO 500
0103 560 PHASE(J)=ATAN(Y/X)
0104 PHASE(J)=57.296*PHASE(J)
0105 IF(X.LT.ZERO) GO TO 520
0106 IF(X.GT.ZERO.AND.Y.LT.ZERO) GO TO 530
0107 GO TO 500
0108 520 PHASE(J)=PHASE(J)+180.0
0109 GO TO 500
0110 530 PHASE(J)=PHASE(J)+360.0
0111 GO TO 500
0112 500 CONTINUE
C
009R WRITE(3,610) (AMP(J),J=1,512)
C
0113 610 FORMAT(10F10.3)
C****
0114 IF(IWR14.EQ.1) WRITE(3,224)
0115 IF(IWR14.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
C TAKE THE INVERSE FOURIER TRANSFORM
IFSET = -1
0116 CALL HARM(SIGNAL,M,INV,S,IFSET,IFERR)
0117 WRITE(3,17) IPERR
0118 IF(IWR15.EQ.1) WRITE(3,225)
0119 IF(IWR15.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
0120 C COMPRESS THE DATA BACK INTO ONE HALF THE ARRAY SO IT WILL BE IN THE
C PROPER FORM FOR A THREE ARRAY COMMON.
DO 271 I1H = 1, L
0121 I1J = 2 * I1H
0122 I1K = I1J - 1
0123 A = REAL(SIGNAL(I1K))
0124 B = REAL(SIGNAL(I1J))
0125 271 SIGNAL(I1H) = CPLY(A,B)
0126 IF(IWR16.EQ.1) WRITE(3,226)
0127 IF(IWR16.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,L)
0128 RETURN
0129 END
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0001 SUBROUTINE TRIGGR(PERIOD,MODE,NUMBER)
0002 COMMON SIGNAL(4096),A(4096),WAF(4096),SPEC(120),DUMF,DUMD
0003 400 FORMAT(7F10.5)
0004 401 FORMAT(3I1)
0005 402 FORMAT(' PULSE WIDTH CORE SHOULD BE ZERO. PROGRAM HALTS ')
0006 403 FORMAT(' NEGATIVE VALUE FOR MODE ')
0007 READ(1,401)IWR1,IWR2,IWR3
0008 READ(1,400)ETRIGU,ETRIGD,TRGDEL
0009 READ(1,400)PFCOFA,PFCONA,PDELA,PPAMA,PNAHA
0010 READ(1,400)PFCOFB,PFCONB,FWDELB,FPANB,PWAMB
0011 READ(1,400)ENORHI,ENORLO,INORDE,ETRIP
C****
0012 PFCOFA=0.0
0013 PFCOFB=0.0
0014 PNAHA=-9.0
0015 PWAMB=-9.0
0016 PPANA=9.0
0017 PAMB=9.0
0018 ETRIP=0.0
0019 WEIGHT=NUMBER/8
C****
0020 WRITE(3,1100)ETRIGU,ETRIGD,TRGDEL
0021 WRITE(3,1101)PFCOFA,PFCONA,PDELA,PPAMA,PNAHA
0022 WRITE(3,1102)PFCOFB,PFCONB,FWDELB,FPANB,PWAMB
0023 WRITE(3,1103)ENORHI,ENORLO,INORDE,ETRIP
0024 1100 FORMAT(' TRIGGER SUBROUTINE',/,' TRIGGER SECTION',/,' TRIGGERS ON'
1,F7.3,' VOLTS FOR INCREASING VOLTAGES AND ',F7.3,' VOLTS FOR DECR
2,ASING',/,' DELAY IS',F15.10,' SECONDS')
0025 1101 FORMAT(' DETECTOR SECTION',/,' DETECTOR A',/,' PULSE WIDTH IS',F
110.7,' TIMES THE FLUTTER SIGNAL PLUS ',F10.7,' SECONDS',/,' DELA
2Y IS',F10.7,' PEAK PULSE VALUE IS',F7.3,' AND RESIDUAL VALUE IS',
3F7.3)
0026 1102 FORMAT(' DETECTOR SECTION',/,' DETECTOR B',/,' PULSE WIDTH IS',F
110.7,' TIMES THE FLUTTER SIGNAL PLUS ',F10.7,' SECONDS',/,' DELA
2Y IS',F10.7,' PEAK PULSE VALUE IS',F7.3,' AND RESIDUAL VALUE IS',
3F7.3)
0027 1103 FORMAT(' NOR CIRCUIT SECTION',/,' OUTPUT VOLTAGES',/,' HIGH--',
1F7.3,' LOW--',F7.3,' DELAY--',F7.3,' TRANSITION VOLT
2AGE--',F7.3)
C
C MODE = 0 OPERATE ON SIGNAL ARRAY
C MODE = 1 OPERATE ON HOW AND FLUTTER ARRAY
IF(MODE.EQ.1.AND.PFCOFA.GT.0.0) GO TO 495
IF(MODE.EQ.1.AND.PFCOFB.GT.0.0) GO TO 495
C SRRIT TRIGGER
C THIS SECTION SCANS THE DATA STREAM FOR CROSSINGS OF THE TRIGGERING
C VOLTAGE. IF THE VOLTAGE CROSSES ETRIGU INCREASING, THEN A VALUE
C OF 100 IS PUT ON THE DATA STREAM AT THAT POINT. LIKEWISE IF THE
C VOLTAGE CROSSES ETRIGD DECREASING, THEN A VALUE OF 100 IS PUT ON
C THE A DATA STREAM AT THAT POINT.
0030 IT = NUMBER - 1
0031 DO 458 IJ = 1, IT
0032 IL = IJ + 1
0033 A(IJ) = 0.0
0034 IF(MODE.EQ.1) GO TO 455
C THIS SECTION IS USED IF THE DATA STREAM IS THE SIGNAL STREAM(NOT

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1 0035 C THE HOW AND FLUTTER STREAM)
2 IF(SIGNAL(IJ).LT.ETRIGD.AND.SIGNAL(IL).GT.ETRIGU) GO TO 452
3 IF(SIGNAL(IJ).GT.ETRIGD.AND.SIGNAL(IL).LT.ETRIGD) GO TO 454
4 SIGNAL(IJ) = 0.0
5 GO TO 456
6 0039 452 SIGNAL(IJ) = 100.0
7 GO TO 456
8 0041 454 A(IJ) = 100.0
9 SIGNAL(IJ) = 0.0
10 GO TO 456
11 C THIS SECTION IS USED IF THE DATA STREAM TO BE USED IS THE HOW AND
12 C FLUTTER STREAM
13 0044 455 IF(WAF(IJ).LT.ETRIGD.AND.WAF(IL).GT.ETRIGU) GO TO 457
14 0045 IF(WAF(IJ).GT.ETRIGD.AND.WAF(IL).LT.ETRIGD) GO TO 459
15 0046 WAF(IJ) = 0.0
16 GO TO 456
17 0048 457 WAF(IJ) = 100.0
18 GO TO 456
19 0050 459 A(IJ) = 100.0
20 WAF(IJ) = 0.0
21 456 CONTINUE
22 C**** APPENDAGE
23 A(NUMBER)=0.0
24 IF(RODE.EQ.1) GO TO 555
25 0056 IF(SIGNAL(NUMBER).LT.ETRIGU.AND.DUMD.GT.ETRIGU) GO TO 552
26 0057 IF(SIGNAL(NUMBER).GT.ETRIGD.AND.DUMD.LT.ETRIGD) GO TO 554
27 0058 SIGNAL(NUMBER)=0.0
28 GO TO 556
29 0059 552 SIGNAL(NUMBER)=100.0
30 GO TO 556
31 0062 554 A(NUMBER)=100.0
32 SIGNAL(NUMBER)=0.0
33 GO TO 556
34 0065 555 CONTINUE
35 0066 IF(WAF(NUMBER).LT.ETRIGU.AND.DUMF.GT.ETRIGU) GO TO 557
36 0067 IF(WAF(NUMBER).GT.ETRIGD.AND.DUMF.LT.ETRIGD) GO TO 559
37 0068 WAF(NUMBER)=0.0
38 GO TO 556
39 0069 557 WAF(NUMBER)=100.0
40 GO TO 556
41 0071 559 A(NUMBER)=100.0
42 WAF(NUMBER)=0.0
43 0073 556 CONTINUE
44 C****
45 0075 IF(LWR1.EQ.1) CALL WRITE(NUMBER)
46 AT THIS POINT DATA IS CONTAINED ON THE TWO VECTORS WHICH GIVE THE
47 PULSES REPRESENTING ZERO CROSSINGS, ONE VECTOR OF UPWARD CROSSINGS
48 C AND ONE FOR DOWNWARD.
49 C DETECTORS A AND B
50 C THIS SECTION SCANS THE DATA STREAM AND THE A STREAM FOR PULSES AND
51 FOR EACH PULSE IT OUTPUTS A PULSE OF SPECIFIED DURATION. IF THE
52 PULSE IS TO BE PUT ON THE SIGNAL CHANNEL, ITS DURATION IS
53 DETERMINED BY THE MAGNITUDE OF THE WAF CHANNEL AT THAT TIME. IF IT
54 IS TO BE PUT ON THE WAF CHANNEL ITS DURATION IS FIXED.
55 C****
56
57

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LOGIC MODIFIED TO CHANGE PULSE HEIGHT

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1 C****
2 DO 460 IK = 1, NUMBER
3   IK = NUMBER - IK + 1
4   IF(MODE.GE.1) GO TO 468
5   CHECK FOR INPUT PULSES
6   IF(SIGNAL(IM).GT.80.0) GO TO 475
7   SIGNAL(IM) = PMAA
8   GO TO 469
9   468 IF(WAF(IM).GT.80.0) GO TO 476
10  WAF(IM) = PMAA
11  469 CONTINUE
12  IF(A(IM).GT.80.0) GO TO 480
13  A(IM) = PMAAB
14  GO TO 490
15  C SET LINE TO NO PULSE VALUE
16  475 SIGNAL(IM) = PMAA
17  A(IM) = PMAAB
18  GO TO 477
19  476 WAF(IM) = PMAA
20  A(IM) = PMAAB
21  477 IPWID=((PHCOFA*WAF(IM)+PWCONA)/PERIOD)+0.5
22  C COMPUTE PULSE HEIGHT FOR A DETECTOR
23  C****
24  TENPA=-PPAMA*WAF(IM)+PPAMA
25  C****
26  C PUT IN PULSES IN DATA LINE
27  IDELAY=(PWELEB/PERIOD)+0.5
28  IN = IDELAY + IN
29  IO=IN+IPWID-1
30  IO=MINO(IO,NUMBER)
31  DO 472 IP = IN,IO
32  IF(MODE.GE.1) GO TO 471
33  C****
34  SIGNAL(IP)=TENPA
35  C****
36  GO TO 472
37  471 WAF(IP) = PMAA
38  472 CONTINUE
39  GO TO 489
40  480 IPWID=((PHCOFB*WAF(IM)+PWCORB)/PERIOD)+0.5
41  C COMPUTE PULSE HEIGHT FOR B DETECTOR
42  C****
43  TRFPB=-PPANB*WAF(IM)+PPANB
44  C****
45  A(IM) = PMAAB
46  IDELAY=(PWELEB/PERIOD)+0.5
47  IN = IDELAY + IN
48  IO=IN+IPWID-1
49  IO=MINO(IO,NUMBER)
50  C PUT PULSE ON LINE (A ARRAY)
51  DO 482 IP = IN,IO
52  C****
53  IF(MODE.GE.1) GO TO 481
54  A(IP)=TRFPB
55  GO TO 482
56  481
57

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1	0117	481 A(IT) = PPAMB
2	0118	482 CONTINUE
3		C****
4	0119	GO TO 489
5	0120	488 WRITE(3,403)
6	0121	489 CONTINUE
7	0122	490 CONTINUE
8	0123	460 CONTINUE
9		C
10		C
11	0124	THIS SECTION MORS THE OUTPUT OF THE A AND B DETECTORS
12	0125	IF(IWR2.EQ.1) CALL WRITE(NUMBER)
13	0126	IXDEL = (XNODE / PERIOD) + 0.5
14	0127	DO 492 IR = 1, NUMBER
15	0128	IS = NUMBER - IR + 1
16	0129	IT = IS + IXDEL
17	0130	IF(IT.GT.NUMBER) GO TO 492
18	0131	IF(NODE) 492,499,497
19		C****
20	0131	499 IF(SIGNAL(IS) - GT.ETRIIP.OR.A(IS) - GT.ETRIIP) GO TO 600
21	0132	IF(SIGNAL(IS) - LT.ETRIIP.AND.A(IS) - LT.ETRIIP) SIGNAL(IT) =
22		1 - AMIN1(SIGNAL(IT), A(IT))
23	0133	GO TO 492
24	0134	600 SIGNAL(IT) = -AHAX1(SIGNAL(IT), A(IT))
25	0135	GO TO 492
26	0136	497 IF(WAF(IS) - GT.ETRIIP.OR.A(IS) - GT.ETRIIP) GO TO 601
27	0137	IF(WAF(IS) - LT.ETRIIP.AND.A(IS) - LT.ETRIIP) WAF(IT) =
28		1 - AMIN1(WAF(IT), A(IT))
29	0138	GO TO 492
30	0139	601 WAF(IT) = -AHAX1(WAF(IT), A(IT))
31		C****
32	0140	492 CONTINUE
33	0141	GO TO 494
34	0142	495 WRITE(3,402)
35	0143	CALL EXIT
36	0144	494 CONTINUE
37	0145	IF(IXDEL.EQ.0) GO TO 496
38	0146	DO 440 IT = 1, IXDEL
39	0147	IF(NODE) 440, 442, 443
40	0148	442 SIGNAL(IT) = ENORLFC
41	0149	GO TO 440
42	0150	443 WAF(IT) = ENORLFC
43	0151	440 CONTINUE
44	0152	496 CONTINUE
45	0153	IF(IWR3.EQ.1) CALL WRITE(NUMBER)
46	0154	RETURN
47	0155	END
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SYMBOL	LOCATION	SYMBOL	COMMON BLOCK / LOCATION	HAP	MAP	MAP SIZE	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
DUMD	C1E4	A	4000			8000	C1E8	SEC	C000	DUMF	C1E0		
SUBPROGRAMS CALLED													
IRCOM#	23C	WHITE	240	EXIT		244	248	RINO	248	ANINI	28C		
AMAX1	250												
SCALAR MAP													
IR1	290	IR2	294	IR3		298	29C	FFIGU	29C	ETRIGD	2A0		
TRDEL	2A4	PWCOFA	2B8	PWCONA		2AC	2B0	PWELA	2B0	PPAMA	2B4		
PMANA	2B8	PWCOFB	2BC	PWCOBA		2C0	2C4	PWDELE	2C4	PPAMB	2C8		
DNAMB	2CC	ENORHI	2D0	ENORLO		2D4	2D8	YWORDE	2D8	ETRIIP	2DC		
WRIGHT	2E0	NUMBER	2E4	MODE		2E8	2EC	IT	2EC	IJ	2FU		
IL	2F4	IK	2F8	IN		30C	310	IPWID	300	PERIOD	304		
TEMPA	308	IDELAY	30C	IN		310	314	IO	314	IP	318		
TEMPB	31C	IXDEL	320	IR		324	328	IS	328				
FORMAT STATEMENT MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
400	32C	401	333	402	339	403	36F	403	36F	1100	391		
1101	42D	1102	4DF	1103	591								
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,MOLIST,DECK,LOAD,MAP													
OPTIONS IN EFFECT NAME = TRIGGE , LINECNT = 58													
STATISTICS SOURCE STATEMENTS = 155, PROGRAM SIZE = 4980													
STATISTICS NO DIAGNOSTICS GENERATED													

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C
0001 SUBROUTINE DELAY (PERIOD,MODE,NUMBER)
0002 COMMON SIGNAL(4096),A(4096),WAF(4096)
0003 DIMENSION TEMP(500)
C
0004 PROGRAM SCANS APPROPRIATE DATA STREAM AND MOVES ALL DATA POINTS
C
0005 AN APPROPRIATE AMOUNT LATER IN TIME.
0006 700 FORMAT(10.5)
0007 401 FORMAT(11)
0008 READ(1,401)IWR1
0009 READ(1,700) DELAY
C
0010 COMPUTE DELAY IN TERMS OF SAMPLE POINTS.
0011 IF(MODE) 750,721,722
0012 722 WRITE(3,1106) DELAY
0013 1104 FORMAT(' DELAY SUBROUTINE, DELAYS DATA IN SIGNAL STREAM',F10.7,
17 '
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57 '
1105 FORMAT(' DELAY SUBROUTINE DELAYS DATA IN WAF STREAM ',F10.7,' SECO
INDS')
0014 723 CONTINUE
0015 IUV = (DELAY / PERIOD)+0.5
0016 IU = NUMBER- IUV
C
0017 FILL UNSHIFTED DATA WITH CYCLIC ARRAY
0018 IF(IUV.EQ.0) GO TO 726
0019 DO 725 IV=1,IUV
0020 IY=IU+IV
0021 IF(MODE)753,730,729
0022 729 TEMP(IY)=SIGNAL(IY)
0023 GO TO 725
0024 730 TEMP(IY)=WAF(IY)
0025 725 CONTINUE
C
0026 DELAY REST OF ARRAY
0027 DO 750 IV = 1, IU
0028 IW = IU - IV + 1
0029 IX = IW + IUV
0030 IF(MODE)753,752,751
0031 751 SIGNAL(IX) = SIGNAL(IW)
0032 GO TO 750
0033 752 WAF(IX) = WAF(IW)
0034 GO TO 750
0035 753 WRITE(3,705)
0036 705 FORMAT(' MODE VALUE IS NEGATIVE')
C
0037 PUT CYCLIC DATA IN FRONT OF ARRAY
0038 IF(IUV.EQ.0) GO TO 761
0039 DO 760 I=1,IUV
0040 IF(MODE) 753,764,762
0041 762 SIGNAL(I)-TEMP(I)
0042 GO TO 760
0043 764 WAF(I)=TEMP(I)
0044 760 CONTINUE
0045 761 CONTINUE

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DELAY

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IF(IWR1.EQ.1) CALL WRITE(NUMBER)
RETURN
END

0045
0046
0047

SYMBOL SIGNAL	LOCATION	SYMBOL	LOCATION	COMMON BLOCK / SYMBOL	MAP SIZE / MAP	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	
	0	A	4000	4000	8000								
SUBPROGRAMS CALLED													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IBCOM#	12C	WRITE	130										
SCALAR MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IWR1	138	DELAY	13C	MODE	140	IIV	144	PERIOD	148	IY	158	IW	15C
IU	14C	NUMBER	150	IY	154								
IX	160	I	164										
ARRAY MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
Temp	168												
FORMAT STATEMENT MAP													
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
700	938	401	93D	1104	943	1105	984	705	9C1				
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,MOLIST,DECK,LOAD,MAP													
OPTIONS IN EFFECT NAME = DELAYP , LINECNT = 58													
STATISTICS SOURCE STATEMENTS = 47,PROGRAM SIZE = 3358													
STATISTICS NO DIAGNOSTICS GENERATED													

```

0001 SUBROUTINE AMPL(MODE,NUMBER)
      C PROGRAM SIMPLY MULTIPLIES ALL VALUES OF THE APPROPRIATE DATA
      C STREAM BY A CONSTANT
      COMMON SIGNAL(4096),A(4096),HAF(4096)
0002 401 FORMAT(1I1)
0003 600 FORMAT(' MODE VALUE IS NEGATIVE')
0004 601 FORMAT(1F10.5)
0005 READ(1,401)IWR1
0006 READ(1,601)GAIN
0007 IP(MODE) 655,621,622
0008 621 WRITE(3,1106) GAIN
0009 1106 FORMAT(' AMPLIFIER SUBROUTINE, PROVIDES GAIN OF ',F10.2,'FOR SIGNA
0010 1L DATA')
0011 GO TO 623
0012 622 WRITE(3,1107) GAIN
0013 1107 FORMAT(' AMPLIFIER SUBROUTINE, PROVIDES GAIN OF ',F10.2,'FOR HAF D
0014 DATA')
0015 623 CONTINUE
0016 DO 655 IU = 1, NUMBER
0017 IP(MODE) 651,652,653
0018 651 WRITE(3,600)
0019 652 SIGNAL(IU) = GAIN* SIGNAL(IU)
0020 GO TO 655
0021 653 HAF(IU) = GAIN * HAF(IU)
0022 655 CONTINUE
0023 IF(IWR1.EQ.1) CALL WRITE(NUMBER)
0024 RETURN
0025 END

```

1	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION
2	A	0	A	4000	A	4000	A	4000	A	4000
3										
4										
5										
6	IBCOM#	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION
7	DC	DC	WRITE	E0	WRITE	E0	WRITE	E0	WRITE	E0
8										
9										
10										
11	IMR1	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION
12	E8	E8	GAIN	EC	GAIN	EC	GAIN	EC	GAIN	EC
13										
14										
15										
16										
17	401	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION	SIGNAL	LOCATION
18	FC	FC	600	102	601	11E	1106	125	1107	165
19										
20										
21										
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1 0001 SUBROUTINE LIMIT(PERIOD,MODE,NUMBER)
2 COMMON SIGNAL(4096),A(4096),WAF(4096)
3 300 FORMAT(4F10.3)
4 301 FORMAT(' ',NEGATIVE VALUE FOR MODE ' ')
5 401 FORMAT(1I1)
6 READ(1,401) IWR1
7 READ(1,300) GAIN1, GAIN2, DELAY, ECLIP
8 WRITE(3,1107) GAIN1,GAIN2,ECLIP,DELAY
9 1107 FORMAT(' SUBROUTINE LIMIT',/, MODES LIMITER WITH GAIN OP ',F7.3,
10 ' BEFORE IT AND ',F7.3,' AFTER',/ ' CLIPPING VALUE IS PIUS OR MINU
11 'S ',F7.3,' VOLTS',/ ' DELAY IS ',F12.8)
12 C GAIN 1--GAIN BEFORE THE CLIPPING STAGE
13 C GAIN2--GAIN AFTER THE CLIPPING STAGE
14 TOTAL = 0.0
15 C COMPUTE AVERAGE SIGNAL LEVEL
16 IF(MODE.GT.0) GO TO 351
17 DO 350 IA = 1, NUMBER
18 350 TOTAL = SIGNAL(IA) + TOTAL
19 GO TO 353
20 351 CONTINUE
21 DO 352 IA = 1, NUMBER
22 352 TOTAL = WAF(IA) + TOTAL
23 353 CONTINUE
24 MEAN = TOTAL / NUMBER
25 IDELAY = (DELAY / PERIOD) + 0.5
26 ETEST = ECLIP / GAIN1
27 ENEG = -ETEST
28 C SCAN DATA STREAM AND LIMIT AMPLIFIED WAVEFORM AT PLUS OR MINUS
29 ECLIP AND THEN AMPLIFY IT.
30 DO 355 IB = 1, NUMBER
31 IC=NUMBER-IB+1
32 IF(MODE) 340, 371, 372
33 371 ESIG = SIGNAL(IC) - MEAN
34 GO TO 375
35 372 ESIG = WAF(IC) - MEAN
36 GO TO 375
37 340 WRITE(3,301)
38 375 IF(ESIG.GT.ETEST) GO TO 360
39 IF(ESIG.LT.ENEG) GO TO 362
40 PSIG = ESIG * GAIN1 * GAIN2
41 GO TO 364
42 360 PSIG = ECLIP * GAIN2
43 GO TO 364
44 362 PSIG = -ECLIP * GAIN2
45 364 ID=IC+IDELAY
46 IF(ID.GT.NUMBER) GO TO 366
47 IF(MODE.GT.0) GO TO 367
48 SIGNAL(ID) = PSIG
49 GO TO 366
50 367 WAF(ID) = PSIG
51 366 CONTINUE
52 355 CONTINUE
53 IF(IDELAY.LE.0) GO TO 390
54 ZERO OUT THE INITIAL PART OF THE DATA STREAM WHICH WAS DELAYED
55 IF(IDELAY.EQ.0) GO TO 390
56
57

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LIMIT

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1	0048	DO 370 IE = 1, IDELAY
2	0049	IF(MODE-GR.1) GO TO 369
3	0050	SIGNAL(IE) = 0.0
4	0051	GO TO 370
5	0052	369 WAF(IE) = 0.0
6	0053	370 CONTINUE
7	0054	390 CONTINUE
8	0055	IF(LIB1.EQ.1) CALL WRITE(NUMBER)
9	0056	RETURN
10	0057	END
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SYMBOL	LOCATION	SYMBOL	LOCATION	COMMON BLOCK / SYMBOL LOCATION	MAP SIZE SYMBOL LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
SIGNAL	0	A	4000	4000	8000						
SUBPROGRAMS CALLED											
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IBCOM#	140	WRITE	144								
SCALAR MAP											
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
INR1	14C	GAIN1	150	GAIN2	154	DELAY	158	ECLIP	15C		
TOTAL	160	MODE	164	IA	168	NUMBER	16C	MEAN	170		
IDELAY	174	PERIOD	178	EDEST	17C	ENEG	180	IB	184		
IC	188	ESIG	18C	ID	190	IE	194				
FORMAT STATEMENT MAP											
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
300	198	301	19F	401	1C0	1107	1C6				
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,HOLIST,DECK,LOAD,MAP											
OPTIONS IN EFFECT NAME = LIMIT , LINECNT = 58											
STATISTICS SOURCE STATEMENTS = 57, PROGRAM SIZE = 1696											
STATISTICS NO DIAGNOSTICS GENERATED											

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```
0001 SUBROUTINE WRITE (NUMBER)
0002 COMMON SIGNAL(4096),A(4096),WAF(4096)
0003 19 FORMAT('1')
0004 20 FORMAT(5H SIG ,10F10.5)
0005 21 FORMAT(5H A ,10F10.5)
0006 22 FORMAT(5H WAF ,10F10.5)
0007 WRITE(3,19)
0008 WRITE(3,20) (SIGNAL(LL),LL=1,NUMBER)
0009 WRITE(3,21) (A(LL),LL=1,NUMBER)
0010 WRITE(3,22) (WAF(LL),LL=1,NUMBER)
0011 RETURN
0012 END
```

SIGNAL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
1	0	A	4000	WAF	8000	C000			
2									
3									
4									
5									
6									
7	A8								
8									
9									
10									
11	AC								
12	LL		E0						
13									
14									
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16									
17	B4		E9						
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COMMON BLOCK / MAP SIZE C000
 WAF 8000

SUBPROGRAMS CALLED

SCALAR MAP
 E0

FORMAT STATEMENT MAP
 E9

OPTICS IN EFFECT ID,EBCDIC,SOURCE,MOLIST,DECK,LOAD,MAP
 OPTICS IN EFFECT NAME = WRITE , LINECNT = 58
 STATISTICS SOURCE STATEMENTS = 12, PROGRAM SIZE = 600
 STATISTICS NO DIAGNOSTICS GENERATED

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0001 SUBROUTINE FLTRM(PERIOD,NUMBER,NUMA,NUMB,INV,S)
C THIS SUBROUTINE CONVERTS THE ROW AND FLUTTER DATA CHANNEL FROM
C THE TIME DOMAIN TO THE FREQUENCY DOMAIN. IT THEN MULTIPLIES
C THE RESULT BY A TRANSFER FUNCTION WHICH IS INPUT AS A QUOTIENT
C OF TWO POLYNOMIALS. THEN THE CHANNEL IS CONVERTED BACK TO THE
C TIME DOMAIN
0002 COMMON SIGNAL(4096),WAF(4096)
0003 COMPLEX WAF,XNUM,XDENOM,QUOTWT
0004 DIMENSION M(3),INV(NNUMB),S(NNUMB),COPM(10),COPD(10)
0005 DIMENSION QUOTNT(32)
0006 200 FORMAT(6I4)
0007 201 FORMAT(1X,10F12.7)
0008 210 FORMAT(' FILTER SUBROUTINE FOR WAF CHANNEL')
0009 221 FORMAT(' ARRAY BEFORE DATA IS REARRANGED PROPERLY')
0010 222 FORMAT(' DATA HAS NOW BEEN REARRANGED IN PROPER CELLS OF ARRAY RE
1ADY FOR TAKING FOURIER TRANSFORM')
0011 223 FORMAT(' OUTPUT OF FOURIER TRANSFORM')
0012 224 FORMAT(' DATA AFTER MULTIPLICATION BY TRANSFER FUNCTION')
0013 225 FORMAT(' DATA AFTER INVERSE TRANSFORMATION')
0014 226 FORMAT(' DATA AFTER REPACKING TO OBTAIN 3 REAL ARRAYS')
0015 230 FORMAT(2I3)
0016 231 FORMAT(5E16.8)
0017 232 FORMAT(1H,2I3)
0018 233 FORMAT(1H,5F16.8)
0019 WRITE(3,210)
0020 READ(1,200) IWR1,IWR2,IWR3,IWR4,IWR5,IWR6
0021 IF(IWR1.EQ.1) WRITE(3,221)
0022 IF(IWR1.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
0023 M(1) = NNUMA
0024 M(2) = 0
0025 M(3) = 0
C NOTE:: WAF ARRAY IS DECLARED COMPLEX, SO THERE ARE ONLY TWO
C ARRAYS INSTEAD OF THREE IN THE COMMON SINCE THE COMPLEX ARRAY
C IS THE SAME SIZE AS TWO STANDARD REAL ARRAYS. HOWEVER, THE DATA
C (ALL REAL DATA) IN THE COMPLEX ARRAY IS ONLY STORED IN THE LAST
C HALF OF THE ARRAY (IN BLTH REAL AND COMPLEX CELLS). THEREFORE
C THE DATA MUST BE SPREAD OUT AMONG THE REAL CELLS THROUGHOUT THE
C ARRAY
C AN ATTEMPT HAS BE MADE TO ACCOMPLISH THAT HERE.
0026 L = NUMBER / 2
0027 LL = L + 1
0028 DO 250 IIA = 1, L
0029 IIB = IIA + L
0030 IIC = IIA * 2
0031 IID = IIC - 1
0032 G = REAL(WAF(IIB))
0033 WAF(IID) = CMPLX(G,0.0)
0034 G = AIMAG(WAF(IIE))
0035 WAF(IIC) = CMPLX(G,0.0)
250 WAF(IIC) = CMPLX(G,0.0)
0036 IF(IWR2.EQ.1) WRITE(3,222)
0037 IF(IWR2.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
C TAKE THE FOURIER TRANSFORM
0038 IFSET = 1
0039 CALL HARM(WAF,M,INV,S,IFSET,IFERR)
0040 WRITE(3,17) IFERR
0041 17 FORMAT(' IFERR = ',I3)

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0042 IF (IHR13.EQ.1) WRITE(3,223)
0043 IF (IHR13.EQ.1) WRITE(3,201) (WAF(I*ST), I*ST=1, NUMBER)
0044 DO 260 IIG = 1, 10
0045 COFN(IIG) = 0.0
0046 260 COFD(IIG) = 0.0
0047 N = 0
0048 NO = 0
0049 C READ IN TRANSFER FUNCTION POLYNOMIALS (2)
0050 READ(1,230) IDGRN, IDGRD
0051 READ(1,231) (COFN(IIE), IIE = 1, IDGRM), CONSN
0052 READ(1,231) (COFD(IIG), IIG = 1, IDGRD), CONSD
0053 WRITE(3,232) IDGRN, IDGRD
0054 WRITE(3,226)
0055 1226 FORMAT(' TRANSFER POLYNOMIALS '/10X, 'NUMERATOR ',30X, 'DENOMINATOR
0056 '1')
0057 DO 228 IABD = 1, 10
0058 IABC = 11 - IABD
0059 228 WRITE(3,227) COFN(IABC), IABC, COFD(IABC), IABC
0060 227 FORMAT(5X, F20.5, '(S**', I2, ')', 6X, F20.5, '(S**', I2, ')')
0061 WRITE(3,229) CONSN, CONSD
0062 229 FORMAT(5X, F20.15, 14X, F20.5)
0063 C COMPUTE THE VALUE OF THE TRANSFER FUNCTION AT EACH FREQUENCY
0064 255 N = N + 1
0065 RPREQ = ((N-1)*6.2831856) / (PERIOD * NUMBER)
0066 RPREQ2 = RPREQ * RPREQ
0067 AREAL = -COFN(10)
0068 AREAL = RPREQ2 * AREAL + COFN(8)
0069 AREAL = RPREQ2 * AREAL - COFN(6)
0070 AREAL = RPREQ2 * AREAL + COFN(4)
0071 AREAL = RPREQ2 * AREAL - COFN(2)
0072 AREAL = RPREQ2 * AREAL + CONSN
0073 AIMIG = COFN(9)
0074 AIMIG = RPREQ2 * AIMIG - COFN(7)
0075 AIMIG = RPREQ2 * AIMIG + COFN(5)
0076 AIMIG = RPREQ2 * AIMIG - COFN(3)
0077 AIMIG = RPREQ2 * AIMIG + COFN(1)
0078 XNUM = CMPLX(AREAL, AIMIG)
0079 AREAL = -COFD(10)
0080 AREAL = RPREQ2 * AREAL + COFD(8)
0081 AREAL = RPREQ2 * AREAL - COFD(6)
0082 AREAL = RPREQ2 * AREAL + COFD(4)
0083 AREAL = RPREQ2 * AREAL - COFD(2)
0084 AREAL = RPREQ2 * AREAL + CONSD
0085 AIMIG = COFD(9)
0086 AIMIG = RPREQ2 * AIMIG - COFD(7)
0087 AIMIG = RPREQ2 * AIMIG + COFD(5)
0088 AIMIG = RPREQ2 * AIMIG - COFD(3)
0089 AIMIG = RPREQ2 * AIMIG + COFD(1)
0090 XDENOM = CMPLX(AREAL, AIMIG)
0091 NO = NO + 1
0092 C QUOTNT(NO) = XNUM / XDENOM
0093 C MULTIPLY THE VALUE OF THE TRANSFER FUNCTION TIMES THE VALUE
0094 OF THE DATA SPECTRUM.
0095 WAF(N) = WAF(N) * QUOTNT(NO)

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0093 IF(N.EQ.1) GO TO 257
0094 NNO = NUMBER - N + 2
0095 IF(N.EQ.NNO) GO TO 257
0096 WAF(NNO) = CONJG(WAF(N))
0097 257 CONTINUE
0098 IF(NO.EQ.32) GO TO 265
0099 IF(N.GE.LL) GO TO 270
0100 GO TO 255
0101 265 CONTINUE
0102 C WRITE(3,238) XNUM,XDENOM,REREQ,KFREQ2
0103 238 FORMAT(' NUMERATOR = ',2E16.6,' DENOMINATOR = ',2E16.6/' F
0104 FREQUENCY = ',F14.2,' SQUARED = ',F14.2)
0105 WRITE(3,240) (QUANT(NI),NI=1,32)
0106 240 FORMAT('X,8E15.8)
0107 C WRITE(3,239) N
0108 239 FORMAT('H ,15)
0109 NO = 0
0110 IF(N.GE.LL) GO TO 270
0111 GO TO 255
0112 270 CONTINUE
0113 IF(IWR14.EQ.1) WRITE(3,224)
0114 IF(LWR14.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
0115 C TAKE THE INVERSE TRANSFORM.
0116 IPSET = -1
0117 CALL HARM(WAF,M,INV,S,IPSET,IPERR)
0118 WRITE(3,17) IPERR
0119 IF(IWR15.EQ.1) WRITE(3,225)
0120 IF(LWR15.EQ.1) WRITE(3,201) (WAF(IST),IST=1,NUMBER)
0121 C COMPRESS THE DATA BACK INTO ONE HALF THE ARRAY SO IT WILL BE IN
0122 THE PROPER FORM FOR A THREE ARRAY COMMON.
0123 DO 271 I1H = 1,L
0124 I1J = L - I1H + 1
0125 I1K = L + I1J
0126 I1L = I1J * 2
0127 I1M = I1K - 1
0128 A = REAL(WAF(I1K))
0129 B = REAL(WAF(I1L))
0130 271 WAF(I1H) = CMPLX(B,A)
0131 LIST=L+1
0132 IF(IWR16.EQ.1) WRITE(3,226)
0133 IP(IWR16) = LIST
0134 RETURN
0135 END

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COMMON BLOCK / MAP SIZE C000
 SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION
 SIGNAL 0 WAP 4000

SUBPROGRAMS CALLED
 SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION
 IBCOM# 12C HARM 130 CDVDS# 134

SCALAR MAP
 SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION
 XNUM 1B8 XDEMOH 1C0 NUHNB 1C8
 IWR13 1D4 IWR14 1D8 IWR15 1E0 IWR16 1E4
 NUMBER 1E8 NNUNA 1FC L 1F4 IIA 1F8
 IIB 1FC IIC 200 IID 204 G 208 IFSET 20C
 IIPRR 210 IIG 214 IIN 218 NO 21C IDGRN 220
 IDGRD 224 IIF 228 CONSM 230 IABD 234
 IABC 238 RFRFQ 23C PERIOD 240 RFRFQ2 244 ARAL 248
 AIMIG 24C NNO 250 IIA 254 IIA 258 IIA 25C
 IIA 260 IIA 264 IIA 268 B 26C LIST 270

ARRAY MAP
 SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION
 N 274 INV 280 S 284 C0FN 288 C0FD 280
 QUOTWT 2DB

FORMAT STATEMENT MAP
 SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION SYMBOL LOCATION
 200 3D8 201 3DE 210 3E7 221 40D 222 43A
 223 498 224 4E9 225 4EC 226 512 230 543
 231 549 232 550 233 559 240 563 17 577
 227 580 229 5D4 238 5E0 240 638 239 644

OPTIONS IN EFFECT ID,EBCDIC,SOURCE,HOLIST,DECK,LOAD,MAP
 OPTIONS IN EFFECT NAME = PLTRM / LINECNT = 58

STATISTICS SOURCE STATEMENTS = / 128, PROGRAM SIZE = 4384

STATISTICS NO DIAGNOSTICS GENERATED

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0001 SUBROUTINE PLTRS(PERIOD,NUMBER,MMUMH,MNUMH,INV,S)
C THIS SUBROUTINE DOES THE SAME AS THE FLTRW SUBROUTINE ONLY IT
C OPERATES ON THE SIGNAL ARRAY INSTEAD OF THE WAF.
0002 COMMON SIGNAL(4096),HAF(4096)
0003 COMPLEX SIGNAL,XNUM,XDENOM,QUOTWT
0004 DIMENSION N(3),INV(NNUMB),S(NNUMB),COFM(10)
0005 DIMENSION COFD(10)
0006 DIMENSION QUOTWT(32)
0007 200 FORMAT(6I1)
0008 201 FORMAT(1X,10F12.7)
0009 210 FORMAT(' FILTER SUBROUTINE FOR SIGNAL CHANNEL ')
0010 221 FORMAT(' ARRAY BEFCRE DATA IS REARRANGED PROPERLY')
0011 222 FORMAT(' DATA HAS NOW BEEN REARRANGED IN PROPER CELLS OF ARRAY RE
12 1ADY FOR TAKING FOURIER TRANSFORM')
0012 223 FORMAT(' OUTPUT OF FOURIER TRANSFORM')
0013 224 FORMAT(' DATA AFTER MULTIPLICATION BY TRANSFER FUNCTION')
0014 225 FORMAT(' DATA AFTER INVERSE TRANSFORMATION')
0015 226 FORMAT(' DATA AFTER REPACKING TO OBTAIN 3 REAL ARRAYS')
0016 230 FORMAT(2I3)
0017 231 FORMAT(5E16.8)
0018 232 FORMAT(1H,2I3)
0019 233 FORMAT(1H,5F16.8)
0020 WRITE(3,210)
0021 READ(1,200) IWR1,IWR2,IWR3,IWR4,IWR5,IWR6
0022 IF(IWR1.EQ.1) WRITE(3,221)
0023 IF(IWR11.EQ.1) WRITE(3,221)
0024 M(1) = MNUMA
0025 M(2) = 0
0026 M(3) = 0
C NOTE: HERE AS IN THE FLTRW SUBROUTINE THE DATA MUST BE
C REDISTRIBUTED AMONG THE REAL AND COMPLEX CELLS OF THE SIGNAL
C ARRAY. THE ONLY DIFFERENCE IS THAT THE DATA MUST BE SHIPPED FROM
C THE LOWER HALF OF THE ARRAY UPWARD INSTEAD OF DOWNWARD.
L = NUMBER / 2
0027 LL = L + 1
0028 90 250 IIA = 1, L
0029 IIB = L - IIA + 1
0030 IIC = IIB * 2
0031 IID = IIC - 1
0032 G = REAL(SIGNAL(IIB))
0033 H = AIMAG(SIGNAL(IIB))
0034 SIGNAL(IID) = CMPLX(G,0.0)
0035 SIGNAL(IIC) = CMPLX(H,0.0)
250 SIGNAL(IIC) = CMPLX(H,0.0)
0036 IF(IWR12.EQ.1) WRITE(3,222)
0037 IF(IWR12.EQ.1) WRITE(3,222)
0038 TAKE THE FOURIER TRANSFORM
C
0039 IPSET = 1
0040 CALL HARM(SIGNAL,M,INV,S,IPSET,IFERR)
0041 WRITE(3,17) IPERR
0042 17 FORMAT(' IPERR = ',I3)
0043 IF(IWR13.EQ.1) WRITE(3,223)
0044 IF(IWR13.EQ.1) WRITE(3,223)
0045 DO 260 IIG = 1, 10
0046 COFD(IIG) = 0.0
0047 260 COFD(IIG) = 0.0
0048 N = 0

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0049 NO = 0
C READ IN TRANSFER FUNCTION POLYNOMIALS (2)
0050 READ(1,230) IDGRN, IDGRD
0051 READ(1,231) (COFN(IIF), IIF = 1, IDGRM), CONSN
0052 READ(1,231) (COFD(IIG), IIG = 1, IDGRD), CONSD
0053 WRITE(3,232) IDGRN, IDGRD
0054 WRITE(3,1226)
0055 1226 FORMAT(' TRANSFER POLYNOMIALS ',10X,' NUMERATOR ',30X,' DENOMINATOR
1')
0056 DO 228 IABD = 1, 10
0057 IABC = 11 - IABD
0058 228 WRITE(3,227) COFN(IABC), IABC, COFD(IABC), IABC
0059 227 FORMAT(5X, E20.5, '(S**', I2, '), 6X, E20.5, '(S**', I2, ')')
0060 WRITE(3,229) CONSN, CONSD
0061 229 FORMAT(5X, P20.15, 14X, P20.5)
C COMPUTE THE VALUES OF THE TRANSFER FUNCTION AT EACH FREQUENCY.
0062 255 N = N + 1
0063 RFEQ = ((N-1)*6.2831856) / (PERIOD * NUMBER)
0064 RFEQ2 = RFEQ*RFEQ
0065 AREAL = - COFN(10)
0066 AREAL = RFEQ2 * AREAL + COFN(8)
0067 AREAL = RFEQ2 * AREAL - COFN(6)
0068 AREAL = RFEQ2 * AREAL + COFN(4)
0069 AREAL = RFEQ2 * AREAL - COFN(2)
0070 AREAL = RFEQ2 * AREAL + COFN(2)
0071 AIMIG = COFN(9)
0072 AIMIG = RFEQ2 * AIMIG - COFN(7)
0073 AIMIG = RFEQ2 * AIMIG + COFN(5)
0074 AIMIG = RFEQ2 * AIMIG - COFN(3)
0075 AIMIG = RFEQ2 * AIMIG + COFN(1)
0076 AIMIG = AIMIG * RFEQ
XNUM = CMPLX(AREAL, AIMIG)
0077 AREAL = -COFD(10)
0078 AREAL = RFEQ2 * AREAL + COFD(8)
0079 AREAL = RFEQ2 * AREAL - COFD(6)
0080 AREAL = RFEQ2 * AREAL + COFD(4)
0081 AREAL = RFEQ2 * AREAL - COFD(2)
0082 AREAL = RFEQ2 * AREAL + COFD(2)
0083 AIMIG = COFD(9)
0084 AIMIG = RFEQ2 * AIMIG - COFD(7)
0085 AIMIG = RFEQ2 * AIMIG + COFD(5)
0086 AIMIG = RFEQ2 * AIMIG - COFD(3)
0087 AIMIG = RFEQ2 * AIMIG + COFD(1)
0088 AIMIG = AIMIG * RFEQ
0089 XDENOM = CMPLX(AREAL, AIMIG)
0090 NO = NO + 1
0091
0092 C QUOTNT(N0) = XNUM / XDENOM
C MULTIPLY THE VALUE OF THE TRANSFER FUNCTION TIMES THE VALUE OF
C THE DATA SPECTRUM
0093 SIGNAL(N) = SIGNAL(N) * QUOTNT(N0)
0094 IF(N.EQ.1) GO TO 257
0095 NNO = NUMBER - N + 2
0096 IF(N.EQ.NNO) GO TO 257
0097 SIGNAL(NNO) = CONJG(SIGNAL(N))
0098 257 CONTINUE
0099 IF(N0.EQ.32) GO TO 265

```

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1 0100 IF(N-GE-LL) GO TO 270
2 GO TO 255
3 0101 265 CONTINUE
4 C WRITE(3,240) (QUCTW(IH),NI=1,32)
5 240 FORMAT(1X,8E15.8)
6 C WRITE(3,239) N
7 239 FORMAT(1H,15)
8 NO = 0
9 IF(N-GE-LL) GO TO 270
10 GO TO 255
11 0108 270 CONTINUE
12 IF(IWR14.EQ.1) WRITE(3,224)
13 IF(IWR14.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
14 C TAKE THE INVERSE FOURIER TRANSFORM
15 IFSET = -1
16 CALL HARM(SIGNAL,M,INV,S,IFSET,IFERR)
17 WRITE(3,17) IFERR
18 IF(IWR15.EQ.1) WRITE(3,225)
19 IF(IWR15.EQ.1) WRITE(3,201) (SIGNAL(IST),IST=1,NUMBER)
20 C COMPRESS THE DATA BACK INTO ONE HALF THE ARRAY SO IT WILL BE IN THE
21 C PROPER FORM FOR A THREE ARRAY COMMON.
22 DO 271 IJH = 1,L
23 IJ = 2 * IJH
24 IJK = IJH
25 A = REAL(SIGNAL(IJK))
26 B = REAL(SIGNAL(IJ))
27 271 SIGNAL(IJK) = CMPLX(A,B)
28 IF(IWR16.EQ.1) WRITE(3,226)
29 RETURN
30 END
31
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SYMBOL	LOCATION	COMMON BLOCK / WAF	LOCATION	MAP SIZE	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
SIGNAL	0		8000						
SUBPROGRAMS CALLED									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
IBCON#	12C	HARH	130	CDVD#	134	CHPY#	138		
SCALAR MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
XNOH	1B8	XDENOH	1C0	MURB	1C8	IHR11	1CC	IHR12	1D0
IWR13	1D4	IWR14	1D8	IWR15	1DC	IWR16	1E0	IST	1E4
NUMBER	1E8	NUMA	1EC	L	1F0	LL	1F4	IIA	1F8
IIB	1FC	IIC	200	IID	204	G	208	H	20C
IFSET	210	IFERR	214	IIG	218	N	21C	NO	220
IDGRN	224	IDGRD	228	IIF	22C	CONSN	230	COMSD	234
IABD	238	IABC	23C	RFREQ	240	PERIOD	244	RFRSQ2	248
ARPAL	24C	ALMIG	250	NNO	254	IIF	258	IIF	25C
IJK	260	A	264	B	268				
ARRAY MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
N	26C	INV	278	S	27C	COFN	280	COPD	2A8
QUOTNT	2D0								
FORMAT STATEMENT MAP									
SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION	SYMBOL	LOCATION
200	300	201	306	210	3DF	221	409	222	436
223	494	224	4B5	225	4E8	226	50E	230	53F
231	545	232	54C	233	555	17	55F	1246	574
227	5AD	229	5D1	240	5DD	239	5E6		
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,NOLIST,DECK,LOAD,MAP									
OPTIONS IN EFFECT NAME = FLTRS / LINECNT = 58									
STATISTICS SOURCE STATEMENTS = 125, PROGRAM SIZE = 4256									
STATISTICS NO DIAGNOSTICS GENERATED									

```

1      C
2      0001 SUBROUTINE PSD(DIN,NUMBER,MNUHA)
3      0002 COMMON SIGNAL(4096),A(4096),WAF(4096),SPEC(120)
4      0003 DIMENSION DATA(4100),INV(512),S(512),AMP(2048)
5      0004 DIMENSION DIN(4096)
6      0005 210 FORMAT('
7      1 5 6 7 8 9 10*)
8      0006 310 FORMAT(I10,10F11.5)
9      0007 410 FORMAT(I10)
10     0008 DO 50 I=1,NUMBER
11     0009 50 DATA(I)=DIN(I)
12     0010 H=MNUHA-1
13     0011 CALL RHRH(DATA,H,INV,S,IPERR)
14     0012 WRITE(3,410) IPERR
15     0013 DO 100 J=1,NUMBER,2
16     0014 JP1=J+1
17     0015 J2=JP1/2
18     0016 AMP(J2)=SQRT(DATA(J)**2+DATA(JP1)**2)
19     0017 100 CONTINUE
20     0018 WRITE(3,210)
21     0019 NWAVE=NUMBER/4
22     0020 NHALF=(NWAVE/20)+1
23     0021 DO 200 J=1,NHALF
24     0022 IBEG=10*J-9
25     0023 IEND=10*J
26     0024 IF(IEND.GT.J2) IEND=J2
27     0025 WRITE(3,310) IBEG,(AMP(K),K=IBEG,IEND)
28     0026 200 CONTINUE
29     0027 SUM=0.0
30     0028 ND2=NUMBER/2
31     0029 DO 300 J=2,ND2
32     0030 SUM=SUM+AMP(J)*AMP(J)
33     0031 300 CONTINUE
34     0032 WRITE(3,510) SUM
35     0033 510 FORMAT(' VARIANCE EQUALS',F12.4)
36     0034 SUM=0.0
37     0035 NDB=NUMBER/8
38     0036 DO 500 J=2,NDB
39     0037 SUM=SUM+AMP(J)*AMP(J)
40     0038 500 CONTINUE
41     0039 WRITE(3,510) SUM
42     0040 DO 400 J=1,120
43     0041 SPEC(J)=AMP(J)
44     0042 400 CONTINUE
45     0043 RETURN
46     0044 END
47
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SYMBOL	LOCATION	SYMBOL	LOCATION	COMMON BLOCK / HAP	HAP SIZE	CIEO	SYMBOL	LOCATION	SYMBOL	LOCATION
SIGNAL	0	A	4000		8000		SPC	C000		
SUBPROGRAMS CALLED										
RRARM	CC	IBCOM#	D0			D4				
SCALAR MAP										
I	FO	NUMBER	F4			F8	WNUMA	PC	IFERR	100
J	104	JP1	108	J2	10C	110	WAVE	114	BHALF	114
IBEG	118	IBND	11C	K	120	124	SUM	128	MD2	128
ND8	12C									
ARRAY MAP										
DATA	130	INV	4140	S	4940	5140	AMP	7140	DIM	7140
FORMAT STATEMENT MAP										
210	7144	310	71EE	410	71C7	71CB	510			
OPTIONS IN EFFECT ID,EBCDIC,SOURCE,NOLLST,DECK,LOAD,HAP										
OPTIONS IN EFFECT NAME = PSD, LINECNT = 58										
STATISTICS SOURCE STATEMENTS = 44, PROGRAM SIZE = 30124										
STATISTICS NO DIAGNOSTICS GENERATED										
STATISTICS NO DIAGNOSTICS THIS STEP 2										

F88-LEVEL LINKAGE EDITOR OPTIONS SPECIFIED MAP,LIST
 DEFAULT OPTION(S) USED - SIZE=(100352,16384)

MODULE MAP

CONTROL SECTION	ENTRY	NAME	ORIGIN	LENGTH	NAME	LOCATION	NAME	LOCATION	NAME	LOCATION	NAME	LOCATION
		MAIN	00	37D8								
		PHOD	37D8	847E								
		PLTRB	BC58	151F4								
		PLFPA	20E50	151C4								
		TRIGGR	36018	1374								
		DELAYP	37390	D1E								
		AMPL	380B0	364								
		LIMIT	38418	6A0								
		WRITE	38AB8	258								
		PLTRW	38D10	1120								
		PLTRS	39E30	10A0								
		PSD	3AED0	75AC								
		IHCSSLOG *	42480	1B6								
		IHCFFMAXB*	42638	C9	ALOG10	42480	ALOG	42498				
		IHCSSAS *	42708	C4	MAX1	42638	HIN1	4264E	AMAX1	42664	ANLN1	4267A
		IHCSSCN *	427D0	1D9	CPY#	42708	CDVD#	42722				
		YRCLSCN *	429B0	26C	COS	427D0	SIN	427E8				
		IHCFFXIT*	42C20	1C	DCOS	429B0	DSIN	429CA				
		HARM *	42C40	1474	EXIT	42C20						
		IHCRCOMH*	440B8	F61	IBCON#	440B8	FDIOCS#	44174	INTSWTCH	44PFE		
		IHCRCOMH2*	45020	65D	SEODASD	45398						
		RANDH *	45680	15E								
		IHCPCVTH*	457E0	119D	ADCON#	457E0	FCVAOUTP	458BA	PCVLOUTP	4591A	FCVZOUTP	45A6A
		IHCFFPNTH*	46980	542	FCVLOUTP	45E18	FCVLOUTP	4631A	PCVCOUTP	46534	INT6SWCH	4681B
		IHCSTATN2*	46EC8	1CB	ARITH#	46980	ADJSTWCH	46DYC				
		IHCFFPIC*	47098	EBE	ATAN2	46EC8	ATAN	46EDC				
		IHCPIOS2*	47P58	52E	PIOSCS#	47098	FIOSBEP	4709E				
		IHCFFXPI*	48488	14F	FIXPI#	48488						
		IHCERRM *	485D8	5D4	ERRON	485D8	IHCERRR	485FO				

LINE	NAME	ORIGIN	LENGTH	NAME	LOCATION	NAME	LOCATION	NAME	LOCATION	NAME	LOCATION
1	ICPHAXI*	48BB0	C9								
2	RHARM *	48C80	62C	MAXO	48BB0	HINO	48BC6	AAIXO	48BDC	ANIXO	48BPF2
3	ICSSQRT*	492B0	145								
4				SQRT	492B0						
5	ICETRCH*	493F8	28E								
6				ICETRCH	493F8	ERRTRA	49400				
7	ICUATBI*	49688	638								
8	ICHOPT *	49CC0	3A0								
9	\$BLANKCCH	4A060	C1B8								
10											
11											
12	ENTRY ADDRESS		00								
13	TOTAL LENGTH		56248								
14											
15	***USERPPOG DOES NOT EXIST BUT HAS BEEN ADDED TO DATA SET										
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APPENDIX E

STANDARD OPERATING PROCEDURES

As mentioned in Section 6.0, a detailed standard operating procedure for z-axis rack alignment was developed for review by CDA personnel. This appendix documents that procedure.

Abbreviations

SR 1 = Scanning Radiometer Number 1
SR 2 = Scanning Radiometer Number 2
IR = Infrared
VIS = Visible
F&W = Flutter and Wow
SRR = Scanning Radiometer Recorder
S/C = Spacecraft
MUX = Multiplexer
DEMUX = Demultiplexer
RT = Real Time (CDA Tape Recorder set to 60 ips)
ST = Slow Time (CDA Tape Recorder set to 30 ips)
A7 Control
Panel = Z-Axis Compensation Rack main control panel
A7J3
A7J4 = Connectors or test points 3, 4, ..., 16 on
: control panel A7
A7J16
DVM = Digital Voltmeter (dc)

Note: The nomenclature RT F&W Discriminator #1, ST F&W Discriminator #2, etc. conforms to the RCA schematic for Rack 48 (last revision dated 5 December 1970). Connector designations are also based on this schematic.

List of Test Equipment

1 ea.	H-P 302 Wave Analyzer
1 ea.	H-P 240B Audio Oscillator
2 ea.	H-P 5245L Counter
1 ea.	H-P 3430A Digital Voltmeter (dc)
1 ea.	Ballentine 320 ac VTVM.

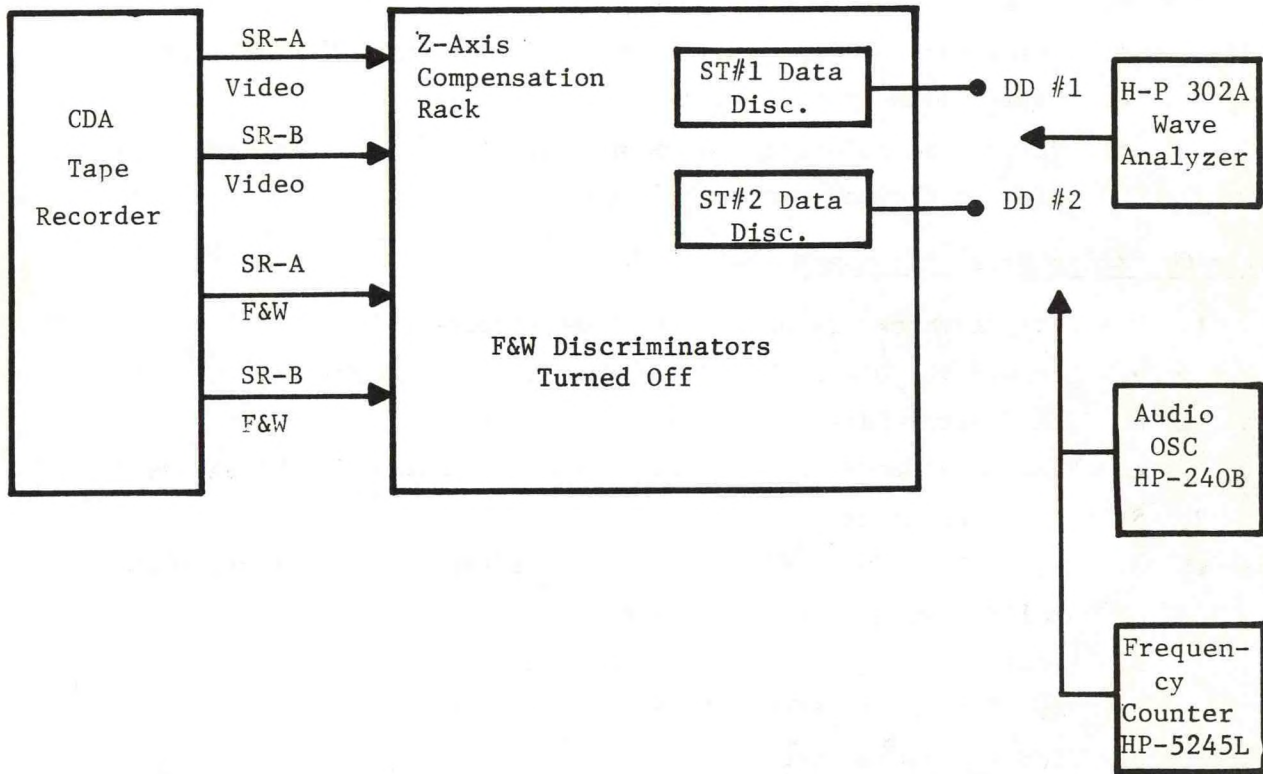
Z-Axis Alignment Standard Operating Procedures - Perform the following

Daily Checks:

- (1) F&W Discriminator Zero Balance
- (2) Data Discriminator and VCO Balance

Initial Set-Up For Delay Adjustment - (This initial set-up should only have to be done once. If pre-pass checks start to vary, this operation should be redone after notifying Suitland)

1. ST Mode Reference Data (Figure E-1)
 - a. Put test tape on recorder and set for ST/Ch A playback and 15 ips.
 - b. Connect H-P 302A Wave Analyzer to DD#1 and tune to f_{fL} (check with audio osc. and frequency counter). Turn off all F&W discriminators.
 - c. Adjust all delay line controls for minimum delay and set control panel for ST #1 operation.
 - d. Playback about 3 min. of tape and record 302A reading. Rewind tape to its starting point.
 - e. Tune HP 302A to f_{fH} (check with audio osc. and frequency counter) and repeat step 1.d.
 - f. Connect HP 302A to DD #2 and repeat steps 1.b. through 1.e. with control panel set to ST #2 operation.
 - g. Set tape recorder for ST/Ch B playback and 15 ips.
 - h. Repeat steps 1.b. through 1.f.
2. ST Mode Alignment (Figure E-1 with F&W Discriminators turned on).
 - a. Put test tape on recorder and set for ST/Ch A playback and 15 ips.
 - b. Set control panel to ST #1 operation and all F&W discriminators turned on.
 - c. Connect HP 302A to DD #1 and tune to f_{fH} (check).
 - d. Start tape recorder and adjust delay unit #1 until a minimum reading is obtained on the 302A. Record reading.
 - e. Rewind test tape to its start point.
 - f. Adjust 302A to f_{fL} and check.
 - g. Start tape recorder and record 302A readings. Let tape play through to the end. Rewind tape.
 - h. Set system for ST/Ch B playback.
 - i. Repeat steps 1.a. through 1.f. but DO NOT ADJUST DELAY LINE (just record readings on 302A).



Use to Set Frequency
of Wave Analyzer

Figure E-1. Initial Set-up for Delay Adjustment.

- j. Set system for ST/Ch A playback and 15 ips.
- k. Set control panel to ST #2 operation and all F&W discriminators turned on.
- l. Connect 302A to DD #2 and tune to f_{fH} (check).
- m. Start tape recorder and adjust delay unit #2 until a minimum reading is obtained on the 302A. Record reading.
- n. Repeat steps l.d. through l.g.
- o. Tune 302A to f_{fH} and check.
- p. Start tape recorder and record 302A reading. Rewind tape.
- q. Adjust 302A to f_{fL} and check.
- r. Start tape recorder and record 302A readings. Let tape play to the end and rewind tape.

Daily Check for Delay Adjustment

- 1. For data playback, connect as follows (Figure E-2).
 - a. Connect HP 302A to DD #1 and tune to f_{fH} (check).
 - b. Set Control Panel to ST #1/Ch A operation.
 - c. Place test tape on tape recorder and set recorder to 15 ips.
- 2. Start tape recorder
 - a. Adjust Delay Unit #1 for minimum reading on 302A (start with smallest delay increment, i.e. 25 μ s).
 - b. Record reading.
 - c. Tune 302A to f_{fL} (check) and record reading.
 - d. Stop and rewind tape.
- 3. Set Control Panel to ST #1/Ch B operation.
 - a. Tune 302A to f_{fH} (check).
 - b. Start tape recorder and record 302A reading. Stop tape.
 - c. Tune 302A to f_{fL} (check).
 - d. Start tape recorder and record 302A reading.
 - e. Stop and rewind tape.
- 4. Set Control Panel to ST #2/Ch A operation.
 - a. Connect 302A to DD #2 and tune to f_{fH} (check).
 - b. Start tape and adjust Delay Unit #2 for minimum reading on 302A (start with smallest delay increment, i.e., 25 μ s).
 - c. Record reading.
 - d. Tune 302A to f_{fL} (check) and record reading.
 - e. Stop and rewind tape.

5. Set Control Panel to ST #2/Ch B operation.
 - a. Repeat steps 3.a through 3.e.
6. Inform DDHS of any changes in Delay Unit Adjustments.

ST OPERATING MODE

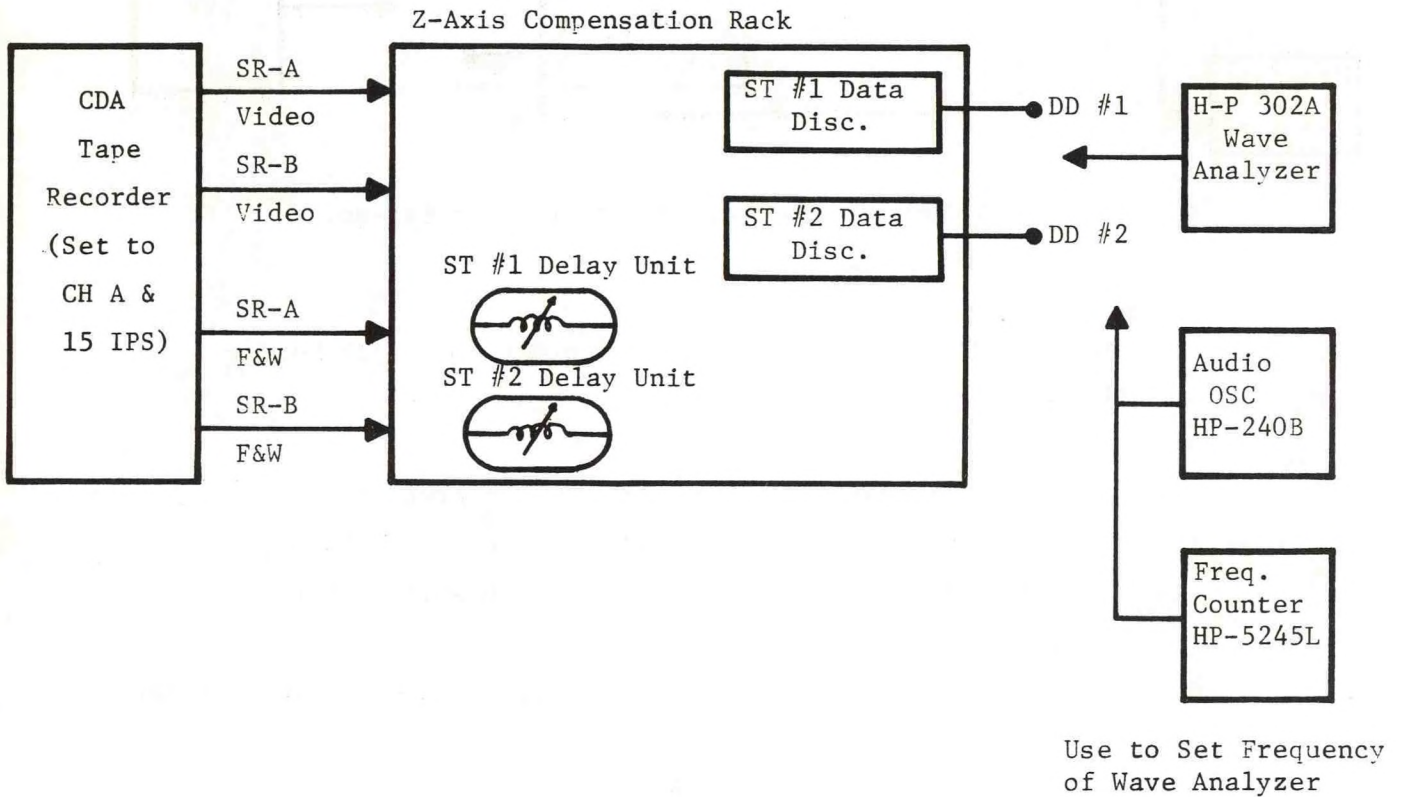


Figure E-2. Daily Check for Delay Adjustment.

OTHER DAILY CHECKS

1. F&W Discriminator Zero Balance (Figure E-3)

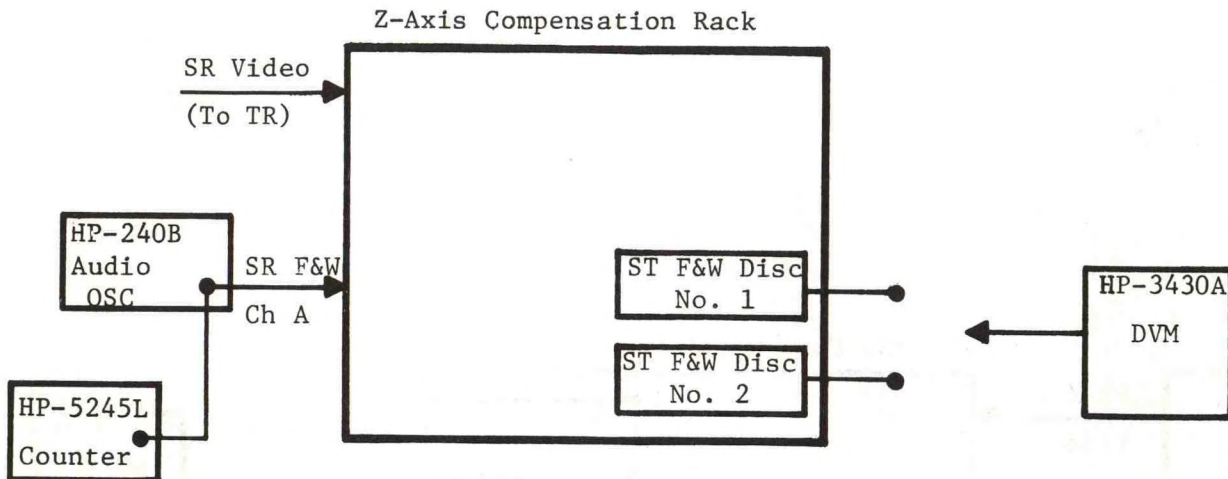


Figure E-3. F&W Discriminator Zero Balance Test Set-Up.

- a. Set Audio Oscillator to 1 v. (rms) output and 6.25 KHz. \pm 20 Hz.
- b. Connect DVM to ST F&W Disc. No. 1.
- c. Switch Control Panel to ST #1 Channel A operation.
- d. Adjust BAL control on front panel of Model 287T Channel Selector Plug-In of ST #1 F&W Reference Discriminator for 0 ± 0.005 volts dc on DVM.
- e. Set BANDEDGE VOLTS Control on RT #1 F&W Reference Discriminator fully clockwise.
- f. Connect DVM to ST F&W Disc. No. 2.
- g. Switch Control Panel to ST #2.
- h. Repeat 1.d. and 1.e. for ST #2 F&W Reference Discriminator.

2. Data Discriminator and VCO Balance (Figure E-4)

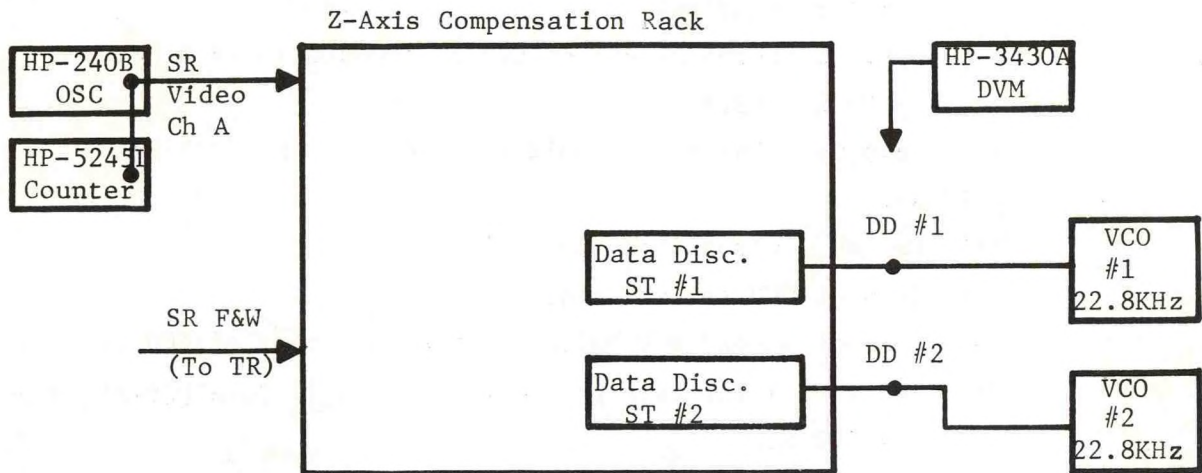


Figure E-4. Data Discriminator and VCO Balance Test Set-Up.

- a. Turn ST #1 and ST #2 F&W Discriminators off. Use DVM on their outputs (see 1. for connectors) to verify 0 volts dc output.
- b. Set Audio Oscillator to 1 volt (rms) output and 22.8 KHz. \pm 20 Hz.
 - (1) Switch Control Panel to ST #1.
 - (2) Connect DVM to DD #1.
 - (3) Connect second H-P 5245L Counter to output of VCO #1.
 - (4) Adjust BAL control of ST #1 Data Discriminator for $0 \pm .005$ volts dc on DVM.
 - (5) Adjust FREQ. Control of VCO #1 for a frequency output of 22.8 KHz. \pm 20 Hz. on second counter.
 - (6) Set Audio Oscillator to 1 volt (rms) output and 26.4 KHz \pm 20 Hz. (UBE)
 - (7) Adjust BANDEDGE VOLTS control on ST #1 Data Discriminator for + 5.0 volts dc on the DVM.
 - (8) Adjust INPUT control of VCO #1 for an output frequency of 26.4 KHz. \pm 20 Hz. (UBE) on second counter.
 - (9) Set Audio Oscillator to 1 volt (rms) output and 19.2 KHz. \pm 20 Hz. (LBE)

- (10) Reading on DVM should be approximately -5.0 volts
(record reading).
 - (11) Record frequency out of VCO #1 (should be 19.2 KHz.
± 20 Hz. LBE).
- c. Set Audio Oscillator to 1 volt (rms) output and 22.8 KHz.
± 20 Hz.
- (1) Switch Control Panel to ST #2.
 - (2) Connect DVM to connector DD #2.
 - (3) Connect second H-P 5245L counter to output of VCO #2.
 - (4) Repeat 2.b.(4) through 2.b.(11) on ST #2 Data Discriminator
and VCO #2.

Master Test Tape Recording

1. In order to align the z-axis rack, it is required that only a single tone be recorded on the visible and/or IR tracks of the SRR. This means that the portion of the SR Processor which multiplexes the SR output with telemetry, step wedge, etc., data must be defeated.
2. The two equipments which will lead to the greatest time delay difference between the SR IR/Visible channel and the F&W channel are the spacecraft multiplexer and the ground-station demultiplexer. In recording the master tape, it is required that MUX, DEMUX and 14-track tape recorder be as similar as possible to the actual operational equipment.
3. The diagram in Figure E-5 indicates roughly how the tape is to be made. No Visible, Data or telemetry are shown since none of these signals are desired. No particular attention has been given to levels; however, attenuators or amplifiers may be necessary. The four cables from the output of the DEMUX to the 14-track tape recorder should all be of equal length. If possible, a virgin tape should be used on the 14-track recorder and it should be completely filled (end-to-end on tracks 5, 7, 9, 11) with test tone data. The two most important points to remember about this test tape are
 - (a) Continuous tones must be recorded on tracks 5, 7, 9, 11 of the 14-track recorder. Thermal vacuum data are not sufficient since they are not constant in amplitude due to the time-multiplexed data on the SR video output.
 - (b) Short of changing the spacecraft connections to eliminate unwanted data, the system should be as close as possible to operational conditions.

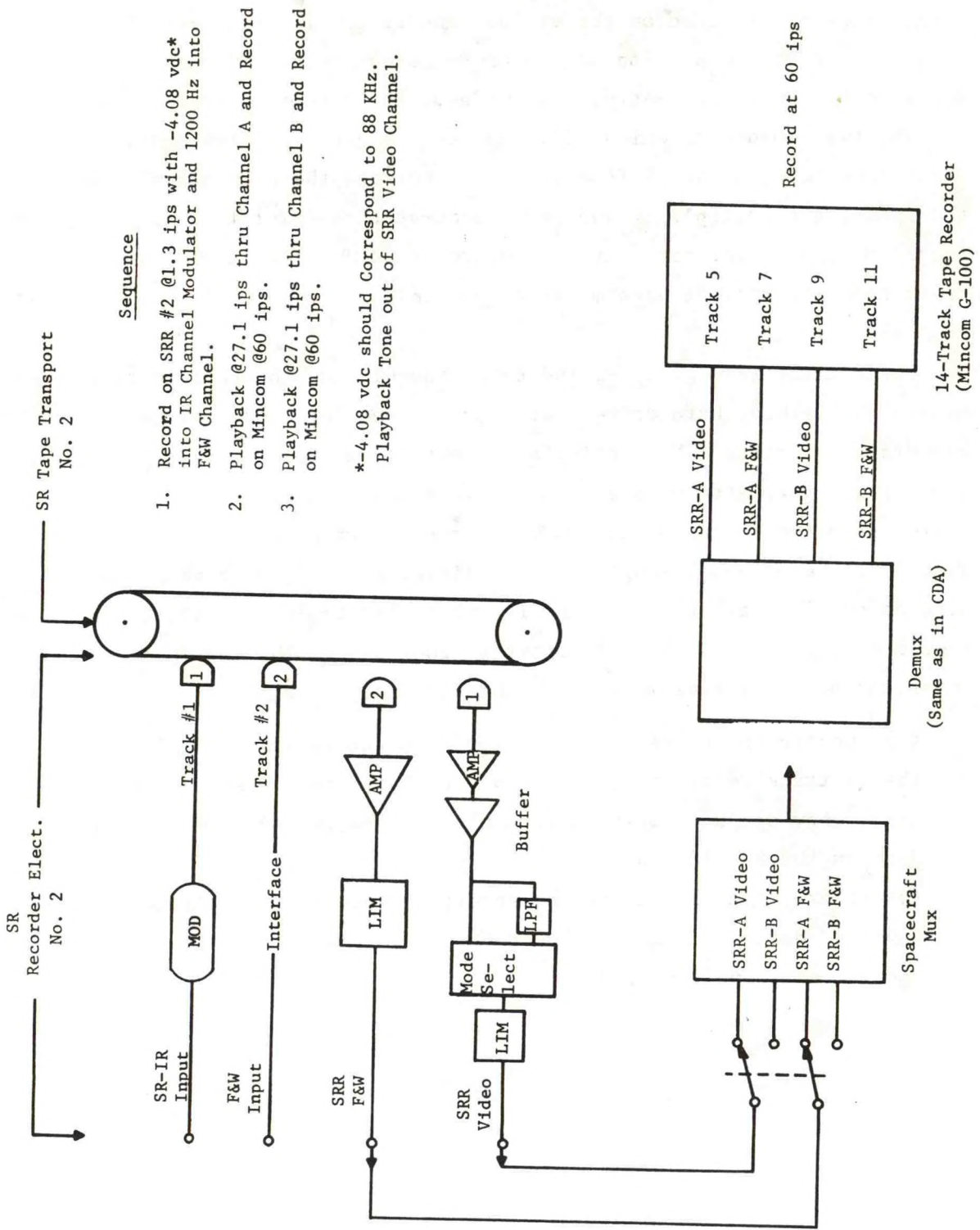


Figure E-5. Master Tape Recording Set-Up.

10.0 REFERENCES

- 2-1. Carlson, A. B.: Communication Systems - An Introduction to Signal and Noise in Electrical Communication. McGraw-Hill, 1968.
- 2-2. Black, H. S.: Modulation Theory. Van Nostrand, 1962.
- 3-1. EMR Model 287A-02 Subcarrier Discriminator (Revision E) - Instruction Manual, EMR Telemetry, April 1970.