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The evaluation of mixing methods in HYSPLIT using measurements from controlled tracer experiments

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Abstract

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The HYSPLIT dispersion model has different options to estimate the turbulent mixing depending on the availability of stability and turbulent parameters in the meteorological data. Dispersion simulations using different mixing options were conducted to simulate two controlled tracer experiments – the Project Sagebrush phase 1 (PSB1) for the sub-kilometer transport and the Cross Appalachian Tracer Experiment (CAPTEX) for the long-range transport. Through the comparisons of velocity variance and the evaluations of tracer concentrations, we evaluated different estimations of the turbulent velocity variance affecting the dispersion results. The mixing options in HYSPLIT are the Beljaars-Holtlag (BH) method, the Kantha-Clayson (KC) method, the turbulent kinetic energy (TKED) option, and the turbulent exchange coefficient (EXCH) option. The KC and EXCH method produced a larger maximum of the vertical velocity variance and at a higher altitude than other mixing options did. The vertical velocity variance profile of the BH scheme had a sharp increase from the surface to the height of the maximum values. The TKED option generated a flat profile with the smallest variation in its value with height. The plumes generated by the BH and TKED method (weaker mixing) had higher concentrations near the surface than those driven by the KC and EXCH option (stronger mixing). The statistical rank for the dispersion result using the TKED option was slightly better than others while the BH mixing generated results with a roughly worse rank. No mixing option always outperformed the other options. HYSPLIT users can select a mixing option according to the scenario and availability of meteorological fields, and use different options to generate dispersion ensembles.

Keywords: HYSPLIT, dispersion, PSB1, CAPTEX, turbulent velocity variance

60 **1. Introduction**

61 To simulate the movement of pollutants in the atmosphere, a Lagrangian model
62 simulates the emission by releasing many particles at the source location over a period of
63 time. By adding a random component according to the dispersive nature of the
64 atmosphere to the advective motion of each particle, the particles released at the source
65 will be transported and mixed in space and time (Draxler and Hess, 1998). The turbulent
66 component of the process is the product of the computer-generated random number and
67 the standard deviation of the turbulent velocity. HYSPLIT, the dispersion model
68 developed by the National Oceanic and Atmospheric Administration Air Resource
69 Laboratory, uses regional and global products from various numerical weather models –
70 the Weather Research and Forecasting (WRF; Powers et al. 2017) model, the Global
71 Forecast System (GFS; Kanamitsu, 1989) model, the Modern-Era Retrospective analysis
72 for Research and Applications (MERRA; Rienecker et al. 2011), the European Center for
73 Medium-Range Weather Forecasts (ECMWF; Dee et al. 2011), etc. Depending on the
74 availability of stability and turbulent parameters in the meteorological data used to drive
75 the dispersion simulation, users can choose different options in HYSPLIT to estimate the
76 turbulent velocity variances (Stein et al. 2015). The estimation can be based on the
77 stability function diagnosed from other meteorological variables such as friction velocity
78 and mixing height. If the meteorological model does not provide them, temperature and
79 wind soundings are used to diagnose the boundary layer stability parameters. Other
80 methods include using the total turbulent kinetic energy (TKE) or mixing diffusivity to
81 calculate the standard deviation of turbulent velocity (Draxler and Hess, 1997).

82 The main goal of this study is to understand the mixing characteristics generated
83 by different estimations of the turbulent velocity variance affecting the dispersion results.
84 Toward this aim, we conducted meteorological simulations with the Advanced Research
85 core of WRF for the Project Sagebrush phase 1 (PSB1; Finn et al. 2016). The WRF
86 output includes variables required for computing stability parameters, as well as total
87 turbulent kinetic energy and turbulent exchange coefficient so that we can compare and
88 evaluate all mixing options in HYSPLIT with observations taken during the tracer
89 experiment. PSB1 consisted of five tracer releases in the afternoons of October 2013 and
90 aimed for the sub-kilometer scale transport with near neutral or unstable stability
91 conditions. Flux measurements, including turbulent velocity variance, are available along
92 with tracer concentration observations, which provides a platform for the direct
93 evaluation of the turbulent variables and the evaluation of dispersion results
94 corresponding to different mixing options. Prior to this study Ngan et al. (2018) assessed
95 the performance of the WRF-HYSPLIT modeling system for the dispersion scenario
96 represented by PSB1, featuring daytime convective conditions at fine spatial (a few
97 hundred meters) and temporal (10-min averaging) scales. The turbulent mixing is an
98 essential component affecting HYSPLIT's performance but not yet investigated in the
99 previous study. Thus, in the current work, we focus on evaluating the turbulent mixing
100 methods available in HYSPLIT and their impacts on dispersion results as compared
101 against PSB1 which offers a unique set of observations for the comparison of both
102 velocity variance and tracer concentration. In addition, we conducted HYSPLIT
103 simulations driven by the WRF data using different mixing options for the Cross
104 Appalachian Tracer Experiment (CATEX; Ferber et al. 1986). Unlike the Sagebrush

105 experiment focusing on a fine spatial and temporal scale, CAPTEX consisting of six 3-h
106 releases aimed to simulate the long-range transport and diffusion of pollutants. The
107 evaluations of dispersion results with measured concentrations provide the insight to
108 assess the performance of different mixing methods.

109 The rest of the paper is organized as follows. Section 2 reviews the different
110 options in HYSPLIT to compute the velocity variance. Section 3 describes the model
111 configurations for the meteorological and dispersion models. In Section 4, we evaluated
112 the velocity variance computed in HYSPLIT with measurements taken during the
113 Sagebrush experiments. The dispersion simulations for the controlled tracer experiment –
114 PSB1 and CAPTEX were compared with measured concentration in Sections 5 and 6,
115 respectively. Finally, Section 7 presents the conclusions and future research directions.

116 **2. Overview of mixing options in HYSPLIT**

117 To compute the transport and mixing of particles, HYSPLIT treats the advection
118 and dispersion processes separately. The advection calculation uses the three-dimensional
119 velocity field while the dispersion calculation requires the standard deviations of the
120 turbulent velocity $\{\sigma_i = [\sigma_w, \sigma_u, \sigma_v]\}$ to add a random component to the advective motion.
121 There are different methods to estimate the standard deviation of turbulent velocity based
122 on the availability of stability and turbulent parameters in the meteorological data. The
123 full list of equations for all parameters associated with each method is in Draxler and
124 Hess (1998). An abstract of the four mixing options available in HYSPLIT is described
125 below.

126 *a. Beljaars-Holtslag (BH) method*

127 Following Beljaars and Holtslag (1991) for a stable surface layer, and Betchov
128 and Yaglom (1971) and Kadar and Perepelkin (1989) for an unstable surface layer, the
129 model computes the normalized profiles for heat and momentum, and then the vertical
130 mixing coefficient according to the profiles and other stability parameters such as friction
131 velocity, convective velocity scale, and Obukhov length. To obtain the vertical velocity
132 variance, the model divides the diagnosed mixing coefficient by a Lagrangian time scale.
133 This option is labeled hereafter as “BH”.

134 *b. Kantha-Clayson (KC) method*

135 Following Kantha and Clayson (2000), the model defines the turbulent velocity
136 variances as a function of friction velocity, convective velocity scale, and boundary layer
137 depth. HYSPLIT uses it as the default when the momentum and heat flux variables are
138 available in the meteorological data. This method (named hereafter “KC”) does not need
139 the intermediate step of computing the mixing coefficient and the use of turbulent time
140 scales.

141 *c. Using the turbulent kinetic energy (TKED)*

142 If the meteorological data provide the turbulent kinetic energy, the model
143 partitions the values to the vertical and horizontal components using the anisotropy ratio.
144 According to experimental data, about one-third of TKE are assigned to the vertical
145 velocity variance while twice as much of the values are partitioned to the horizontal
146 components. HYSPLIT uses this as default anisotropy. However, users can let the model
147 compute the anisotropy factors according to the Kantha-Clayson equations instead of
148 using a partitioning factor constant in space and time. This option is labeled hereafter as
149 “TKED”.

150 *d. Using the turbulent exchange coefficient (EXCH)*

151 This method computes the velocity variance by dividing the turbulent exchange
152 coefficient by the vertical Lagrangian time scale, which is set to 100 s following Draxler
153 and Hess (1998). This option is labeled hereafter as “EXCH” and is newly added to
154 HYSPLIT with using the WRF meteorology. The turbulent exchange coefficient is
155 computed within the user-selected planetary boundary layer (PBL) parameterization in
156 WRF. The two classes of PBL approaches are 1.5-order TKE based schemes and first-
157 order diagnostic K-profile schemes. The former diagnoses the exchange coefficient as a
158 function of the mixing length, stability function, and prognostic TKE while the latter
159 computes it from variables such as velocity scale, PBL height, and Prandtl number (Shin
160 and Dudhia, 2016).

161 **3. Experimental Data and Model Configurations**

162 The Project Sagebrush phase 1 tracer fields experiment took place at the Idaho
163 National Laboratory (43.59 N and 112.94 W) during October 2013 to understand sub-
164 kilometer dispersion by performing continuous 2.5-h inert tracer (SF₆) releases over flat
165 terrain (Finn et al. 2016). Tracer releases were conducted on five afternoons (intensive
166 observation periods, or IOPs) under either neutral or unstable stability conditions. The
167 measurement network consisted of five concentric arcs located from 200 – 3200 m away
168 from the release location. Tracer samples were obtained starting 30 minutes after the
169 release in 10-min intervals. Comprehensive meteorological measurements, including
170 turbulent velocity variance data, were available during the experimental period.

171 The WRF Version 3.7 was used to generate meteorological data for the controlled
172 tracer experiments. The domain configuration and physic options followed Ngan et al.
173 (2018) for PSB1. In this study, we selected the Mellor-Yamada-Nakanishi-Niino (MYNN)
174 2.5 level TKE scheme (Nakanishi and Niino, 2006) for the planetary boundary layer
175 (PBL) parameterization and the corresponding MYNN surface layer scheme which works
176 together with the Noah land surface model (Chen and Dudhia, 2001) as lower boundary
177 conditions to provide the surface forcing for the vertical transport (Shin et al. 2012). The
178 evaluations in Ngan et al. (2018) showed that the meteorological data for IOP4 and IOP5
179 featuring unstable conditions with moderate winds were simulated well by WRF.
180 However, the model performance was degraded due to the underestimation of strong
181 winds in IOP3 with neutral conditions and the inaccurate prediction of wind direction in
182 IOP2 featuring unstable conditions with light winds. This study did not include IOP1 due
183 to the sampling network not observing the plume (Finn et al. 2015). HYSPLIT
184 simulations were configured following Ngan et al. (2018); 250,000 Lagrangian particles
185 were released and lasted two-and-a-half hours. The tracer concentration was calculated
186 by summing particles in the volume of 100 x 100 m and from the surface to 25 m above
187 ground. Time averaging was set to 10 minutes. HYSPLIT was driven by WRF model
188 output with a horizontal resolution of 0.333-km (the most inner WRF domain) and a
189 temporal resolution of 5 minutes. A sensitivity test on the meteorological grid and its
190 impact on the dispersion results for tracer releases in PSB1 was presented in Ngan et al.
191 (2018). The analysis shows that under the meteorological conditions represented by PSB1,
192 the HYSPLIT results for IOP 2, 4, and 5 were not sensitive to the grid resolution of the

193 WRF data. The mixing options described in Section 2 were used to simulate four IOPs
194 conducted in PSB1.

195 CAPTEX took place in the northeastern United State and southeastern Canada
196 from mid-September through the end of October 1983. An inert perfluorocarbon tracer
197 were released to simulate the transport and dispersion of pollutants at scales of hundred to
198 a thousand kilometers (Ferber et al. 1986). Six 3-h releases were conducted at Dayton,
199 Ohio during the afternoon (releases 1-4) and at Sudbury, Ontario, Canada during the
200 nighttime (releases 5 and 7). The measurement network included 85 ground-level stations
201 distributed 300 – 800 km from the source, providing 3- and 6-h average tracer
202 concentrations for three-day periods after the tracer release. WRF data with a horizontal
203 resolution of 9 km was the meteorological input to drive HYSPLIT. The WRF simulation
204 was initialized by the WRF archived dataset and nested in the coarse resolution domain
205 introduced in Ngan and Stein (2017). The simulation used the MYNN 2.5 level TKE-
206 based PBL scheme and its corresponding surface layer scheme, while other physics
207 options followed Ngan and Stein (2017). The hourly meteorological files were used to
208 drive HYSPLIT simulations running with the four mixing options. A concentration grid
209 with ~25-km horizontal resolution was set for the simulations with one vertical layer
210 from 0 – 100 m above ground. Detailed information of each release is described in Ngan
211 and Stein (2017).

212 **4. Comparisons of the velocity variances**

213 Figure 1 is the layout of the sampling arcs for the tracer concentration and the
214 meteorological observation taken during PSB1. The velocity variance (or the standard

215 deviation of velocity) was measured at six locations and different heights (Table 1) with
216 two sodars at the ASC and ART stations, and 3-d sonic anemometers at the other velocity
217 variance sites (Finn et al. 2016). The measurement of TKE by the ASC site tended to
218 match well to the measurement of TKE by the five other sites using the 3-d sonic
219 anemometer while the TKE measurement at the ART site was an order of magnitude
220 higher than the others. Note that the vertical turbulence measurements at these two sodar
221 sites are roughly similar in magnitude much of the time. The difference between two
222 sodars for the observed TKE arises from the measurements along the u and v beams
223 (Finn et al. 2015). Thus, we excluded the ART sodar results that are probably not reliable
224 for the model comparison. This section discusses the velocity variance estimated by
225 different mixing options in HYSPLIT and shows the evaluations with observations taken
226 during PSB1.

227 *a. Comparisons of the vertical velocity variances*

228 The vertical velocity variance determines how the particles released at the source
229 location are dispersed in space and time. Figure 2 (a – d) is the profile of the vertical
230 velocity variance from HYSPLIT using four different mixing options during 12 – 15
231 MST on October 5th, 2013 (IOP2). Both BH and KC methods diagnose the vertical
232 velocity variance based upon state variables and variables relevant to the PBL stability.
233 Depending on the stability regimes and the altitudes (within the surface layer, in the PBL,
234 or in the free atmosphere), the model has a different set of equations to diagnose the
235 mixing of particles (Draxler and Hess, 1998). Other than the maximum at the middle of
236 PBL, the profile of BH and KC mixing options had a secondary maximum transitioning
237 from the top of the PBL to the free atmosphere (Figure 2 a and b). The vertical velocity

238 variance profile from the KC option had a small peak within the surface layer while the
239 one from the BH option went to almost zero values near the surface. As shown in Figure
240 2 c and d, the vertical velocity variance profiles from TKED and EXCH options looked
241 quite different. These two methods depend on the profile of TKE and exchange
242 coefficient provided by WRF, respectively. The definition of TKE is the summation of
243 velocity variances (horizontal and vertical) divided by two that represents the strength of
244 turbulence in the flow. It is computed in WRF's PBL schemes (the MYNN schemes in
245 this study) using the prognostic TKE equation. The turbulent exchange coefficient is a
246 scalar to relate the turbulent flux to the gradient of the associated mean variable. The
247 MYNN PBL scheme diagnoses the exchange coefficient according to the prognostic TKE,
248 a mixing length, and a stability function (Nakanishi and Niino, 2006).

249 There are studies, such as Munoz-Esparza et al. (2018), Ferrero et al. (2018), and
250 Hari Prasad et al. (2017), showing the problem of the TKE estimation produced by
251 various WRF's TKE-based PBL schemes. Ferrero et al. (2018) evaluated several PBL
252 parameterizations available in WRF with experimental data conducted in Turin, Italy.
253 The results showed the underestimation of the model TKE in comparison with the
254 measurements (anemometer at 25 m height) in a summer month and less underestimation
255 of TKE in a winter month. We compared the predicted TKE from WRF with observed
256 TKE taken at 30 m height of the GRI tower during PSB1. In addition to the MYNN run,
257 other simulations were conducted with different TKE-based PBL schemes, including the
258 Bougeault and Lacarrere scheme (BouLac; Bougeault and Lacarrere, 1989), the Quasi-
259 Normal Scale Elimination scheme (QNSE; Pergaud et al. 2009), the UW boundary layer
260 scheme (UW; Bretherton and Park 2009), the Mellor-Yamada-Janjic (MYJ; Janjic, 1994),

261 and the Grenier-Bretherton-McCaa (GBM; Grenier and Bretherton 2001). The
262 comparison showed all modeled TKE values were underestimated (Figure 3). Among
263 various PBL schemes, the BouLac underpredicted the least and MYNN was the second
264 least underprediction of TKE. The run using MYJ and QNSE schemes underpredicted the
265 most. The length scales and TKE prediction cause the differences in turbulent exchange
266 coefficient computed by various PBL schemes. Among the six schemes, the GMB and
267 UW schemes produced larger exchange coefficient while the QNSE and BouLac had
268 smaller values during PSB1 (not shown). Thus, these meteorological uncertainties may
269 have impact on the dispersion result when we use TKED and EXCH mixing options to
270 estimate the turbulent velocity variance.

271 The observational tower at the ASC station provides vertical profiles of velocity
272 variance from 30 – 150 m. Observed vertical velocity variance at ASC ranges from 0.2 –
273 $0.9 \text{ m}^2\text{s}^{-2}$ with the maximum at about 100 m height (Figure 2e). Note that the stability
274 condition on the day of IOP2 was unstable with low wind speeds. The KC and EXCH
275 option generated a maximum vertical velocity variance of about $1.5 \text{ m}^2\text{s}^{-2}$ at an altitude of
276 about 500 m. The TKED profile had the smallest maximum values (about $0.5 \text{ m}^2\text{s}^{-2}$)
277 among all and a smooth decrease with height from a maximum value to a minimum value
278 in the free atmosphere. In the BH case, the vertical velocity variance profile at about 100
279 m height was similar to the observations but the maximum value was slightly
280 underestimated. Figure 4 is the vertical velocity variance profiles for IOP5 (12 – 15 MST
281 on October 18th, 2013), which was a weakly unstable condition with moderate wind
282 speeds. The modeled vertical velocity variance had less variation throughout the
283 afternoon than the observed values. In comparison with other options, the EXCH profile

284 showed larger temporal variability. Note that the sodar measurements for the turbulent
285 velocity variance available in PSB1 were limited to 30 – 150 m height. The study of Berg
286 et al. (2017) using year-long vertical variance data from Doppler Lidar data for the
287 convective boundary layer showed that the maximum of the composite vertical velocity
288 variance was about $1.2 \text{ m}^2\text{s}^{-2}$ at about 200 – 700 m height. Thus, the velocity variance
289 measurements from PSB1 were insufficient to evaluate the simulated maximum vertical
290 velocity variance, which might occur at the altitude above the sodar could reach.

291 The comparison of vertical velocity variance at and below 30 m was done using
292 measurements of 3-d sonic anemometers at the FLX station (3.2 m; Figure 5) and the
293 GRI station (30 m; Figure 6). The magnitude of the observed vertical velocity variance in
294 the afternoons of four IOPs was about $0.2 \text{ m}^2\text{s}^{-2}$ near the surface (3.2 m height). IOP 3
295 was an exception that its value went up to $0.6 \text{ m}^2\text{s}^{-2}$. As discussed in Finn et al. (2015),
296 tracer releases in PSB1 were conducted on days with unstable (or weakly unstable)
297 stability conditions but IOP3 experienced a neutral condition with strong wind speeds.
298 The meteorological evaluation presented in Ngan et al. (2018) showed that WRF failed to
299 generate the rapid increase of high wind speeds observed during IOP3 causing negative
300 bias for the friction velocity. Thus, we expected the KC option would underestimate the
301 turbulent mixing because the velocity variances were diagnosed as a function of friction
302 velocity. In general, the KC and TKED mixing methods overestimated the vertical
303 velocity variance (except IOP3) while the EXCH mixing slightly underestimated it. At 30
304 m height (GRI station), the observed vertical velocity variance was about $0.4 - 0.6 \text{ m}^2\text{s}^{-2}$.
305 The KC, TKED, and EXCH options generated the values comparable to the
306 measurements while the vertical velocity variance from KC was larger than those from

307 other mixing options. The vertical velocity variance generated by the BH method was
308 underestimated the most in the comparison with measurements at both 3.2 m and 30 m.

309 *b. Estimation of the horizontal velocity variances*

310 The mixing methods determine the way the meteorological data are processed to
311 compute vertical and horizontal turbulence. In this study, the horizontal velocity variance
312 was obtained in proportion to the vertical component. Figure 7 is the time series of
313 horizontal velocity variance at the FLX station. The magnitude was about $1.2 - 1.8 \text{ m}^2\text{s}^{-2}$
314 in the afternoon during the period of tracer release. For the BH mixing scheme, the
315 diagnosed turbulence is portioned equally between the vertical and horizontal component
316 resulting in a larger negative bias in the horizontal velocity variance. For the KC and
317 TKED mixing options, the calculation has more turbulence going into the horizontal
318 component than the BH method does (Stein et al. 2015). The horizontal velocity variance
319 in KC and TKED mixing were comparable to the measured values with a small
320 underestimation. The underestimations of horizontal velocity variances were more
321 significant in IOP3 than other episodes because of the under-prediction of the wind fields
322 and vertical mixing.

323 Using velocity variance measurements taken at different locations and heights in
324 the area of the sampling array, we computed the ratio of the horizontal and vertical
325 components (Table 1). The right-most column of the table includes the data only in the
326 afternoon of four IOP days. The ratio was in the range of $4.5 - 5.8$ for data measured near
327 the surface at 3.2 m or 4 m height. It became smaller, ranging about $1.5 - 2.6$, when using
328 data observed at higher levels (30 m or 45 m). The sodar measurement at the ASC station
329 showed the ratio of horizontal and vertical velocity variance got to about a one to one

330 ratio at 130 m. For the EXCH mixing option, we selected the maximum (5.8733) and
 331 minimum value (1.5430) of the ratios at near surface and 45 m height, respectively. They
 332 were applied to compute the horizontal velocity variance. Two cases, labeled as “EXCH”
 333 and “EXCHm” using the maximum and minimum ratios, respectively, were included in
 334 Figure 7. With a larger scaling factor, EXCH had a larger horizontal velocity variance
 335 than EXCHm which used a smaller scaling factor. However, both cases underestimated
 336 horizontal velocity variance in comparison with the measurements at 3.2 m height. For
 337 the comparison with data at 30 m height, the underestimation decreased.

338 **5. Dispersion results for PSB1**

339 We conducted HYSPLIT simulations performed with different turbulent mixing
 340 parameterizations and driven by WRF meteorological model output for the four IOPs
 341 from PSB1. The mixing options described in the previous section were labeled as BH,
 342 KC, TKED and EXCH. For the mixing option using WRF’s turbulent exchange
 343 coefficient, we conducted two simulations “EXCH” and “EXCHm” by applying the
 344 maximum and minimum ratio of the horizontal and vertical component of measured
 345 velocity variance. The statistical evaluation followed Draxler (2006) which introduced a
 346 cumulative score (so called the Rank, ranging from 0 to 4) including four normalized
 347 components – the correlation coefficient (R), fractional bias (FB), figure-of-merit in
 348 space (FMS), and Kolmogorov-Smirnov parameter (KSP).

$$349 \quad Rank = R^2 + 1 - \left| \frac{FB}{2} \right| + \frac{FMS}{100} + \left(1 - \frac{KSP}{100} \right)$$

350 Figure 8 shows the statistical rank of five dispersion simulations for each IOP in
 351 PSB1. The model performed differently with varying mixing options for different

352 episodes, but no one mixing option always produced a better result. In general, the range
353 of statistical scores of simulations using different mixing options for IOP4 and IOP5 was
354 smaller than those for the other two IOPs, possibly due to WRF more accurately
355 simulating the wind patterns during IOP4 and IOP5 than IOP2 and IOP3. Other than the
356 dispersion process in which the estimation of turbulent velocity variance is an essential
357 component, the advection process driven by the mean winds determines the movement of
358 the tracer plume. In the IOP4 and IOP5 scenarios, the tracer plume was transported by
359 northwesterly flows steadily from the source toward the outer arcs of the sampling array
360 and without much variation throughout the release duration. In general, the rank for
361 EXCH was better than EXCHm for all four episodes because the larger horizontal
362 velocity variance in the EXCH simulation generated a wider plume. However, the
363 dispersion result was not very sensitive to the horizontal velocity variance since the wind
364 shear was the dominant factor for the spreading of the plume in the horizontal direction.

365 IOP2 had the lowest rank among all four episodes due to the inaccurate prediction
366 of varying wind directions associated with the light winds. The modeled plume was
367 narrower and further downwind, going northeastward to the outer arcs of the sampling
368 array, than the observed plume (Figure 9). In this case, the strong mixing produced by
369 the KC and EXCH method was able to disperse particles more, which resulted in less
370 overestimation (smaller FB in the rank bar-chart) of the tracer concentration compared to
371 other cases. We notice the underprediction of TKE in the comparison of the observed
372 values at the ASC station (not shown) that caused the weak mixing in the TKED method.
373 A sensitivity test was conducted using two times of TKE values from WRF to drive a
374 dispersion simulation with the TKED mixing option. This result had better statistical

375 scores (Rank=1.67) compared to the result shown in Figure 9 (Rank=1.47) because the
376 stronger mixing was able to improve the overprediction of the surface concentration and
377 the coverage of the plume.

378 For IOP3, even though the rank had better statistical scores than IOP2, the
379 simulated plume went out of the sampling array at the beginning of the release. The
380 weaker mixing generated by the BH and TKED method resulted in higher concentrations
381 near the source location (better FB in the rank bar-chart) than EXCH did. However, the
382 BH plume was narrow due to the significant underestimation of the horizontal velocity
383 variance that resulted in getting the worst rank. For the scenario of IOP3, the strong
384 mixing in the EXCH simulation caused more underprediction of surface concentration
385 (worse FB) than other cases. Compared to the TKED plume (Figure 10d), the EXCH
386 plume had a lower concentration and was slightly wider. The surface wind measurements
387 indicated strong southwesterly winds during the tracer release while WRF generated light
388 wind speeds and varying wind directions until southwesterly winds picked up during the
389 second hour of the release (Ngan et al. 2018). The underestimation of the turbulence near
390 the surface in the KC mixing option (referring to Figure 5 and Figure 6) due to the
391 negative bias in the wind speed and friction velocity might cause less mixing than others.
392 As shown in the difference plot (Figure 10c), the KC case had more particles
393 accumulating near the source location (in the area within the 200-m arc) while the TKED
394 run moved particles farther away.

395 **6. Dispersion results for CAPTEX**

396 HYSPLIT simulations driven by WRF with 9-km grid spacing were conducted
397 using the four mixing options for the six releases during CAPTEX. Figure 11 shows the
398 time series of vertical velocity variance profiles for 24 hours after the beginning of an
399 afternoon tracer release at Dayton, Ohio (CAPTEX 1). The KC and EXCH mixing had
400 the maximum vertical velocity variance at the 10th model layer (~900 m) during the
401 afternoon hours (17 – 21 UTC). The maximum values were smaller and occurred at the
402 lower layers in the other two mixing methods. The profile of the vertical velocity
403 variance generated by the TKED method was flat with values ranging from about 1.0 –
404 $1.4 \text{ m}^2\text{s}^{-2}$ from the surface to the middle of the PBL where the maximum was observed.
405 However, the profile in the EXCH mixing option had large gradients near the surface (the
406 lowest 3 model layers, 0 – 70 m) and at the top of PBL (13th – 15th model layer, 1.5 – 2.0
407 km). During the nighttime, close to zero vertical velocity variance values were produced
408 by the EXCH mixing. This is due to a constant Lagrangian time scale that was used for
409 the daytime unstable condition. Unlike PSB1 episodes that all occurred in the afternoon
410 with well-mixed conditions, for scenarios like CAPTEX experiencing different stability
411 conditions throughout the day, a time-varying Lagrangian time scale will be more
412 appropriate for estimating the turbulent velocity variance. Figure 12 is an example of
413 CAPTEX 7, which was a nighttime release at Sudbury, Ontario, Canada. Similar patterns
414 for the vertical velocity variance profile were observed in other releases of CAPTEX.

415 The BH and KC simulations had similar horizontal and vertical distribution
416 patterns of particles for CAPTEX 1 and resulted in comparable statistical ranks (Figure
417 13). There were more particles moved to upper levels and less particles stayed in the
418 lowest 500 m in the TKED simulation. In general, particles were mixed to higher

419 altitudes in the TKED option since its vertical velocity variance profile extended to
420 higher levels than others. In the EXCH case, particles near the surface (the lowest 500 m)
421 moved slower than the particles above. That may be due to the almost zero vertical
422 mixing during the nighttime, resulting in particles remaining over Lake Erie and Lake
423 Ontario and positive bias of tracer concentration in those area. For CAPTEX 7, the 48-
424 hour averaged concentration patterns generated by the KC and TEKD mixing were
425 similar as shown in Figure 14. The tracer plume in EXCH was narrow at the beginning of
426 the episode and then became wider in the downwind area that resulted in worse statistical
427 scores than other simulations. The constant turbulent time scale used in the EXCH option
428 for computing vertical velocity variances might cause too little mixing at night and
429 overestimation during daytime. Overall, the statistical rank for all six CAPTEX episodes
430 (Table 2) shows that the TKED mixing had good performance while the BH options
431 produced the worst results. For individual episodes, except CAPTEX 2 in which all four
432 mixing options performed similarly, there was no one scheme that always outperforms
433 the other options. It is appropriate to keep various options for users to choose depending
434 on different scenarios or to create dispersion ensembles.

435 **7. Summary and discussion**

436 The turbulent velocity variance is an essential variable in HYSPLIT to determine
437 the mixing of particles. There are different options available in the model to estimate the
438 turbulent velocity variance according to the stability and turbulent variables provided by
439 the meteorological data. In this study, we conducted HYSPLIT simulations driven by
440 WRF meteorology and using different mixing methods for two control tracer experiments
441 – PSB1 and CAPTEX that aimed for the sub-kilometer and long-range transport,

442 respectively. Through the comparisons of turbulent velocity variance (only for PSB1) and
443 the evaluation of tracer concentrations with measurements, we assessed the performance
444 of different mixing options affecting the dispersion results.

445 The KC and EXCH mixing options produced a larger maximum of the vertical
446 velocity variance than other mixing options did. Simulated maximum vertical velocity
447 variance occurred at an altitude of about 500 m, which is above the tower measurement
448 available in the PSB1. The vertical velocity variance profile obtained from the BH
449 method had a sharp increase from the surface to the height of the maximum values (about
450 200 m). The TKED case had a flat vertical velocity variance profile with the smallest
451 variation in its value with height and maximum compared to other cases. The comparison
452 with measurements near the surface (height at 3.2 m and 30 m) taken during the PSB1
453 showed that the BH scheme underestimated vertical velocity variance while the KC
454 option slightly overestimated it. The dispersion results for IOP4 and IOP5 (weak unstable
455 conditions with moderate winds) were less sensitive to the mixing option than the runs
456 for IOP2 (unstable with light winds) and IOP3 (neutral with strong winds). The plumes
457 generated by the BH and TKED method (less disperse due to the weaker vertical velocity
458 variance) had higher concentrations near the surface than those driven by the KC and
459 EXCH option (stronger mixing). The larger horizontal velocity variance in the EXCH
460 generated a slightly wider plume than the one in the EXCHm simulation. HYSPLIT
461 simulations using different mixing options were conducted for six CAPTEX episodes.
462 The statistical rank for the TKED run was slightly better than others while the BH mixing
463 generated results with the worst rank. For scenarios like CAPTEX experiencing different

464 stability conditions throughout the day, a time-varying Lagrangian time scale may be
465 more appropriate for estimating the turbulent velocity variance.

466 The model performed differently with the four mixing options in varying
467 scenarios. No one mixing option always outperformed the other options. HYSPLIT users
468 can select a mixing option according to their scenario and availability of meteorological
469 fields, as well as use different mixing options to generate dispersion ensembles. The KC
470 and BH methods re-compute various stability parameters with assumptions for different
471 stability conditions to obtain the turbulent velocity variance for the dispersion process.
472 Errors due to the process of re-diagnosing variables may be carried to the dispersion
473 simulation. However, the advantage of these two methods is that unlike the other options,
474 no extra variable is required. If only basic meteorological parameters such as wind,
475 temperature, and pressure are available, HYSPLIT has an alternative option to estimate
476 the boundary layer stability parameters for computing the turbulent velocity variance
477 (Stein et al. 2015).

478 The TKED and EXCH options depend on the mixing variables (TKE and
479 exchange coefficient, respectively) provided by WRF. If the meteorological data provide
480 well-simulated TKE fields, HYSPLIT can obtain the velocity variance by partitioning the
481 horizontal and vertical components. Thus, the main concern for HYSPLIT is to set a
482 reasonable anisotropy ratio. Note that there is no TKE output if a first-order K-profile
483 PBL scheme is used for running the meteorological simulation. The underestimation of
484 TKE values by WRF in the unstable condition shown in the comparison with
485 measurements from PSB1 needs further investigation. For the EXCH option, the
486 turbulent exchange coefficient is needed, but it is not commonly available in

487 meteorological model output or reanalysis products that can be used to drive HYSPLIT.
488 Different PBL schemes have their ways of computing the exchange coefficient, and the
489 results are rarely evaluated. It is recommended to use a time-varying Lagrangian time
490 scale to estimate the velocity variance with the turbulent exchange coefficient. The
491 uncertainty of TKE and exchange coefficient prediction may influence the dispersion
492 simulation when the velocity variance is computed by the TKED or EXCH mixing option.
493 For future works, we are interested in an evaluation of modeled vertical velocity variance
494 with long-term observations that may further give us insight how each mixing option
495 performs for stable nighttime conditions and unstable daytime conditions. Such
496 measurements may be found in the DCNet research network (Hicks et al. 2013) and
497 Doppler Lidar data (Berg et al. 2017). The DCNet data are measurements at six suburban
498 areas in the eastern United States while Lidar measurements can provide data covering
499 the entire PBL. With continuous measurements, the velocity variance evaluation is not
500 limited to certain days or stability scenarios. Furthermore, Project Sagebrush Phase 2
501 (PSB2; Finn et al. 2018), which was conducted in 2016, consisted of four IOPs during
502 very unstable conditions and four IOPs during very stable conditions. Similar to the setup
503 of PSB1, velocity variance observations are available along with tracer concentration
504 measurements that can be used to evaluate HYSPLIT's turbulent mixing options and their
505 impact on dispersion results.

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 649 different mixing options. The shaded color is 48-hour averaged model concentrations
 650 while color-coded circles are measured concentrations. Rank of each simulation is noted
 651 in each panel. Unit: log(pg/m⁻³).
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653 **Table 1 The ratio of u- and w-variance computed by using measurements taken during the**
 654 **Sagebrush experiment.**

Station name	Measurement Height (m)	All data in October	Data on the day of IOPs	Data during 12-18MST on IOP days
G1	4	3.7041	4.1874	4.5567
G2	30	2.4748	2.6607	2.6127
R1	45	1.8743	1.8830	1.9990
R2	3.2	4.2582	4.5396	4.5487
R3	3.2	4.4776	5.1804	5.3276
R4	3.2	4.6456	5.6300	5.8733
FLX	3.2	3.9803	4.6829	5.3066
ASC	30	-	1.5909	1.8236
	40	-	1.4331	1.5430
	50	-	1.4335	1.4650
	60	-	1.3115	1.3045
	70	-	1.1898	1.2175
	80	-	1.1499	1.1052
	100	-	1.0902	1.0343
	130	-	1.0646	1.0058
	160	-	1.1152	0.8208

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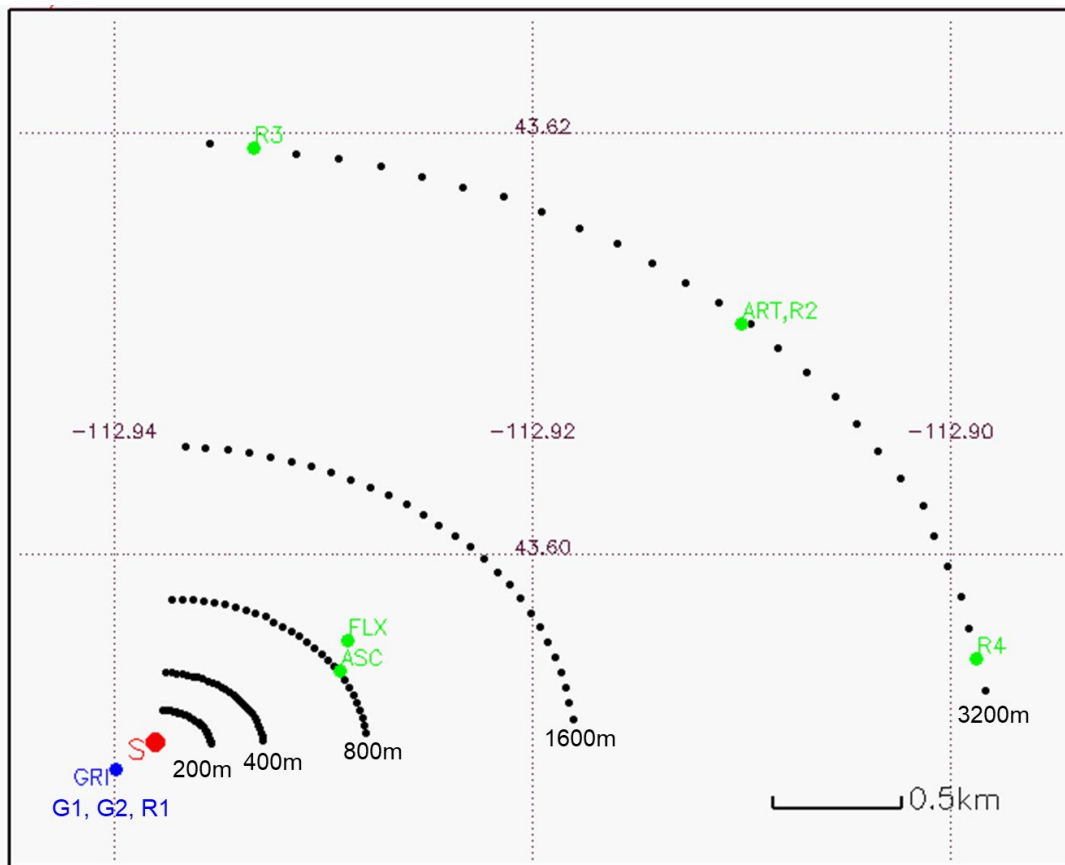
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657 **Table 2 Rank corresponding to HYSPLIT model results for six CAPTEX tracer releases.**

Release	BH	KC	TKED	EXCH
R1	2.49	2.50	2.62	2.38
R2	2.78	2.72	2.73	2.79
R3	1.98	1.95	2.11	2.13
R4	2.14	2.18	2.16	2.49
R5	2.64	2.52	2.65	2.68
R7	2.25	2.36	2.33	2.12
All ^a	2.35	2.49	2.51	2.44

658 ^a All data points from six releases are used.

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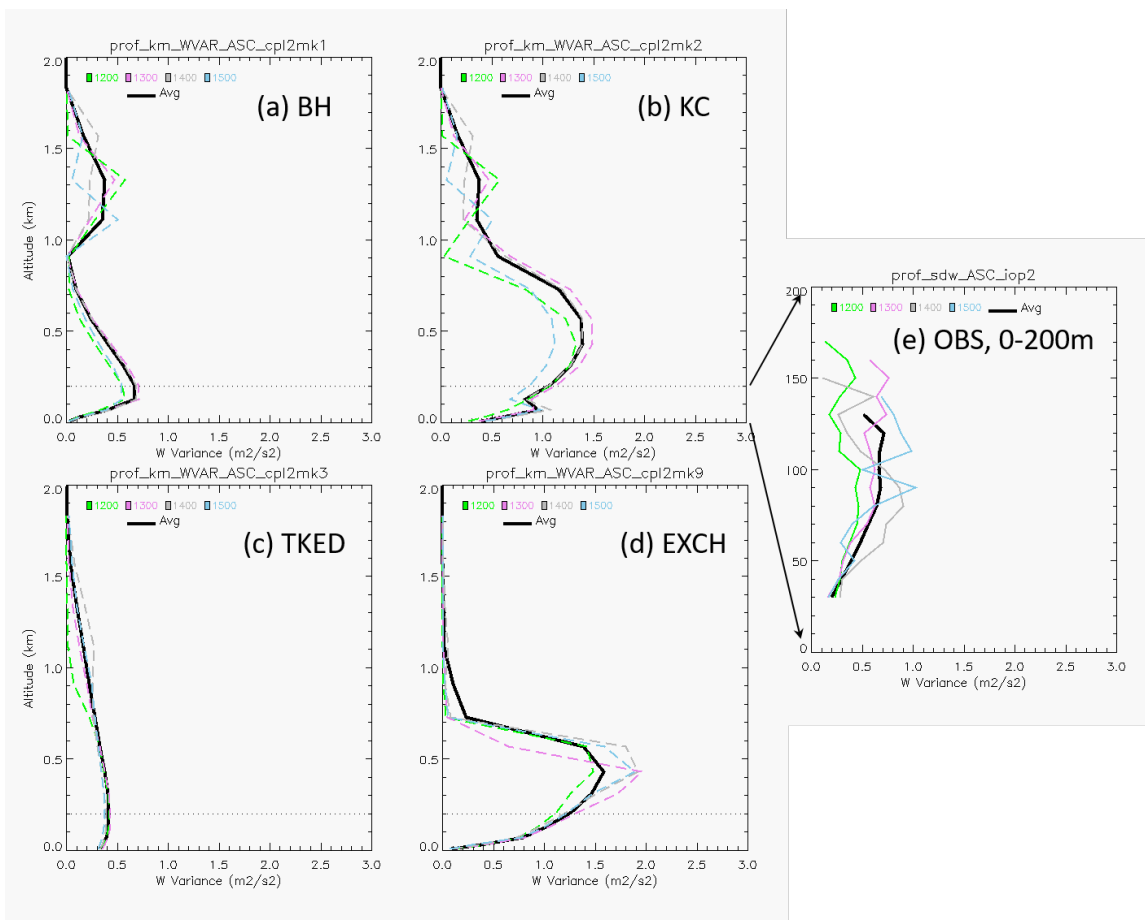


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 663 variance were taken at stations labeled as GRI, FLX, R2, R3, and R4 while the measurements for
 664 standard deviation of velocity were taken at stations labeled as ASC and ART.

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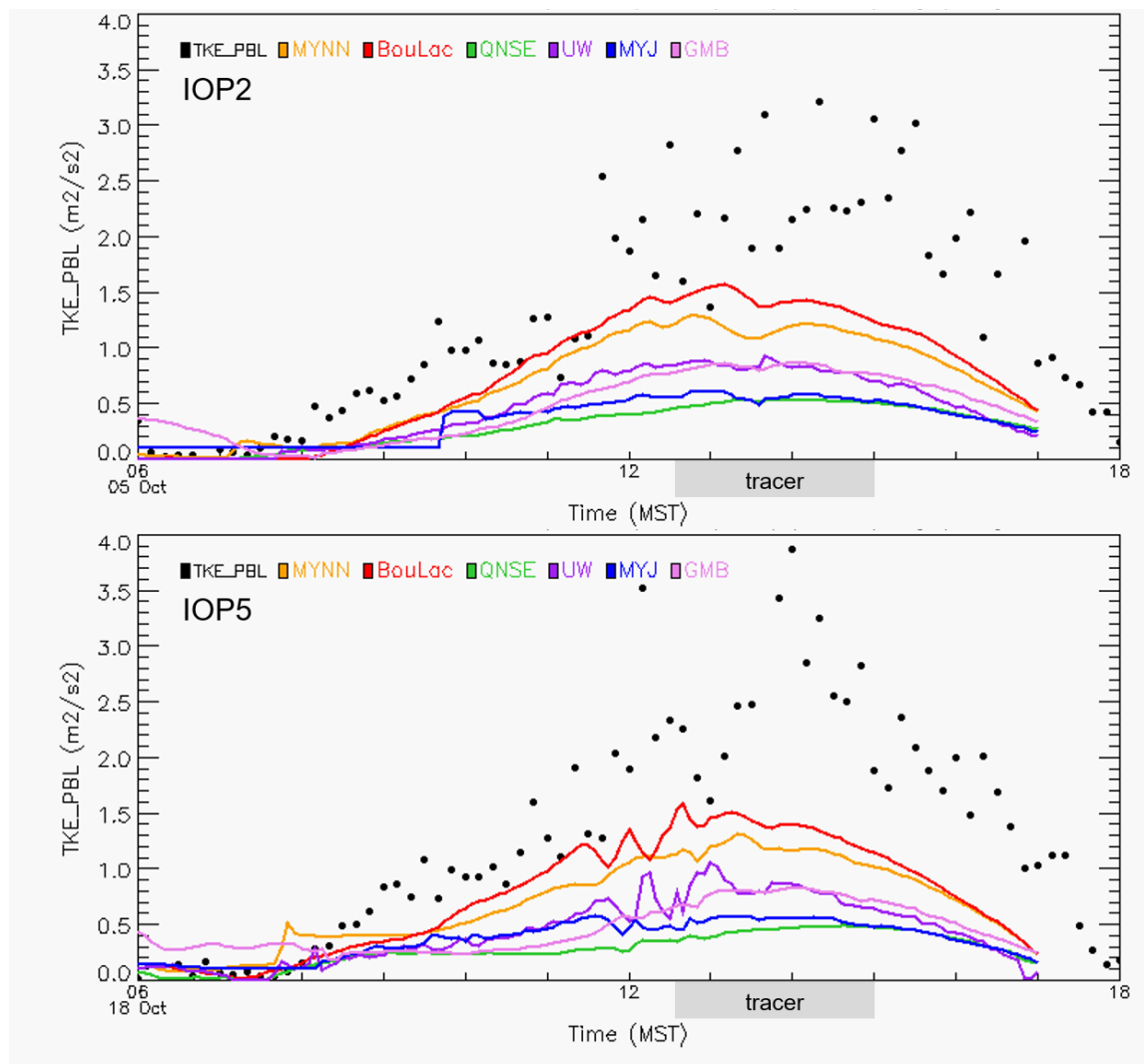
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15 MST on October 5th, 2013.

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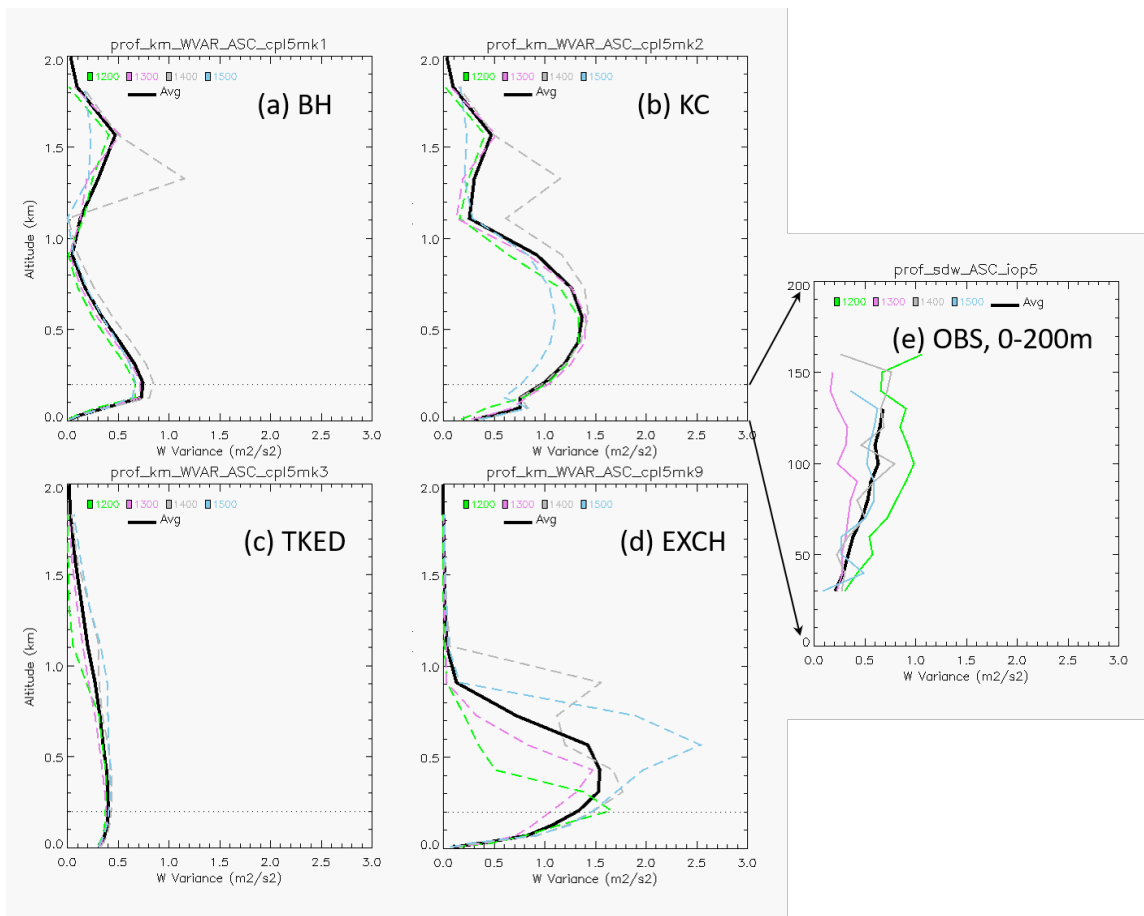


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Figure 3 The time series of observed and modeled TKE (m^2s^{-2}) at the GRI tower (30 m height) for IOP2 and IOP5 from WRF simulations using different TKE-based PBL schemes.

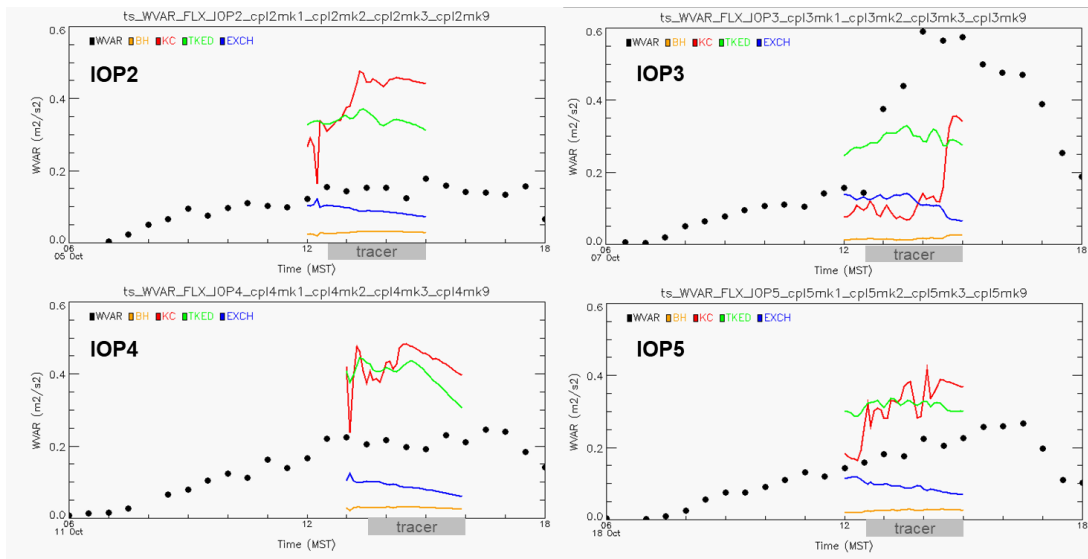


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Figure 4 The same as Figure 2 but for IOP 5, 12 – 15 MST on October 18th, 2013.

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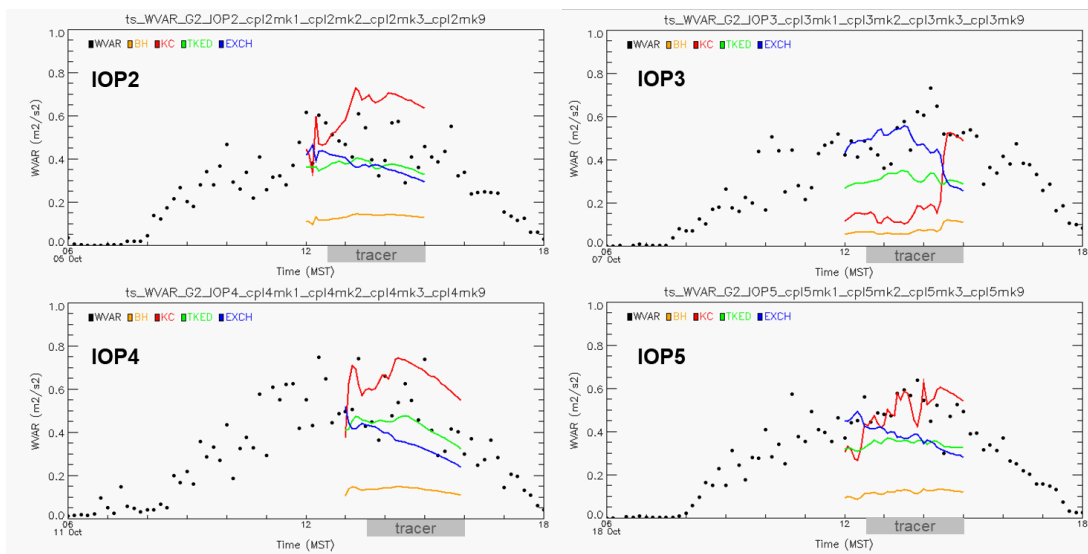
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Figure 5 Time series of observed and modeled vertical velocity variance from HYSPLIT. The measurements were taken at the FLX station at 3.2 m height and modeled values were at 1st model layer at 10 m.

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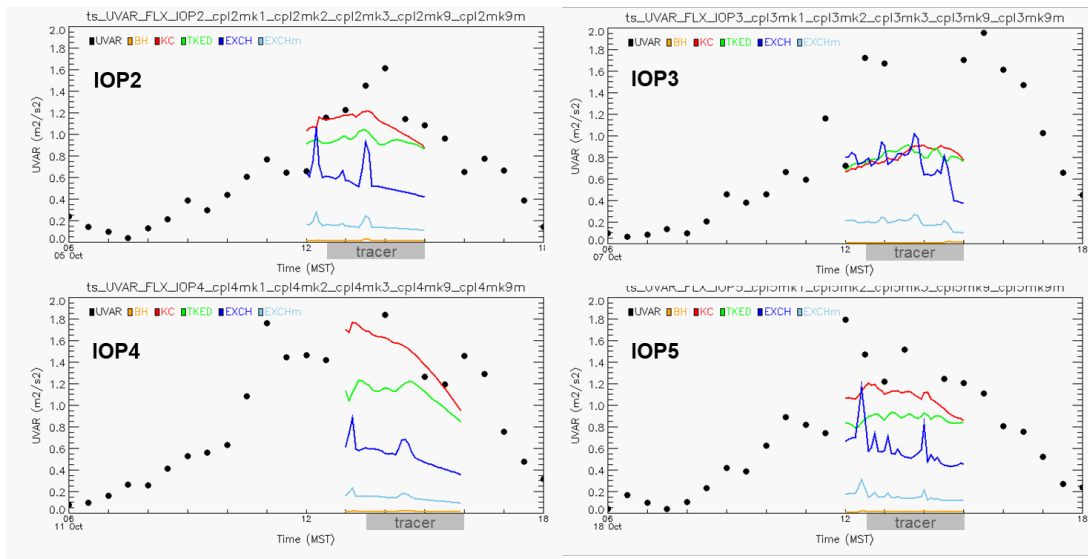
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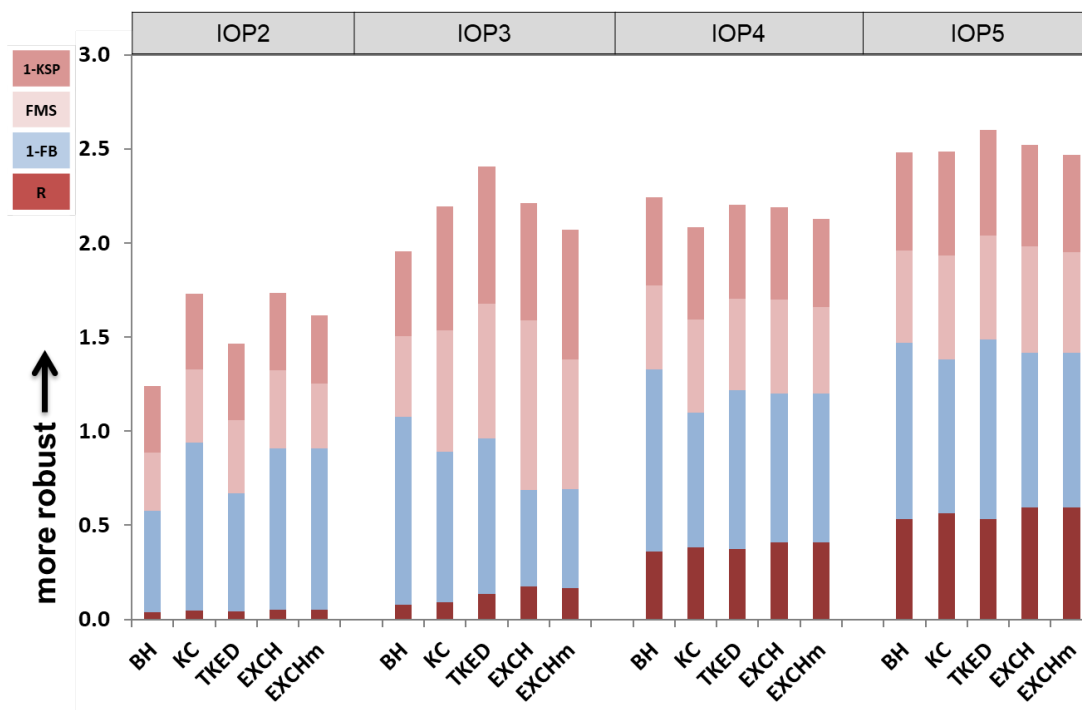
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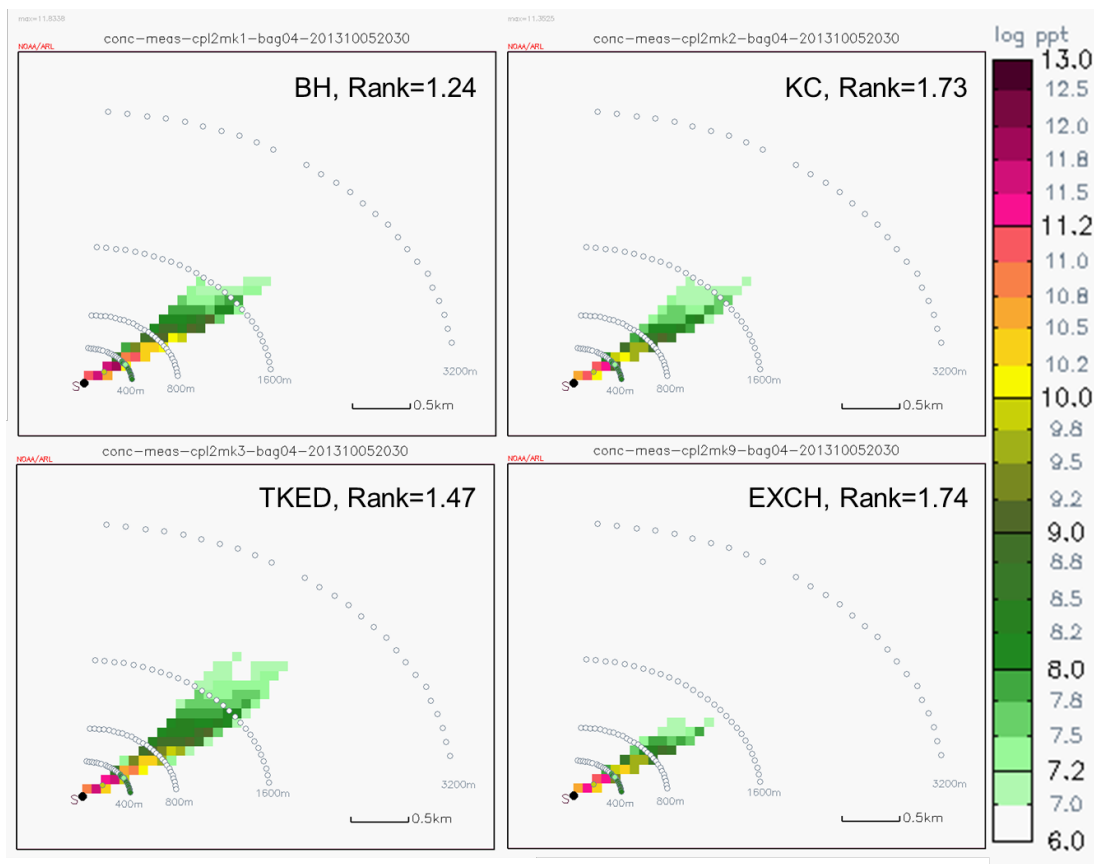
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Figure 7 The same as Figure 5, except for the horizontal velocity variance.



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Figure 8 The statistical Rank of HYSPLIT results using different mixing options.

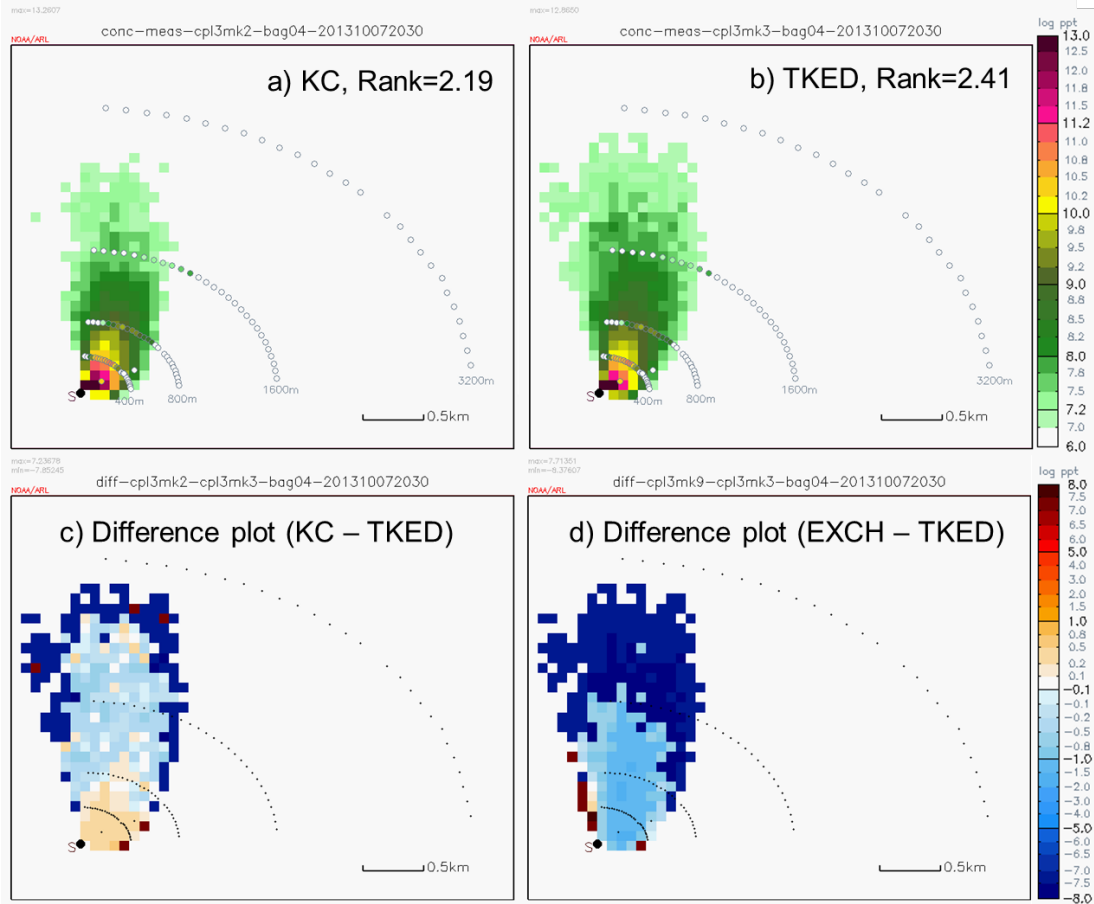


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696 **Figure 9 Tracer concentration plots for IOP 2 at 2030 UTC on October 5th, 2013 from HYSPLIT**697 **simulations using different mixing options. The shaded color is model concentrations while color-**698 **coded circles are measured concentrations. Rank of each simulation is noted in each panel. Unit: log**699 **ppt.**

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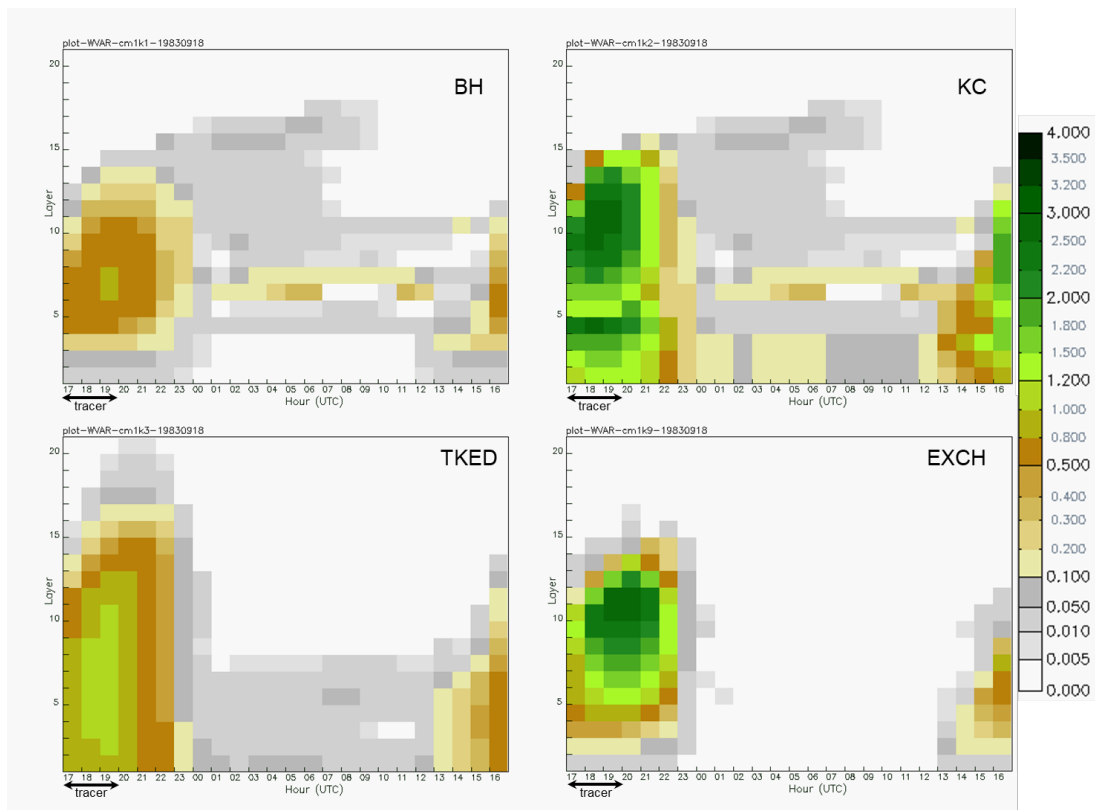
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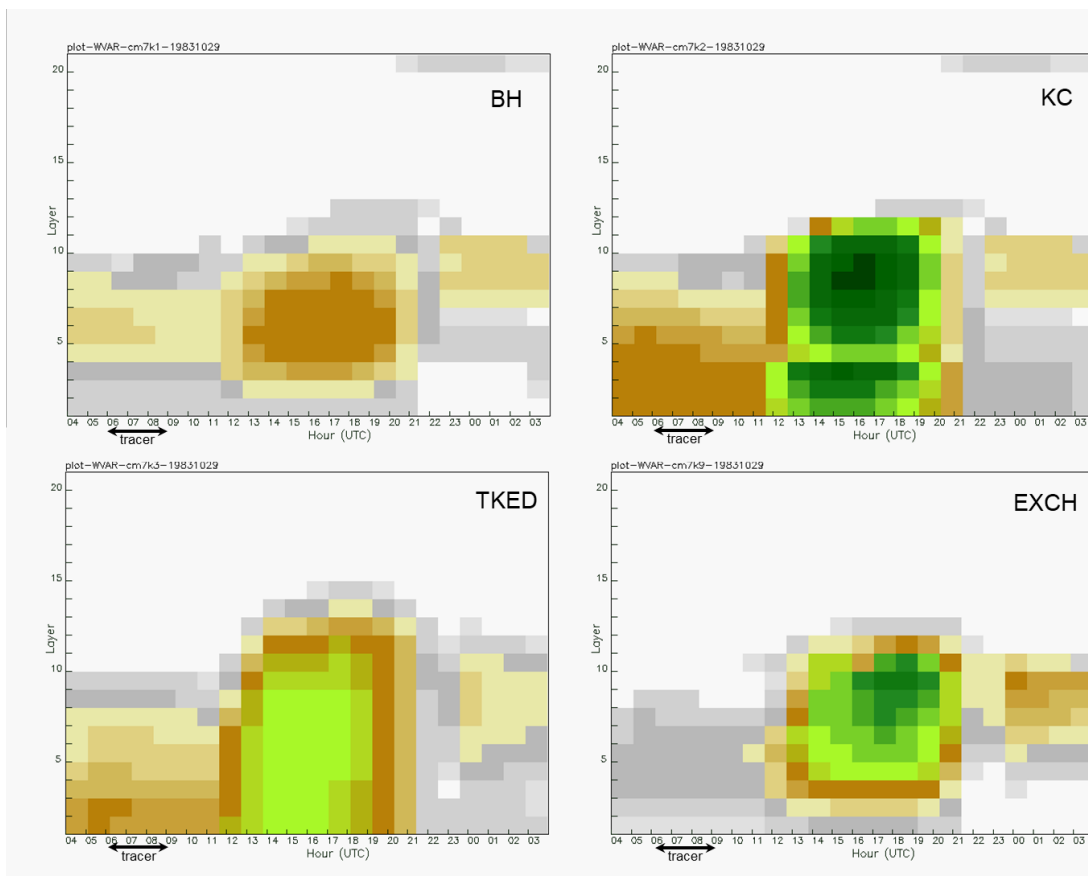
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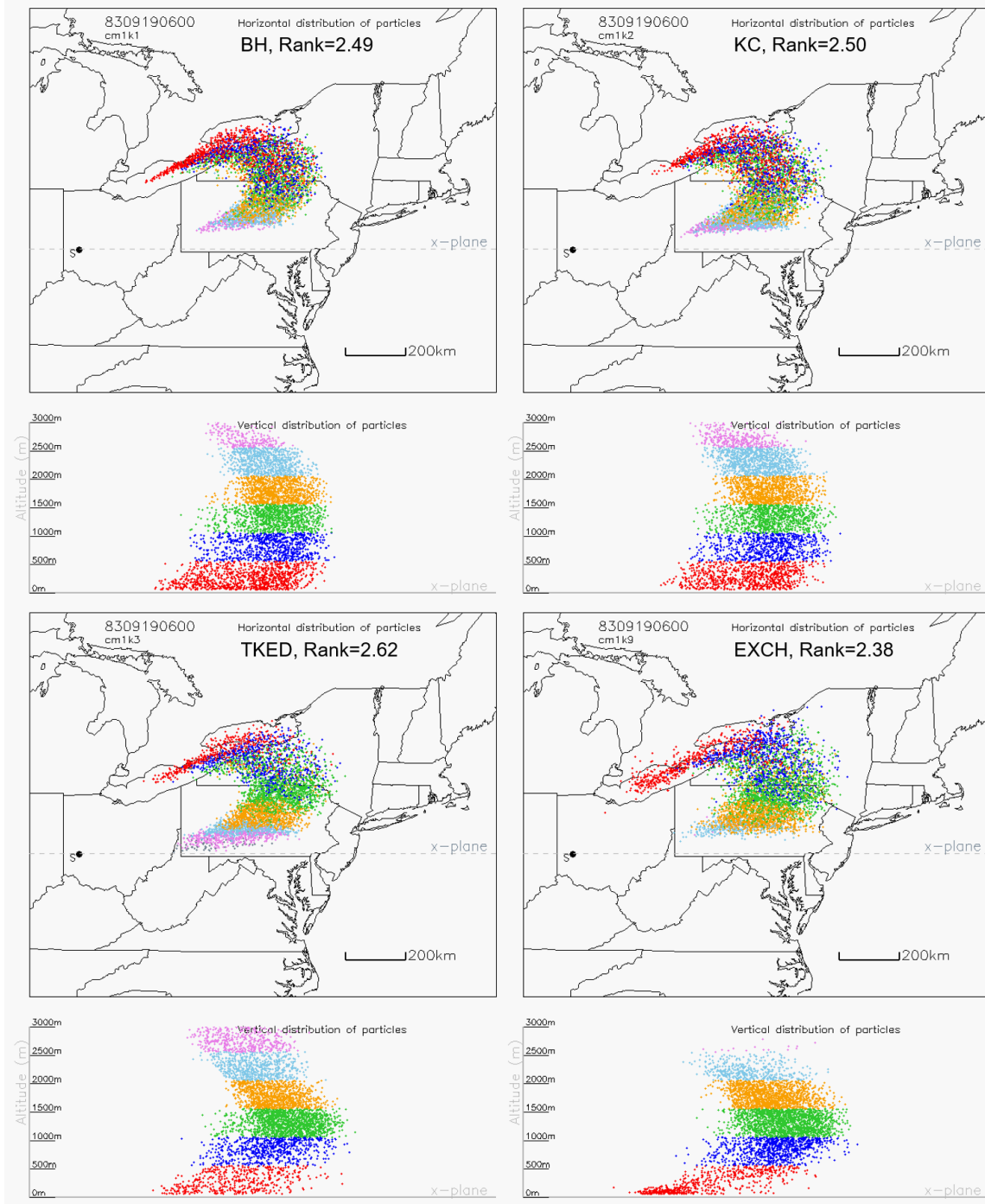
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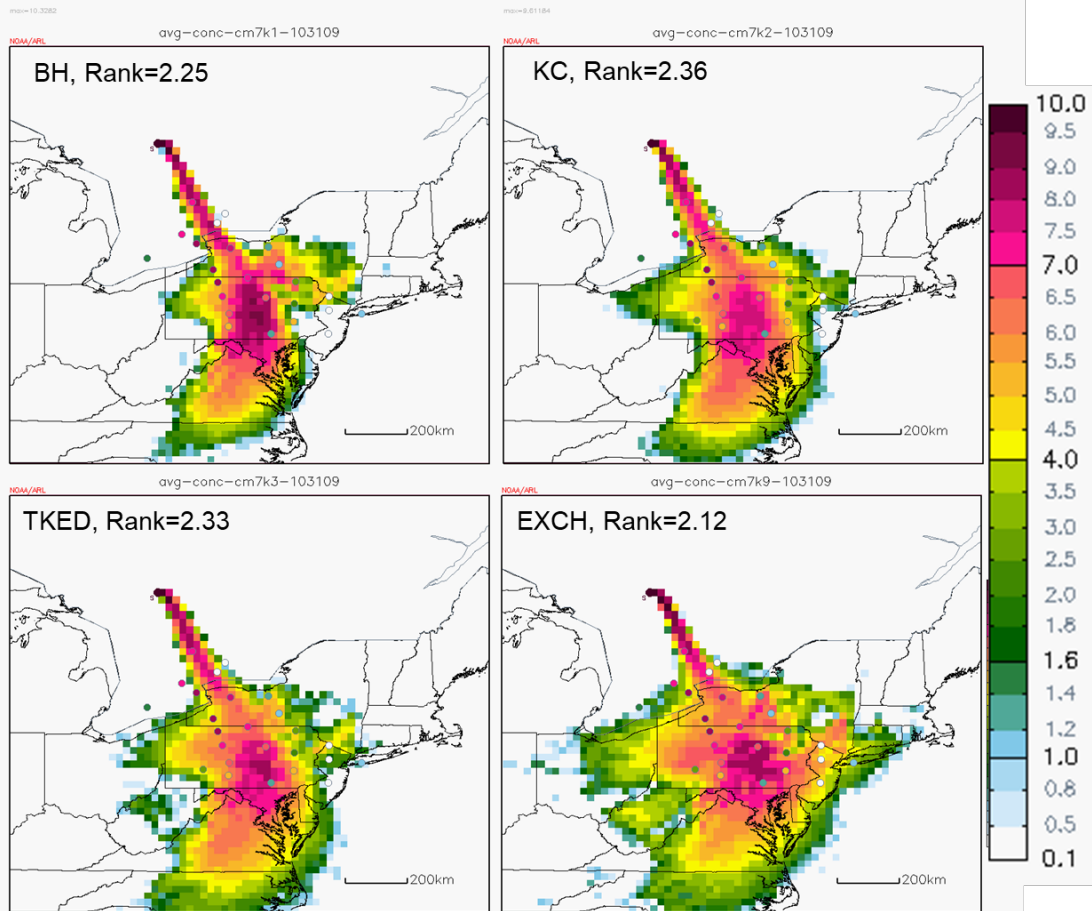
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Figure 14 Tracer concentration plots for CAPTEX 7 from HYSPLIT simulations using different mixing options. The shaded color is 48-hour averaged model concentrations while color-coded circles are measured concentrations. Rank of each simulation is noted in each panel. Unit: $\log(\text{pg}/\text{m}^3)$.