

## NOAA Atlas 14

# Precipitation-Frequency Atlas of the United States 

Volume 7 Version 2.0: Alaska

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Silver Spring,
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## Table of Contents

1. Abstract ..... 1
2. Preface to Volume 7 ..... 1
3. Introduction ..... 3
3.1. Objective .....  3
3.2. Approach and deliverables .....  3
4. Frequency analysis .....  5
4.1. Project area ..... 5
4.2. Precipitation data collection and formatting ..... 7
4.3. Annual maximum series extraction ..... 9
4.4. Station screening ..... 11
4.5. AMS screening and quality control ..... 16
4.5.1. Outliers ..... 16
4.5.2. Correction for constrained observations ..... 17
4.5.3. Bias correction for precipitation undercatch ..... 17
4.5.4. Inconsistencies across durations ..... 17
4.5.5. Trend analysis ..... 18
4.6. Precipitation frequency estimates with confidence limits at stations ..... 18
4.6.1. Overview of methodology and related terminology. ..... 18
4.6.2. Regionalization ..... 20
4.6.3. AMS-based estimates ..... 23
4.6.4. PDS-based estimates ..... 25
4.6.5. Confidence limits ..... 25
4.7. Rainfall frequency estimates with confidence limits at stations ..... 26
4.7.1. Background ..... 26
4.7.2. Extraction of rainfall data. ..... 26
4.7.3. Rainfall frequency estimation ..... 27
4.8. Derivation of grids ..... 28
4.8.1. Mean annual maximum precipitation. ..... 28
4.8.2. Precipitation frequency estimates with confidence limits ..... 29
5. Precipitation Frequency Data Server ..... 32
5.1. Introduction ..... 32
5.2. Underlying data ..... 32
5.3. Products available on the Precipitation Frequency Data Server ..... 33
6. Peer review ..... 41
7. Comparison with previous NOAA publications ..... 41
Acknowledgements ..... acknowledgements-1
A. 1 List of stations used to prepare precipitation frequency estimates ..... A.1-1
A. 2 Bias correction report ..... A. 2-1
A. 3 Annual maximum series trend analysis. ..... A.3-1
A. 4 Regional L-moment ratios ..... A.4-1
A. 5 PRISM report ..... A.5-1
A. 6 Peer review comments and responses ..... A.6-1
A. 7 Temporal distributions of heavy precipitation ..... A. $7-1$
A. 8 Seasonality ..... A.8-1
Glossary ..... glossary-1
References ..... references-1

## 1. Abstract

NOAA Atlas 14 contains precipitation frequency estimates for the United States and U.S. affiliated territories with associated $90 \%$ confidence intervals and supplementary information on temporal distribution of heavy precipitation, analysis of seasonality and trends in annual maximum series data, etc. It includes pertinent information on development methodologies and intermediate results. The results are published through the Precipitation Frequency Data Server (http://hdsc.nws.noaa.gov/hdsc/pfds).

The Atlas is divided into volumes based on geographic sections of the country. The Atlas is intended as the U.S. Government source of precipitation frequency estimates and associated information for the United States and U.S. affiliated territories.

## 2. Preface to Volume 7

NOAA Atlas 14 Volume 7 contains precipitation frequency estimates for selected durations and frequencies with $90 \%$ confidence intervals and supplementary information on temporal distribution of heavy precipitation, analysis of seasonality and trends in annual maximum series data, etc., for the state of Alaska. The results are published through the Precipitation Frequency Data Server (PFDS) (http://hdsc.nws.noaa.gov/hdsc/pfds).

This project was a collaborative effort between the Hydrometeorological Design Studies Center within the Office of Hydrologic Development of the National Oceanic and Atmospheric Administration's National Weather Service and the Water and Environmental Research Center of the University of Alaska Fairbanks.

Any use of trade names in this publication is for descriptive purposes only and does not imply endorsement by the U.S. Government.

Citation and version history. This documentation and associated artifacts such as maps, grids, and point-and-click results from the PFDS are part of a whole with a single version number and can be referenced as:

Sanja Perica, Douglas Kane, Sarah Dietz, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Svetlana Stuefer, Amy Tidwell, Carl Trypaluk, Dale Unruh, Michael Yekta, Erica Betts, Geoffrey Bonnin, Sarah Heim, Lillian Hiner, Elizabeth Lilly, Jayashree Narayanan, Fenglin Yan, Tan Zhao (2012). NOAA Atlas 14 Volume 7 Version 2.0, Precipitation-Frequency Atlas of the United States, Alaska. NOAA, National Weather Service, Silver Spring, MD.

The version number has the format P.S where P is a primary version number representing a number of successive releases of primary information. Primary information is essentially the data. S is a secondary version number representing successive releases of secondary information. Secondary information includes documentation and metadata. S reverts to zero (or nothing; i.e., Version 2 and Version 2.0 are equivalent) when $P$ is incremented. When new information is completed and added (such as draft documentation) without changing any prior information, the version number is not incremented.

The primary version number is stamped on the artifact or is included as part of the filename where the format does not allow for a version stamp (for example, files with gridded precipitation frequency estimates). All location-specific output from the PFDS is stamped with the version number and date of download.

Table 2.1 lists the version history associated with the NOAA Atlas 14 Volume 7 precipitation frequency project and indicates the nature of changes made.

Table 2.1. Version history of NOAA Atlas 14 Volume 7.

| Version <br> number | Date | Notes |
| :--- | :--- | :--- |
| Version 1.0 | August 2011 | Draft data used in peer review |
| Version 2.0 | February 2012 | Final data released |

## 3. Introduction

### 3.1. Objective

NOAA Atlas 14 Volume 7 provides precipitation frequency estimates for the state of Alaska for 5minute through 60 -day durations at 1 -year through 1,000 -year average recurrence intervals. The estimates and associated bounds of $90 \%$ confidence intervals are provided at 30 arc-seconds resolution. The Atlas also includes information on temporal distributions and seasonal information for data used in the frequency analysis. In addition, trends in annual maximum series data were also examined.

The information in NOAA Atlas 14 Volume 7 supersedes precipitation frequency estimates for Alaska contained in the following publications:
a. Technical Paper No. 47, Probable Maximum Precipitation and Rainfall-Frequency Data for Alaska for Areas to 400 Square Miles, Durations to 24 Hours, and Return Periods from 1 to 100 Years (Miller, 1963);
b. Technical Paper No. 52, Two- to Ten-Day Precipitation for Return Periods of 2 to 100 Years in Alaska (Miller, 1965).

### 3.2. Approach and deliverables

Precipitation frequency estimates have been computed for a range of frequencies and durations using a regional frequency analysis approach based on L-moment statistics calculated from annual maximum series. This section provides an overview of the approach; greater detail is provided in Section 4.

Annual maximum series were extracted from precipitation measurements recorded at 15 -minute to 1-day time increments obtained from various sources; 5 - to 60 -minute annual maxima series were also obtained from corresponding monthly maxima. The table in Appendix A. 1 gives detailed information on all stations whose data were used in the frequency analysis. The annual maximum series data were screened for erroneous measurements. An attempt to quantify rain gauge undercatch during extreme events and to apply a bias correction to the annual maximum data was unsuccessful; more details are provided in Appendix A.2. The 1-day and 1-hour annual maximum series data were also analyzed for potential trends (Appendix A.3).

A region of influence approach was used for the regional L-moments computation at each station across all durations. A variety of probability distribution functions were examined for each region and duration and the most suitable distribution was selected. Distribution parameters, and consequently precipitation frequency estimates, were determined for each duration based on the mean of the annual maximum series at the station and the regionally determined higher order L-moments. Higher order L-moments were smoothed across durations to ensure consistency in precipitation frequency estimates. L-moments for all stations used in frequency analysis across daily durations are listed in Appendix A.4. Due to the lack of suitable stations recording precipitation at sub-daily intervals, precipitation frequency estimates for hourly durations were calculated by assuming that standardized statistics were constant across hourly durations. Sub-hourly durations were computed from corresponding 1-hour estimates by applying scaling factors.

Partial duration series-based precipitation frequency estimates were calculated indirectly from the annual maximum series using Langbein's formula.

Frequency analysis was also done on rainfall (i.e., liquid precipitation only) data for durations up to 24 hours, but analysis of the limited available data showed that for the range of durations there was very little difference between the rainfall and total precipitation magnitudes across all frequencies.

A Monte-Carlo simulation approach was used to produce upper and lower bounds of $90 \%$ confidence intervals for the precipitation frequency estimates.

Grids of precipitation frequency estimates and $90 \%$ confidence intervals were determined based on mean annual maxima grids and at-station precipitation frequency estimates. The mean annual maxima grids for daily and hourly durations were derived from at-station mean annual maxima using a hybrid statistical-geographic approach for mapping climate data (Appendix A.5). The grids of precipitation frequency estimates and confidence limits for all frequencies were then derived in an iterative process using the inherently strong linear relationship that exists between mean annual maxima and precipitation frequency estimates at the 2 -year recurrence interval and between precipitation frequency estimates at consecutive frequencies for a given duration. The resulting grids were examined and adjusted in cases where inconsistencies occurred between durations and frequencies. Scaling factors were used to derive grids for sub-hourly durations. Both spatially interpolated and point estimates at selected durations and frequencies were subject to external peer review (Appendix A.6).

Climate regions were delineated based on characteristics of annual maxima data. The regions were used in the extraction of annual maximum series, calculations of temporal distributions, and in a seasonality analysis. For the temporal and seasonality analyses, regions were grouped to increase sample sizes. Temporal distributions, expressed in probability terms as cumulative percentages of precipitation totals, were computed for precipitation magnitudes with less than $50 \%$ exceedence probability for selected durations (Appendix A.7). The seasonality analysis was done on annual maxima by tabulating the number of annual maxima exceeding several selected threshold frequencies for selected durations (Appendix A.8).

NOAA Atlas 14 Volume 7 precipitation frequency estimates for any location in the project area are available in a variety of formats through the Precipitation Frequency Data Server (PFDS) at http://hdsc.nws.noaa.gov/hdsc/pfds (via a point-and-click interface); more details are provided in Section 5. Additional types of results and information available there include:

- ASCII grids of partial duration series-based and annual maximum series-based precipitation frequency estimates and related confidence intervals for a range of durations and frequencies with associated Federal Geographic Data Committee-compliant metadata;
- cartographic maps of partial duration series-based precipitation frequency estimates for selected frequencies and durations;
- annual maximum series used in the analysis;
- temporal distributions;
- seasonality analysis of annual maxima.

Cartographic maps were created to serve as visual aids and are not recommended for estimating precipitation frequency estimates. Users are advised to take advantage of the PFDS interface or the underlying ASCII grids for obtaining precipitation frequency estimates. Precipitation frequency estimates from this Atlas are estimates for a point location and are not directly applicable for an area.

## 4. Frequency analysis

### 4.1. Project area

The project area, shown in Figure 4.1.1, encompasses the entire state of Alaska. Alaska is the largest state in the United States with land covering 586,412 square miles $\left(1,518,800 \mathrm{~km}^{2}\right)$. It is also the most northern state reaching into the Arctic Circle. It is mostly surrounded by water with the Arctic Ocean and the Beaufort and the Chukchi Seas to the north, the Bering Sea to the west and the Pacific Ocean and Gulf of Alaska to the south. The Aleutian Islands, a chain of 300 small volcanic islands, extend over 1,200 miles ( $1,900 \mathrm{~km}$ ) westward into the Pacific. Canada borders the land to the east. Two mountain ranges dominate the topography - the Brooks Range in the northern Arctic region and the Alaska Range in the south, separated by an interior plateau. The land north of the Brooks Range, termed the North Slope, is primarily uninhabited tundra but with a few villages and the northernmost U.S. city, Barrow. The interior is primarily uninhabited wilderness but also includes the city of Fairbanks, the second largest city in Alaska. The Alaska Range houses the highest point in the United States, Mt. McKinley which is 20,320 feet above sea level. Most of the population lives in the southcentral region near Anchorage and along the southern coast. The state capital, Juneau, resides in southeast Alaska on the strip of land closest to the lower contiguous United States.


Figure 4.1.1. Project area for NOAA Atlas 14 Volume 7.

Climatology of heavy precipitation. The climatology of heavy precipitation in Alaska varies widely across the state and depends on latitude, elevation and the distance from the coast. The northern portion of Alaska lies within Arctic Circle where the Arctic Ocean along the northern coast is frozen about eight months of the year. This, combined with the low elevation, the dominance of the polar high, and the blockage of moisture from the south due to the Brooks Range, causes the northern region to receive the least amount of precipitation in the state.

During the summer months, a large area of high pressure that resides over the northern Pacific Ocean, the North Pacific High, dominates much of the state below the Arctic. Radiational warming due to increased hours of sunlight helps to destabilize the atmosphere creating areas of convection in the interior region. The convective storms can be triggered and intensified by the passing of an upper-level trough or a cold front, which are more prevalent during the warm season. Under the right large-scale pressure pattern, strong southwest flow over Alaska can bring warm moist subtropical air from the Pacific into the state. The remnants of tropical systems can be picked up in this flow and supply additional moisture for the air mass as it surges northeast over the Alaska Range. Such was the case in August 1967 when the Fairbanks area received more than half of its annual precipitation amount in less than a week.

Towards the end of summer, the polar jet stream moves south in the North Pacific away from the Arctic circle and a persistent flow of large-scale low pressure systems begins to develop. Strong thermal gradients, ample moisture and the semi-permanent Aleutian low over the southwest islands allow for the genesis and intensification of these sub-polar cyclones before they move into western Alaska or travel along the southern coast. This is the typical storm track for low pressure systems in the North Pacific causing these regions to receive some of the highest annual maximum rainfall totals in North America. Occasionally, these storms can become as strong as hurricanes producing damaging winds, storm surge and heavy precipitation.

During the winter and early spring, the track of these storms tends to move further south over the Gulf of Alaska where the large mountain chains over western North America act as a barrier to the westerly flow causing the low pressure systems to stall. During this scenario copious amount of rainfall can fall over the southern coast and southeast Alaska. The high elevations along the southern coast provide strong lifting on the windward sides which can create some of the heaviest rainfalls in the state. Most of the moisture in the air is released on the windward side of the mountain and as air flows down the leeward side it is much drier creating a rain shadow effect. Coastal lows can also develop right off-shore and intensify quickly advecting relatively warm moist air from the Pacific northward up over the mountainous coast.

Based on the characteristics of annual maximum series (AMS) data used in the precipitation frequency analysis, seven climate regions were formed and used in this project for AMS extraction (Section 4.3) and portrayal of temporal distributions (Appendix A.7) and the seasonality of annual maximum data (Appendix A.8). Initial regions were formed based on the climatological classification from The Climate of Alaska (Shulski and Wendler, 2007) and then refined to depict wet seasons of annual maxima across a range of durations by assessing the periods in which the majority of annual maxima occur (see Section 4.3 for more details). Consideration was also given to spatial variations in 24-hour mean annual maxima (MAM) and monthly maxima for n-minute durations. The final climatic regions are shown in Figure 4.1.2.

The Arctic region receives the least amount of precipitation and has the lowest MAMs across durations in the state. The Interior region has slightly higher mean annual precipitation (MAP) as well as higher MAMs than the Arctic region but is still quite dry. Similarly, the West Coast region also has only slightly higher MAP and MAMs than the Arctic. The Southwest Interior region contains a portion of the Alaska Range and is a transitional region between the dry north and wet south. MAMs and MAP are higher here than in the northern regions especially at higher elevations, but values are not as high as the southern coastal regions.

Islands in the Southwest Islands region are fairly low in elevation, but their location in the middle of the North Pacific Ocean allows for long durations of light rainfall. Cook Inlet region is very similar in climate to the transitional Southwest Interior region except it is prone to higher rainfalls at longer durations which is similar to the other coastal regions. Storms often travel along the southern coast or through the Gulf of Alaska and then slow down as they approach the steep terrain along the southeast coast. The high elevations along the coast in South/Southeast Coast region provide strong lifting on the windward sides which can create some of the heaviest rainfalls in the state and therefore the largest MAP and MAM values.

To increase sample sizes for temporal and seasonality analyses, regions were grouped in two larger regions. The Arctic, Interior, West Coast and Southwest Interior regions comprise the Northern Region and the Southwest Islands, Cook Inlet, and South/Southeast Coast regions comprise the Southern Region.


Figure 4.1.2. Seven climatic regions used in NOAA Atlas 14 Volume 7.

### 4.2. Precipitation data collection and formatting

Precipitation measurements were obtained for 1,689 stations from a number of federal and state agencies, the University of Alaska Fairbanks (UAF), and Environment Canada. The majority of the stations were from the National Weather Service (NWS) Cooperative Observer Program's database maintained by the NOAA's National Climatic Data Center (NCDC). Each station was assigned a unique six digits identification number (station ID) where first two digits were common for all
stations from the same data provider in order to have a uniform system of numbering. Except for NCDC stations, assigned identification numbers do not match identification numbers assigned by agencies that provided the data. A list of all agencies that provided the data for this project together with abbreviated names used in this document and the first two digits of stations' identification numbers are shown in Table 4.2.1. The $19^{\text {th }}$ Century Forts and Voluntary Observers data received from the Midwestern Region Climate Center were appended to the corresponding stations in the NCDC's DSI-3200 dataset.

All data were formatted to a common format at one of three base durations that corresponded to the original reporting period: 15 -minute, 1 -hour, or 1-day. Where available, records extended through May 2011. Table 4.2.2 lists the total number of stations that were obtained and formatted for each reporting interval. In addition, monthly maxima for various n-minute durations (5-minute through 60 -minute) were obtained for 36 NCDC stations; they were used to develop scaling factors used for sub-hourly precipitation frequency estimates (Section 4.6.3).

Table 4.2.1. Agencies that provided data for the project with their dataset names, abbreviations, data reporting interval and common first two digits of station identification numbers.

| Data provider | Dataset name | Abbrev. | Reporting interval | Common digits |
| :---: | :---: | :---: | :---: | :---: |
| Alaska Dept. of Transportation | Road Weather Information System | RWIS | 1-day,1-hour | 60 |
| Environment Canada | N/A | ENV CANADA | 1-day,1-hour | 21 |
| Midwestern Region Climate Center | 19th Century Forts and Voluntary Observers Database | NCDC | 1-day | 50 |
| National Climatic Data Center | DSI-3200 | NCDC | 1-day | 50 |
|  | DSI-3240 | NCDC | 1-hour | 50 |
|  | DSI-3260 | NCDC | 15-min | 50 |
|  | Integrated Surface Hourly | ISH | 1-hour | 70 |
| National Interagency Fire Center, Western Region Climate Center | Remote Automatic Weather Stations | RAWS | 1-hour | 80 |
| National Weather Service and Federal Aviation Administration | Automated Surface Observing System | ASOS | 1-hour | 55 |
| Natural Resources Conservation Service | SNOwpack TELemetry | SNOTEL | 1-day, 1-hour | 10 |
| United States Geological Survey | N/A | USGS | 1-day | 90 |
| University of Alaska Fairbanks | Arctic Long-Term Ecological Research | ARCTIC LTER | 1-day, 1-hour | 30 |
|  | Arctic Transitions in the LandAtmosphere System | ATLAS | 1-hour | 41 |
|  | Bonanza Creek Long-Term Ecological Research | BONANZA <br> LTER | 1-hour | 31 |
|  | Water \& Environmental Research Center, North Slope | WERC | 1-hour | 40 |

Table 4.2.2. The number of stations that were obtained per reporting interval.

| Data reporting <br> interval | Number of <br> stations |
| :--- | :---: |
| 1-day | 913 |
| 1-hour | 667 |
| 15-minute | 73 |

### 4.3. Annual maximum series extraction

The precipitation frequency analysis approach used in this project is based on analysis of annual maximum series (AMS) across a range of durations. AMS for each station were obtained by extracting the highest precipitation amount for a particular duration in each successive calendar year. AMS at stations were extracted for all durations equal to and longer than the base duration (or reporting interval) up to 60 days. AMS for the 1 -day through 60 -day durations were compiled from daily and hourly records ( 15 -minute data were not used because they had too few data years). To accomplish this, hourly data were first aggregated to constrained 1-day (hours 0 to 24) values before extracting 1-day and longer duration annual maxima. Hourly data were also used to compile AMS for 1-hour through 12 -hour durations.

The procedure for developing an AMS from a precipitation dataset used specific criteria designed to extract only reasonable maxima if a year was incomplete or had accumulated data. Accumulated data occurred in some records where observations were not taken regularly, so recorded numbers represent accumulated amounts over extended periods of time. Since the precipitation distribution over the period is unknown, the total amount was distributed uniformly across the whole period. All annual maxima that resulted from accumulated data were flagged and went through screening to ensure that the incomplete data did not result in erroneously low maxima (Section 4.5.1).

The criteria for AMS extraction were designed to exclude maxima if there were too many missing or accumulated data during the year and more specifically during critical months when precipitation maxima were most likely to occur ("wet season"). Wet seasons were resolved by assessing the periods in which two-thirds of annual maxima occurred at each station and by inspecting histograms of annual maxima for the 1-day and 1-hour durations in a region. The final wet season months were allocated for each of the seven climatic regions described in Section 4.1; they are shown in Table 4.3.1.

Table 4.3.1. Wet season months for each region for daily and sub-daily durations.

| Region | Wet season months |  |
| :--- | :---: | :---: |
|  | Daily durations | Sub-daily durations |
| Arctic | June - September | June - August |
| West Coast | June - October | June - September |
| Interior | June - October | June - August |
| Southwest Islands | July - February | July - November |
| Southwest Interior | July - December | July - December |
| Cook Inlet | July - December | July - December |
| South/Southeast Coast | August - January | August - December |

The flowchart in Figure 4.3.2 depicts the AMS extraction criteria for all durations. Various thresholds for acceptable amounts of missing or accumulated data were applied to the year and wet season. In Alaska, data are not always collected during the cold, dry winter months. Assuming that
annual maxima are most likely to occur during wet months and that missing data during cold months can be neglected, the criterion for missing data within the entire year was essentially omitted for this project (to accomplish this within the current software's framework, up to $90 \%$ of measurements were allowed to be missing during a year). To determine the allowable amount of missing data during the wet season for each climate region, the impact of various allowable percentages on number of extracted years of data was examined. Results suggested that allowing missing data for up to $1 / 3$ of the wet season ( $\sim 33 \%$ ) was adequate, particularly given that later quality control efforts screen low outliers in the AMS (Section 4.5.1).


Figure 4.3.2. Criteria used to extract annual maxima. Data quality codes were assigned based on acceptance and rejection; $\mathrm{D}_{\text {thresh }}$ depends on duration.

The extracted maximum value for a given year had to pass through all of the criteria in the flowchart to be accepted. For example, in a year with less than $33 \%$ of measurements missing during the assigned wet season, if more than $66 \%$ of measurements were accumulated, then the maxima for that year for that duration was (conditionally) rejected. If the year had between $33 \%$ and $66 \%$ accumulated data, then it was further screened by assessing the lengths of the accumulated periods. If the lengths of accumulation periods for more than $33 \%$ of the accumulated data were equal to or longer than threshold accumulation period lengths ( $\mathrm{D}_{\text {thresh }}$ ), then a maximum for that year was rejected. Threshold accumulation period lengths matched the selected duration for durations less than 2 days, were equal to half of duration period for durations between 2 days and 20 days, and were equal 15 days for durations of 30 days or longer. If the year had less than $33 \%$ accumulated data, the extracted maximum was passed to another set of criteria for accumulations during its wet season, etc.

If a rejected annual maximum was higher than $95 \%$ of the accepted maxima at that station, then it was kept in the series. Also, if a rejected 1-day annual maximum was higher than any accumulated amount in a year, then it was kept in the series. Years in which a maximum was rejected were marked as missing in the series. Various codes were assigned to both, accepted and rejected maxima, based on the amount of missing and accumulated data in each year (see Figure 4.3.1) to assist in further quality control of AMS described in Section 4.5.1.

### 4.4. Station screening

Station screening was done in the following order: a) examination of geospatial data, b) screening for duplicate stations, c) screening for duplicate records at co-located daily, hourly, and/or 15-minute stations and extending records using data from co-located stations, c) screening nearby stations for potentially merging records or removing shorter, less reliable records in station dense areas, and d) screening for sufficient number of years with usable data.

Geospatial data. Latitude, longitude, and elevation data for all stations were screened for errors. Several stations had to be re-located because they plotted in the ocean or were clearly misplaced based on inspection of satellite images and maps. Misplacement was typically the result of no seconds recorded in latitude and longitude data. There were also several stations with no elevation data; for those stations, elevation was estimated from high-resolution digital elevation model (DEM) grids.

Duplicate stations. In some instances, the same station was reported by more than one source. For example, NCDC's hourly data from the DSI-3240 dataset were also included in their ISH dataset. Duplicate stations were kept only in one of the datasets.

Co-located stations. Co-located stations were defined as stations that have the same geospatial data, but report precipitation amounts at different time intervals. The screening of co-located stations was done as follows:

- If co-located 15 -minute and hourly stations provided data for the same period and there were no differences in AMS for constrained 1-hour maxima (15-minute data aggregated based on the clock hour), only the 15 -minute station was retained and used to extract AMS for all longer durations. For this project area, aggregated 15 -minute data were used to extend AMS at some hourly stations, but no 15 -minute stations had sufficient length to be included directly in the analysis.
- If an hourly station provided data for the same period as a co-located daily station and there were no differences in AMS for constrained 1-day maxima (1-hour data aggregated from 0 to 24 hours), only the hourly station was retained and used to extract AMS for all durations.
- If periods of record at co-located hourly and daily stations were consistent but did not completely overlap, aggregated data from the hourly station were used to extend the record of the daily station.
- If the daily station had a longer period of record than co-located hourly station, both stations were retained.

Nearby stations. Nearby stations were defined as stations located within five miles with consideration to elevation differences. Their records were considered for merging to increase record lengths. The Student's two-sample $t$-test at the $90 \%$ confidence level was used to ensure that the annual maximum series of merged stations were from the same population.

Record length. Record length was characterized by the number of years for which annual maxima could be extracted (i.e., data years) rather than the entire period of record. Typically, in other NOAA Atlas 14 volumes, only stations with at least 30 data years were considered for frequency analysis, with allowances made for isolated stations or stations recording at very short intervals. Since there were not enough stations that satisfied that requirement in Alaska, all stations with 15 data years or more were included in the initial dataset. Several isolated and/or hourly stations with 9-10 years of data were also retained.

Figure 4.4.1 shows histograms for the number of data years of stations available for frequency analysis across daily and hourly durations after all the screenings were done. No 15 -minute stations had sufficient number of data years to be included in the analysis. The average and median record lengths as well as corresponding ranges of record lengths are given in Table 4.4.1.


Figure 4.4.1. Number of stations used for precipitation frequency analysis grouped by record length. for daily and hourly durations.

Table 4.4.1. Record length statistics for stations used in frequency analysis for different durations.

| Duration (D) | Number of | Record length (data years) |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  | average | median | range |
| Daily (1-day $\leq \mathrm{D} \leq 60$-day) | 396 | 32 | 25 | $9-103$ |
| Hourly (1-hr $\leq \mathrm{D}<24$-hr) | 121 | 18 | 15 | $10-49$ |

Locations of stations recording precipitation data at 1-day intervals that were used in the frequency analysis are shown in Figure 4.4.2 and locations of stations recording at 1-hour and nminute intervals are shown in Figure 4.4.3. More detailed information on each station whose data was used to calculate precipitation frequency estimates is given in three tables in Appendix A.1. The first table in the appendix lists stations in Alaska. The second table lists Canadian stations at the border with Alaska. The third table lists n-minute stations that were not directly used in frequency analysis but assisted in calculation of constrained correction factors (see Section 4.5.2) and precipitation frequency estimates at sub-hourly durations (see Section 4.6.3). Information provided for each station includes: source, name, identification number and data reporting interval, as well as latitude, longitude, elevation, and period of record. All adjusted geospatial data are shown in bold font in the latitude, longitude, and/or elevation columns. Bold font in the period of record column was used to indicate stations whose records were extended with the data from co-located stations or whose records were lengthened by merging with another station. The metadata from the station listed as the 'Post-merge station ID' was retained in the dataset for the merged record; the metadata for this station will reflect the combined periods of records in bold text. If an hourly and a daily station with different IDs were co-located, then the metadata, including ID, of the daily station shown in the 'Colocated station ID' column of the table should be used to locate the hourly station on the PFDS web page.


Figure 4.4.2. Map of stations recording at 1-day intervals used in frequency analysis.


Figure 4.4.3. Map of stations recording at 1 -hour (red circles) and n-minute intervals (green circles) used in the analysis.

### 4.5. AMS screening and quality control

### 4.5.1. Outliers

For this project, outliers are defined as annual maxima which depart significantly from the trend of the corresponding remaining maxima. Since data at both high and low extremities can considerably affect precipitation frequency estimates, they have to be carefully investigated and either corrected or removed from the AMS if due to measurement errors. The high and low outliers thresholds from the Grubbs-Beck statistical test (Interagency Advisory Committee on Water Data, 1982) and the median +/- two standard deviations thresholds were used to identify low and high outliers for all durations. An example of outlier examination is shown in Figure 4.5.1. Low outliers which frequently came from years with missing and/or accumulated data were typically removed from the annual maximum series. All values identified as high outliers were mapped with concurrent measurements at nearby stations. Questionable values that could not be confirmed were investigated further using climatological observation forms, monthly storm data reports and other historical weather events publications. Depending on the outcome of each investigation, values were either kept as is, corrected, or removed from the datasets. For example, statistical tests indicated two high outliers in 24-hour AMS at Angoon station (50-0310): 15.20 inches recorded on October 12, 1982 and 5 inches recorded on November 14, 1931. Further investigation showed that both measurements were likely clerical errors (e.g., measurements were recorded times a magnitude of ten) and were removed from the dataset. It is interesting to note that the 15.20 inches amount has been frequently cited in literature as the official 24-hour record precipitation amount for Alaska. At the time of publication, the Alaska state climatologist is reviewing this finding.


Figure 4.5.1. Outlier examination of 24 -hour AMS at station $50-0310$. Data quality codes were assigned to all annual maxima during the extraction process (Section 4.3).

### 4.5.2. Correction for constrained observations

Daily durations. The majority of daily AMS data used in this project came from daily stations at which readings were taken once every day at fixed times (constrained observations). Due to the fixed beginning and ending of observation times at daily stations, it is to be expected that extracted (constrained) annual maxima were lower than the true (unconstrained) maxima, especially for shorter daily durations. To account for the likely failure of capturing the true-interval maxima, correction factors were applied to constrained AMS. The correction factor for each daily duration was estimated as the coefficient of a zero-intercept regression model using concurrent (occurring within $+/-1$ day) constrained and unconstrained annual maxima from hourly stations as independent and dependent model variables, respectively. Correction factors for all daily durations are given in Table 4.5.1.

Table 4.5.1. Correction factors applied to constrained AMS data across daily durations.

| Duration (days) | 1 | 2 | 3 | 4 | 7 | $>7$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Correction factor | 1.12 | 1.05 | 1.04 | 1.03 | 1.02 | 1.00 |

Hourly durations. Similar adjustments were needed on hourly AMS data to account for the effects of constrained 'clock hour' on observations. The correction factors for hourly AMS were developed using co-located hourly (constrained) and $n$-minute (unconstrained) concurrent annual maxima; they are shown in Table 4.5.2.

Table 4.5.2. Correction factors applied to constrained AMS data across hourly durations.

| Duration (hours) | 1 | 2 | 3 | 6 | $>6$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Correction factor | 1.08 | 1.04 | 1.02 | 1.01 | 1.00 |

Sub-hourly durations. No correction factors were applied to durations under 1-hour.

### 4.5.3. Bias correction for precipitation undercatch

All precipitation gauges undercatch the true precipitation amounts to some degree. The amount of undercatch amount depends on a number of factors, with wind speed being the principal factor. Correction of the undercatch bias, is typically done through empirical equations, such as those resulting from World Meteorological Organization initiated studies (Goodison et al., 1998; Yang et al., 1998), but they require local meteorological data, such as type of precipitation (liquid, solid or mixed) and wind speed, and information on a gauge type and whether it is shielded or not. Due to a lack of wind data and information on installation of wind shields for stations in Alaska, it was concluded that the bias correction cannot be done accurately. Therefore, bias correction for precipitation undercatch was not applied on the annual maxima used in this project. Additional information on this analysis can be found in Appendix A.2.

### 4.5.4. Inconsistencies across durations

At co-located stations, it was not unusual that corresponding annual maxima differed for some years during their overlapping periods of record. Related 1-day AMS at co-located daily and hourly stations were compared and each pair of significantly different estimates was investigated. Effort was made to identify the source of the error and to correct erroneous observations across all durations that were affected.

Annual maxima at each station were also compared across all durations in each year to ensure that the extracted amount for a longer duration was at least equal to the corresponding amount for the successive shorter duration. Inconsistencies of this type occurred at stations with a significant number of missing and/or accumulated data and resulted from different AMS extraction rules applied
for different durations (Section 4.3), or from the correction for constrained observations (Section 4.5.2). In those cases, shorter duration annual maxima were used to replace annual maxima extracted for longer durations. Typically, adjustments of this type were very small.

### 4.5.5. Trend analysis

Precipitation frequency analysis methods used in NOAA Atlas 14 volumes are based on the assumption of a stationary climate over the period of observation (and application). Statistical tests for trends in AMS and the main findings for this project area are described in more detail in Appendix A.3. Briefly, the stationarity assumption was tested by applying a parametric $t$-test and nonparametric Mann-Kendal test for trends in the 1-day and 1 -hour annual maximum series data at 5\% significance level. Only stations with at least 40 years of data were tested for trends. There were only 12 hourly stations with sufficient period of record and neither test detected any type of trend on a single station. For the 1 -day duration, there were 154 stations with at least 40 years of data. Test results were generally in agreement; positive trends were detected at $8 \%$ of stations and negative trends at $7 \%$ of stations; no statistically-significant trends were detected in about $85 \%$ of stations. Spatial maps did not reveal any spatial cohesiveness in positive or negative trends in AMS.

The relative magnitude of any trend in AMS was also assessed for the state as a whole. AMS were rescaled by corresponding mean values and then regressed against time. The regression results were tested as a set against a null hypothesis of zero serial correlation. The null hypothesis of no trends in AMS data could not be rejected at 5\% significance level.

Therefore, the assumption of stationary climate was accepted for this project area and no adjustment of AMS magnitudes was recommended.

### 4.6. Precipitation frequency estimates with confidence limits at stations

### 4.6.1. Overview of methodology and related terminology

Precipitation magnitude-frequency relationships at individual stations have been computed using a regional frequency analysis approach based on L-moment statistics. Frequency analyses were carried out on annual maximum series (AMS) for the following fifteen durations: 1 -hour, 2 -hour, 3 -hour, 6 hour, 12 -hour, 1 -day, 2-day, 3 -day, 4 -day, 7 -day, 10 -day, 20 -day, 30 -day, 45 -day and 60 -day. Frequency estimates based on partial duration series (PDS), which include all amounts for a specified duration at a given station above a pre-defined threshold regardless of year, were developed from AMS data using a formula that allows for conversion between AMS and PDS frequencies.
Precipitation frequency estimates at four sub-hourly durations (5-minute, 10 -minute, 15 -minute, 30 minute) were derived from corresponding hourly estimates using scaling factors. To assess the uncertainty in estimates, $90 \%$ confidence intervals were constructed on AMS and PDS frequency curves.

Frequency analysis involves mathematically fitting an assumed distribution function to the data. The following distribution functions were analyzed in this project with the aim to identify a distribution that will provide accurate precipitation frequency estimates for the project area across all frequencies and durations: 3-parameter Generalized Extreme Value (GEV), Generalized Normal, Generalized Pareto, Generalized Logistic and Pearson Type III distributions; 4-parameter Kappa distribution; and 5-parameter Wakeby distribution.

When fitting a distribution to a precipitation annual maximum series extracted at a given location (and selected duration), the result is a frequency distribution relating precipitation magnitude to its annual exceedance probability (AEP). The inverse of the AEP is frequently referred to as the average recurrence interval (ARI), also known as return period. When used with the AMS-based frequency analysis, ARI does not represent the "true" average period between exceedances of a given precipitation magnitude, but the average period between years in which a given precipitation
magnitude is exceeded at least once. Those two average periods can be considerably different for more frequent events. The 'true' average recurrence interval (ARI) between cases of a particular magnitude can be obtained through frequency analysis of PDS.

Differences in magnitudes of corresponding frequency estimates (i.e., quantiles) from the two series are negligible for ARIs greater than about 15 years, but notable at smaller ARIs (especially for $\mathrm{ARI} \leq 5$ years). Because the PDS can include more than one event in any particular year, the results from a PDS analysis are considered to be more reliable for designs based on frequent events (e.g., Laurenson, 1987). To avoid confusion, herein the term AEP is used with AMS frequency analysis and ARI with PDS frequency analysis. The term 'frequency' is interchangeably used to specify the ARI and AEP.

L-moments (Hosking and Wallis, 1997) provide an alternative way of describing frequency distributions to traditional product moments (conventional moments) or maximum likelihood approach. Since sample estimators of L-moments are linear combinations of ranked observations, they are less susceptible to the presence of outliers in the data than conventional moments and are well suited for the analysis of data that exhibit significant skewness. L-moments typically used to calculate parameters of various frequency distributions include $1^{\text {st }}$ and $2^{\text {nd }}$ order L-moments: Llocation $\left(\lambda_{1}\right)$ and L-scale $\left(\lambda_{2}\right)$, and the following L-moment ratios: L-CV ( $\tau$ ), L-skewness ( $\tau_{3}$ ), and Lkurtosis $\left(\tau_{4}\right)$. L-CV, which stands for "coefficient of L-variation", is calculated as the ratio of L-scale to L-location $\left(\lambda_{2} / \lambda_{1}\right)$. L-skewness and L-kurtosis represent ratios of the $3^{\text {rd }}$ order $\left(\lambda_{3}\right)$ and $4^{\text {th }}$ order $\left(\lambda_{4}\right)$ L-moments to the $2^{\text {nd }} \operatorname{order}\left(\lambda_{2}\right)$ L-moment, respectively, and thus are independent of scale.

One of the primary problems in precipitation frequency analysis is the need to provide estimates for average recurrence intervals that are significantly longer than available records. Regional approaches, which use data from stations that are expected to have similar frequency distributions have been shown to yield more accurate estimates of extreme quantiles than approaches that use only data from a single station. The number of stations used to define a region should be large enough to smooth variability in at-station estimates, but also small enough that regional estimates still adequately represent local conditions. The region of influence approach (Burn, 1990) used in this volume defines regions such that each station has its own region with a potentially unique combination of nearby stations. Stations are selected based on the maximum allowable distance from the target station that is defined in a geographic space and in a space of selected statistical attribute variables. Like with other regionalization approaches, there is level of subjectivity involved in the process, for example, in choosing attribute variables, selecting the maximum allowable distances as well as attributes' weights and transformations for similarity distance algorithms. One of the main advantages of the region of influence approach is that it results in a smooth transition in estimates across regional boundaries, which is very relevant for the mapping of precipitation frequency estimates.

A frequency curve that is calculated from sample data represents some average estimate of the population frequency curve, but there is a high probability that the true value actually lies above or below the sample estimate. Confidence limits determine values between which one would expect the true value to lie with certain confidence. The width of a confidence interval between the upper and lower confidence limits is affected by a number of factors, such as the degree of confidence, sample size, exceedance probability, distribution selection, and so on. Simulation-based procedures were used to estimate confidence limits of a $90 \%$ confidence interval on frequency curves.

Precipitation frequency estimates from this Atlas are point estimates, and are not directly applicable for an area. The conversion of a point to an areal estimate is usually done by applying an appropriate areal reduction factor to the average of the point estimates within the subject area. Areal reduction factors are generally a function of the size of an area and the duration of the precipitation. Since there are no areal reduction factors developed specifically for Alaska, the depth-area-duration curves from the Technical Paper No. 47 (Miller, 1963), that are identical to curves from the Technical

Paper No. 29 (U.S. Weather Bureau, 1960) developed for the contiguous United States, could be used for that purpose.

### 4.6.2. Regionalization

Initial regions for each station were created by grouping the closest 10 stations. Stations were then added to or removed from regions based on examination of their distance from a target station, elevation difference, inspection of their locations with respect to mountain ridges, etc. (see an example in Figure 4.6.1) and assessment of similarities/dissimilarities in the progression of relevant L-moment statistics across durations compared with other stations in the region (see Figure 4.6.2). Typically, final regions included between 5 to 9 stations with a cumulative number of data years between 150 and 250 for daily durations and 40 and 80 for hourly durations. However, since there were large portions of the project area with very few stations, final numbers of stations per region were as low as a single station and/or have less than 20 data years, especially for hourly durations.

Regional L-moments calculation. For a given duration, regional estimates of L-moment ratios (LCV, L-skewness and L-kurtosis) were obtained by averaging corresponding station-specific estimates weighted by record lengths. Regional L-moment ratios were then used to estimate higher order Lmoments at each station.

Station dependence. Since stations were selected based on geographic proximity to a target station, it was possible that extracted annual maxima at nearby stations came from the same storm events. Dependence in AMS data for stations within a region was analyzed using a $t$-test for the significance of a correlation coefficient at the $5 \%$ level. Analysis indicated that cross-correlation among stations was statistically significant for several regions in areas with more dense network of rain gauges and that the number of dependent station pairs increased with duration length. The impact of station dependence on precipitation frequency estimates is considered to be minimal (e.g., Hosking and Wallis, 1997), so it was not addressed in the calculation of precipitation frequency estimates. However, it was accounted for during the construction of confidence intervals on estimates where it could have noticeable influence (see Section 4.6.5).


Figure 4.6.1. An example of spatial plot with accompanying interactive table used to add or remove stations from a region for station Delta 6N (50-2339).


Figure 4.6.2. An example of plots of L-moments (left panels), MAM/MAM ${ }_{1 \text {-day }}$ and L-moment ratios (right panels) across durations for a region. Thick red lines show statistics for target station (station 50-2339); thin colored lines show statistics for other stations in the region; thick dashed red lines show corresponding regional estimates.

### 4.6.3. AMS-based estimates

Choice of distribution. A goodness-of-fit test based on L-moment statistics for 3-parameter distributions, as suggested by Hosking and Wallis (1997), was used to assess which of the 3parameter distributions listed in Section 4.6 .1 provide acceptable fit to the AMS data. Inspection of probability plots for 1-hour, 1-day and 10-day durations, like the one shown in Figure 4.6.3, and results of $\chi 2$-tests were also considered during distribution selection. The tests were inconclusive; there was not a single distribution that was consistently better than others. The decision was made to adopt the GEV distribution across all stations and for all durations for a number of reasons. GEV is a distribution generally recommended for analysis of extreme events. Based on the tests' results, GEV distribution provided an acceptable fit for most of the stations across a majority of durations. Finally, although it is not required to use the same type of distribution across all durations and/or regions, changes in distribution type for different durations or regions often lead to considerable discontinuities in frequency estimates across durations or between nearby locations, particularly at rarer frequencies.


Figure 4.6.3. Probability plots for selected distributions for 1-day AMS at Chitina station (50-1824).
Frequency estimates for daily durations. For each station and for each duration 1-day and longer, regional L-moment statistics were used to calculate the parameters of the GEV distribution and to produce precipitation frequency estimates for the following annual exceedance probabilities (AEPs): $1 / 2(50 \%), 1 / 5,1 / 10,1 / 25,1 / 50,1 / 100,1 / 200,1 / 500$ and $1 / 1000$. This calculation was repeated for all durations and for all stations. Since regional L-moments, and consequently, precipitation frequency estimates, were calculated independently for each duration, resulting depth-durationfrequency (DDF) curves did not always look smooth. Smoothing of L-moments by cubic spline functions improved the shape of DDF curves. Figure 4.6.4 illustrates precipitation depth-durationfrequency curves before and after smoothing of L-moments for Snettisham Power Plant station (508584). Appendix A. 4 lists the final L-moments at each station for 1-day through 60-day durations.


Figure 4.6.4. Precipitation frequency estimates for a range of durations for selected AEPs for station Snettisham Power Plant (50-8584). Blue lines represent original estimates; black lines represent estimates obtained after L-moments were smoothed across durations.

Frequency estimates for hourly durations. Regional L-moment statistics were used to calculate the parameters of the GEV distribution and to produce hourly precipitation frequency estimates for the same set of AEPs as for daily durations. This calculation was repeated for all hourly durations and for all stations. For a significant number of stations, it was observed that resulting precipitation frequency estimates were implausible and that the evolution of estimates across durations was frequently erratic, especially for AEPs of $1 / 100(1 \%)$ or less. Further investigation indicated that in the majority of anomalous cases, small sample sizes resulted in unreliable higher order moments (especially $\lambda_{3}$ ) which consequently resulted in irrational variations in estimates across hourly durations. First order moments (i.e., mean annual maxima) were less affected by the sample size. An attempt to smooth L-moments using similar approaches as for daily durations failed. Finally, it was decided to use ratios of the relatively stable first order moments at hourly durations to first order 24hour moments and apply them to 24 -hour precipitation frequency estimates to develop hourly frequency estimates. In other words, an assumption was made that mean annual maxima (MAMs) vary across hourly durations, but that ratios of quantiles for different AEPs and corresponding MAMs remain constant.

Frequency estimates for sub-hourly durations. 5-minute, 10-minute, 15 -minute and 30-minute estimates were calculated using scaling factors from 60 -minute estimates. The scaling factors were developed through analysis of average ratios of $n$-minute annual maxima to corresponding unconstrained 60 -minute annual maxima. N-minute annual maximum data for this analysis came from 36 NCDC n-minute stations that had records of monthly maxima data for durations from 5 minutes through 60 minutes (a list of n-minute stations is available in Table A.1.3 of Appendix A.1).

Given the relatively little available data and after reviewing the ratios by region, it was decided that the final scaling factors would be calculated by taking averages of quality controlled ratios from all stations in the project area. The scaling factors for the 5 -minute, 10 -minute, 15 -minute, and 30 minute durations are given in Table 4.6.1.

Table 4.6.1. Scaling factors for n -minute durations.

| Duration (minutes) | 5 | 10 | 15 | 30 |
| :--- | :---: | :---: | :---: | :---: |
| Scaling factor | 0.35 | 0.47 | 0.55 | 0.73 |

### 4.6.4. PDS-based estimates

PDS-based precipitation frequency estimates were calculated indirectly from the Langbein's formula (Langbein, 1949) that transforms a PDS-based average recurrence interval (ARI) to an annual exceedance probability (AEP):

$$
\operatorname{AEP}=1-\exp \left(-\frac{1}{\text { ARI }}\right) .
$$

PDS-based frequency estimates were calculated for the same durations as AMS-based estimates for $1-, 2-, 5-, 10-, 25-, 50-, 100-, 200-, 500-$ and 1,000 -year ARIs. Selected ARIs were first converted to AEPs using the above formula and then used to calculate precipitation frequency estimates for daily and hourly durations following the same regional approach and using the same L-moments that were used in the AMS analysis. For sub-hourly durations, PDS-based based frequency estimates were calculated using the same scaling factors that were used to estimate AMS-based frequency estimates.

### 4.6.5. Confidence limits

A Monte Carlo simulation procedure, as described in Hosking and Wallis (1997), was used to construct $90 \%$ confidence intervals (i.e., $5 \%$ and $95 \%$ confidence limits) on both AMS-based and PDS-based precipitation frequency curves. It should be noted that confidence intervals constructed through this approach account for uncertainties in distribution parameters, but not for other sources of uncertainties (for example, distribution selection), that could also significantly impact the total error, particularly at rarer frequencies.

Since the station dependence analysis (Section 4.6.2) indicated that for regions with more dense station network, AMS data from different stations could be correlated (especially for longer durations), the algorithm was adjusted to account for inter-station correlation. At each station, 1,000 simulated data sets per duration were used to generate precipitation quantiles. Estimates were sorted from smallest to largest and the $50^{\text {th }}$ value was selected as the lower confidence limit and the $950^{\text {th }}$ value was selected as the upper confidence limit.

Due to significant differences in record lengths across hourly and daily durations, it is expected that confidence intervals for hourly durations are much wider than corresponding intervals at daily durations. Because of very short records, similar to precipitation frequency estimates, confidence limits fluctuated a lot from duration to duration and confidence intervals were often wider than corresponding intervals for 24 -hour duration. To address this, confidence limit estimates were smoothed across durations and restricted by the corresponding value at 24 -hour duration.

### 4.7. Rainfall frequency estimates at stations

### 4.7.1. Background

Precipitation frequency estimates from Section 4.6 represent precipitation magnitudes regardless of the type of precipitation. For some applications it may be important to differentiate frequency estimates from liquid precipitation (i.e., rainfall) only. For example, rainfall is treated differently from snowfall in watershed modeling because of different runoff producing mechanisms - while rainfall generates runoff almost immediately, snowfall generally goes into storage until it melts and produces runoff at a later date.

In Alaska, due to geo-climatic conditions, the contribution of snowfall to the total yearly precipitation amount is significant. However, that does not necessarily translate to its significant participation in precipitation annual maximum series (AMS). To explore differences in total and liquid-only precipitation frequency estimates, concurrent rainfall and precipitation AMS were extracted at stations which had information useful for distinguishing the type of precipitation. Rainfall frequency analysis was done for durations up to 24 hours, which are of most interest to design projects relying on peak flows.

### 4.7.2. Extraction of rainfall data

Different methodologies were developed in order to segregate liquid from solid precipitation, depending on the type of data that was available in each dataset. More details on the type of data used for rainfall segregation for each dataset are given in Table 4.7.1. In the table, it is also indicated how many stations had at least 10 years of data which was the minimum number of years for a station to be considered for this analysis.

Table 4.7.1. Type of data used for segregation of liquid from total precipitation and number of stations per dataset.

| Recording <br> interval | Data source: dataset | Type of data available | Number of <br> stations |
| :--- | :--- | :--- | :---: |
| 1-day | Environment Canada | precipitation, rainfall | 55 |
|  | NCDC: TD3200 | precipitation, snowfall, air temperature | 281 |
|  | UAF: Arctic LTER | warm season precipitation | 0 |
|  | USDA: SNOTEL | precipitation, temperature | 39 |
|  | USGS | precipitation, air temperature | 2 |
| 1-hour | Environment Canada | precipitation, rainfall | 12 |
|  | NCDC: TD3240 and ISH | precipitation, rainfall, air temperature at <br> nearby daily NCDC station | 4 |
|  | RAWS | precipitation, air temperature | 78 |
|  | UAF: WERC - North Slope | warm season precipitation | 0 |
|  | UAF: Bonanza Creek LTER | warm season precipitation | 0 |
|  | UAF: Arctic LTER | warm season precipitation | 0 |

Stations from datasets that provided precipitation measurements only during warm months were not used in this analysis (shaded gray in the table) since it was assumed that all precipitation at those stations was liquid precipitation. Simultaneous rainfall and precipitation data were available only in the Environment Canada datasets. NCDC ISH also included rainfall-only data but there were not enough annual maxima at these stations to be useful in the analysis. For the NCDC TD3200 dataset, which contained records of precipitation and snowfall, the following three methods for the extraction of rainfall were considered:

1. For days with zero or missing snowfall, precipitation was assumed to be rainfall; for days with recorded snowfall, all precipitation was assumed to be snowfall.
2. Recorded snowfall amounts were first converted to snow water equivalent using the 10 to 1 rule, which assumes that the density of the snow is $1 / 10$ of the density of water. Rainfall amounts were then calculated as the difference between precipitation and snow water equivalent.
3. Recorded snowfall amounts were converted to snow water equivalent using the 10 to 1 rule. For days when the snow water equivalent was less than $1 / 3$ of the total precipitation amount, total precipitation was treated as a rainfall; otherwise it was assumed to be snowfall.

For other datasets, average daily air temperature measured at that station or at the nearest station from a different dataset was used to assign the type of precipitation. During cold months, all precipitation was considered snowfall. During warm months, pre-determined average daily air temperature thresholds were used to differentiate snowfall from rainfall. Warm (wet) and cold (dry) seasons were defined for each climate region in Section 4.3. Table 4.7.2 lists temperature thresholds for each climate region.

Table 4.7.2. Average daily air temperature threshold values used to segregate rainfall values from total precipitation for each climate region.

| Region | Temperature <br> threshold ( ${ }^{( } \mathbf{F}$ ) |
| :--- | :---: |
| Arctic | 32 |
| West Coast | 33 |
| Interior | 33 |
| Southwest Islands | 35 |
| Southwest Interior | 34 |
| Cook Inlet | 34 |
| South/Southeast Coast | 36 |

### 4.7.3. Rainfall frequency estimation

Concurrent rainfall and total precipitation annual maximum series were extracted for stations that had at least 10 years of data for the following durations: 1 -hour, 3 -hour, 6 -hour, 12 -hour and 24 -hour. Separate rainfall and precipitation frequency analyses were conducted using the Generalized Extreme Value (GEV) distribution with parameters estimated from L-moment statistics. For sub-daily durations, there was no real difference in frequency estimates between total and liquid precipitation. For the 24 -hour duration, for about half of the stations, precipitation AMS were made up almost exclusively of rainfall (an example is shown in panel a) of Figure 4.7.1). For about $23 \%$ of stations, solid precipitation annual maxima were among the more frequent events in total precipitations AMS (panel b); for approximately $12 \%$ of stations, solid precipitation annual maxima were among the highest amounts in AMS (panel c); and for about $15 \%$ of stations, the majority of total precipitation AMS were from solid precipitation (panel d).

Ratios of rainfall and precipitation frequency estimates were typically higher than 0.96 suggesting little difference between the two. For the NCDC 3200 dataset, findings were similar regardless of the method of segregation used. Moreover, when ratios were plotted on a map for selected annual exceedance probabilities, no spatial patterns were observed. Unfortunately, only a handful of stations were available at higher altitudes (above 3,000 feet) - nine daily stations and no hourly stations. So, assessing the effect of elevation on differences between rainfall and total precipitation frequencies was not feasible.

In conclusion, given that there were very few high-altitude stations and that the analysis of all available stations showed minor differences between rainfall and precipitation frequency estimates, it was decided not to provide separate rainfall frequency estimates in NOAA Atlas 14 Volume 7.


Figure 4.7.1. Probability distributions for the 24 -hour precipitation and rainfall annual maximum series at stations (a) $50-1325$, (b) $50-0546$, (c) $50-1824$, and (d) $50-1977$. The red line and red circles indicate the rainfall distribution and AMS data and the black line and black circles indicate the total precipitation distribution and AMS data.

### 4.8. Derivation of grids

### 4.8.1. Mean annual maximum precipitation

Mean annual maximum (MAM) grids served as the basis for deriving gridded precipitation frequency estimates at different frequencies and durations. The station mean annual maximum values for the 15 selected durations between 60 minutes and 60 days were spatially interpolated to produce corresponding mean annual maximum grids at 30 arc-seconds (on average around $928 \times 928$ meters or 3,045 by 3,045 feet) resolution using a hybrid statistical-geographic approach for mapping climate data named Parameter-elevation Regressions on Independent Slopes Model (PRISM) developed by Oregon State University's PRISM Climate Group (e.g., Daly et al., 2002).

Intermediate review of mean annual maxima grids suggested that in a two areas of varied terrain, where the lack of stations unduly influenced expected spatial patterns, it was beneficial to add mean annual maximum estimates for selected locations to anchor the spatial interpolation. MAMs were estimated across durations at the two locations shown in Table 4.8.1. Additionally, MAMs of one or more durations were adjusted at fifteen locations where inspection of spatial patterns indicated that estimates were not consistent with estimates at nearby stations or with climatological expectations.

Table 4.8.1. Locations where mean annual maxima were estimated to anchor spatial interpolation.

| Location ID | Location name | Latitude | Longitude | Elevation <br> $(\mathbf{f t})$ |
| :---: | :--- | :---: | :---: | :---: |
| $99-9998$ | Big Port Walter Mountain | 56.3966 | -134.7627 | 3020 |
| $99-9999$ | Mount Isto | 69.2003 | -143.8019 | 2730 |

Appendix A. 5 provides detailed information on the PRISM-based methodology for creating mean annual maxima grids. In summary, a unique regression function was developed for each target grid cell to derive mean annual maximum values for each duration that accounted for the difference between an observing station and the target cell's mean annual precipitation, topographic facet, coastal proximity, the distance of an observing station to the target cell, etc. Because of the limited number of stations recording at durations shorter than 1 day, sub-daily mean annual maximum data were developed for daily-only stations for 60 -minute through 12-hour durations (see Appendix A. 5 for more detail).

Jacknife cross-validation indicated that, for this project area, overall bias was less than 1 percent and the mean absolute error was less than 11 percent across all durations. However, given that so few stations were available in Alaska, and that cross-validation errors could be calculated only at stations, true interpolation errors in many parts of the state may be higher.

### 4.8.2. Precipitation frequency estimates with confidence limits

Estimates for 60-minute through 60-day durations. The HDSC-developed spatial interpolation technique termed 'CRAB' for the Cascade, Residual Add-Back (Parzybok and Yekta, 2003) which was used in previous NOAA Atlas 14 volumes to convert mean annual maximum grids into grids of AMS-based and PDS-based precipitation frequency estimates failed to produce spatial patterns in line with expected climatological patterns, especially for ARIs of 100 -years or more. That was especially the case in areas with very few stations and/or near stations with relatively short periods of record. The major limitation that caused CRAB's failure is that residuals, which are calculated for each station to quantify the difference between at-station estimates and initial gridded estimates, were spread across vast areas.

For that reason, an alternative interpolation technique was developed for this project area. Similar to CRAB , this technique derives grids along the frequency dimension for a given duration. Hence, the evolution of frequency-dependent spatial patterns for a given duration is independent of other durations. Also, similar to the CRAB process, it utilizes the inherently strong linear relationship that exists between mean annual maxima and precipitation frequency estimates for the 2 -year average recurrence interval (ARI), as well as between precipitation frequency estimates for consecutive ARIs. Figure 4.8.1 shows an example of the relationship between the 50 -year and 100 -year estimates for the entire project area for the 24 -hour duration. The $\mathrm{R}^{2}$ value here of 0.998 is very close to 1.0 , which was common for all relationships. The slope coefficient of 1.0995 can be thought of as an average domain-wide ratio between 100 -year and 50 -year quantiles for 24 -hour duration. In CRAB, this type of equation would be calculated using all stations in the project area and used to establish an initial grid of 100 -year precipitation frequency estimates, which would then be adjusted using a grid of residuals. However, when individual ratios were calculated for stations in the project area and plotted
on a map, the ratios clearly indicated regional patterns (see an example for 100-year 24-hour in Figure 4.8.2). The alternative interpolation technique used in this project is appropriate to interpolate such regional patterns.


Figure 4.8.1. Scatter plot of 100-year versus 50 -year precipitation frequency estimates based on 24hour annual maximum series. Linear regression line is also shown.


Figure 4.8.2 Spatially interpolated ratios used to calculate 24 -hour 100-year precipitation frequency grid from the 50 -year grid.

For each duration, the cascade began with the PRISM-derived mean annual maximum (MAM) grid as the initial predictor grid and the 2-year precipitation frequency estimates as the subsequent grid. Ratios between the 2 -year estimates and corresponding MAM estimates for each station were spatially interpolated to a grid by applying an inverse-distance-weighting algorithm that uses the nine closest stations not more than 100 miles apart. Gridded MAM estimates were then multiplied by
corresponding gridded ratios to create a grid of 2-year precipitation frequency estimates. In the subsequent run, ratios between the 5-year and 2-year estimates were interpolated and used to calculate 5 -year precipitation grid from the 2 -year grid, and so forth. 2 -year precipitation frequency estimates were also used to create a grid of 1-year estimates.

To ensure consistency in grid cell values across all durations and frequencies, duration-based internal consistency checks were conducted (e.g., 24-hour estimate less than 12 -hour estimate). For inconsistent cases, the longer duration grid cell value was adjusted by multiplying the shorter duration grid cell value by 1.01 to provide a $1 \%$ difference between the values. After grid cell consistency was ensured across durations, it was performed across frequencies to ensure that there were no frequencybased inconsistencies caused by the adjustment.

A jack-knife cross-validation technique (Shao and Tu, 1995) was used to evaluate the spatial interpolation technique's performance for interpolating precipitation frequency estimates. It was cost prohibitive to re-create the PRISM mean annual maximum grids for each cross-validation iteration. For this reason, the cross-validation results reflect the accuracy of the interpolation procedure based on the same mean annual maximum grids. Figure 4.8 .3 shows validation results for 100-year, 24hour estimates as a histogram representing the distribution of differences in 100-year 24-hour estimates with and without each station. For more than $86 \%$ of stations in the project area, differences were less than $\pm 10 \%$. Errors of more than $\pm 20 \%$ occurred at several hourly stations scattered throughout the state. Given the vastness of the project area and the limited number of stations with relatively short periods of record, overall, the spatial interpolation technique adequately reproduced values. However, similar to the MAM interpolation, given that cross-validation errors could be calculated only at stations, true interpolation errors in many parts of the state may be even higher.


Figure 4.8.3. NOAA Atlas 14 Volume 7 jackknife cross-validation results for 100 -year 24 -hour estimates.

Estimates for sub-hourly durations. Precipitation frequency grids for sub-hourly durations were derived by multiplying the 60 -minute precipitation frequency grids by corresponding scaling factors (see Table 4.6.1).

Confidence limits. Grids of upper and lower limits of the $90 \%$ confidence interval for the precipitation frequency estimates were derived using same procedures that were used to create grids of precipitation frequency estimates.

## 5. Precipitation Frequency Data Server

### 5.1. Introduction

NOAA Atlas 14 precipitation frequency estimates are delivered entirely in digital form in order to make the estimates more widely available and to provide them in various formats. The Precipitation Frequency Data Server (PFDS; http://hdsc.nws.noaa.gov/hdsc/pfds/) is a point-and-click interface developed as the primary web portal for precipitation frequency estimates and associated information.

### 5.2. Underlying data

The PFDS operates from a set of ASCII grids of precipitation frequency estimates and lower and upper bounds of the $90 \%$ confidence interval. The grids can be downloaded from the website and imported into a Geographical Information System (GIS). Table 5.2.1 shows the complete set of average recurrence intervals and durations for which PDS-based frequency estimates with $95 \%$ confidence limits are available from the PFDS for any location in the project area. Similarly, Table 5.2.2 shows the complete set of annual exceedance probabilities and durations for which AMS-based frequency estimates with confidence limits are available from the PFDS for any particular location.

The ASCII grids, which represent the official estimates, have the following pertinent metadata:

- Resolution: 30 arc-seconds (on average around $928 \times 928$ meters or 3,045 by 3,045 feet);
- Units: inches*1000 (integer);
- Projection: geographic (longitude/latitude);
- Datum: NAD 83.

Table 5.2.1. Average recurrence intervals and durations for which PDS-based precipitation frequency estimates with $90 \%$ confidence intervals are available from the PFDS.

| Duration | Average recurrence interval (ARI) |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{1 - y r}$ | $\mathbf{2 - y r}$ | $\mathbf{5 - y r}$ | $\mathbf{1 0}$-yr | 25-yr | 50-yr | $\mathbf{1 0 0}$-yr | 200-yr | 500-yr | 1,000-yr |
| 5-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 10-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 15-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 30-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 60-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 2-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 3-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 6-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 12-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 24-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 2-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 3-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 4-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 7-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 10-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 20-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 30-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 45-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 60-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |

Table 5.2.2. Annual exceedance probabilities and durations for which AMS-based precipitation frequency estimates with $90 \%$ confidence intervals are available from the PFDS.

| Duration | Annual exceedance probability (AEP) |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{1 / 2}$ | $\mathbf{1 / 5}$ | $\mathbf{1 / 1 0}$ | $\mathbf{1 / 2 5}$ | $\mathbf{1 / 5 0}$ | $\mathbf{1 / 1 0 0}$ | $\mathbf{1 / 2 0 0}$ | $\mathbf{1 / 5 0 0}$ | $\mathbf{1 / 1 0 0 0}$ |
| 5-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 10-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 15-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 30-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 60-minute | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 2-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 3-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 6-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 12-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 24-hour | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 2-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 3-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 4-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 7-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 10-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 20-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 30-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 45-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 60-day | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |

### 5.3. Products available on the Precipitation Frequency Data Server

The PFDS homepage (http://hdsc.nws.noaa.gov/hdsc/pfds/) has a clickable map of the United States. Upon clicking on Alaska or selecting the state name from the drop-down menu, an interactive map of Alaska and its surrounding area is displayed (see Figure 5.3.1). A location for which precipitation frequency estimates are needed can be selected by:

- Manually entering latitude and longitude coordinates in decimal degrees (negative numbers should be entered for southern hemisphere latitudes and for western hemisphere longitudes);
- Selecting a station from a pull-down list;
- Dragging the red cursor to a location on the map;
- Double clicking anywhere on the map;
- Clicking on an observing station on the map (after selecting "show stations on map" and zooming in).
From the menu at the top of the page, a user can select PDS-based or AMS-based precipitation frequency estimates, units and whether estimates should be displayed as precipitation depths or intensities.


Figure 5.3.1. Initial view of the interactive map of Alaska.
After a location is selected, all precipitation frequency and confidence limit estimates from the underlying grids are extracted and the output is displayed directly below the map in three separate tabs: 'PF tabular', 'PF graphical' and 'Supplementary information'. A printer-friendly version of the precipitation frequency estimates with some supplementary information can be obtained by selecting the "Print Page" icon above the output display (see Figure 5.3.2). The printed page will include metadata information about the selected point in the header, tabular and graphical representations of the estimates, and maps of the location.

The 'PF tabular' tab provides data tables of the precipitation frequency depths (or intensities) showing also the lower and upper bounds of the $90 \%$ confidence interval. These data can be downloaded as comma-separated values (csv format) from a selection beneath the tables (see Figure 5.3.2).

| PF tabular |  | PF graphical |  | Supplementary information |  |  | Print Page |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PDS-based precipitation frequency estimates with 90\% confidence intervals (in inches) ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |
| Duration | Average recurrence interval (years) |  |  |  |  |  |  |  |  |  |
|  | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.093 <br> $(0.068-0.130)$ | $\begin{gathered} 0.123 \\ (0.089-0.174) \end{gathered}$ | $\begin{gathered} 0.174 \\ (0.123-0.251) \end{gathered}$ | $\begin{gathered} 0.216 \\ (0.151-0.316) \end{gathered}$ | $\begin{gathered} 0.274 \\ (0.188-0.408) \end{gathered}$ | $\begin{array}{c\|} \hline 0.319 \\ (0.215-0.483) \\ \hline \end{array}$ | $\begin{gathered} 0.364 \\ (0.242-0.559) \end{gathered}$ | $\begin{gathered} 0.430 \\ (0.281-0.670) \\ \hline \end{gathered}$ | $\begin{gathered} 0.518 \\ (0.333-0.823) \\ \hline \end{gathered}$ | $\begin{gathered} 0.584 \\ (0.370-0.942) \end{gathered}$ |
| 10-min | $\begin{gathered} 0.125 \\ (0.091-0.175) \end{gathered}$ | $\begin{gathered} 0.165 \\ (0.119-0.233) \end{gathered}$ | $\begin{gathered} 0.234 \\ (0.166-0.337) \end{gathered}$ | $\begin{gathered} 0.290 \\ (0.203-0.424) \end{gathered}$ | $\begin{gathered} 0.368 \\ (0.252-0.549) \end{gathered}$ | $\begin{gathered} 0.428 \\ (0.289-0.648) \end{gathered}$ | $\begin{gathered} 0.488 \\ (0.324-0.750) \end{gathered}$ | $\begin{array}{c\|} \hline 0.578 \\ (0.378-0.901) \end{array}$ | $\begin{gathered} 0.695 \\ (0.446-1.11) \end{gathered}$ | $\begin{gathered} 0.784 \\ (0.496-1.26) \end{gathered}$ |
| 15-min | $\begin{gathered} 0.146 \\ (0.107-0.204) \end{gathered}$ | $\begin{gathered} 0.194 \\ (0.140-0.274) \end{gathered}$ | $\begin{gathered} 0.273 \\ (0.194-0.393) \end{gathered}$ | $\begin{gathered} 0.340 \\ (0.237-0.497) \end{gathered}$ | $\begin{gathered} 0.431 \\ (0.295-0.642) \end{gathered}$ | $\begin{gathered} 0.501 \\ (0.338-0.758) \end{gathered}$ | $\begin{gathered} 0.571 \\ (0.379-0.877) \end{gathered}$ | $\begin{gathered} 0.676 \\ (0.442-1.05) \end{gathered}$ | $\begin{gathered} 0.813 \\ (0.522-1.29) \end{gathered}$ | $\begin{gathered} 0.918 \\ (0.581-1.48) \end{gathered}$ |
| 30-min | $\begin{gathered} 0.194 \\ (0.142-0.271) \end{gathered}$ | $\begin{gathered} 0.257 \\ (0.186-0.363) \end{gathered}$ | $\begin{gathered} 0.363 \\ (0.257-0.523) \end{gathered}$ | $\begin{gathered} 0.451 \\ (0.315-0.659) \end{gathered}$ | $\begin{gathered} 0.572 \\ (0.392-0.853) \end{gathered}$ | $\begin{gathered} 0.665 \\ (0.448-1.01) \end{gathered}$ | $\begin{gathered} 0.758 \\ (0.504-1.16) \end{gathered}$ | $\begin{gathered} 0.897 \\ (0.587-1.40) \end{gathered}$ | $\begin{gathered} 1.08 \\ (0.693-1.72) \end{gathered}$ | $\begin{gathered} 1.22 \\ (0.771-1.96) \end{gathered}$ |
| 60-min | $\begin{gathered} 0.266 \\ (0.194-0.372) \end{gathered}$ | $\begin{gathered} 0.352 \\ (0.254-0.498) \end{gathered}$ | $\begin{gathered} 0.497 \\ (0.352-0.716) \end{gathered}$ | $\begin{gathered} 0.618 \\ (0.432-0.903) \end{gathered}$ | $\begin{gathered} 0.783 \\ (0.536-1.17) \end{gathered}$ | $\begin{gathered} 0.911 \\ (0.614-1.38) \end{gathered}$ | $\begin{gathered} 1.04 \\ (0.690-1.60) \end{gathered}$ | $\begin{gathered} 1.23 \\ (0.804-1.92) \end{gathered}$ | $\begin{gathered} 1.48 \\ (0.949-2.35) \end{gathered}$ | $\begin{gathered} 1.67 \\ (1.06-2.69) \end{gathered}$ |
| 2-hr | $\begin{gathered} 0.327 \\ (0.239-0.457) \end{gathered}$ | $\begin{gathered} 0.433 \\ (0.313-0.612) \end{gathered}$ | $\begin{gathered} 0.612 \\ (0.434-0.881) \end{gathered}$ | $\begin{gathered} 0.762 \\ (0.532-1.11) \end{gathered}$ | $\begin{gathered} 0.966 \\ (0.661-1.44) \end{gathered}$ | $\begin{gathered} 1.12 \\ (0.757-1.70) \end{gathered}$ | $\begin{gathered} 1.28 \\ (0.849-1.96) \end{gathered}$ | $\begin{gathered} 1.51 \\ (0.989-2.36) \end{gathered}$ | $\begin{gathered} 1.82 \\ (1.17-2.89) \end{gathered}$ | $\begin{gathered} 2.05 \\ (1.30-3.31) \end{gathered}$ |
| 3-hr | $\begin{gathered} 0.363 \\ (0.265-0.507) \end{gathered}$ | $\begin{gathered} 0.480 \\ (0.346-0.679) \end{gathered}$ | $\begin{gathered} 0.680 \\ (0.482-0.979) \end{gathered}$ | $\begin{gathered} 0.846 \\ (0.591-1.24) \end{gathered}$ | $\begin{gathered} 1.07 \\ (0.735-1.60) \end{gathered}$ | $\begin{gathered} 1.25 \\ (0.840-1.89) \end{gathered}$ | $\begin{gathered} 1.42 \\ (0.942-2.18) \end{gathered}$ | $\begin{gathered} 1.68 \\ (1.10-2.62) \\ \hline \end{gathered}$ | $\begin{gathered} 2.02 \\ (1.30-3.21) \end{gathered}$ | $\begin{gathered} 2.28 \\ (1.44-3.67) \end{gathered}$ |
| 6-hr | $\begin{gathered} 0.481 \\ (0.351-0.672) \\ \hline \end{gathered}$ | $\begin{gathered} 0.638 \\ (0.461-0.902) \end{gathered}$ | $\begin{gathered} 0.900 \\ (0.638-1.30) \end{gathered}$ | $\begin{gathered} 1.12 \\ (0.781-1.63) \end{gathered}$ | $\begin{gathered} 1.42 \\ (0.971-2.11) \end{gathered}$ | $\begin{gathered} 1.65 \\ (1.11-2.50) \end{gathered}$ | $\begin{gathered} 1.88 \\ (1.25-2.89) \end{gathered}$ | $\begin{gathered} 2.23 \\ (1.46-3.47) \end{gathered}$ | $\begin{gathered} 2.68 \\ (1.72-4.26) \end{gathered}$ | $\begin{gathered} 3.02 \\ (1.91-4.88) \end{gathered}$ |
| 12-hr | $\begin{gathered} 0.634 \\ (0.463-0.886) \end{gathered}$ | $\begin{gathered} 0.841 \\ (0.607-1.19) \end{gathered}$ | $\begin{gathered} 1.17 \\ (0.828-1.68) \end{gathered}$ | $\begin{gathered} 1.44 \\ (1.01-2.11) \end{gathered}$ | $\begin{gathered} 1.84 \\ (1.26-2.74) \end{gathered}$ | $\begin{gathered} 2.15 \\ (1.45-3.26) \end{gathered}$ | $\begin{gathered} 2.49 \\ (1.65-3.82) \end{gathered}$ | $\begin{gathered} 2.94 \\ (1.93-4.59) \end{gathered}$ | $\begin{gathered} 3.55 \\ (2.28-5.64) \end{gathered}$ | $\begin{gathered} 4.00 \\ (2.53-6.45) \end{gathered}$ |
| 24-hr | $\begin{gathered} 0.824 \\ (0.748-0.918) \end{gathered}$ | $\begin{gathered} 1.09 \\ (0.978-1.23) \end{gathered}$ | $\begin{gathered} 1.49 \\ (1.31-1.72) \end{gathered}$ | $\begin{gathered} 1.83 \\ (1.58-2.14) \end{gathered}$ | $\begin{gathered} 2.33 \\ (1.96-2.79) \end{gathered}$ | $\begin{gathered} 2.76 \\ (2.28-3.37) \end{gathered}$ | $\begin{gathered} 3.22 \\ (2.62-4.00) \end{gathered}$ | $\begin{gathered} 3.81 \\ (3.05-4.82) \end{gathered}$ | $\begin{gathered} 4.59 \\ (3.59-5.93) \end{gathered}$ | $\begin{gathered} 5.18 \\ (3.99-6.81) \end{gathered}$ |
| 2-day | $\begin{gathered} 0.995 \\ (0.903-1.11) \end{gathered}$ | $\begin{gathered} \mathbf{1 . 3 1} \\ (1.18-1.48) \end{gathered}$ | $\begin{gathered} 1.78 \\ (1.56-2.05) \end{gathered}$ | $\begin{gathered} 2.17 \\ (1.87-2.55) \end{gathered}$ | $\begin{gathered} 2.75 \\ (2.32-3.30) \end{gathered}$ | $\begin{gathered} 3.25 \\ (2.69-3.97) \end{gathered}$ | $\begin{gathered} 3.79 \\ (3.08-4.70) \end{gathered}$ | $\begin{gathered} 4.46 \\ (3.56-5.63) \end{gathered}$ | $\begin{gathered} 5.34 \\ (4.17-6.90) \end{gathered}$ | $\begin{gathered} 6.01 \\ (4.62-7.89) \end{gathered}$ |
| 3-day | $\begin{gathered} 1.10 \\ (0.999-1.23) \end{gathered}$ | $\begin{gathered} 1.45 \\ (1.30-1.63) \end{gathered}$ | $\begin{gathered} 1.96 \\ (1.72-2.26) \end{gathered}$ | $\begin{gathered} 2.39 \\ (2.06-2.80) \end{gathered}$ | $\begin{gathered} 3.02 \\ (2.54-3.62) \end{gathered}$ | $\begin{gathered} 3.55 \\ (2.93-4.33) \end{gathered}$ | $\begin{gathered} 4.12 \\ (3.35-5.12) \end{gathered}$ | $\begin{gathered} 4.83 \\ (3.86-6.11) \end{gathered}$ | $\begin{gathered} 5.77 \\ (4.51-7.46) \end{gathered}$ | $\begin{gathered} 6.48 \\ (4.99-8.52) \end{gathered}$ |
| 4-day | $\begin{gathered} 1.19 \\ (1.08-1.32) \end{gathered}$ | $\begin{gathered} 1.55 \\ (1.39-1.75) \end{gathered}$ | $\begin{gathered} 2.09 \\ (1.84-2.41) \end{gathered}$ | $\begin{gathered} 2.54 \\ (2.19-2.98) \end{gathered}$ | $\begin{gathered} 3.21 \\ (2.70-3.85) \end{gathered}$ | $\begin{gathered} 3.76 \\ (3.11-4.59) \end{gathered}$ | $\begin{gathered} 4.37 \\ (3.55-5.43) \end{gathered}$ | $\begin{gathered} 5.11 \\ (4.09-6.46) \end{gathered}$ | $\begin{gathered} 6.09 \\ (4.77-7.87) \\ \hline \end{gathered}$ | $\begin{gathered} 6.84 \\ (5.26-8.98) \end{gathered}$ |
| 7-day | $\begin{gathered} 1.42 \\ (1.29-1.58) \end{gathered}$ | $\begin{gathered} 1.82 \\ (1.63-2.05) \end{gathered}$ | $\begin{gathered} 2.41 \\ (2.12-2.78) \end{gathered}$ | $\begin{gathered} 2.91 \\ (2.51-3.41) \end{gathered}$ | $\begin{gathered} 3.65 \\ (3.07-4.38) \end{gathered}$ | $\begin{gathered} 4.27 \\ (3.53-5.22) \end{gathered}$ | $\begin{gathered} 4.95 \\ (4.03-6.15) \end{gathered}$ | $\begin{gathered} 5.80 \\ (4.64-7.34) \end{gathered}$ | $\begin{gathered} 6.93 \\ (5.42-8.95) \end{gathered}$ | $\begin{gathered} 7.78 \\ (5.98-10.2) \end{gathered}$ |
| 10-day | $\begin{gathered} 1.61 \\ (1.46-1.79) \end{gathered}$ | $\begin{gathered} 2.03 \\ (1.82-2.29) \end{gathered}$ | $\begin{gathered} 2.66 \\ (2.33-3.06) \end{gathered}$ | $\begin{gathered} 3.19 \\ (2.75-3.74) \end{gathered}$ | $\begin{gathered} 3.98 \\ (3.35-4.77) \end{gathered}$ | $\begin{gathered} 4.64 \\ (3.84-5.67) \end{gathered}$ | $\begin{gathered} 5.37 \\ (4.37-6.67) \end{gathered}$ | $\begin{gathered} 6.29 \\ (5.02-7.94) \end{gathered}$ | $\begin{gathered} 7.49 \\ (5.86-9.68) \end{gathered}$ | $\begin{gathered} 8.41 \\ (6.47-11.0) \end{gathered}$ |
| 20-day | $\begin{gathered} 2.20 \\ (2.00-2.45) \end{gathered}$ | $\begin{gathered} 2.73 \\ (2.44-3.08) \end{gathered}$ | $\begin{gathered} 3.49 \\ (3.06-4.03) \end{gathered}$ | $\begin{gathered} 4.13 \\ (3.56-4.84) \end{gathered}$ | $\begin{gathered} 5.06 \\ (4.26-6.07) \end{gathered}$ | $\begin{gathered} 5.83 \\ (4.83-7.12) \end{gathered}$ | $\begin{gathered} 6.67 \\ (5.42-8.28) \end{gathered}$ | $\begin{gathered} 7.65 \\ (6.11-9.66) \end{gathered}$ | $\begin{gathered} 8.94 \\ (6.99-11.5) \end{gathered}$ | $\begin{gathered} 9.91 \\ (7.62-13.0) \end{gathered}$ |
| 30-day | $\begin{gathered} 2.76 \\ (2.50-3.07) \end{gathered}$ | $\begin{gathered} 3.39 \\ (3.04-3.83) \end{gathered}$ | $\begin{gathered} 4.29 \\ (3.76-4.94) \\ \hline \end{gathered}$ | $\begin{gathered} 5.03 \\ (4.33-5.89) \end{gathered}$ | $\begin{gathered} 6.08 \\ (5.12-7.29) \\ \hline \end{gathered}$ | $\begin{gathered} 6.95 \\ (5.75-8.48) \\ \hline \end{gathered}$ | $\begin{gathered} 7.87 \\ (6.40-9.78) \\ \hline \end{gathered}$ | $\begin{gathered} 8.88 \\ (7.10-11.2) \\ \hline \end{gathered}$ | $\begin{gathered} 10.2 \\ (7.98-13.2) \\ \hline \end{gathered}$ | $\begin{gathered} 11.2 \\ (8.62-14.7) \\ \hline \end{gathered}$ |
| 45-day | $\begin{gathered} 3.50 \\ (3.18-3.90) \end{gathered}$ | $\begin{gathered} 4.29 \\ (3.84-4.84) \end{gathered}$ | $\begin{gathered} 5.38 \\ (4.72-6.20) \end{gathered}$ | $\begin{gathered} 6.24 \\ (5.37-7.31) \end{gathered}$ | $\begin{gathered} 7.42 \\ (6.25-8.91) \end{gathered}$ | $\begin{gathered} 8.37 \\ (6.92-10.2) \end{gathered}$ | $\begin{gathered} 9.35 \\ (7.60-11.6) \end{gathered}$ | $\begin{gathered} 10.3 \\ (8.26-13.1) \end{gathered}$ | $\begin{gathered} 11.6 \\ (9.10-15.0) \end{gathered}$ | $\begin{gathered} 12.6 \\ (9.70-16.6) \end{gathered}$ |
| 60-day | $\begin{gathered} 4.07 \\ (3.69-4.53) \\ \hline \end{gathered}$ | $\begin{gathered} 5.03 \\ (4.51-5.68) \end{gathered}$ | $\begin{gathered} 6.29 \\ (5.52-7.25) \\ \hline \end{gathered}$ | $\begin{gathered} 7.22 \\ (6.23-8.47) \end{gathered}$ | $\begin{gathered} 8.44 \\ (7.11-10.1) \\ \hline \end{gathered}$ | $\begin{gathered} 9.35 \\ (7.74-11.4) \end{gathered}$ | $\begin{gathered} 10.2 \\ (8.33-12.7) \end{gathered}$ | $\begin{gathered} 11.1 \\ (8.89-14.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12.3 \\ (9.59-15.9) \end{gathered}$ | $\begin{gathered} 13.1 \\ (10.1-17.3) \\ \hline \end{gathered}$ |
| ${ }^{1}$ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). <br> Numbers in parenthesis are PF estimates at lower and upper bounds of the $90 \%$ confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is $5 \%$. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. <br> Please refer to NOAA Atlas 14 document for more information. |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |

## Main Link Categories: <br> Home IOHD

Figure 5.3.2. Precipitation frequency data for a selected location in tabular format.
The 'PF graphical' tab has two sub-tabs. The first, 'Curves', shows two basic types of output based on the user's selection of data type: depth-duration-frequency (DDF) or intensity-durationfrequency (IDF) graphs. The PFDS provides DDF and IDF graphs in two different formats: with duration and with frequency on x-axis. An example of the DDF graph in both formats is given in Figure 5.3.3; an example of the IDF graph with duration on $x$-axis is shown in Figure 5.3.4. Both, DDF and IDF graphs can be built from either AMS or PDS data, depending on the user's selection of time series type. The second sub-tab, 'PF estimates with confidence intervals' shows plots of the precipitation magnitude-frequency curve with upper and lower confidence limits for a selected duration (see example in Figure 5.3.5).


Figure 5.3.3. Sample depth-duration-frequency curves built from the PDS data with duration on the x -axis (top figure) and average recurrence interval on the x -axis (bottom figure).


Figure 5.3.4. Sample intensity-duration-frequency (IDF) graph with duration on the x -axis.


## Supplementary information



Figure 5.3.5. Sample of a magnitude-frequency plot with the upper and lower bounds of the $90 \%$ confidence interval for 24 -hour duration.

Lastly, the 'Supplementary information' tab provides links to additional data and information for that location:

## - NOAA Atlas 14 Volume 7 document.

- Precipitation frequency grids in GIS compatible formats. Grids are available for AMS- and PDS-based estimates for all combinations of durations and average recurrence intervals or annual exceedance probabilities, respectively (as shown in Tables 5.2.1 and 5.2.2). Users are advised to review the Federal Geographic Data Committee (FGDC) compliant metadata before using any of the GIS datasets (http://hdsc.nws.noaa.gov/hdsc/pfds/meta/na14_vol7_ak_grid_metadata.xml).
- Cartographic maps of precipitation frequency estimates. Cartographic maps show contour lines created from gridded PDS-based precipitation frequency estimates for selected durations and average recurrence intervals. Figure 5.3.6 shows an excerpt from a cartographic map. Maps were created to serve as visual aids and are not recommended for interpolating precipitation frequency estimates. Users are advised to retrieve point precipitation frequency values from the PFDS interface which accesses the gridded data directly.


Figure 5.3.6. An excerpt of a cartographic map for 2-year ARI and 24-hour duration.

- Temporal distributions. Temporal distributions of precipitation amounts exceeding precipitation frequency estimates for the 2 -year recurrence interval are provided for 6 -hour, 12hour, 24 -hour, and 96 -hour durations for delineated climate regions. The temporal distributions for the duration are expressed in probability terms as cumulative percentages of precipitation totals. To provide detailed information on the varying temporal distributions, separate temporal distributions were derived for four precipitation cases defined by the duration quartile in which the greatest percentage of the total precipitation occurred. Figure 5.3.7 shows as an example the regional temporal distribution curves of all precipitation cases for the 6-hour and 24-hour durations. See Appendix A. 7 for more information.
- Seasonality analysis. The seasonality graphs (an example is shown in Figure 5.3.8) show the percentage of annual maxima for a given duration that exceeded the NOAA Atlas 14 precipitation frequency estimates for the duration and selected annual exceedance probabilities in each month for various climate regions. Results are provided for the 60 -minute, 24 -hour, 2 -day, and 10 -day durations and for annual exceedance probabilities of $1 / 2,1 / 5,1 / 10,1 / 25,1 / 50$, and $1 / 100$. Seasonality graphs are not intended to be used to derive seasonal precipitation frequency estimates. See Appendix A. 8 for more information.


Figure 5.3.7. Sample temporal distribution curves for 6-hour (left panel) and 12-hour (right panel).
24-nr duration Based on 163 stations and 5616 cumulative years of record


| Annual exceedance <br> probability |
| :---: |
| $-1 / 2$ |
| $-1 / 5$ |
| $-1 / 10$ |
| $-1 / 25$ |
| $-1 / 50$ |
| $-1 / 100$ |

Figure 5.3.8. Sample 24-hour seasonal exceedance graph.

- Rainfall frequency estimates. Given that there were very few high-altitude stations and that the analysis of available stations showed only minor differences between rainfall and precipitation frequency estimates, it was decided not to provide separate rainfall frequency estimates in NOAA Atlas 14 Volume 7. See Section 4.7 for more information.
- Time series data. Annual maximum series precipitation data used in frequency analysis is available for gauged locations.
- Information on nearby climate stations (via NCDC).
- Watershed information (via the Environmental Protection Agency).

Some of the NOAA Atlas 14 data products can also be accessed through the left menu bar on the PFDS web page, including:

- ASCII grids of precipitation frequency estimates,
- cartographic maps,
- temporal distributions,
- annual maximum series datasets,
- associated documentation.

Answers to frequently asked questions (FAQ) are available via links on the PFDS web site. Inquiries regarding the use of the PFDS or its data can be addressed by emailing HDSC.Questions@noaa.gov.

## 6. Peer review

A peer review of the Alaska precipitation frequency project's preliminary results was carried out during a four week period starting on August 2, 2011. The request for review was sent via email to the members of the HDSC list-server from all over the United States and other interested parties in Alaska. Potential reviewers were asked to evaluate the reasonableness of point precipitation frequency estimates as well as their spatial patterns. The review included the following items:
a. List of all stations used in the analysis. The list included information on station name, state, source of data, assigned station identification number, latitude, longitude, elevation, and period of record. It also showed information if the station was merged with another station, if the station was co-located with another station with a different ID, and if metadata at the station were changed.
b. List of all stations that were received, but not considered in analysis. This list contained stations that were not used, either because there was another station with a longer period of record nearby, station data were not reliable, or the station period of record was not long enough and it was not a candidate for merging with any nearby station.
c. Spatially-interpolated mean annual maxima for 60 -minute, 24 -hour and 10 -day durations.
d. Spatially-interpolated precipitation frequency estimates for 60 -minute, 24 -hour and 10 -day durations and for 2-year and 100-year average recurrence intervals.
e. At-station depth-duration-frequency curves for 60 -minute to 10 -day durations and for 2 -year to 100 -year average recurrence intervals (ARI).
The reviews provided critical feedback that improved estimates. Reviewers' comments regarding station metadata, at-station precipitation frequency estimates and their spatial patterns, and supplemental information along with HDSC responses can be found in Appendix A.6.

## 7. Comparison with previous NOAA publications

The precipitation frequency estimates in NOAA Atlas 14 Volume 7 supersede the estimates for Alaska previously published in the following publications:
a. Technical Paper No. 47, Probable Maximum Precipitation and Rainfall-Frequency Data for Alaska for Areas to 400 Square Miles, Durations to 24 Hours, and Return Periods from 1 to 100 Years (Miller, 1963);
b. Technical Paper No. 52, Two-to-Ten-Day Precipitation for Return Periods of 2 to 100 Years in Alaska (Miller, 1965).
Precipitation frequency estimates at the 100 -year average recurrence interval from NOAA Atlas 14 Volume 7 were examined in relation to corresponding estimates from Technical Paper No. 47 (TP47) for 60-minute and 24-hour durations. Corresponding TP47 paper maps (Figures 3-24 and 353 , respectively) were geo-referenced. Isopluvial contours were digitized and converted to gridded format using standard spatial interpolation tools available in ArcGIS for the comparison.

The maps in Figures 7.1 and 7.2 illustrate the differences between new and old estimates. On average, 60 -minute precipitation frequency estimates increased by 0.21 inches; at specific locations estimates changed between -0.72 and 1.26 inches. Differences in 100 -year 24-hour precipitation frequency estimates ranged between -9.27 and 11.17 inches, but on average estimates changed very little (decreased by 0.18 inches).


Figure 7.1. Differences in 100-year 60-minute estimates (in inches) between NOAA Atlas 14 and TP47.


Figure 7.2. Differences in 100-year 24-hour estimates (in inches) between NOAA Atlas 14 and TP47.

The differences in estimates between the two publications are attributed to a number of factors, including errors in digitizing and converting contours to grids for TP47 estimates, improved frequency analysis approaches and interpolation techniques used in NOAA Atlas 14 (see Section 4), and above all, to the increase in the number of stations and periods of record across all durations used in frequency analysis.

Technical Paper No. 47 was published in 1963, so potentially about 50 additional data years were available at stations used in TP47 for the NOAA Atlas 14 analyses. For the 24-hour duration, a total of 211 stations with an average period of record of 18 years (ranging from 1 to 54 years) were used for frequency analysis in TP47, while in NOAA Atlas 14 Volume 7 a total of 396 stations with an average of 32 data years per station ( 9 to 103 years) were used. Figure 7.3 shows record lengths for daily stations used in each publication.


Figure 7.3. Number of daily stations used for precipitation frequency analysis versus record length shown as years of record for TP47 and data years for NOAA Atlas 14 Volume 7 (data years may be shorter than years of record due to missing data at stations).

Also, since 1963, stations have been added at higher elevations (Table 7.1). This is crucial since more than 50 percent of the land in Alaska lies at an elevation that is higher than 1,000 feet and about $20 \%$ of the land is above 3,000 feet.

Table 7.1. Number of daily stations used for precipitation frequency analysis for TP47 and NOAA Atlas 14 Volume 7 grouped by elevation.

| Number of daily stations | TP47 | NOAA Atlas 14 |
| :---: | :---: | :---: |
| Total used in analysis | 211 | 396 |
| Above $1,000 \mathrm{ft}$ | 26 | 134 |
| Above $3,000 \mathrm{ft}$ | 0 | 10 |

The difference in available data between the two studies is even more pronounced for hourly durations. In TP47, only 9 stations were available, with an average record length of less than 10 years (ranging from 1 to 20 years). For NOAA Atlas 14, 121 stations with an average of 18 years (rainging from 10 to 49 data years) were available. Figure 7.4 shows record lengths for hourly stations used in each publication. The maximum elevation of hourly stations in TP47 was 500 feet, while in NOAA Atlas 14 hourly stations were found as high as 3,000 feet.


Figure 7.4. Number of hourly stations used for precipitation frequency analysis for TP47 (years of record) and NOAA Atlas 14 Volume 7 (data years).

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| Cost-merge | Co-located <br> station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record <br> station ID |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| Station name | $50-0522$ |  |  | 1 -day | NCDC | $\mathbf{5 7 . 0 8 1 6}$ | $-\mathbf{- 1 3 4 . 8 3 3 0}$ | 20 |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | CAPE NEWENHAM | 50-1314 |  |  | 1-day | NCDC | 58.6445 | -162.0635 | 475 | 9/1953-11/1984 |
| 1 | CAPE ROMANZOF | 50-1318 |  |  | 1-day | NCDC | 61.7667 | -166.0500 | 434 | 5/1953-2/1985 |
| $\stackrel{\sim}{0}$ | CAPE SARICHEF | 50-1325 |  |  | 1-day | NCDC | 54.5960 | -164.9240 | 177 | 3/1952-12/1980 |
| $\stackrel{\rightharpoonup}{\square}$ | CAPE SPENCER | 50-1334 |  |  | 1-day | NCDC | 58.1988 | -136.6402 | 89 | 11/1936-8/1974 |
| $<$ | CAPE ST ELIAS | 50-1321 |  |  | 1-day | NCDC | 59.7984 | -144.5988 | 49 | 7/1936-7/1974 |
| E | Caribou Peak | 80-0425 |  |  | 1-hour | RAWS | 65.1738 | -147.4910 | 1564 | 6/1990-12/2010 |
| $\stackrel{\rightharpoonup}{8}$ | CENTRAL \#2 | 50-1458 | 50-1466 |  | 1-day | NCDC | 65.5833 | -144.8000 | 869 | 5/1905-5/1954 |
| $\checkmark$ | CENTRAL \#2 | 50-1466 |  |  | 1-day | NCDC | 65.5667 | -144.7667 | 920 | 5/1905-7/2010 |
| 8 | CHALKYITSIK | 80-0440 |  |  | 1-hour | RAWS | 66.5906 | -144.3411 | 450 | 6/1997-12/2010 |
| 0. | CHANDALAR LAKE | 50-1492 |  |  | 1-day | NCDC | 67.5167 | -148.5000 | 1895 | 6/1963-7/2010 |
| N | CHANDALAR LAKE | 50-5354 | 50-1492 |  | 1-day | NCDC | 67.5000 | -148.5000 | 1899 | 6/1963-5/1965 |
| $\bigcirc$ | CHATANIKA | 80-0460 |  |  | 1-hour | RAWS | 65.0191 | -148.5800 | 1450 | 5/1990-12/2010 |
|  | CHENA HOT SPRINGS | 50-1574 |  |  | 1-day | NCDC | 65.0500 | -146.0500 | 1201 | 8/1962-7/2010 |
|  | CHICKEN | 50-1684 |  |  | 1-day | NCDC | 64.1000 | -141.9167 | 1799 | 5/1911-7/2010 |
|  | CHICKEN | 80-0480 |  | 50-1684 | 1-hour | RAWS | 64.0857 | -141.8775 | 2859 | 9/1998-12/2010 |
|  | CHINIAK | 50-1763 |  |  | 1-day | NCDC | 57.6167 | -152.3667 | 157 | 8/1928-12/2000 |
|  | CHISANA | 80-0540 |  |  | 1-hour | RAWS | 62.1333 | -142.0833 | 3318 | 7/1988-12/2010 |
|  | CHISTOCHIN | 80-0560 |  |  | 1-hour | RAWS | 62.5682 | -144.6538 | 1800 | 6/2001-12/2010 |
|  | CHITINA | 50-1824 |  |  | 1-day | NCDC | 61.5167 | -144.4333 | 600 | 3/1917-12/2010 |
|  | CHITNA | 80-0600 |  | 50-1824 | 1-hour | RAWS | 61.5153 | -144.4380 | 594 | 10/1998-12/2010 |
|  | CHULITNA RIVER | 50-1926 |  |  | 1-day | NCDC | 62.8333 | -149.9167 | 1350 | 1/1971-7/2010 |
|  | CIRCLE CITY | 50-1977 |  |  | 1-day | NCDC | 65.8333 | -144.0667 | 598 | 7/1900-10/1999 |
|  | CIRCLE HOT SPRINGS | 50-1987 |  |  | 1-day | NCDC | 65.4833 | -144.6000 | 935 | 7/1935-7/2010 |
|  | CLEAR 4 N | 50-2005 |  |  | 1-day | NCDC | 64.3500 | -149.0500 | 495 | 12/1965-11/2001 |
|  | CLEARWATER | 50-2019 | 50-2350 |  | 1-day | NCDC | 64.0500 | -145.5167 | 1100 | 10/1964-8/1994 |
|  | COLD BAY AP | 50-2102 |  |  | 1-day | NCDC | 55.2167 | -162.7333 | 78 | 6/1942-8/2010 |
|  | COLDFOOT | 50-2104 | 10-0958 |  | 1-day | NCDC | 67.2500 | -150.1833 | 1050 | 9/1993-4/2000 |
|  | COLDFOOT | 10-0958 |  |  | 1-day | SNOTEL | 67.2531 | -150.1836 | 1040 | 10/1970-9/2010 |
|  | COLDFOOT CAMP | 50-2103 | 50-2104 |  | 1-day | NCDC | 67.2667 | -150.2333 | 1102 | 10/1970-5/1977 |
|  | COLLEGE 5 NW | 50-2112 |  |  | 1-day | NCDC | 64.9333 | -147.8833 | 950 | 8/1976-7/2010 |
|  | COLLEGE OBSY | 50-2107 |  |  | 1-day | NCDC | 64.8667 | -147.8333 | 621 | 5/1948-7/2010 |
| D | COLVILLE VILLAGE | 50-2126 |  |  | 1-day | NCDC | 70.4333 | -150.4167 | 5 | 12/1996-7/2010 |


| $\underset{0}{2}$ | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | COOPER LAKE | 10-0959 |  |  | 1-day | SNOTEL | 60.3902 | -149.6935 | 1200 | 10/1981-9/2010 |
| , | COOPER LAKE PROJECT | 50-2144 |  |  | 1-day | NCDC | 60.4000 | -149.6667 | 505 | 7/1959-3/2004 |
| \% | COOPER LANDING KENAI R | 50-2147 |  |  | 1-day | NCDC | 60.5000 | -149.8167 | 419 | 9/1941-12/2010 |
| - | COPPER CTR | 50-2156 |  |  | 1-day | NCDC | 61.9667 | -145.3167 | 1000 | 7/1902-4/1982 |
| - | CORDOVA M K SMITH AP | 50-2177 |  |  | 1-day | NCDC | 60.4833 | -145.4500 | 31 | 5/1909-8/2010 |
| $\stackrel{\square}{0}$ | CORDOVA NORTH | 50-2173 |  |  | 1-day | NCDC | 60.5576 | -145.7528 | 25 | 9/1899-6/2010 |
| $\stackrel{8}{8}$ | COTTONWOOD | 80-0640 |  |  | 1-hour | RAWS | 65.3458 | -155.9361 | 1310 | 6/1991-9/2010 |
| $\stackrel{\rightharpoonup}{2}$ | CRAB BAY | 50-2222 | 50-7738 |  | 1-day | NCDC | 60.0667 | -147.9833 | 69 | 1/1975-4/1979 |
| $\bigcirc$ | CRAIG | 50-2227 |  |  | 1-day | NCDC | 55.4833 | -133.1500 | 13 | 10/1936-7/2010 |
| 0 | CROOKED CREEK | 50-2247 |  |  | 1-day | NCDC | 61.8667 | -158.2500 | 125 | 7/1911-10/1974 |
| N | DELTA 5 NE | 50-2350 |  |  | 1-day | NCDC | 64.0833 | -145.6167 | 1060 | 10/1964-7/2010 |
| $\bigcirc$ | DELTA 6N | 50-2339 |  |  | 1-day | NCDC | 64.1167 | -145.7500 | 1048 | 8/1996-7/2010 |
|  | DELTA JUNCTION 20 SE | 50-2352 |  |  | 1-day | NCDC | 63.9667 | -145.1000 | 1125 | 11/1980-7/2010 |
|  | DILLINGHAM AP | 50-2457 |  |  | 1-day | NCDC | 59.0500 | -158.5167 | 86 | 6/1919-5/2005 |
|  | DRY CREEK | 50-2568 |  |  | 1-day | NCDC | 63.6833 | -144.6000 | 1350 | 8/1996-7/2010 |
|  | DUTCH HARBOR | 50-2586 | 50-2587 |  | 1-day | NCDC | 53.9167 | -166.5000 | 50 | 6/1905-9/1920 |
|  | DUTCH HARBOR | 50-2587 |  |  | 1-day | NCDC | 53.9000 | -166.5333 | 13 | 6/1905-7/2010 |
|  | EAGLE | 50-2607 |  |  | 1-day | NCDC | 64.7833 | -141.2000 | 840 | 11/1901-7/2010 |
|  | EAGLE | 80-0720 |  | 50-2607 | 1-hour | RAWS | 64.7761 | -141.1619 | 880 | 1/1976-12/2010 |
|  | EAGLE | 50-2607 | 80-0720 |  | 1-hour | NCDC | 64.7856 | -141.2036 | 850 | 1/1976-6/2008 |
|  | EIELSON FLD | 50-2707 |  |  | 1-day | NCDC | 64.6667 | -147.1000 | 547 | 10/1946-7/2010 |
|  | EKLUTNA | 50-2717 | 50-5883 |  | 1-day | NCDC | 61.4657 | -149.3410 | 30 | 5/1941-2/1955 |
|  | EKLUTNA LAKE | 50-2725 |  |  | 1-day | NCDC | 61.4033 | -149.1456 | 879 | 6/1946-8/1976 |
|  | EKLUTNA PROJECT | 50-2730 |  |  | 1-day | NCDC | 61.4747 | -149.1728 | 38 | 1/1952-1/1998 |
|  | EKLUTNA WTP | 50-2737 |  |  | 1-day | NCDC | 61.4500 | -149.3167 | 640 | 5/1941-7/2010 |
|  | ELDRED ROCK | 50-2770 |  |  | 1-day | NCDC | 58.9715 | -135.2212 | 52 | 3/1941-7/1973 |
|  | ELFIN COVE | 50-2785 |  |  | 1-day | NCDC | 58.1950 | -136.3528 | 20 | 1/1975-7/2010 |
|  | EMMONAK | 50-2825 |  |  | 1-day | NCDC | 62.7833 | -164.4833 | 14 | 9/1977-1/1994 |
|  | EUREKA | 50-2952 |  |  | 1-day | NCDC | 61.9500 | -147.1667 | 3342 | 7/1953-9/1968 |
|  | FAIRBANKS F.O. | 10-0215 |  |  | 1-day | SNOTEL | 64.8602 | -147.7889 | 450 | 10/1982-9/2009 |
|  | FAIRBANKS INTL AP | 50-2968 |  |  | 1-day | NCDC | 64.8000 | -147.8833 | 432 | 7/1948-8/2010 |
| > | FAIRBANKS INTL AP | 50-2968 |  |  | 1-hour | NCDC | 64.8039 | -147.8761 | 432 | 9/1949-4/2011 |


| Cost-merge | Co-located <br> station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record <br> station ID |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Station name | $50-2968$ | $50-2968$ |  | $15-\mathrm{min}$ | NCDC | 64.8000 | -147.8833 | 432 | $1 / 2000-4 / 2011$ |
| FAIRBANKS INTL AP | $80-0780$ |  |  | 1 -hour | RAWS | $\mathbf{6 3 . 7 3 6 8}$ | $\mathbf{- 1 5 4 . 1 4 2 0}$ | 775 | $8 / 1996-12 / 2010$ |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | GUARD ISLAND LIGHT STN | 50-3454 |  |  | 1-day | NCDC | 55.4459 | -131.8812 | 20 | 11/1940-6/1969 |
| 1 | GULKANA | 90-0001 |  |  | 1-day | USGS | 63.2667 | -145.4167 | 4856 | 10/1967-9/2009 |
| $\stackrel{\sim}{0}$ | GULKANA AP | 50-3465 |  |  | 1-day | NCDC | 62.1667 | -145.4500 | 1570 | 3/1909-8/2010 |
| $\stackrel{\rightharpoonup}{\square}$ | GUSTAVUS | 50-3475 |  |  | 1-day | NCDC | 58.4167 | -135.7167 | 40 | 4/1923-7/2010 |
| $<$ | HAINES | 50-3495 | 50-3490 |  | 1-day | NCDC | 59.2167 | -135.4333 | 257 | 9/1948-9/1953 |
| O | HAINES 40 NW | 50-3504 |  |  | 1-day | NCDC | 59.4500 | -136.3667 | 820 | 6/1927-7/2010 |
| $\stackrel{\rightharpoonup}{8}$ | HAINES AP | 50-3490 |  |  | 1-day | NCDC | 59.2500 | -135.5167 | 31 | 1/1882-8/2010 |
| $\checkmark$ | HAINES TERMINAL | 50-3500 |  |  | 1-day | NCDC | 59.2667 | -135.4500 | 175 | 9/1957-7/1988 |
| 8 | HALIBUT COVE | 50-3530 |  |  | 1-day | NCDC | 59.5972 | -151.2314 | 30 | 9/1975-1/1998 |
| 0. | HAYCOCK | 80-1020 |  |  | 1-hour | RAWS | 65.2017 | -161.1550 | 177 | 5/1988-11/2010 |
| $\cdots$ | HAYES RIVER | 50-3573 |  |  | 1-day | NCDC | 61.9833 | -152.0833 | 1000 | 11/1980-7/2010 |
| $\bigcirc$ | HEALY | 50-3581 | 50-3585 |  | 1-day | NCDC | 63.8500 | -148.9500 | 1244 | 2/1920-4/1973 |
|  | HEALY 2 NW | 50-3585 |  |  | 1-day | NCDC | 63.8833 | -149.0167 | 1490 | 2/1920-7/2010 |
|  | HELMUT | 80-1060 |  |  | 1-hour | RAWS | 67.7465 | -144.1640 | 2800 | 9/1988-9/2010 |
|  | HIDDEN FALLS HATCHERY | 50-3605 |  |  | 1-day | NCDC | 57.2167 | -134.8667 | 22 | 10/1992-7/2010 |
|  | HODZANA | 80-1100 |  |  | 1-hour | RAWS | 66.7417 | -148.6767 | 1075 | 6/1991-12/2010 |
|  | HOGATZA | 80-1120 |  |  | 1-hour | RAWS | 66.2167 | -155.6667 | 685 | 5/1988-12/2010 |
|  | HOLY CROSS | 50-3655 |  |  | 1-day | NCDC | 62.1833 | -159.7667 | 20 | 4/1892-5/1975 |
|  | HOMER | 80-1140 |  |  | 1-hour | RAWS | 59.7458 | -151.2083 | 715 | 5/1998-12/2010 |
|  | HOMER 5 NW | 50-3670 | 50-9144 |  | 1-day | NCDC | 59.6833 | -151.6333 | 1132 | 3/1952-8/1973 |
|  | HOMER 8 NW | 50-3672 |  |  | 1-day | NCDC | 59.7460 | -151.6375 | 1080 | 10/1977-7/2010 |
|  | HOMER 9 E | 50-3682 |  |  | 1-day | NCDC | 59.7167 | -151.3333 | 512 | 10/1973-7/2010 |
|  | HOMER AP | 50-3665 |  |  | 1-day | NCDC | 59.6500 | -151.4833 | 64 | 9/1932-8/2010 |
|  | HOMER RSCH CTR | 50-3680 | 50-3682 |  | 1-day | NCDC | 59.7000 | -151.3167 | 279 | 10/1973-1/1979 |
|  | HOONAH | 50-3695 |  |  | 1-day | NCDC | 58.1167 | -135.4500 | 40 | 5/1941-7/2010 |
|  | HOONAH | 80-1180 |  |  | 1-hour | RAWS | 57.7867 | -135.1665 | 450 | 9/1989-12/2010 |
|  | HOPE | 50-3720 |  |  | 1-day | NCDC | 60.9000 | -149.6333 | 180 | 3/1979-7/2010 |
|  | HUGHES | 50-3765 |  |  | 1-day | NCDC | 66.0667 | -154.2333 | 545 | 3/1941-1/1970 |
|  | ILIAMNA AP | 50-3905 |  |  | 1-day | NCDC | 59.7500 | -154.9000 | 183 | 3/1920-8/2010 |
|  | IMNAVIAT BASIN A | 40-1100 | 40-1110 |  | 1-hour | WERC | 68.6100 | -149.3036 | 3048 | 5/1985-12/1993 |
|  | IMNAVIAT BASIN B | 40-1110 |  | 10-0968 | 1-hour | WERC | 68.6163 | -149.3036 | 3048 | 5/1985-1/2010 |
| D | IMNAVIAT CREEK | 10-0968 |  |  | 1-day | SNOTEL | 68.6169 | -149.3003 | 3050 | 10/1980-9/2010 |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | $\begin{array}{c\|} \hline \text { Base } \\ \text { duration } \end{array}$ | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | INDIAN MTN | 50-3910 |  |  | 1-day | NCDC | 65.9833 | -153.6833 | 1220 | 8/1966-1/1985 |
| - | INDIAN PASS | 10-0946 |  |  | 1-day | SNOTEL | 61.0677 | -149.4795 | 2350 | 10/1979-9/2010 |
| $\stackrel{\sim}{\circ}$ | INNOKO | 80-1220 |  |  | 1-hour | RAWS | 63.3817 | -158.8220 | 930 | 3/1988-12/2010 |
| - | INTRICATE BAY | 50-3933 |  |  | 1-day | NCDC | 59.5500 | -154.5000 | 120 | 8/1959-7/2006 |
| $<$ | JATAHMUND | 80-1240 |  |  | 1-hour | RAWS | 62.6000 | -142.0833 | 2300 | 7/1990-12/2010 |
| ) | JUNEAU 9 NW | 50-4110 | 50-4103 |  | 1-day | NCDC | 58.4167 | -134.5333 | 121 | 7/1965-6/1980 |
| $\stackrel{\rightharpoonup}{8}$ | JUNEAU AP | 50-4100 |  |  | 1-hour | NCDC | 58.3567 | -134.5638 | 3 | 9/1949-5/2011 |
| $\stackrel{\rightharpoonup}{<}$ | JUNEAU DWTN | 50-4092 | 50-4094 |  | 1-day | NCDC | 58.3021 | -134.4196 | 171 | 1/1890-6/1965 |
| $\bigcirc$ | JUNEAU DWTN | 50-4094 |  |  | 1-day | NCDC | 58.3000 | -134.4167 | 25 | 1/1890-7/2010 |
| 0 | JUNEAU FORECAST OFFICE | 50-4103 |  |  | 1-day | NCDC | 58.4000 | -134.5667 | 106 | 7/1939-7/2010 |
| N | JUNEAU INTL AP | 50-4100 |  |  | 1-day | NCDC | 58.3500 | -134.5833 | 12 | 9/1936-8/2010 |
| $\bigcirc$ | KAIYUH | 80-1280 |  |  | 1-hour | RAWS | 64.4256 | -158.1058 | 110 | 8/1997-10/2010 |
|  | KAKE | 50-4155 |  |  | 1-day | NCDC | 56.9667 | -133.9000 | 70 | 5/1919-4/1992 |
|  | KAKE | 80-1300 |  |  | 1-hour | RAWS | 56.9739 | -133.6600 | 400 | 9/1989-12/2010 |
|  | KALSIN BAY | 50-4161 | 50-1763 |  | 1-day | NCDC | 57.5667 | -152.4500 | 20 | 8/1928-6/1931 |
|  | KANUTI | 80-1320 |  |  | 1-hour | RAWS | 66.0933 | -152.1700 | 825 | 8/1990-12/2010 |
|  | KASILOF 3 NW | 50-4425 |  |  | 1-day | NCDC | 60.3699 | -151.3669 | 70 | 11/1925-10/1997 |
|  | KAVET | 80-1340 |  |  | 1-hour | RAWS | 67.1386 | -159.0436 | 235 | 5/1993-12/2010 |
|  | KELLY | 80-1360 |  |  | 1-hour | RAWS | 67.9333 | -162.3000 | 412 | 4/1990-12/2010 |
|  | KENAI 9N | 50-4550 |  |  | 1-day | NCDC | 60.6667 | -151.3167 | 126 | 6/1967-4/2007 |
|  | KENAI LAKE | 80-1380 |  |  | 1-hour | RAWS | 60.3628 | -149.3864 | 475 | 9/1989-12/2010 |
|  | KENAI MOOSE PENS | 10-0966 |  |  | 1-day | SNOTEL | 60.7261 | -150.4756 | 300 | 10/1983-9/2010 |
|  | KENAI MUNI AP | 50-4546 |  |  | 1-day | NCDC | 60.5833 | -151.2333 | 91 | 5/1899-8/2010 |
|  | KENAI NWR | 80-1400 |  |  | 1-hour | RAWS | 60.5917 | -150.3167 | 400 | 6/1988-12/2010 |
|  | KENNECOTT | 50-4555 |  |  | 1-day | NCDC | 61.4833 | -142.8833 | 2210 | 12/1916-8/1947 |
|  | KETCHIKAN INTL AP | 50-4590 |  |  | 1-day | NCDC | 55.3500 | -131.7167 | 76 | 9/1910-8/2010 |
|  | KETCHIKAN INTL AP | 50-4590 | 55-0073 | 55-0073 | 15-min | NCDC | 55.3500 | -131.7167 | 76 | 2/2005-4/2011 |
|  | KEYSTONE RIDGE | 50-4621 |  |  | 1-day | NCDC | 64.9167 | -148.2667 | 1600 | 8/1996-7/2010 |
|  | KIANA | 80-1420 |  |  | 1-hour | RAWS | 66.9767 | -160.4375 | 150 | 4/1988-12/2010 |
|  | KILBUCK | 80-1440 |  |  | 1-hour | RAWS | 60.3404 | -160.1600 | 1910 | 1/1992-12/2010 |
|  | KILLISNOO | 50-4689 | 50-0310 |  | 1-day | NCDC | 57.4694 | -134.5694 | 20 | 1/1893-2/1932 |
| > | KING SALMON AP | 50-4766 |  |  | 1-day | NCDC | 58.6833 | -156.6500 | 47 | 6/1917-7/2010 |


| Cost-merge | Co-located <br> station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record <br> station ID | Station name |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| KITOI BAY | $50-4812$ |  |  | 1 -day | NCDC | 58.1833 | -152.3667 | 60 | $11 / 1954-7 / 2010$ |


| $\underset{O}{Z}$ | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MATANUSKA VALLEY 9 | 50-5728 | 50-6875 |  | 1-day | NCDC | 61.6500 | -149.2000 | 420 | 7/1941-10/1954 |
| $\stackrel{ }{ }$ | MAY CREEK | 50-5810 |  |  | 1-day | NCDC | 61.3500 | -142.6833 | 1503 | 11/1963-12/2010 |
| \% | MAY CREEK | 80-1600 |  | 50-5810 | 1-hour | RAWS | 61.3424 | -142.6922 | 1600 | 5/1990-12/2010 |
| ゅ | MC CARTHY 1 NE | 50-5752 | 50-5754 |  | 1-day | NCDC | 61.4333 | -142.9167 | 1601 | 11/1919-9/1976 |
| $<$ | MC CARTHY 1 NE | 50-5754 | 50-5757 |  | 1-day | NCDC | 61.4333 | -142.9000 | 1540 | 10/1976-2/1983 |
| E | MCCARTHY 3 SW | 50-5757 |  |  | 1-day | NCDC | 61.4167 | -143.0000 | 1250 | 11/1919-7/2010 |
| $\stackrel{\rightharpoonup}{\circ}$ | MCGRATH AP | 50-5769 |  |  | 1-day | NCDC | 62.9500 | -155.6000 | 333 | 4/1939-8/2010 |
| $\stackrel{\rightharpoonup}{2}$ | MCGRATH AP | 50-5769 |  |  | 1-hour | NCDC | 62.9575 | -155.6102 | 333 | 7/1950-4/2010 |
| $\bigcirc$ | MCKINLEY PARK | 50-5778 |  |  | 1-day | NCDC | 63.7167 | -148.9667 | 2069 | 1/1923-7/2010 |
| 0. | MCNEIL CANYON | 10-1003 |  |  | 1-day | SNOTEL | 59.7452 | -151.2598 | 1320 | 10/1986-9/2010 |
| N | MENDENHALL | 50-5851 | 50-4110 |  | 1-day | NCDC | 58.4000 | -134.5333 | 89 | 7/1939-4/1944 |
| $\bigcirc$ | METLAKATLA | 50-5853 | 50-0352 |  | 1-day | NCDC | 55.0833 | -131.5667 | -999 | 1/1893-7/1894 |
|  | MIDDLE FORK BRADLEY | 10-1064 |  |  | 1-day | SNOTEL | 59.7595 | -150.7637 | 2300 | 10/1990-9/2010 |
|  | MILE 39 STEESE | 50-5873 | 50-5880 |  | 1-day | NCDC | 65.1833 | -147.2500 | 750 | 2/1998-3/2000 |
|  | MILE 41 STEESE | 50-5879 | 50-5880 |  | 1-day | NCDC | 65.2000 | -147.2000 | 879 | 9/1972-4/1977 |
|  | MILE 42 STEESE | 50-5880 |  |  | 1-day | NCDC | 65.2167 | -147.1667 | 1000 | 9/1972-7/2010 |
|  | MINCHUMINA | 50-5366 | 50-5881 |  | 1-day | NCDC | 63.8833 | -152.2833 | 702 | 1/1945-5/1967 |
|  | MINCHUMINA | 50-5881 |  |  | 1-day | NCDC | 63.9067 | -152.2975 | 1025 | 1/1945-12/2010 |
|  | MINERAL LAKES | 50-5882 |  |  | 1-day | NCDC | 62.9500 | -143.3833 | 2098 | 8/1996-1/2011 |
|  | MIRROR LAKE SCOUT CAMP | 50-5883 | 50-2737 |  | 1-day | NCDC | 61.4333 | -149.4000 | 405 | 11/1985-4/2004 |
|  | MONAHAN FLAT | 10-1094 |  |  | 1-day | SNOTEL | 63.3050 | -147.6489 | 2710 | 10/1983-9/2010 |
|  | MONUMENT CREEK | 10-0949 |  |  | 1-day | SNOTEL | 65.0775 | -145.8736 | 1850 | 10/1980-9/2010 |
|  | MONUMENT CREEK | 10-0949 |  |  | 1-hour | SNOTEL | 65.0775 | -145.8736 | 1850 | 7/1991-7/2009 |
|  | MOOSE PASS 3 NW | 50-5894 |  |  | 1-day | NCDC | 60.5000 | -149.4333 | 463 | 7/1941-10/2004 |
|  | MOOSE RUN | 50-5896 | 50-6769 |  | 1-day | NCDC | 61.2500 | -149.6667 | 394 | 1/1965-1/1971 |
|  | MOOSE VALLEY | 50-5898 |  |  | 1-day | NCDC | 59.4050 | -135.8923 | 400 | 1/1908-3/1958 |
|  | MOSES POINT | 50-6058 |  |  | 1-day | NCDC | 64.7000 | -162.0500 | 20 | 3/1943-7/1967 |
|  | MT. RYAN | 10-0948 |  |  | 1-day | SNOTEL | 65.2506 | -146.1524 | 2800 | 10/1981-9/2010 |
|  | MUNSON RIDGE | 10-0950 |  |  | 1-day | SNOTEL | 64.8517 | -146.2122 | 3100 | 10/1980-9/2010 |
|  | MUNSON RIDGE | 10-0950 |  |  | 1-hour | SNOTEL | 64.8517 | -146.2122 | 3100 | 7/1992-5/2010 |
|  | NABESNA | 50-6147 |  |  | 1-day | NCDC | 62.4000 | -143.0000 | 2899 | 10/1966-7/2010 |
| > | NAKNEK | 50-6166 | 50-4766 |  | 1-day | NCDC | 58.6833 | -156.6500 | 49 | 6/1917-7/1955 |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | NAKNEK | 50-4766 |  |  | 1-hour | NCDC | 58.6833 | -156.6500 | 49 | 10/1962-4/2010 |
| > | NAPTOWNE | 50-6227 | 50-8727 |  | 1-day | NCDC | 60.5333 | -150.7500 | 249 | 9/1950-9/1954 |
| $\stackrel{\sim}{0}$ | NELCHINA HWY CAMP | 50-6270 |  |  | 1-day | NCDC | 61.9833 | -146.8667 | 2485 | 4/1969-5/1983 |
| $\stackrel{\square}{\square}$ | NENANA MUNI AP | 50-6309 |  |  | 1-day | NCDC | 64.5500 | -149.0667 | 360 | 12/1916-5/2011 |
| $<$ | NIKISKI TERMINAL | 50-6403 | 50-4550 |  | 1-day | NCDC | 60.6833 | -151.3833 | 110 | 6/1967-1/1978 |
| E | NINILCHIK | 50-6441 |  |  | 1-day | NCDC | 60.0500 | -151.6667 | 121 | 10/1940-1/2011 |
| $\stackrel{\rightharpoonup}{8}$ | NINILCHIK | 80-1720 |  | 50-6441 | 1-hour | RAWS | 60.0433 | -151.6656 | 130 | 4/1995-1/2011 |
| $\checkmark$ | NOATAK | 80-1740 |  |  | 1-hour | RAWS | 68.0708 | -158.7042 | 985 | 4/1990-1/2011 |
| 8 | NOME MUNI AP | 50-6496 |  |  | 1-day | NCDC | 64.5167 | -165.4500 | 13 | 8/1900-8/2010 |
| 0. | NOME WSO AP | 50-6496 |  |  | 1-hour | NCDC | 64.5111 | -165.4400 | 13 | 9/1949-4/2010 |
| N | NORTH DUTCH ISLAND CAA | 50-6562 |  |  | 1-day | NCDC | 60.7667 | -147.8000 | 39 | 8/1943-1/1957 |
| $\bigcirc$ | NORTH POLE | 50-6581 |  |  | 1-day | NCDC | 64.7500 | -147.3333 | 475 | 10/1968-7/2010 |
|  | NORTHWAY AP | 50-6586 |  |  | 1-day | NCDC | 62.9667 | -141.9333 | 1712 | 10/1942-8/2010 |
|  | NORUTAK | 80-1760 |  |  | 1-hour | RAWS | 66.8333 | -154.3333 | 800 | 5/1990-11/2010 |
|  | NUKA GLACIER | 10-1037 |  |  | 1-day | SNOTEL | 59.6980 | -150.7117 | 1250 | 10/1985-9/2010 |
|  | NUKA RIVER | 10-1488 | 10-1037 |  | 1-day | SNOTEL | 59.6667 | -150.6833 | 1300 | 10/1985-9/1990 |
|  | NULATO | 50-6656 |  |  | 1-day | NCDC | 64.7272 | -158.0791 | 112 | 8/1917-7/2004 |
|  | NUNIVAK ISLAND | 50-6727 |  |  | 1-day | NCDC | 60.3833 | -166.2000 | 52 | 9/1923-2/1973 |
|  | NYAC | 50-6760 |  |  | 1-day | NCDC | 60.9807 | -159.9974 | 449 | 10/1926-9/1963 |
|  | OIL WELL ROAD E P | 50-6769 | 50-3163 |  | 1-day | NCDC | 61.2333 | -149.7167 | 371 | 11/1967-7/1974 |
|  | ORCA | 50-6844 | 50-2173 |  | 1-day | NCDC | 60.5791 | -145.7165 | 100 | 9/1899-3/1908 |
|  | OUZINKIE | 50-6853 |  |  | 1-day | NCDC | 57.9333 | -152.5000 | 40 | 5/1989-8/2007 |
|  | PAAQ PALMER MUNICIPAL | 55-0112 |  | 50-6870 | 1-hour | ASOS | 61.6000 | -149.0800 | 233 | 1/1973-5/2011 |
|  | PABE BETHEL AIRPORT | 55-0016 | 50-0754 |  | 1-hour | ASOS | 60.7800 | -161.8000 | 151 | 1/1950-5/2011 |
|  | PACV CORDOVA/MILE 13 | 55-0032 |  | 50-2177 | 1-hour | ASOS | 60.5000 | -145.5000 | 43 | 1/1950-5/2011 |
|  | PAEN KENAI MUNICIPAL | 55-0072 |  | 50-4546 | 1-hour | ASOS | 60.5700 | -151.2500 | 95 | 1/1950-5/2011 |
|  | PAFM AMBLER | 55-0004 |  | 50-0249 | 1-hour | ASOS | 67.1000 | -157.8500 | 289 | 2/1988-5/2011 |
|  | PAGY SKAGWAY | 55-0143 |  | 50-8525 | 1-hour | ASOS | 59.4700 | -135.3000 | 16 | 1/1973-5/2011 |
|  | PAHN HAINES BOAT HARBOR | 55-0055 |  | 50-3490 | 1-hour | ASOS | 59.2300 | -135.4300 | 33 | 1/1950-5/2011 |
|  | PAHY HYDABURG SEAPLANE | 55-0064 |  |  | 1-hour | ASOS | 55.2063 | -132.8283 | 0 | 7/1996-5/2011 |
|  | PAIL ILIAMNA ARPT | 55-0066 |  | 50-3905 | 1-hour | ASOS | 59.7500 | -154.9200 | 161 | 1/1998-5/2011 |
| p | PAJN JUNEAU INTL AIRPORT | 55-0068 | 50-4100 |  | 1-hour | ASOS | 58.3700 | -134.5800 | 23 | 1/1950-5/2011 |


| $\underset{O}{Z}$ | Station name | Station ID | Post-merge station ID | Co-located station ID | Base duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PAKT KETCHIKAN INTL ARPT | 55-0073 |  | 50-4590 | 1-hour | ASOS | 55.3500 | -131.7000 | 95 | 12/1996-5/2011 |
| - | PAKW KLAWOCK | 55-0080 |  |  | 1-hour | ASOS | 55.5800 | -133.0800 | 49 | 12/1980-5/2011 |
| \% | PALH LAKE HOOD SEAPLANE | 55-0087 |  |  | 1-hour | ASOS | 61.1800 | -149.9700 | 72 | 1/1994-5/2011 |
| ゅ | PALMER 1 N | 50-6871 | 50-6875 |  | 1-day | NCDC | 61.6167 | -149.1000 | 220 | 11/1954-12/1977 |
| < | PALMER 4 SE | 50-6873 | 50-7352 |  | 1-day | NCDC | 61.5333 | -149.0833 | 102 | 6/1956-9/1960 |
| - | PALMER 5 NW | 50-6875 |  |  | 1-day | NCDC | 61.6500 | -149.2000 | 630 | 7/1941-12/1977 |
| $\stackrel{\sim}{\circ}$ | PALMER JOB CORPS | 50-6870 |  |  | 1-day | NCDC | 61.5926 | -149.1014 | 220 | 11/1948-7/2010 |
| $\stackrel{\rightharpoonup}{2}$ | PAMR MERRILL FIELD | 55-0096 |  |  | 1-hour | ASOS | 61.2200 | -149.8500 | 138 | 1/1950-5/2011 |
| $\bigcirc$ | PAOR NORTHWAY | 55-0110 |  | 50-6586 | 1-hour | ASOS | 62.9700 | -141.9300 | 1722 | 1/2000-5/2011 |
| 0. | PASD SAND POINT | 55-0131 |  | 50-8183 | 1-hour | ASOS | 55.3200 | -160.5200 | 23 | 6/1980-5/2011 |
| N | PASI SITKA/JAPONSKI ARPT | 55-0142 |  | 50-8494 | 1-hour | ASOS | 57.0700 | -135.3500 | 66 | 12/1996-5/2011 |
| $\bigcirc$ | PASO SELDOVIA | 55-0135 |  | 50-8355 | 1-hour | ASOS | 59.4500 | -151.7000 | 33 | 6/1997-5/2011 |
|  | PATA TANANA/CALHOUN MEM | 55-0154 |  | 50-9014 | 1-hour | ASOS | 65.1700 | -152.1000 | 220 | 12/1999-5/2011 |
|  | PATK TALKEETNA | 55-0153 |  | 50-8976 | 1-hour | ASOS | 62.3000 | -150.1000 | 358 | 1/1950-5/2011 |
|  | PAVL KIVALINA AIRPORT | 55-0079 |  |  | 1-hour | ASOS | 67.7300 | -164.5400 | 10 | 8/1998-5/2011 |
|  | PAWD SEWARD | 55-0136 |  | 50-8371 | 1-hour | ASOS | 60.1200 | -149.4500 | 59 | 1/1973-5/2011 |
|  | PAWI WAINWRIGHT AIRPORT | 55-0164 |  |  | 1-hour | ASOS | 70.6200 | -159.8500 | 89 | 8/1957-5/2011 |
|  | PAXSON | 50-7095 | 50-7097 |  | 1-day | NCDC | 63.0321 | -145.4975 | 2696 | 8/1917-12/1967 |
|  | PAXSON | 50-7097 |  |  | 1-day | NCDC | 63.0333 | -145.5000 | 2699 | 8/1917-1/2010 |
|  | PAXSON | 80-1820 |  | 50-7105 | 1-hour | RAWS | 62.9453 | -145.5014 | 2670 | 8/1996-1/2011 |
|  | PAXSON RIVER | 50-7105 |  |  | 1-day | NCDC | 62.9500 | -145.5000 | 2752 | 10/1968-1/2011 |
|  | PELICAN | 50-7141 |  |  | 1-day | NCDC | 57.9568 | -136.2220 | 12 | 2/1967-7/2010 |
|  | PETERSBURG | 50-7233 | 50-7251 |  | 1-day | NCDC | 56.8128 | -132.9539 | 52 | 5/1924-8/1983 |
|  | PETERSBURG 1 | 50-7251 |  |  | 1-day | NCDC | 56.8000 | -132.9500 | 107 | 5/1924-7/2010 |
|  | PLANT MATERIALS CTR | 50-7352 |  |  | 1-day | NCDC | 61.5333 | -149.0833 | 67 | 8/1941-1/1994 |
|  | PLATINUM | 50-7365 |  |  | 1-day | NCDC | 59.0167 | -161.7833 | 20 | 10/1939-6/1964 |
|  | POINT HOPE | 50-7431 |  |  | 1-day | NCDC | 68.3500 | -166.8000 | 10 | 3/1924-2/1982 |
|  | POINT LAY | 50-7442 |  |  | 1-day | NCDC | 69.7500 | -163.0500 | 13 | 9/1941-3/1958 |
|  | POINT MACKENZIE | 50-7444 | 10-1002 |  | 1-day | NCDC | 61.4167 | -150.0833 | 160 | 12/1980-10/2008 |
|  | POINT MACKENZIE | 10-1002 |  |  | 1-day | SNOTEL | 61.3897 | -150.0218 | 200 | 10/1983-9/2010 |
|  | POINT RETREAT | 50-7451 |  |  | 1-day | NCDC | 58.4114 | -134.9550 | 20 | 2/1945-7/1973 |
| > | POORMAN | 80-1900 |  |  | 1-hour | RAWS | 64.0847 | -155.5680 | 930 | 6/1988-1/2011 |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | PORCUPINE CREEK | 50-7465 | 50-5506 |  | 1-day | NCDC | 59.3677 | -136.2885 | 1601 | 6/1927-9/1936 |
| $\stackrel{ }{ }$ | PORT ALEXANDER | 50-7557 |  |  | 1-day | NCDC | 56.2500 | -134.6500 | 12 | 9/1949-7/2010 |
| \% | PORT ALSWO | 80-1920 |  | 50-7570 | 1-hour | RAWS | 60.1958 | -154.3200 | 260 | 6/1992-1/2011 |
| $\stackrel{\rightharpoonup}{\square}$ | PORT ALSWORTH | 50-7570 |  |  | 1-day | NCDC | 60.2000 | -154.3167 | 260 | 4/1940-1/2011 |
| $<$ | PORT HEIDEN | 50-7700 |  |  | 1-day | NCDC | 56.9500 | -158.6167 | 92 | 10/1942-10/1988 |
| - | PORT SAN JUAN | 50-7738 |  |  | 1-day | NCDC | 60.0500 | -148.0667 | 40 | 1/1975-7/2010 |
| $\stackrel{\sim}{\circ}$ | PORTAGE | 50-7486 | 50-7494 |  | 1-day | NCDC | 60.8500 | -148.9833 | 39 | 6/1936-10/1949 |
| $\checkmark$ | PORTAGE 1 S | 50-7494 |  |  | 1-day | NCDC | 60.8167 | -148.9833 | 40 | 6/1936-2/1995 |
| 9 | PREACHER | 80-1940 |  |  | 1-hour | RAWS | 65.9233 | -145.0300 | 1038 | 8/1993-1/2011 |
| \%. | PROSPECT CREEK | 50-7778 | 10-0962 |  | 1-day | NCDC | 66.8167 | -150.6667 | 955 | 10/1970-4/2001 |
| N | PUNTILLA | 50-7783 |  |  | 1-day | NCDC | 62.0833 | -152.7333 | 1832 | 1/1942-7/2010 |
| $\bigcirc$ | QUARTZ CRE | 80-1980 |  |  | 1-hour | RAWS | 65.4000 | -164.6500 | 427 | 5/1988-1/2011 |
|  | RABBIT CRE | 80-2000 |  |  | 1-hour | RAWS | 61.0844 | -149.7283 | 1480 | 5/1993-1/2011 |
|  | RADIOVILLE | 50-7854 |  |  | 1-day | NCDC | 57.6000 | -136.1500 | 20 | 5/1936-10/1950 |
|  | RAMPART | 50-7891 | 50-7900 |  | 1-day | NCDC | 65.5000 | -150.2500 | 381 | 6/1905-8/1933 |
|  | RAMPART 2 | 50-7900 |  |  | 1-day | NCDC | 65.5000 | -150.1333 | 400 | 6/1905-7/1977 |
|  | RENEE | 80-2040 |  |  | 1-hour | RAWS | 62.7100 | -146.6181 | 2600 | 6/1999-1/2011 |
|  | RHOADS CREEK | 10-0236 |  |  | 1-day | SNOTEL | 63.9333 | -145.3333 | 1225 | 10/1987-9/2009 |
|  | RICHARDSON | 50-7977 |  |  | 1-day | NCDC | 64.2833 | -146.3333 | 889 | 4/1917-7/1971 |
|  | RIKAS LANDING | 50-7989 | 50-9793 |  | 1-day | NCDC | 64.1500 | -145.8500 | 1268 | 6/1969-11/1982 |
|  | ROCK RIDGE DRIVE | 50-8025 |  |  | 1-day | NCDC | 61.1167 | -149.7500 | 840 | 10/1965-10/1980 |
|  | ROUND LAKE | 80-2080 |  |  | 1-hour | RAWS | 64.6847 | -153.9400 | 570 | 8/1992-1/2011 |
|  | RUSSIAN MISSION | 50-8054 |  |  | 1-day | NCDC | 61.7833 | -161.3167 | 50 | 7/1928-10/1987 |
|  | SAGWON | 10-0238 |  |  | 1-day | SNOTEL | 69.4242 | -148.6926 | 1000 | 10/1982-10/2009 |
|  | SAGWON | 40-1410 |  | 10-0238 | 1-hour | WERC | 69.4262 | -148.6909 | 902 | 10/1986-10/2009 |
|  | SALCHA | 50-8140 |  |  | 1-day | NCDC | 64.5000 | -146.9833 | 680 | 9/1975-6/2010 |
|  | SALCHA | 80-2120 |  |  | 1-hour | RAWS | 64.5900 | -146.1400 | 1000 | 12/1996-12/2010 |
|  | SALMON CREEK BEACH | 50-8168 | 50-4092 |  | 1-day | NCDC | 58.3167 | -134.4667 | -999 | 1/1917-7/1921 |
|  | SALMON TROUT | 80-2140 |  |  | 1-hour | RAWS | 66.8125 | -141.6200 | 2210 | 7/1988-1/2011 |
|  | SAND POINT | 50-8183 |  |  | 1-day | NCDC | 55.3167 | -160.5167 | 22 | 9/1941-5/2011 |
|  | SELAWIK | 80-2160 |  |  | 1-hour | RAWS | 66.6033 | -159.1125 | 105 | 6/1991-1/2011 |
| > | SELDOVIA | 50-8350 | 50-8355 |  | 1-day | NCDC | 59.4333 | -151.7000 | 20 | 1/1918-6/1964 |


| Z | Station name | Station ID | Post-merge station ID | Co-located station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | SELDOVIA DOCK | 50-8355 |  |  | 1-day | NCDC | 59.4333 | -151.7000 | 30 | 1/1918-5/2011 |
| $\stackrel{ }{ }$ | SEVEN MILE | 80-2180 |  | 50-3082 | 1-hour | RAWS | 65.9383 | -149.8550 | 823 | 3/1988-1/2011 |
| $\stackrel{\sim}{0}$ | SEWARD | 50-8371 |  |  | 1-day | NCDC | 60.1167 | -149.4500 | 30 | 2/1908-9/2008 |
| $\stackrel{\rightharpoonup}{\square}$ | SEWARD 19 N | 50-8377 |  |  | 1-day | NCDC | 60.3500 | -149.3500 | 454 | 11/1986-7/2010 |
| $<$ | SEWARD 8 NW | 50-8375 |  |  | 1-day | NCDC | 60.1833 | -149.6333 | 410 | 7/1983-3/2010 |
| - | SHEEP MTN | 50-8407 | 50-8945 |  | 1-day | NCDC | 61.8000 | -147.6833 | 2279 | 7/1943-5/1966 |
| $\stackrel{\sim}{\circ}$ | SHEEP MTN LODGE | 50-8409 |  |  | 1-day | NCDC | 61.8167 | -147.5000 | 2799 | 7/1943-7/2010 |
| $\checkmark$ | SHEMYA AFB | 50-8419 |  |  | 1-day | NCDC | 52.7167 | -174.1000 | 122 | 7/1943-3/1995 |
| 9 | SHISHMAREF | 50-8437 |  |  | 1-day | NCDC | 66.2506 | -166.0821 | 10 | 10/1919-10/1973 |
| \%. | SITKA JAPONSKI AP | 50-8494 |  |  | 1-day | NCDC | 57.0500 | -135.3667 | 14 | 9/1944-8/2010 |
| N | SITKA MAGNETIC OBSY | 50-8503 |  |  | 1-day | NCDC | 57.0500 | -135.3333 | 67 | 11/1867-12/1989 |
| - | SITKINAK | 50-8512 |  |  | 1-day | NCDC | 56.5833 | -153.9167 | 20 | 11/1960-1/1981 |
|  | SKAGWAY | 50-8525 |  |  | 1-day | NCDC | 59.4531 | -135.3183 | 35 | 11/1898-8/2010 |
|  | SKAGWAY 1 NW | 50-8532 | 50-8528 |  | 1-day | NCDC | 59.4680 | -135.3193 | 570 | 11/1972-8/1981 |
|  | SKAGWAY AP | 50-8528 | 50-8525 |  | 1-day | NCDC | 59.4667 | -135.3167 | 20 | 7/1965-8/2010 |
|  | SKWENTNA | 50-8536 |  |  | 1-day | NCDC | 61.9667 | -151.1833 | 150 | 7/1939-7/2010 |
|  | SLANA | 50-8547 |  |  | 1-day | NCDC | 62.7167 | -143.9833 | 2191 | 4/1957-11/2007 |
|  | SLANA AP | 50-8550 | 50-8547 |  | 1-day | NCDC | 62.7167 | -143.9167 | 2419 | 7/1974-10/1977 |
|  | SLIDE MTN | 50-8556 | 50-6270 |  | 1-day | NCDC | 61.9833 | -146.7833 | 2450 | 4/1969-10/1976 |
|  | SNETTISHAM | 10-0001 | 50-8584 |  | 1-day | SNOTEL | 58.1356 | -133.7287 | 25 | 10/1995-9/2009 |
|  | SNETTISHAM PWR PLT | 50-8584 |  |  | 1-day | NCDC | 58.1422 | -133.7390 | 20 | 9/1964-7/2010 |
|  | SNOWSHOE LAKE | 50-8594 |  |  | 1-day | NCDC | 62.0333 | -146.6667 | 2299 | 10/1963-7/2010 |
|  | SOLOMAN GULCH | 10-0240 |  |  | 1-day | SNOTEL | 61.0830 | -146.3039 | 30 | 10/1990-9/2008 |
|  | SOURDOUGH 1 N | 50-8625 |  |  | 1-day | NCDC | 62.5333 | -145.5167 | 1959 | 9/1971-9/1996 |
|  | SPARREVOHN | 50-8666 |  |  | 1-day | NCDC | 61.1000 | -155.5500 | 1580 | 5/1953-1/1985 |
|  | ST MARYS | 50-8105 |  |  | 1-day | NCDC | 62.0500 | -163.1667 | 311 | 7/1967-5/2000 |
|  | ST MARYS AP | 50-8107 | 50-8105 |  | 1-day | NCDC | 62.0667 | -163.3000 | 320 | 9/1980-6/1991 |
|  | ST PAUL ISLAND AP | 50-8118 |  |  | 1-day | NCDC | 57.1667 | -170.2167 | 35 | 9/1892-8/2010 |
|  | ST PAUL ISLAND AP | 50-8118 |  |  | 1-hour | NCDC | 57.1594 | -170.2222 | 35 | 10/1949-4/2010 |
|  | STERLING | 50-8727 | 50-3196 |  | 1-day | NCDC | 60.5333 | -150.7500 | 180 | 10/1954-4/1968 |
|  | STONEY | 80-2320 |  |  | 1-hour | RAWS | 61.0639 | -153.8964 | 1250 | 6/1992-1/2011 |
| > | STONEY RIVER | 80-2340 |  |  | 1-hour | RAWS | 61.6467 | -156.4333 | 265 | 9/1990-1/2011 |


| Cost-merge | Co-located <br> station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record <br> station ID |  |  |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Station name | $10-0955$ |  |  |  | 1 -day | SNOTEL | 60.6171 | -149.5314 | 1400 |
| $10 / 1988-9 / 2010$ |  |  |  |  |  |  |  |  |  |
| SUMMIT CREEK | $50-8811$ |  |  | 1 -day | NCDC | 63.3333 | -149.1333 | 2410 | $8 / 1905-10 / 1976$ |


| Cost-merge | Co-located <br> station ID | Base <br> duration | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record <br> station ID |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| Station name | $10-1449$ |  |  | 1 -day | SNOTEL | 60.7805 | -149.1831 | 1880 | $10 / 1982-9 / 2010$ |



| Station name | $\begin{gathered} \hline \text { Station } \\ \text { ID } \\ \hline \end{gathered}$ | $\begin{array}{c}\text { Post-merge } \\ \text { station ID }\end{array}$ | Co-located station ID | Base duration | Source of data | Latitude | Longitude | $\begin{gathered} \hline \begin{array}{c} \text { Elevation } \\ \text { (ft) } \end{array} \\ \hline \hline \end{gathered}$ | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FRASER CAMP | 21-8036 |  |  | 1-day | ENV CANADA | 59.7164 | -135.0450 | 2850 | 8/1980-2/2007 |
| GOOD HOPE LAKE | 21-3245 |  |  | 1-day | ENV CANADA | 59.3000 | -129.2833 | 2524 | 8/1973-6/1986 |
| GRAHAM INLET | 21-3255 |  |  | 1-day | ENV CANADA | 59.6000 | -134.1833 | 2164 | 7/1973-2/2007 |
| GREEN ISLAND | 21-3298 |  |  | 1-day | ENV CANADA | 54.5686 | -130.7083 | 39 | 10/1978-5/2009 |
| HAINES APPS NO 2 | 21-3315 |  |  | 1-day | ENV CANADA | 59.5139 | -136.4750 | 1310 | 2/1956-6/1974 |
| HAINES JUNCTION | 21-0630 |  |  | 1-day | ENV CANADA | 60.7725 | -137.5803 | 1953 | 10/1944-5/2009 |
| ISKUT RANCH | 21-3672 |  |  | 1-day | ENV CANADA | 57.8667 | -130.0167 | 2801 | 6/1976-5/1994 |
| KLONDIKE | 21-0679 |  |  | 1-day | ENV CANADA | 64.4539 | -138.2156 | 3190 | 6/1966-2/2007 |
| KOMAKUK BEACH A | 21-0685 |  |  | 1-day | ENV CANADA | 69.5833 | -140.1833 | 24 | 8/1958-6/1993 |
| LANGARA | 21-4500 |  |  | 1-day | ENV CANADA | 54.2553 | -133.0581 | 133 | 7/1936-6/2009 |
| LANGARA | 21-4500 |  |  | 1-hour | ENV CANADA | 54.2553 | -133.0581 | 133 | 5/1982-7/2006 |
| MASSET AIRPORT | 21-4920 |  |  | 1-day | ENV CANADA | 54.0275 | -132.1253 | 25 | 6/1897-2/2007 |
| MASSET CFS | 21-4945 | 21-4955 |  | 1-day | ENV CANADA | 54.0333 | -132.0667 | 40 | 11/1971-2/1981 |
| MASSET TOW HILL | 21-4955 | 21-4920 |  | 1-day | ENV CANADA | 54.0333 | -131.9667 | 7 | 9/1981-5/1986 |
| MILL BAY | 21-5130 |  |  | 1-day | ENV CANADA | 55.0000 | -129.7500 | 10 | 1/1915-3/1959 |
| MULE CREEK | 21-5248 |  |  | 1-day | ENV CANADA | 59.7833 | -136.6000 | 2899 | 9/1970-10/1986 |
| NAAS HARBOUR | 21-5275 |  |  | 1-day | ENV CANADA | 54.9333 | -129.9333 | 20 | 2/1900-8/1929 |
| NASS CAMP | 21-5384 |  |  | 1-day | ENV CANADA | 55.2375 | -129.0294 | 951 | 1/1924-2/2007 |
| OGILVIE RIVER | 21-0794 |  |  | 1-day | ENV CANADA | 65.3603 | -138.3053 | 1959 | 5/1971-2/2007 |
| OLD CROW A | 21-0800 | 21-0805 |  | 1-day | ENV CANADA | 67.5706 | -139.8392 | 824 | 9/1951-2/2007 |
| OLD CROW RCS | 21-0805 |  |  | 1-day | ENV CANADA | 67.5706 | -139.8392 | 824 | 9/1951-5/2009 |
| PLEASANT CAMP | 21-6197 | 50-3504 |  | 1-day | ENV CANADA | 59.4500 | -136.3667 | 900 | 5/1974-5/2009 |
| PORT SIMPSON | 21-6336 |  |  | 1-day | ENV CANADA | 54.5667 | -130.4333 | 26 | 6/1886-6/1910 |
| PORTER CREEK WAHL | 21-0907 |  |  | 1-day | ENV CANADA | 60.7667 | -135.1167 | 2339 | 11/1989-1/2005 |
| PREMIER | 21-6420 |  |  | 1-day | ENV CANADA | 56.0505 | -130.0219 | 1345 | 1/1926-9/1996 |
| PRINCE RUPERT | 21-6480 | 21-6481 |  | 1-day | ENV CANADA | 54.2833 | -130.3833 | 170 | 8/1908-12/1962 |
| PRINCE RUPERT A | 21-6481 | 21-6483 |  | 1-day | ENV CANADA | 54.2925 | -130.4447 | 116 | 5/1962-3/2006 |
| PRINCE RUPERT A | 21-6481 |  | 21-6483 | 1-hour | ENV CANADA | 54.2925 | -130.4447 | 116 | 10/1969-2/2005 |
| PRINCE RUPERT AWOS | 21-6483 |  |  | 1-day | ENV CANADA | 54.2861 | -130.4447 | 116 | 8/1908-5/2009 |
| PRINCE RUPERT MONT CIRC | 21-6488 |  |  | 1-day | ENV CANADA | 54.3203 | -130.2900 | 197 | 8/1959-5/2009 |
| PRINCE RUPERT R PARK | 21-6492 |  |  | 1-day | ENV CANADA | 54.3000 | -130.3333 | 298 | 8/1959-9/1997 |
| PRINCE RUPERT SHAWATLANS | 21-6493 |  |  | 1-day | ENV CANADA | 54.3333 | -130.2500 | 36 | 7/1966-6/1999 |


| Z | Station name | $\begin{gathered} \hline \text { Station } \\ \text { ID } \\ \hline \end{gathered}$ | Post-merge station ID | Co-located station ID | $\begin{gathered} \hline \text { Base } \\ \text { duration } \end{gathered}$ | Source of data | Latitude | Longitude | Elevation <br> (ft) | Period of record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROCK RIVER | 21-0935 |  |  | 1-hour | ENV CANADA | 66.9811 | -136.2181 | 2398 | 9/1974-12/1988 |
|  | SNAG A | 21-1000 |  |  | 1-day | ENV CANADA | 62.3667 | -140.4000 | 1924 | 8/1943-9/1966 |
| O | STEWART | 21-7740 | 21-7745 |  | 1-day | ENV CANADA | 55.9500 | -129.9833 | 15 | 9/1910-4/1967 |
| ゅ | STEWART A | 21-7742 |  |  | 1-day | ENV CANADA | 55.9361 | -129.9850 | 24 | 9/1910-2/2007 |
| , | STEWART BCHPA | 21-7745 | 21-7742 |  | 1-day | ENV CANADA | 55.9500 | -129.9833 | 40 | 10/1967-5/1976 |
| E | STEWART RIVER | 21-1033 |  |  | 1-day | ENV CANADA | 63.3167 | -139.4333 | 1175 | 4/1976-9/1993 |
| ${ }_{\sigma}$ | SWEDE CREEK | 21-1070 |  |  | 1-day | ENV CANADA | 64.0233 | -139.5623 | 1050 | 7/1918-1/1929 |
| $\nu$ | TELEGRAPH CREEK | 21-8040 |  |  | 1-day | ENV CANADA | 57.9000 | -131.1667 | 600 | 7/1942-9/1999 |
| $\bigcirc$ | TELEGRAPH CREEK | 21-8041 |  |  | 1-day | ENV CANADA | 57.9000 | -131.3333 | 820 | 5/1979-6/2000 |
| $0$ | TELEGRAPH CREEK | 21-8041 |  |  | 1-hour | ENV CANADA | 57.9073 | -131.1640 | 820 | 5/1979-9/1999 |
| N | TODAGIN RANCH | 21-8202 |  |  | 1-day | ENV CANADA | 57.6000 | -130.0667 | 2949 | 8/1973-3/1992 |
| $\bigcirc$ | TODAGIN RANCH | 21-8202 |  |  | 1-hour | ENV CANADA | 57.6000 | -130.0667 | 2949 | 6/1975-10/1991 |
|  | TRIPLE ISLAND | 21-8250 |  |  | 1-day | ENV CANADA | 54.2947 | -130.8803 | 68 | 6/1989-5/2009 |
|  | UNUK RIVER ESKAY CREEK | 21-8535 |  |  | 1-day | ENV CANADA | 56.6525 | -130.4461 | 2909 | 9/1989-2/2007 |
|  | WHITEHORSE | 21-1290 | 21-1300 |  | 1-day | ENV CANADA | 60.7167 | -135.0500 | 2086 | 11/1904-3/1942 |
|  | WHITEHORSE A | 21-1300 |  |  | 1-day | ENV CANADA | 60.7100 | -135.0683 | 2316 | 11/1904-5/2009 |
|  | WHITEHORSE A | 21-1300 |  |  | 1-hour | ENV CANADA | 60.7100 | -135.0683 | 2316 | 5/1960-9/2002 |
|  | WHITEHORSE RIVERDALE | 21-1400 |  |  | 1-day | ENV CANADA | 60.7100 | -135.0272 | 2099 | 9/1969-5/2009 |
|  | WOLF CREEK | 21-1601 | 21-0115 |  | 1-day | ENV CANADA | 60.5000 | -134.9500 | 2499 | 6/1985-5/1989 |

Table A.1.3. List of stations used in the analysis for constrained to unconstrained observation correction factors (see Section 4.5.2) and n-minute scaling factors (see Section 4.6.3) showing station name, state, station ID, source of data, latitude,
longitude, elevation, and period of record.

| Name | Station ID | Source of data | Latitude | Longitude | Elevation (ft) | Period of record |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| ANCHORAGE INTL AP | $50-0280$ | NCDC | 61.1689 | -150.0278 | 132 | $1 / 1973-12 / 2009$ |
| ANCHORAGE LAKE HOOD AP | $50-0277$ | NCDC | 61.1781 | -149.9664 | 90 | $3 / 2005-12 / 2009$ |
| ANNETTE WSO AP | $50-0352$ | NCDC | 55.0389 | -131.5786 | 109 | $1 / 1973-12 / 2009$ |
| BARROW WSO AP | $50-0546$ | NCDC | 71.2833 | -156.7814 | 31 | $1 / 1984-12 / 2009$ |
| BARTER ISLAND WSO AP | $50-0558$ | NCDC | 70.1333 | -143.6333 | 39 | $1 / 1984-1 / 1990$ |
| BETHEL AP | $50-0754$ | NCDC | 60.7850 | -161.8292 | 102 | $1 / 1984-12 / 2009$ |
| BETTLES AP | $50-0761$ | NCDC | 66.9161 | -151.5089 | 642 | $1 / 1984-12 / 2009$ |
| BIG DELTA FAA/AMOS AP | $50-0770$ | NCDC | 63.9950 | -145.7183 | 1268 | $1 / 1984-12 / 2009$ |
| COLD BAY AP | $50-2102$ | NCDC | 55.2208 | -162.7325 | 78 | $1 / 1973-12 / 2009$ |
| CORDOVA AP | $50-2177$ | NCDC | 60.4914 | -145.4511 | 31 | $1 / 1984-12 / 2009$ |
| DEADHORSE | $50-2316$ | NCDC | 70.1917 | -148.4772 | 61 | $3 / 2005-12 / 2009$ |
| FAIRBANKS INTL AP | $50-2968$ | NCDC | 64.8039 | -147.8761 | 432 | $1 / 1973-12 / 2009$ |
| GULKANA AP | $50-3465$ | NCDC | 62.1603 | -145.4569 | 1571 | $1 / 1984-12 / 2009$ |
| HAINES AP | $50-3490$ | NCDC | 59.2433 | -135.5094 | 15 | $2 / 2005-12 / 2009$ |
| HOMER AP | $50-3665$ | NCDC | 59.6428 | -151.4872 | 64 | $1 / 1984-12 / 2009$ |
| ILIAMNA AP | $50-3905$ | NCDC | 59.7539 | -154.9069 | 183 | $2 / 2005-12 / 2009$ |
| JUNEAU AP | $50-4100$ | NCDC | 58.3567 | -134.5639 | -999 | $1 / 1973-12 / 2009$ |
| KENAI AP | $50-4546$ | NCDC | 60.5797 | -151.2392 | 91 | $1 / 1984-12 / 2009$ |
| KETCHIKAN | $50-4590$ | NCDC | 55.3567 | -131.7117 | 76 | $2 / 2005-12 / 2009$ |
| KING SALMON AP | $50-4766$ | NCDC | 58.6828 | -156.6564 | 47 | $1 / 1973-12 / 2009$ |
| KLAWOCK AP | $50-4901$ | NCDC | 55.5800 | -133.0750 | 12 | $3 / 2005-12 / 2009$ |
| KODIAK AP | $50-4988$ | NCDC | 57.7511 | -152.4856 | 19 | $1 / 2000-12 / 2009$ |
| KODIAK NAVY AIR STN | $50-4986$ | NCDC | 57.7500 | -152.5000 | 13 | $1 / 1984-5 / 1997$ |
| KOTZEBUE WSO AP | $50-5076$ | NCDC | 66.8850 | -162.5967 | 10 | $1 / 1984-12 / 2009$ |
| MCGRATH AP | $50-5769$ | NCDC | 62.9575 | -155.6103 | 333 | $1 / 1973-12 / 2009$ |
| NOME WSO AP | $50-6496$ | NCDC | 64.5111 | -165.4400 | 13 | $1 / 1984-12 / 2009$ |
| NORTHWAY AP | $50-6586$ | NCDC | 62.9614 | -141.9292 | 1713 | $1 / 1984-12 / 2009$ |
| PALMER AP | $50-6867$ | $50-8494$ | NCDC | 61.5961 | -149.0917 | 230 |
| NITKA JAPONSKI AP | $50-8528$ | NCDC | 57.0483 | -135.3600 | 14 | $1 / 1984-12 / 20099$ |
| SKAGWAY AP | $50-8118$ | NCDC | 59.4556 | -135.3239 | 20 | $2 / 2005-12 / 2009$ |
| ST PAUL ISLAND AP |  | -170.2222 | 35 | $1 / 1973-12 / 2009$ |  |  |


| Name | Station ID | Source of data | Latitude | Longitude | Elevation (ft) | Period of record |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| TALKEETNA AP | $50-8976$ | NCDC | 62.3200 | -150.0950 | 350 | $1 / 1984-12 / 2009$ |
| TANANA AP | $50-9014$ | NCDC | 65.1744 | -152.1069 | 227 | $1 / 1984-12 / 2009$ |
| UNALAKLEET WSO AP | $50-9564$ | NCDC | 63.8833 | -160.8000 | 18 | $1 / 1984-5 / 1997$ |
| VALDEZ MUNI AP | $50-9685$ | NCDC | 61.1314 | -146.2433 | 105 | $1 / 1984-5 / 1997$ |
| YAKUTAT AP | $50-9941$ | NCDC | 59.5119 | -139.6711 | 33 | $1 / 1973-12 / 2009$ |

# Alaskan Precipitation Bias Corrections 

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Our goal was to make bias corrections for undercatch to all Alaskan precipitation data used in this study, including Canadian precipitation data along the eastern Alaskan border. Because of the sparse data network in Alaska, we used all acceptable precipitation data regardless of the collecting party and gauge type in our frequency estimation. A large majority of the instruments were the standard 8 -inch National Weather Service (NWS) orifice gauge, but not all. Another challenge was determining when during their life span (especially for older stations of long duration) that Alter shields were added to the 8 -inch NWS orifice gauges.

The best designed gauges do not collect $100 \%$ of falling precipitation, and gauges of different designs have different catch efficiencies; for example those of the United States and Canada. It is also clear that gauges where the top of the gauge is flush with the ground, with surrounding vegetation, or with some mechanical device like a wind shield, will catch more precipitation than those lacking such features.

The three most significant reasons for gauge undercatch are surface wetting, evaporation and wind. For precipitation intensity/duration/frequency (IDF) studies, wind is the most important variable to consider. The World Meteorological Organization (WMO) Solid Precipitation Measurement Intercomparison study (Goodison et al., 1998) was initiated at 26 sites in 13 countries in the northern hemisphere winter of 1986/1987. Several other published papers (Yang et al., 1998; Yang et al., 1999; Yang et al., 2000; and others) followed up on this study and reported on related results, such as equations for correcting undercatch of liquid precipitation for the 8 -inch NWS orifice gauge.

The final outcome of the WMO study was a set of equations to correct for the undercatch of daily precipitation for the various gauges used in these 13 countries. As one might expect, there is considerable difference in the design, shape, size, construction materials, wind shield design and orifice height of each gauge type used (Sevruk and Klemm, 1989). All the studied gauges were compared against the Double Fence Intercomparison Reference (DFIR), a shielded Tretyakov gauge at 3 meters in height with an octagonal vertical double-fence shield. It was acknowledged that a gauge situated in a natural bush shelter provided the best estimate of "ground true" precipitation, but since bushes are not available in all climatic regions, an artificial shield was selected. Researchers also conceded that this gauge comes closest to the "true ground precipitation" when compared against other gauges, but the DFIR is still not an ideal gauge and therefore still suffers from undercatch. The equations for undercatch corrections require only one variable, wind; these equations, though, were only derived to correct 24 hour precipitation. All gauges used in the WMO study performed better for rainfall precipitation than for solid precipitation.

Ideally, we would identify the type of gauge used at each station in the Alaskan analysis and make bias corrections based on the results reported in the WMO Report No. 67 (Goodison, et al., 1998) for solid precipitation and in Yang et al. (1998) for liquid precipitation, but a number of discrepancies exist between the WMO methodologies and the historical data available to our study.

Numerous types of precipitation gauges used over the years in Alaska have been identified (8-inch NWS orifice standard rain gauge, Wyoming gauge system, 4 -inch diameter plastic gauge, 12 -inch diameter gauge; in addition, some of these have been fitted at some point with wind or Alter shields). In the WMO study, only national gauges were evaluated; therefore just the 8 -inch orifice gauge and the

Wyoming system were evaluated for the United States. Further complicating the problem was that Canada has its own type of precipitation gauge (AES Type B for rain, Nipher gauge for snow). As indicated earlier, each gauge type has different catch efficiency and clearly the performance is enhanced if the gauge has a wind shield.

In effect, if we had a hypothetical true precipitation event of 1 inch in 24 hours, each measurement gauge would yield a different value, and all would report less than the original 1 inch of precipitation. We planned to make bias corrections to the precipitation data so that each gauge type would report close to the same value, even though all would still report less than the 1 inch hypothetical value since all gauges are imperfect. According to the results of the WMO study (Yang et al., 1998), for a $3 \mathrm{~m} / \mathrm{s}$ wind speed, a standard 8-inch NWS precipitation gauge equipped with an Alter shield will undercatch the amount of liquid precipitation by $8.3 \%$ ( $21.8 \%$ for solid precipitation); for a non-shielded gauge, the undercatch is $11.1 \%$ ( $45.2 \%$ for solid precipitation).

So that the user of this report can grasp the possible magnitude of change at an actual station with an 8 -inch NWS orifice shielded gauge, we calculated undercatch of the annual maximum 24 hour event at Annette, a small village in southeast Alaska, for a 25 year period (1984-2008). The average wind speed for these storms was 20.2 feet $/ \mathrm{sec}(6.2 \mathrm{~meters} / \mathrm{sec})$ and the average undercatch of the annual maximum over this period was estimated to be $15.1 \%$. These annual maximums are rain events that mostly occur in September and October. As this station is near the coast, it is likely to be a windier environment than non-coastal stations; therefore the percentage of undercatch would be greater than for less windy noncoastal areas.

For this study, to make the desired daily bias corrections at each site, we need good historical data on the type of gauge, when a wind shield was added and daily wind data. The plan was to make bias corrections for undercatch at all stations where the collected data is used; clearly, making corrections for a fraction of the stations is not acceptable. However, while we know the type of gauge (with a few exceptions), for most sites we do not know when wind shields were added as very little information on this event is recorded. While information such as moving gauges and installing new gauges were recorded, seldom was it noted when an Alter shield was added to a site. In addition, for many of the remote daily weather stations, we also lack wind data as it is not recorded. Also, a limitation of the WMO study is that the authors only derived equations for correcting daily precipitation, not for other durations (such as hourly). Because of this lack of information and data inconsistency over the whole study period, we were unable to make precipitation gauge undercatch corrections to the precipitation data used in this study.

## References

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## Appendix A. 3 Annual maximum series trend analysis

## 1. Selection of statistical tests for detection of trends in AMS

Precipitation frequency analysis methods used in NOAA Atlas 14 volumes are based on the assumption of stationary climate over the period of observation (and application). To meet the stationarity criterion, the annual maximum series data must be free from trends during the observation period. A number of parametric and non-parametric statistical tests are available for the detection and/or quantification of trends. Selection of an appropriate statistical test requires consideration of the data tested and the limitations of the test.

Annual maximum series (AMS) were first graphed for each station in the project area to examine the time series and to observe general types of trends in the data. Visual inspection of time series plots indicated that there were no abrupt changes or apparent cycles in the AMS, but suggested the possibility of slight trends at some locations. Changes appeared to be gradual and approximately linear.

The null hypothesis that there are no trends in annual maximum series was tested on 1-hour and 1-day AMS data at each station in the project area with at least 40 years of data. The hypothesis was tested at each station separately and for the state as a whole at the level of significance $\alpha=5 \%$. Atstation trends were inspected using the parametric $t$-test and non-parametric Mann-Kendall test (Maidment, 1993). Both tests are extensively used for trend analysis in environmental sciences and are appropriate for records that have undergone a gradual change. The tests are fairly robust, readily available, and easy to use and interpret. Since each test is based on different assumptions and different test statistics, the rationale was that if both tests have similar outcomes there can be more confidence about the results. If the outcomes were different, it would provide an opportunity to investigate reasons for discrepancies.

Parametric tests in general have been shown to be more powerful than non-parametric tests when the data are approximately normally distributed and when the assumption of homoscedasticity (homogeneous variance) holds (Hirsch et al., 1991), but are less reliable when those assumptions do not hold. The parametric $t$-test for trend detection is based on linear regression, and therefore checks only for a linear trend in data. A linear trend assumption seemed adequate here, since, time series plots indicated if any, monotonic, linear changes in AMS. The Pearson correlation coefficient ( $r$ ) was used as a measure of linear association between annual maximum series data and time for the $t$-test. The hypothesis that the data are not dependent on time (and also that they are independent and normally distributed values) was tested using the test statistic $t$ that follows Student's distribution as defined as:

$$
t=\frac{r \sqrt{n-2}}{\sqrt{1-r^{2}}}
$$

where $n$ is the record length of the AMS. The hypothesis is rejected when the absolute value of the computed $t$-statistic is greater than the critical value obtained from Student's distribution with $(n-2)$ degrees of freedom and exceedance probability of $\alpha / 2 \%$, where $\alpha$ is the significance level. The sign of the $t$-statistic defines the direction of the trend, positive or negative.

Non-parametric tests have advantages over parametric tests since they make no assumption of probability distribution and are performed without specifying whether trend is linear or nonlinear. They are also more resilient to outliers in data because they do not operate on data directly. One of the disadvantages of non-parametric tests is that they do not account for the magnitude of the data. The Mann-Kendall test was selected among various non-parametric tests because it can accommodate missing values in a time series, which was a frequent occurrence in the AMS data. The Mann-
NOAA Atlas 14 Volume 7 Version 2.0

Kendall test compares the relative magnitudes of annual maximum data. If annual maximum values are indexed based on time, and $x_{i}$ is the annual maximum value that corresponds to year $t_{i}$, then the Mann-Kendall statistic is given by:

$$
S=\sum_{k=1}^{n-1} \sum_{i=k+1}^{n} \operatorname{sign}\left(x_{i}-x_{k}\right)
$$

The test statistic $Z$ is then computed using a normal approximation and standardization of the statistic $S$. The null hypothesis that there is no trend in the data is rejected at significance level $\alpha$ if the computed $Z$ value is greater, in absolute terms, than the critical value obtained from standard normal distribution that has probability of exceedance of $\alpha / 2 \%$. The sign of the statistic defines the direction of the trend, positive or negative.

In addition to an at-station trend analysis, the relative magnitude of any trend in AMS for the state as a whole was assessed by linear regression techniques. 1-hour and 1-day station-specific AMS for stations with at least 40 years of data were rescaled by corresponding mean annual maximum values and then regressed against time, where time was defined as year of occurrence minus 1900. The regression results from all stations were tested against a null hypothesis of zero serial correlation (zero regression slopes).

## 2. Trend analysis results and conclusion

The null hypothesis that there are no trends in annual maximum series was tested on 1-hour and 1-day AMS data at each station in the project area with at least 40 years of data. For the 1 -hour duration, 12 stations satisfied the record length criterion; for the 1-day duration, the number of stations was 154. The $t$-test and Mann-Kendall test for trends were applied to test the hypothesis. Results from both tests were very similar. Both tests indicated no statistically-significant trends at any station in the 1hour data, and in about $85 \%$ of stations with 1 -day data (details in Table A.3.1). In the 1-day dataset, positive trends were detected in about $8 \%$ of stations, and negative trends in about $7 \%$ of stations. The spatial distribution of the Mann-Kendall and $t$-test trend analysis results for 1-day AMS are shown in Figure A.3.1.

Table A.3.1. Trend analysis results based on $t$-test and Mann-Kendall (M-K) test for 1-hour and 1-day AMS data.

| Number of stations | 1-hour |  | 1-day |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\boldsymbol{t}$-test | M-K test | $\boldsymbol{t}$ t-test | M-K test |
| no trend | 12 | 12 | 130 | 132 |
| positive trend | 0 | 0 | 13 | 13 |
| negative trend | 0 | 0 | 11 | 9 |
| Total | 12 | 12 | 154 | 154 |

Results from the regional trend analysis also indicated that the null hypothesis that there are no trends in AMS in the state of Alaska as a whole could not be rejected at $5 \%$ significance level. Because tests at both the 1-hour and 1-day durations indicated no statistically-significant trends in the data, the assumption of stationary climate was accepted for this project area and no adjustment to AMS data was recommended.


Figure A.2.1. Spatial distribution of Mann-Kendall test and $t$-test trend results for 1-day AMS. Red plus signs indicate locations where the Mann-Kendal test detected positive trends in AMS data and green negative signs indicate locations with negative trends. Similarly, red circles indicate locations where $t$-test indicated positive trends and green circles locations with negative trends.

## Appendix A. 4 List of L-moments ( $\lambda_{1}, \lambda_{2}, \lambda_{3}$ ) for 1-day through 60-day durations

Table A.4.1. $\lambda_{1}$ moments.

| $\begin{gathered} \text { Station } \\ \text { ID } \\ \hline \hline \end{gathered}$ | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10-0208 | 1.327 | 1.614 | 1.870 | 2.069 | 2.456 | 2.747 | 3.646 | 4.435 | 5.542 | 6.605 |
| 10-0215 | 1.106 | 1.323 | 1.517 | 1.669 | 1.959 | 2.182 | 2.914 | 3.583 | 4.495 | 5.290 |
| 10-0236 | 1.229 | 1.540 | 1.811 | 1.989 | 2.231 | 2.405 | 3.147 | 3.915 | 4.991 | 5.889 |
| 10-0238 | 0.768 | 0.923 | 1.062 | 1.171 | 1.385 | 1.548 | 2.091 | 2.587 | 3.231 | 3.730 |
| 10-0240 | 3.085 | 4.018 | 4.879 | 5.618 | 7.381 | 8.737 | 12.118 | 14.783 | 18.409 | 22.015 |
| 10-0241 | 4.498 | 6.170 | 7.713 | 9.036 | 12.111 | 14.626 | 22.100 | 28.679 | 38.116 | 47.578 |
| 10-0946 | 2.528 | 3.099 | 3.624 | 4.072 | 5.111 | 5.931 | 8.182 | 10.058 | 12.692 | 15.337 |
| 10-0947 | 1.535 | 1.844 | 2.125 | 2.355 | 2.848 | 3.234 | 4.408 | 5.442 | 6.833 | 8.051 |
| 10-0948 | 1.270 | 1.613 | 1.921 | 2.164 | 2.642 | 3.009 | 4.208 | 5.298 | 6.709 | 7.808 |
| 10-0949 | 1.363 | 1.824 | 2.236 | 2.556 | 3.177 | 3.639 | 5.054 | 6.283 | 7.981 | 9.572 |
| 10-0950 | 1.634 | 2.125 | 2.561 | 2.890 | 3.491 | 3.934 | 5.335 | 6.572 | 8.338 | 10.088 |
| 10-0951 | 1.095 | 1.360 | 1.603 | 1.805 | 2.247 | 2.606 | 3.756 | 4.809 | 6.207 | 7.355 |
| 10-0952 | 1.446 | 1.821 | 2.162 | 2.438 | 3.023 | 3.470 | 4.761 | 5.857 | 7.350 | 8.735 |
| 10-0955 | 1.949 | 2.368 | 2.753 | 3.078 | 3.827 | 4.407 | 5.964 | 7.243 | 8.936 | 10.466 |
| 10-0956 | 3.966 | 4.926 | 5.797 | 6.508 | 8.017 | 9.194 | 12.791 | 15.961 | 20.207 | 23.883 |
| 10-0957 | 1.318 | 1.651 | 1.959 | 2.223 | 2.830 | 3.330 | 4.882 | 6.284 | 8.170 | 9.779 |
| 10-0958 | 1.227 | 1.540 | 1.816 | 2.019 | 2.368 | 2.628 | 3.571 | 4.471 | 5.661 | 6.592 |
| 10-0959 | 2.818 | 3.541 | 4.189 | 4.691 | 5.669 | 6.393 | 8.548 | 10.389 | 12.963 | 15.468 |
| 10-0961 | 0.677 | 0.801 | 0.911 | 0.995 | 1.155 | 1.273 | 1.644 | 1.971 | 2.427 | 2.859 |
| 10-0962 | 1.266 | 1.576 | 1.850 | 2.052 | 2.399 | 2.656 | 3.547 | 4.373 | 5.530 | 6.579 |
| 10-0964 | 3.289 | 4.309 | 5.239 | 6.009 | 7.713 | 9.010 | 12.656 | 15.721 | 19.343 | 21.847 |
| 10-0966 | 1.299 | 1.527 | 1.745 | 1.950 | 2.533 | 3.004 | 4.035 | 4.810 | 5.814 | 6.769 |
| 10-0967 | 1.939 | 2.304 | 2.644 | 2.942 | 3.672 | 4.262 | 5.876 | 7.232 | 8.997 | 10.505 |
| 10-0968 | 1.299 | 1.506 | 1.695 | 1.853 | 2.200 | 2.488 | 3.475 | 4.421 | 5.714 | 6.798 |
| 10-1002 | 1.342 | 1.599 | 1.839 | 2.050 | 2.576 | 2.997 | 4.079 | 4.955 | 6.166 | 7.380 |
| 10-1003 | 1.772 | 2.094 | 2.390 | 2.640 | 3.211 | 3.667 | 5.005 | 6.167 | 7.717 | 9.062 |
| 10-1037 | 4.120 | 5.744 | 7.201 | 8.347 | 10.606 | 12.332 | 17.979 | 23.112 | 29.515 | 34.098 |
| 10-1064 | 3.219 | 4.128 | 4.947 | 5.604 | 6.952 | 7.992 | 11.314 | 14.304 | 17.965 | 20.501 |
| 10-1094 | 1.170 | 1.491 | 1.784 | 2.027 | 2.555 | 2.972 | 4.240 | 5.358 | 6.867 | 8.192 |
| 10-1291 | 1.255 | 1.553 | 1.812 | 1.988 | 2.243 | 2.427 | 3.157 | 3.884 | 4.916 | 5.827 |
| 10-1444 | 1.053 | 1.271 | 1.464 | 1.608 | 1.860 | 2.054 | 2.770 | 3.468 | 4.464 | 5.371 |
| 10-1449 | 3.333 | 4.250 | 5.086 | 5.781 | 7.319 | 8.512 | 11.887 | 14.736 | 18.603 | 22.185 |
| 10-9909 | 1.210 | 1.562 | 1.882 | 2.141 | 2.687 | 3.115 | 4.461 | 5.668 | 7.304 | 8.731 |
| 21-0115 | 0.836 | 0.990 | 1.128 | 1.237 | 1.456 | 1.623 | 2.132 | 2.576 | 3.211 | 3.843 |
| 21-0160 | 1.208 | 1.523 | 1.803 | 2.012 | 2.377 | 2.662 | 3.770 | 4.888 | 6.438 | 7.727 |
| 21-0163 | 1.394 | 1.704 | 1.980 | 2.186 | 2.547 | 2.824 | 3.848 | 4.848 | 6.259 | 7.511 |
| 21-0182 | 1.092 | 1.312 | 1.508 | 1.653 | 1.904 | 2.100 | 2.859 | 3.624 | 4.688 | 5.577 |
| 21-0200 | 0.889 | 1.009 | 1.118 | 1.206 | 1.385 | 1.526 | 1.993 | 2.424 | 2.995 | 3.456 |
| 21-0330 | 3.184 | 4.305 | 5.328 | 6.178 | 8.044 | 9.525 | 14.004 | 17.949 | 23.397 | 28.435 |
| 21-0402 | 0.839 | 0.996 | 1.138 | 1.252 | 1.479 | 1.659 | 2.288 | 2.887 | 3.702 | 4.381 |
| 21-0446 | 3.757 | 4.894 | 5.933 | 6.798 | 8.699 | 10.218 | 14.892 | 19.057 | 24.758 | 29.878 |
| 21-0468 | 1.241 | 1.432 | 1.609 | 1.761 | 2.114 | 2.409 | 3.346 | 4.206 | 5.371 | 6.364 |
| 21-0560 | 0.967 | 1.120 | 1.258 | 1.370 | 1.607 | 1.792 | 2.365 | 2.875 | 3.588 | 4.258 |
| 21-0630 | 1.137 | 1.309 | 1.462 | 1.578 | 1.792 | 1.949 | 2.439 | 2.867 | 3.476 | 4.075 |
| 21-0679 | 1.031 | 1.213 | 1.381 | 1.524 | 1.857 | 2.132 | 2.986 | 3.758 | 4.847 | 5.877 |
| 21-0685 | 0.686 | 0.814 | 0.928 | 1.017 | 1.193 | 1.328 | 1.756 | 2.141 | 2.661 | 3.115 |
| 21-0794 | 0.994 | 1.170 | 1.330 | 1.462 | 1.745 | 1.971 | 2.670 | 3.294 | 4.182 | 5.044 |
| 21-0805 | 0.921 | 1.087 | 1.234 | 1.343 | 1.536 | 1.684 | 2.241 | 2.788 | 3.540 | 4.164 |
| 21-0907 | 0.842 | 0.972 | 1.091 | 1.187 | 1.383 | 1.543 | 2.110 | 2.661 | 3.457 | 4.208 |
| 21-0935 | 1.261 | 1.436 | 1.597 | 1.733 | 2.036 | 2.282 | 3.027 | 3.687 | 4.640 | 5.600 |
| 21-1000 | 1.237 | 1.448 | 1.638 | 1.790 | 2.091 | 2.332 | 3.182 | 3.997 | 5.104 | 6.014 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-1

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21-1033 | 1.000 | 1.219 | 1.412 | 1.552 | 1.787 | 1.957 | 2.546 | 3.090 | 3.786 | 4.305 |
| 21-1050 | 1.749 | 2.259 | 2.707 | 3.022 | 3.529 | 3.884 | 5.070 | 6.131 | 7.578 | 8.864 |
| 21-1070 | 0.705 | 0.853 | 0.988 | 1.098 | 1.331 | 1.508 | 2.019 | 2.453 | 3.031 | 3.543 |
| 21-1086 | 3.137 | 3.948 | 4.703 | 5.369 | 7.021 | 8.357 | 11.917 | 14.860 | 18.952 | 23.014 |
| 21-1300 | 0.812 | 0.960 | 1.093 | 1.197 | 1.394 | 1.548 | 2.082 | 2.588 | 3.274 | 3.847 |
| 21-1400 | 0.913 | 1.070 | 1.208 | 1.305 | 1.451 | 1.563 | 2.059 | 2.594 | 3.352 | 3.980 |
| 21-1440 | 1.471 | 1.714 | 1.942 | 2.145 | 2.650 | 3.073 | 4.295 | 5.360 | 6.845 | 8.257 |
| 21-2340 | 1.102 | 1.267 | 1.419 | 1.551 | 1.859 | 2.117 | 2.920 | 3.651 | 4.684 | 5.661 |
| 21-3245 | 1.323 | 1.683 | 2.001 | 2.233 | 2.643 | 2.923 | 3.713 | 4.352 | 5.247 | 6.167 |
| 21-3255 | 0.909 | 1.100 | 1.272 | 1.409 | 1.685 | 1.895 | 2.525 | 3.071 | 3.801 | 4.440 |
| 21-3298 | 3.779 | 4.777 | 5.688 | 6.445 | 8.079 | 9.418 | 13.841 | 17.975 | 23.789 | 29.103 |
| 21-3315 | 2.858 | 3.564 | 4.215 | 4.771 | 6.057 | 7.092 | 10.100 | 12.704 | 16.287 | 19.624 |
| 21-3672 | 1.048 | 1.270 | 1.473 | 1.645 | 2.032 | 2.344 | 3.311 | 4.179 | 5.259 | 6.040 |
| 21-4500 | 2.230 | 2.800 | 3.340 | 3.835 | 5.126 | 6.256 | 9.622 | 12.650 | 17.016 | 21.360 |
| 21-4920 | 1.969 | 2.432 | 2.874 | 3.284 | 4.377 | 5.336 | 8.122 | 10.595 | 14.098 | 17.493 |
| 21-5130 | 3.438 | 4.554 | 5.565 | 6.384 | 8.086 | 9.431 | 13.702 | 17.564 | 23.100 | 28.519 |
| 21-5248 | 1.854 | 2.154 | 2.435 | 2.685 | 3.319 | 3.833 | 5.191 | 6.310 | 7.817 | 9.223 |
| 21-5275 | 3.439 | 4.580 | 5.616 | 6.465 | 8.277 | 9.696 | 13.953 | 17.670 | 22.997 | 28.360 |
| 21-5384 | 2.313 | 2.973 | 3.565 | 4.032 | 4.962 | 5.668 | 7.837 | 9.737 | 12.409 | 14.987 |
| 21-6336 | 3.180 | 4.416 | 5.532 | 6.429 | 8.259 | 9.703 | 14.378 | 18.649 | 24.743 | 30.602 |
| 21-6420 | 3.668 | 4.612 | 5.507 | 6.322 | 8.455 | 10.268 | 15.315 | 19.650 | 25.718 | 31.616 |
| 21-6483 | 3.535 | 4.521 | 5.431 | 6.211 | 8.002 | 9.492 | 14.223 | 18.564 | 24.625 | 30.154 |
| 21-6488 | 5.016 | 6.251 | 7.401 | 8.411 | 10.867 | 12.900 | 18.803 | 23.955 | 31.028 | 37.542 |
| 21-6492 | 4.232 | 5.499 | 6.667 | 7.670 | 9.992 | 11.901 | 17.777 | 23.060 | 30.175 | 36.296 |
| 21-6493 | 4.716 | 5.965 | 7.123 | 8.132 | 10.548 | 12.532 | 18.289 | 23.297 | 30.256 | 36.846 |
| 21-7742 | 3.424 | 4.481 | 5.453 | 6.278 | 8.171 | 9.684 | 14.046 | 17.796 | 23.060 | 28.209 |
| 21-8036 | 2.087 | 2.673 | 3.201 | 3.624 | 4.482 | 5.154 | 7.341 | 9.339 | 12.038 | 14.340 |
| 21-8040 | 1.030 | 1.201 | 1.354 | 1.469 | 1.681 | 1.843 | 2.409 | 2.943 | 3.619 | 4.098 |
| 21-8041 | 1.221 | 1.460 | 1.672 | 1.830 | 2.113 | 2.316 | 2.943 | 3.485 | 4.235 | 4.949 |
| 21-8202 | 1.127 | 1.336 | 1.528 | 1.692 | 2.071 | 2.371 | 3.209 | 3.917 | 4.887 | 5.806 |
| 21-8250 | 1.962 | 2.334 | 2.696 | 3.043 | 4.047 | 4.936 | 7.298 | 9.299 | 12.162 | 15.110 |
| 21-8535 | 3.372 | 4.405 | 5.348 | 6.132 | 7.861 | 9.211 | 13.086 | 16.385 | 21.014 | 25.574 |
| 30-1100 | 1.217 | 1.434 | 1.634 | 1.805 | 2.201 | 2.520 | 3.429 | 4.207 | 5.309 | 6.412 |
| 30-1110 | 1.218 | 1.435 | 1.636 | 1.807 | 2.204 | 2.522 | 3.430 | 4.208 | 5.310 | 6.412 |
| 40-1220 | 1.247 | 1.422 | 1.587 | 1.736 | 2.113 | 2.437 | 3.406 | 4.274 | 5.524 | 6.768 |
| 40-1250 | 1.146 | 1.311 | 1.466 | 1.603 | 1.936 | 2.226 | 3.179 | 4.082 | 5.316 | 6.356 |
| 40-1300 | 0.718 | 0.809 | 0.891 | 0.959 | 1.099 | 1.218 | 1.682 | 2.162 | 2.779 | 3.196 |
| 40-1510 | 0.553 | 0.626 | 0.696 | 0.761 | 0.938 | 1.088 | 1.488 | 1.823 | 2.280 | 2.708 |
| 50-0026 | 2.618 | 3.106 | 3.558 | 3.948 | 4.846 | 5.622 | 8.312 | 10.936 | 14.556 | 17.610 |
| 50-0230 | 1.071 | 1.264 | 1.439 | 1.583 | 1.889 | 2.127 | 2.851 | 3.486 | 4.343 | 5.100 |
| 50-0243 | 4.011 | 5.121 | 6.122 | 6.922 | 8.568 | 9.811 | 13.474 | 16.607 | 20.848 | 24.707 |
| 50-0249 | 1.386 | 1.703 | 1.994 | 2.243 | 2.816 | 3.273 | 4.634 | 5.827 | 7.235 | 8.158 |
| 50-0280 | 1.357 | 1.585 | 1.797 | 1.982 | 2.433 | 2.790 | 3.720 | 4.477 | 5.510 | 6.514 |
| 50-0310 | 1.896 | 2.420 | 2.901 | 3.305 | 4.199 | 4.931 | 7.295 | 9.475 | 12.489 | 15.171 |
| 50-0332 | 1.411 | 1.778 | 2.109 | 2.374 | 2.917 | 3.334 | 4.640 | 5.801 | 7.332 | 8.604 |
| 50-0352 | 3.878 | 4.907 | 5.868 | 6.719 | 8.805 | 10.565 | 15.806 | 20.468 | 27.104 | 33.591 |
| 50-0363 | 3.966 | 5.290 | 6.503 | 7.527 | 9.823 | 11.692 | 17.533 | 22.813 | 30.071 | 36.560 |
| 50-0433 | 2.976 | 3.342 | 3.702 | 4.054 | 5.093 | 6.046 | 8.703 | 11.037 | 14.447 | 18.003 |
| 50-0452 | 3.201 | 3.820 | 4.388 | 4.866 | 5.925 | 6.802 | 9.682 | 12.374 | 16.133 | 19.518 |
| 50-0464 | 2.531 | 3.186 | 3.792 | 4.318 | 5.556 | 6.591 | 9.783 | 12.671 | 16.739 | 20.576 |
| 50-0522 | 4.922 | 6.672 | 8.298 | 9.720 | 13.123 | 15.970 | 24.632 | 32.411 | 43.113 | 52.761 |
| 50-0546 | 0.517 | 0.606 | 0.686 | 0.751 | 0.886 | 0.990 | 1.299 | 1.567 | 1.932 | 2.266 |
| 50-0558 | 0.719 | 0.847 | 0.960 | 1.043 | 1.180 | 1.281 | 1.634 | 1.962 | 2.390 | 2.725 |
| 50-0657 | 5.537 | 7.080 | 8.506 | 9.737 | 12.605 | 15.001 | 22.525 | 29.398 | 39.020 | 47.890 |
| 50-0676 | 3.974 | 5.232 | 6.394 | 7.397 | 9.749 | 11.684 | 17.459 | 22.562 | 29.822 | 36.947 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-2

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-0685 | 1.999 | 2.418 | 2.805 | 3.137 | 3.918 | 4.542 | 6.270 | 7.724 | 9.743 | 11.711 |
| 50-0707 | 1.252 | 1.475 | 1.676 | 1.835 | 2.147 | 2.391 | 3.219 | 3.991 | 5.018 | 5.845 |
| 50-0754 | 1.152 | 1.425 | 1.674 | 1.879 | 2.322 | 2.678 | 3.821 | 4.866 | 6.265 | 7.436 |
| 50-0761 | 1.044 | 1.252 | 1.445 | 1.612 | 2.014 | 2.332 | 3.176 | 3.867 | 4.810 | 5.716 |
| 50-0770 | 1.246 | 1.485 | 1.698 | 1.861 | 2.163 | 2.396 | 3.217 | 3.997 | 5.057 | 5.944 |
| 50-0788 | 3.046 | 4.046 | 4.952 | 5.685 | 7.250 | 8.411 | 11.515 | 14.022 | 17.465 | 20.872 |
| 50-0910 | 1.110 | 1.342 | 1.551 | 1.717 | 2.048 | 2.310 | 3.188 | 4.007 | 5.188 | 6.328 |
| 50-1201 | 3.938 | 5.153 | 6.300 | 7.344 | 10.033 | 12.357 | 19.255 | 25.426 | 33.905 | 41.559 |
| 50-1220 | 1.320 | 1.586 | 1.827 | 2.024 | 2.442 | 2.766 | 3.740 | 4.589 | 5.727 | 6.725 |
| 50-1230 | 0.684 | 0.802 | 0.908 | 0.988 | 1.136 | 1.249 | 1.631 | 1.984 | 2.504 | 3.036 |
| 50-1240 | 4.843 | 6.648 | 8.306 | 9.710 | 12.950 | 15.461 | 22.204 | 27.744 | 35.092 | 41.760 |
| 50-1243 | 1.400 | 1.728 | 2.021 | 2.244 | 2.659 | 2.975 | 4.055 | 5.059 | 6.434 | 7.624 |
| 50-1251 | 3.038 | 3.955 | 4.803 | 5.531 | 7.279 | 8.616 | 11.859 | 14.368 | 17.882 | 21.635 |
| 50-1269 | 2.860 | 3.616 | 4.311 | 4.904 | 6.249 | 7.371 | 11.010 | 14.394 | 19.091 | 23.276 |
| 50-1308 | 3.829 | 5.394 | 6.795 | 7.883 | 9.992 | 11.571 | 16.432 | 20.675 | 26.682 | 32.579 |
| 50-1312 | 1.158 | 1.504 | 1.806 | 2.011 | 2.314 | 2.524 | 3.283 | 3.988 | 4.926 | 5.685 |
| 50-1314 | 2.071 | 2.672 | 3.207 | 3.615 | 4.366 | 4.944 | 6.991 | 8.939 | 11.593 | 13.817 |
| 50-1318 | 1.707 | 2.184 | 2.618 | 2.971 | 3.726 | 4.311 | 6.036 | 7.522 | 9.614 | 11.666 |
| 50-1321 | 3.423 | 4.666 | 5.789 | 6.693 | 8.541 | 10.001 | 14.788 | 19.189 | 25.258 | 30.640 |
| 50-1325 | 1.701 | 2.129 | 2.516 | 2.825 | 3.462 | 3.948 | 5.426 | 6.718 | 8.376 | 9.692 |
| 50-1334 | 4.548 | 6.014 | 7.345 | 8.432 | 10.740 | 12.552 | 18.065 | 22.919 | 29.912 | 36.984 |
| 50-1466 | 0.980 | 1.181 | 1.361 | 1.501 | 1.773 | 1.984 | 2.700 | 3.368 | 4.288 | 5.092 |
| 50-1492 | 0.962 | 1.103 | 1.231 | 1.336 | 1.560 | 1.737 | 2.295 | 2.797 | 3.472 | 4.052 |
| 50-1574 | 1.342 | 1.681 | 1.983 | 2.214 | 2.652 | 2.976 | 3.967 | 4.824 | 6.064 | 7.345 |
| 50-1684 | 1.288 | 1.510 | 1.711 | 1.877 | 2.232 | 2.514 | 3.394 | 4.183 | 5.216 | 6.050 |
| 50-1763 | 3.896 | 4.991 | 5.989 | 6.812 | 8.618 | 10.007 | 13.802 | 16.924 | 21.635 | 27.171 |
| 50-1824 | 1.586 | 1.853 | 2.091 | 2.272 | 2.623 | 2.862 | 3.438 | 3.868 | 4.484 | 5.197 |
| 50-1926 | 2.405 | 3.110 | 3.742 | 4.232 | 5.180 | 5.889 | 8.090 | 10.023 | 12.654 | 15.023 |
| 50-1977 | 0.903 | 1.026 | 1.137 | 1.225 | 1.401 | 1.536 | 1.968 | 2.356 | 2.907 | 3.438 |
| 50-1987 | 1.028 | 1.267 | 1.476 | 1.623 | 1.852 | 2.018 | 2.644 | 3.250 | 4.084 | 4.790 |
| 50-2005 | 1.262 | 1.530 | 1.772 | 1.967 | 2.369 | 2.673 | 3.564 | 4.325 | 5.308 | 6.115 |
| 50-2102 | 2.135 | 2.513 | 2.860 | 3.155 | 3.825 | 4.373 | 6.063 | 7.581 | 9.717 | 11.737 |
| 50-2107 | 1.091 | 1.314 | 1.513 | 1.668 | 1.968 | 2.195 | 2.939 | 3.614 | 4.526 | 5.308 |
| 50-2112 | 1.123 | 1.351 | 1.555 | 1.714 | 2.019 | 2.255 | 3.043 | 3.772 | 4.765 | 5.623 |
| 50-2126 | 0.522 | 0.600 | 0.674 | 0.746 | 0.957 | 1.136 | 1.554 | 1.882 | 2.342 | 2.827 |
| 50-2144 | 2.412 | 3.106 | 3.731 | 4.227 | 5.243 | 5.986 | 8.032 | 9.707 | 11.891 | 13.812 |
| 50-2147 | 1.939 | 2.307 | 2.630 | 2.865 | 3.258 | 3.546 | 4.560 | 5.507 | 6.878 | 8.213 |
| 50-2156 | 1.241 | 1.370 | 1.489 | 1.591 | 1.821 | 2.010 | 2.615 | 3.171 | 3.901 | 4.483 |
| 50-2173 | 6.810 | 9.194 | 11.349 | 13.084 | 16.681 | 19.456 | 28.048 | 35.653 | 45.547 | 53.555 |
| 50-2177 | 4.825 | 6.362 | 7.760 | 8.908 | 11.378 | 13.309 | 19.091 | 24.134 | 30.994 | 37.193 |
| 50-2227 | 3.827 | 4.829 | 5.772 | 6.623 | 8.786 | 10.635 | 16.044 | 20.827 | 27.577 | 34.090 |
| 50-2247 | 0.993 | 1.203 | 1.395 | 1.555 | 1.905 | 2.192 | 3.125 | 3.990 | 5.172 | 6.197 |
| 50-2339 | 1.270 | 1.580 | 1.852 | 2.046 | 2.357 | 2.588 | 3.476 | 4.350 | 5.536 | 6.492 |
| 50-2350 | 1.270 | 1.515 | 1.734 | 1.903 | 2.220 | 2.469 | 3.374 | 4.254 | 5.449 | 6.427 |
| 50-2352 | 1.192 | 1.469 | 1.710 | 1.874 | 2.107 | 2.277 | 3.003 | 3.757 | 4.766 | 5.517 |
| 50-2457 | 1.425 | 1.780 | 2.101 | 2.359 | 2.884 | 3.299 | 4.673 | 5.943 | 7.665 | 9.129 |
| 50-2568 | 1.319 | 1.642 | 1.925 | 2.126 | 2.442 | 2.678 | 3.600 | 4.519 | 5.825 | 6.980 |
| 50-2587 | 3.186 | 4.130 | 4.972 | 5.618 | 6.835 | 7.750 | 10.727 | 13.411 | 17.096 | 20.396 |
| 50-2607 | 1.037 | 1.190 | 1.331 | 1.448 | 1.703 | 1.913 | 2.616 | 3.280 | 4.197 | 4.995 |
| 50-2707 | 1.175 | 1.450 | 1.693 | 1.873 | 2.188 | 2.424 | 3.245 | 4.013 | 5.086 | 6.051 |
| 50-2725 | 0.978 | 1.133 | 1.274 | 1.394 | 1.663 | 1.880 | 2.546 | 3.141 | 3.940 | 4.630 |
| 50-2730 | 1.403 | 1.658 | 1.886 | 2.064 | 2.408 | 2.679 | 3.637 | 4.556 | 5.825 | 6.912 |
| 50-2737 | 1.243 | 1.475 | 1.686 | 1.858 | 2.219 | 2.503 | 3.392 | 4.188 | 5.322 | 6.428 |
| 50-2770 | 2.691 | 3.531 | 4.293 | 4.916 | 6.248 | 7.276 | 10.309 | 12.926 | 16.393 | 19.388 |
| 50-2785 | 4.197 | 5.218 | 6.185 | 7.066 | 9.367 | 11.330 | 16.822 | 21.554 | 28.349 | 35.296 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-3

| $\begin{aligned} & \text { Station } \\ & \text { ID } \end{aligned}$ | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-2820 | 1.227 | 1.459 | 1.671 | 1.848 | 2.243 | 2.555 | 3.475 | 4.273 | 5.359 | 6.345 |
| 50-2825 | 1.144 | 1.391 | 1.618 | 1.810 | 2.253 | 2.602 | 3.588 | 4.423 | 5.563 | 6.631 |
| 50-2952 | 1.352 | 1.658 | 1.930 | 2.135 | 2.511 | 2.789 | 3.681 | 4.474 | 5.592 | 6.660 |
| 50-2968 | 1.096 | 1.268 | 1.423 | 1.550 | 1.819 | 2.031 | 2.699 | 3.298 | 4.116 | 4.838 |
| 50-2988 | 1.407 | 1.733 | 2.027 | 2.266 | 2.767 | 3.153 | 4.301 | 5.293 | 6.722 | 8.193 |
| 50-3009 | 1.390 | 1.593 | 1.784 | 1.956 | 2.393 | 2.763 | 3.850 | 4.812 | 6.053 | 7.042 |
| 50-3072 | 2.308 | 2.973 | 3.586 | 4.111 | 5.319 | 6.307 | 9.332 | 12.041 | 15.690 | 18.845 |
| 50-3082 | 0.909 | 0.985 | 1.058 | 1.129 | 1.331 | 1.511 | 2.005 | 2.434 | 3.029 | 3.596 |
| 50-3085 | 1.148 | 1.415 | 1.662 | 1.874 | 2.372 | 2.779 | 4.002 | 5.086 | 6.559 | 7.870 |
| 50-3160 | 1.410 | 1.867 | 2.271 | 2.565 | 3.062 | 3.422 | 4.649 | 5.769 | 7.283 | 8.573 |
| 50-3163 | 1.274 | 1.513 | 1.732 | 1.915 | 2.326 | 2.650 | 3.584 | 4.386 | 5.464 | 6.430 |
| 50-3196 | 1.206 | 1.430 | 1.635 | 1.805 | 2.173 | 2.469 | 3.381 | 4.195 | 5.380 | 6.587 |
| 50-3198 | 2.594 | 3.400 | 4.131 | 4.726 | 5.979 | 6.975 | 10.231 | 13.226 | 17.087 | 20.037 |
| 50-3205 | 1.000 | 1.214 | 1.404 | 1.547 | 1.806 | 2.001 | 2.642 | 3.223 | 4.134 | 5.206 |
| 50-3212 | 1.052 | 1.196 | 1.330 | 1.447 | 1.722 | 1.954 | 2.693 | 3.376 | 4.317 | 5.149 |
| 50-3226 | 1.374 | 1.562 | 1.736 | 1.888 | 2.262 | 2.559 | 3.341 | 3.981 | 4.830 | 5.605 |
| 50-3275 | 1.323 | 1.630 | 1.906 | 2.121 | 2.537 | 2.854 | 3.893 | 4.836 | 6.074 | 7.068 |
| 50-3294 | 2.621 | 3.521 | 4.352 | 5.065 | 6.736 | 8.074 | 11.827 | 15.008 | 19.453 | 23.814 |
| 50-3299 | 1.735 | 2.138 | 2.497 | 2.769 | 3.264 | 3.638 | 4.897 | 6.057 | 7.739 | 9.399 |
| 50-3454 | 2.386 | 3.084 | 3.732 | 4.299 | 5.662 | 6.782 | 9.956 | 12.679 | 16.661 | 20.905 |
| 50-3465 | 1.012 | 1.188 | 1.345 | 1.468 | 1.703 | 1.885 | 2.506 | 3.086 | 3.873 | 4.540 |
| 50-3475 | 2.402 | 3.058 | 3.666 | 4.192 | 5.441 | 6.460 | 9.393 | 11.926 | 15.507 | 19.047 |
| 50-3490 | 2.891 | 3.753 | 4.539 | 5.193 | 6.639 | 7.763 | 10.946 | 13.634 | 17.361 | 20.970 |
| 50-3500 | 2.586 | 3.346 | 4.040 | 4.615 | 5.889 | 6.872 | 9.588 | 11.844 | 15.040 | 18.322 |
| 50-3504 | 2.870 | 3.545 | 4.165 | 4.692 | 5.903 | 6.868 | 9.619 | 11.966 | 15.235 | 18.397 |
| 50-3530 | 2.498 | 3.071 | 3.592 | 4.020 | 4.943 | 5.660 | 7.784 | 9.623 | 12.077 | 14.222 |
| 50-3573 | 2.254 | 2.839 | 3.356 | 3.734 | 4.376 | 4.851 | 6.563 | 8.188 | 10.369 | 12.140 |
| 50-3585 | 1.312 | 1.607 | 1.871 | 2.075 | 2.466 | 2.760 | 3.679 | 4.491 | 5.642 | 6.767 |
| 50-3605 | 4.051 | 5.397 | 6.659 | 7.785 | 10.593 | 12.975 | 20.014 | 26.258 | 35.111 | 43.711 |
| 50-3655 | 1.347 | 1.612 | 1.854 | 2.052 | 2.472 | 2.814 | 3.955 | 5.026 | 6.500 | 7.778 |
| 50-3665 | 1.589 | 1.899 | 2.185 | 2.429 | 2.996 | 3.451 | 4.763 | 5.892 | 7.480 | 9.035 |
| 50-3672 | 1.707 | 2.072 | 2.408 | 2.693 | 3.348 | 3.875 | 5.430 | 6.788 | 8.666 | 10.420 |
| 50-3682 | 1.534 | 1.814 | 2.071 | 2.291 | 2.795 | 3.205 | 4.456 | 5.571 | 7.067 | 8.352 |
| 50-3695 | 2.541 | 3.242 | 3.887 | 4.433 | 5.674 | 6.677 | 9.661 | 12.279 | 15.998 | 19.658 |
| 50-3720 | 1.896 | 2.176 | 2.425 | 2.612 | 2.941 | 3.203 | 4.283 | 5.417 | 7.023 | 8.380 |
| 50-3765 | 1.658 | 1.955 | 2.217 | 2.406 | 2.721 | 2.944 | 3.690 | 4.358 | 5.243 | 5.976 |
| 50-3905 | 1.852 | 2.205 | 2.529 | 2.802 | 3.411 | 3.904 | 5.433 | 6.807 | 8.689 | 10.368 |
| 50-3910 | 1.584 | 2.118 | 2.578 | 2.869 | 3.225 | 3.469 | 4.512 | 5.570 | 6.928 | 7.858 |
| 50-3933 | 2.099 | 2.566 | 2.992 | 3.345 | 4.121 | 4.724 | 6.450 | 7.917 | 9.904 | 11.726 |
| 50-4094 | 3.486 | 4.519 | 5.462 | 6.248 | 7.966 | 9.361 | 13.850 | 17.970 | 23.655 | 28.716 |
| 50-4100 | 2.397 | 3.066 | 3.679 | 4.195 | 5.348 | 6.277 | 9.089 | 11.577 | 15.131 | 18.644 |
| 50-4103 | 3.321 | 4.274 | 5.152 | 5.902 | 7.605 | 9.031 | 13.708 | 18.088 | 24.140 | 29.451 |
| 50-4155 | 2.326 | 3.001 | 3.632 | 4.192 | 5.600 | 6.732 | 9.685 | 12.102 | 15.262 | 18.058 |
| 50-4425 | 1.323 | 1.595 | 1.843 | 2.046 | 2.488 | 2.830 | 3.807 | 4.634 | 5.786 | 6.904 |
| 50-4546 | 1.348 | 1.626 | 1.879 | 2.085 | 2.522 | 2.867 | 3.943 | 4.907 | 6.246 | 7.484 |
| 50-4550 | 1.559 | 1.899 | 2.204 | 2.442 | 2.900 | 3.250 | 4.368 | 5.372 | 6.825 | 8.286 |
| 50-4555 | 1.782 | 2.168 | 2.509 | 2.761 | 3.198 | 3.524 | 4.669 | 5.744 | 7.243 | 8.582 |
| 50-4590 | 5.826 | 7.552 | 9.133 | 10.458 | 13.392 | 15.771 | 23.230 | 29.975 | 39.382 | 48.060 |
| 50-4621 | 1.320 | 1.658 | 1.963 | 2.206 | 2.704 | 3.073 | 4.094 | 4.929 | 6.175 | 7.611 |
| 50-4766 | 1.169 | 1.409 | 1.629 | 1.814 | 2.224 | 2.565 | 3.693 | 4.754 | 6.236 | 7.564 |
| 50-4812 | 2.418 | 3.083 | 3.691 | 4.200 | 5.318 | 6.235 | 9.230 | 12.010 | 15.821 | 19.132 |
| 50-4964 | 1.491 | 1.900 | 2.262 | 2.528 | 2.994 | 3.326 | 4.357 | 5.249 | 6.454 | 7.537 |
| 50-4988 | 3.186 | 4.008 | 4.750 | 5.345 | 6.561 | 7.514 | 10.571 | 13.342 | 17.226 | 20.841 |
| 50-4991 | 2.853 | 3.619 | 4.312 | 4.875 | 6.063 | 6.978 | 9.679 | 12.004 | 15.275 | 18.482 |
| 50-5076 | 0.857 | 1.043 | 1.211 | 1.345 | 1.615 | 1.823 | 2.486 | 3.083 | 3.845 | 4.428 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-4

| $\begin{gathered} \text { Station } \\ \text { ID } \\ \hline \end{gathered}$ | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-5136 | 0.614 | 0.694 | 0.767 | 0.828 | 0.964 | 1.074 | 1.423 | 1.739 | 2.110 | 2.338 |
| 50-5318 | 1.188 | 1.364 | 1.524 | 1.658 | 1.950 | 2.188 | 2.943 | 3.633 | 4.594 | 5.472 |
| 50-5397 | 1.145 | 1.292 | 1.428 | 1.543 | 1.801 | 2.017 | 2.759 | 3.470 | 4.422 | 5.182 |
| 50-5454 | 5.196 | 7.204 | 9.044 | 10.590 | 14.025 | 16.833 | 25.923 | 34.308 | 45.314 | 54.040 |
| 50-5464 | 1.392 | 1.691 | 1.958 | 2.165 | 2.554 | 2.854 | 3.877 | 4.832 | 6.159 | 7.341 |
| 50-5499 | 2.328 | 3.046 | 3.705 | 4.261 | 5.503 | 6.523 | 9.824 | 12.875 | 16.940 | 20.273 |
| 50-5519 | 8.932 | 11.376 | 13.644 | 15.619 | 20.347 | 24.239 | 35.580 | 45.477 | 59.275 | 72.402 |
| 50-5534 | 1.019 | 1.202 | 1.370 | 1.513 | 1.839 | 2.102 | 2.897 | 3.600 | 4.549 | 5.382 |
| 50-5604 | 6.364 | 8.870 | 11.150 | 13.022 | 17.025 | 20.208 | 30.165 | 39.107 | 51.608 | 63.273 |
| 50-5607 | 1.485 | 1.934 | 2.339 | 2.663 | 3.321 | 3.834 | 5.510 | 7.042 | 9.094 | 10.811 |
| 50-5644 | 1.429 | 1.696 | 1.940 | 2.143 | 2.592 | 2.942 | 3.943 | 4.795 | 5.939 | 6.971 |
| 50-5733 | 1.230 | 1.477 | 1.700 | 1.877 | 2.232 | 2.508 | 3.404 | 4.220 | 5.354 | 6.383 |
| 50-5757 | 1.543 | 1.877 | 2.172 | 2.388 | 2.762 | 3.039 | 4.031 | 4.969 | 6.219 | 7.224 |
| 50-5769 | 1.208 | 1.428 | 1.629 | 1.797 | 2.163 | 2.461 | 3.421 | 4.302 | 5.540 | 6.685 |
| 50-5778 | 1.575 | 1.874 | 2.141 | 2.350 | 2.760 | 3.067 | 4.006 | 4.822 | 5.967 | 7.072 |
| 50-5810 | 1.331 | 1.563 | 1.776 | 1.955 | 2.361 | 2.677 | 3.578 | 4.343 | 5.308 | 6.067 |
| 50-5880 | 1.332 | 1.671 | 1.975 | 2.212 | 2.676 | 3.028 | 4.138 | 5.125 | 6.504 | 7.801 |
| 50-5881 | 1.167 | 1.349 | 1.516 | 1.659 | 1.985 | 2.256 | 3.113 | 3.898 | 5.022 | 6.107 |
| 50-5882 | 1.376 | 1.628 | 1.854 | 2.030 | 2.370 | 2.632 | 3.496 | 4.287 | 5.350 | 6.245 |
| 50-5894 | 2.216 | 2.739 | 3.223 | 3.637 | 4.635 | 5.383 | 7.132 | 8.461 | 10.189 | 11.819 |
| 50-5898 | 2.422 | 3.064 | 3.647 | 4.123 | 5.149 | 5.929 | 8.077 | 9.847 | 12.418 | 15.208 |
| 50-6058 | 1.479 | 1.778 | 2.053 | 2.286 | 2.822 | 3.246 | 4.471 | 5.526 | 6.849 | 7.868 |
| 50-6147 | 1.171 | 1.477 | 1.747 | 1.945 | 2.287 | 2.537 | 3.410 | 4.221 | 5.254 | 6.017 |
| 50-6270 | 1.147 | 1.338 | 1.512 | 1.659 | 1.988 | 2.254 | 3.063 | 3.783 | 4.780 | 5.698 |
| 50-6309 | 1.247 | 1.477 | 1.684 | 1.848 | 2.187 | 2.439 | 3.159 | 3.763 | 4.582 | 5.345 |
| 50-6441 | 1.698 | 1.992 | 2.262 | 2.487 | 2.992 | 3.385 | 4.489 | 5.417 | 6.720 | 8.021 |
| 50-6496 | 1.231 | 1.532 | 1.803 | 2.019 | 2.459 | 2.798 | 3.873 | 4.836 | 6.111 | 7.168 |
| 50-6562 | 4.875 | 6.305 | 7.623 | 8.749 | 11.369 | 13.467 | 19.490 | 24.663 | 31.624 | 37.856 |
| 50-6581 | 1.110 | 1.287 | 1.448 | 1.580 | 1.860 | 2.081 | 2.772 | 3.392 | 4.209 | 4.881 |
| 50-6586 | 1.252 | 1.422 | 1.576 | 1.703 | 1.971 | 2.191 | 2.973 | 3.734 | 4.741 | 5.514 |
| 50-6656 | 1.150 | 1.386 | 1.605 | 1.795 | 2.251 | 2.617 | 3.635 | 4.498 | 5.594 | 6.474 |
| 50-6727 | 1.106 | 1.298 | 1.468 | 1.591 | 1.793 | 1.953 | 2.644 | 3.389 | 4.459 | 5.370 |
| 50-6760 | 1.613 | 1.912 | 2.195 | 2.454 | 3.135 | 3.718 | 5.385 | 6.843 | 8.767 | 10.395 |
| 50-6853 | 3.262 | 4.181 | 5.017 | 5.704 | 7.189 | 8.347 | 11.792 | 14.783 | 18.871 | 22.617 |
| 50-6870 | 1.266 | 1.516 | 1.741 | 1.917 | 2.263 | 2.531 | 3.407 | 4.206 | 5.297 | 6.250 |
| 50-6875 | 1.525 | 1.823 | 2.096 | 2.327 | 2.856 | 3.271 | 4.431 | 5.407 | 6.723 | 7.932 |
| 50-7097 | 1.385 | 1.724 | 2.026 | 2.260 | 2.701 | 3.043 | 4.248 | 5.395 | 6.924 | 8.145 |
| 50-7105 | 1.202 | 1.436 | 1.651 | 1.834 | 2.248 | 2.588 | 3.684 | 4.694 | 5.938 | 6.792 |
| 50-7141 | 5.937 | 8.015 | 9.942 | 11.617 | 15.653 | 18.892 | 27.764 | 35.201 | 45.276 | 54.644 |
| 50-7251 | 4.078 | 5.312 | 6.451 | 7.430 | 9.713 | 11.575 | 17.043 | 21.818 | 28.676 | 35.611 |
| 50-7352 | 1.313 | 1.525 | 1.717 | 1.875 | 2.211 | 2.480 | 3.343 | 4.130 | 5.222 | 6.211 |
| 50-7365 | 1.504 | 1.795 | 2.058 | 2.269 | 2.694 | 3.039 | 4.292 | 5.519 | 7.150 | 8.407 |
| 50-7431 | 0.892 | 1.054 | 1.198 | 1.310 | 1.522 | 1.686 | 2.247 | 2.773 | 3.510 | 4.178 |
| 50-7442 | 0.742 | 0.874 | 1.001 | 1.119 | 1.450 | 1.720 | 2.383 | 2.919 | 3.482 | 3.793 |
| 50-7451 | 3.188 | 4.260 | 5.216 | 5.944 | 7.285 | 8.309 | 11.820 | 15.098 | 19.810 | 24.325 |
| 50-7494 | 2.980 | 4.123 | 5.150 | 5.960 | 7.568 | 8.794 | 12.695 | 16.186 | 20.786 | 24.571 |
| 50-7557 | 5.797 | 7.283 | 8.657 | 9.843 | 12.584 | 14.916 | 22.648 | 29.971 | 40.233 | 49.427 |
| 50-7570 | 1.379 | 1.660 | 1.915 | 2.121 | 2.552 | 2.887 | 3.908 | 4.805 | 6.102 | 7.425 |
| 50-7700 | 1.417 | 1.647 | 1.851 | 2.002 | 2.262 | 2.463 | 3.253 | 4.054 | 5.191 | 6.185 |
| 50-7738 | 4.625 | 6.038 | 7.367 | 8.564 | 11.618 | 14.193 | 21.592 | 28.052 | 36.533 | 43.628 |
| 50-7783 | 1.314 | 1.607 | 1.867 | 2.064 | 2.428 | 2.701 | 3.625 | 4.476 | 5.581 | 6.436 |
| 50-7854 | 3.974 | 5.307 | 6.524 | 7.538 | 9.756 | 11.554 | 17.268 | 22.477 | 29.827 | 36.736 |
| 50-7900 | 0.958 | 1.143 | 1.307 | 1.432 | 1.668 | 1.841 | 2.376 | 2.840 | 3.494 | 4.132 |
| 50-7977 | 1.279 | 1.555 | 1.803 | 1.996 | 2.375 | 2.662 | 3.589 | 4.424 | 5.508 | 6.367 |
| 50-8025 | 1.326 | 1.626 | 1.895 | 2.105 | 2.517 | 2.827 | 3.786 | 4.626 | 5.780 | 6.836 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-5

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-8054 | 1.214 | 1.452 | 1.676 | 1.879 | 2.411 | 2.848 | 3.994 | 4.940 | 6.180 | 7.275 |
| 50-8105 | 1.106 | 1.384 | 1.636 | 1.840 | 2.264 | 2.600 | 3.711 | 4.738 | 6.044 | 7.006 |
| 50-8118 | 1.231 | 1.410 | 1.582 | 1.742 | 2.170 | 2.555 | 3.739 | 4.832 | 6.384 | 7.848 |
| 50-8140 | 1.337 | 1.612 | 1.856 | 2.039 | 2.367 | 2.615 | 3.494 | 4.326 | 5.456 | 6.403 |
| 50-8183 | 2.010 | 2.469 | 2.890 | 3.243 | 4.047 | 4.673 | 6.408 | 7.858 | 9.822 | 11.651 |
| 50-8355 | 2.646 | 3.217 | 3.743 | 4.193 | 5.251 | 6.082 | 8.344 | 10.225 | 12.660 | 14.734 |
| 50-8371 | 3.955 | 5.061 | 6.070 | 6.909 | 8.774 | 10.213 | 14.249 | 17.639 | 22.074 | 25.904 |
| 50-8375 | 4.353 | 5.683 | 6.878 | 7.817 | 9.707 | 11.089 | 14.927 | 18.073 | 22.495 | 27.019 |
| 50-8377 | 3.639 | 4.390 | 5.074 | 5.637 | 6.871 | 7.810 | 10.426 | 12.608 | 15.444 | 17.877 |
| 50-8409 | 1.351 | 1.625 | 1.867 | 2.040 | 2.320 | 2.530 | 3.355 | 4.177 | 5.273 | 6.105 |
| 50-8419 | 1.677 | 1.941 | 2.186 | 2.396 | 2.882 | 3.292 | 4.613 | 5.841 | 7.616 | 9.341 |
| 50-8437 | 0.850 | 0.950 | 1.042 | 1.121 | 1.301 | 1.455 | 2.006 | 2.550 | 3.251 | 3.749 |
| 50-8494 | 3.790 | 4.830 | 5.788 | 6.602 | 8.454 | 9.971 | 14.655 | 18.869 | 24.776 | 30.312 |
| 50-8503 | 3.935 | 4.979 | 5.944 | 6.774 | 8.714 | 10.312 | 15.129 | 19.412 | 25.461 | 31.279 |
| 50-8512 | 2.656 | 3.150 | 3.596 | 3.957 | 4.684 | 5.284 | 7.516 | 9.750 | 12.850 | 15.443 |
| 50-8525 | 2.320 | 2.894 | 3.412 | 3.826 | 4.674 | 5.312 | 7.161 | 8.729 | 10.852 | 12.806 |
| 50-8536 | 1.934 | 2.377 | 2.776 | 3.096 | 3.755 | 4.256 | 5.734 | 7.000 | 8.755 | 10.428 |
| 50-8547 | 1.483 | 1.753 | 1.998 | 2.196 | 2.614 | 2.932 | 3.854 | 4.638 | 5.733 | 6.806 |
| 50-8584 | 5.574 | 7.850 | 9.939 | 11.704 | 15.733 | 18.914 | 27.783 | 35.233 | 46.024 | 57.499 |
| 50-8594 | 1.059 | 1.252 | 1.424 | 1.555 | 1.792 | 1.978 | 2.677 | 3.370 | 4.348 | 5.209 |
| 50-8625 | 1.069 | 1.318 | 1.541 | 1.717 | 2.065 | 2.333 | 3.221 | 4.035 | 5.143 | 6.096 |
| 50-8666 | 1.575 | 1.891 | 2.186 | 2.446 | 3.088 | 3.611 | 5.032 | 6.221 | 7.878 | 9.514 |
| 50-8811 | 1.502 | 1.833 | 2.130 | 2.364 | 2.832 | 3.188 | 4.290 | 5.260 | 6.612 | 7.885 |
| 50-8882 | 1.790 | 2.304 | 2.765 | 3.125 | 3.822 | 4.356 | 6.107 | 7.704 | 9.854 | 11.680 |
| 50-8915 | 1.409 | 1.767 | 2.083 | 2.317 | 2.724 | 3.023 | 4.016 | 4.916 | 6.181 | 7.368 |
| 50-8976 | 1.964 | 2.444 | 2.879 | 3.232 | 3.976 | 4.548 | 6.229 | 7.673 | 9.676 | 11.588 |
| 50-8987 | 1.554 | 1.803 | 2.024 | 2.190 | 2.499 | 2.719 | 3.379 | 3.939 | 4.669 | 5.289 |
| 50-9014 | 1.147 | 1.356 | 1.549 | 1.714 | 2.091 | 2.396 | 3.294 | 4.077 | 5.148 | 6.124 |
| 50-9035 | 1.126 | 1.382 | 1.618 | 1.820 | 2.289 | 2.655 | 3.616 | 4.394 | 5.516 | 6.735 |
| 50-9102 | 1.082 | 1.303 | 1.500 | 1.649 | 1.918 | 2.122 | 2.833 | 3.501 | 4.389 | 5.104 |
| 50-9121 | 2.870 | 3.908 | 4.862 | 5.668 | 7.522 | 8.957 | 12.829 | 16.016 | 20.233 | 24.031 |
| 50-9144 | 1.579 | 1.845 | 2.093 | 2.310 | 2.836 | 3.278 | 4.629 | 5.847 | 7.535 | 9.077 |
| 50-9249 | 1.176 | 1.464 | 1.724 | 1.932 | 2.356 | 2.684 | 3.725 | 4.661 | 5.897 | 6.920 |
| 50-9313 | 1.268 | 1.478 | 1.663 | 1.793 | 1.995 | 2.145 | 2.711 | 3.267 | 4.080 | 4.866 |
| 50-9385 | 1.269 | 1.478 | 1.661 | 1.792 | 2.006 | 2.164 | 2.742 | 3.297 | 4.074 | 4.762 |
| 50-9399 | 3.122 | 4.131 | 5.067 | 5.883 | 7.823 | 9.452 | 14.488 | 19.056 | 25.380 | 31.110 |
| 50-9410 | 2.584 | 3.159 | 3.678 | 4.096 | 4.967 | 5.631 | 7.579 | 9.246 | 11.588 | 13.893 |
| 50-9421 | 1.019 | 1.221 | 1.403 | 1.548 | 1.837 | 2.069 | 2.889 | 3.678 | 4.729 | 5.556 |
| 50-9460 | 4.059 | 5.075 | 5.992 | 6.729 | 8.246 | 9.413 | 13.017 | 16.198 | 20.443 | 24.083 |
| 50-9489 | 1.299 | 1.612 | 1.895 | 2.124 | 2.606 | 2.972 | 4.008 | 4.875 | 6.122 | 7.428 |
| 50-9511 | 3.119 | 3.856 | 4.523 | 5.060 | 6.168 | 7.029 | 9.685 | 12.033 | 15.431 | 18.890 |
| 50-9539 | 0.972 | 1.108 | 1.227 | 1.307 | 1.422 | 1.501 | 1.790 | 2.061 | 2.431 | 2.749 |
| 50-9564 | 1.160 | 1.452 | 1.713 | 1.919 | 2.322 | 2.632 | 3.646 | 4.570 | 5.818 | 6.883 |
| 50-9641 | 1.096 | 1.306 | 1.495 | 1.644 | 1.942 | 2.171 | 2.901 | 3.557 | 4.437 | 5.185 |
| 50-9686 | 3.103 | 4.158 | 5.119 | 5.913 | 7.671 | 9.003 | 12.567 | 15.465 | 19.448 | 23.371 |
| 50-9702 | 4.743 | 6.011 | 7.226 | 8.361 | 11.440 | 14.159 | 22.044 | 29.050 | 38.807 | 47.918 |
| 50-9739 | 1.090 | 1.345 | 1.573 | 1.749 | 2.086 | 2.341 | 3.167 | 3.913 | 4.935 | 5.847 |
| 50-9759 | 1.292 | 1.595 | 1.866 | 2.076 | 2.473 | 2.776 | 3.779 | 4.697 | 5.968 | 7.110 |
| 50-9765 | 1.320 | 1.706 | 2.050 | 2.311 | 2.793 | 3.152 | 4.312 | 5.352 | 6.771 | 8.029 |
| 50-9790 | 1.843 | 2.230 | 2.580 | 2.860 | 3.442 | 3.876 | 5.083 | 6.079 | 7.486 | 8.927 |
| 50-9793 | 1.216 | 1.479 | 1.714 | 1.891 | 2.216 | 2.462 | 3.312 | 4.106 | 5.193 | 6.127 |
| 50-9829 | 6.683 | 9.554 | 12.152 | 14.253 | 18.667 | 22.047 | 31.878 | 40.254 | 52.308 | 64.809 |
| 50-9861 | 1.883 | 2.191 | 2.471 | 2.702 | 3.204 | 3.597 | 4.769 | 5.790 | 7.148 | 8.319 |
| 50-9869 | 1.235 | 1.517 | 1.765 | 1.945 | 2.248 | 2.468 | 3.221 | 3.913 | 4.867 | 5.718 |
| 50-9883 | 1.869 | 2.074 | 2.270 | 2.453 | 2.942 | 3.386 | 4.828 | 6.201 | 8.033 | 9.495 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-6

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-9919 | 3.212 | 4.135 | 4.988 | 5.723 | 7.444 | 8.864 | 13.139 | 16.941 | 22.324 | 27.531 |
| 50-9930 | 4.027 | 5.232 | 6.341 | 7.284 | 9.431 | 11.189 | 16.622 | 21.512 | 28.287 | 34.475 |
| 50-9941 | 5.381 | 6.938 | 8.371 | 9.593 | 12.386 | 14.684 | 21.837 | 28.311 | 37.229 | 45.240 |
| 55-0064 | 4.384 | 5.570 | 6.656 | 7.570 | 9.601 | 11.264 | 16.638 | 21.595 | 28.236 | 33.750 |
| 55-0079 | 0.898 | 1.043 | 1.178 | 1.294 | 1.571 | 1.790 | 2.350 | 2.798 | 3.501 | 4.414 |
| 55-0080 | 3.240 | 4.038 | 4.786 | 5.455 | 7.108 | 8.540 | 13.061 | 17.248 | 22.998 | 28.023 |
| 55-0087 | 1.375 | 1.589 | 1.792 | 1.977 | 2.472 | 2.866 | 3.757 | 4.431 | 5.363 | 6.354 |
| 55-0096 | 1.244 | 1.426 | 1.599 | 1.758 | 2.188 | 2.543 | 3.441 | 4.167 | 5.156 | 6.113 |
| 55-0164 | 0.587 | 0.646 | 0.702 | 0.752 | 0.878 | 0.986 | 1.315 | 1.612 | 2.014 | 2.362 |
| 80-0100 | 1.402 | 1.575 | 1.735 | 1.874 | 2.195 | 2.463 | 3.327 | 4.126 | 5.166 | 5.972 |
| 80-0120 | 1.382 | 1.629 | 1.852 | 2.032 | 2.398 | 2.686 | 3.596 | 4.416 | 5.648 | 6.985 |
| 80-0140 | 1.015 | 1.129 | 1.238 | 1.336 | 1.588 | 1.807 | 2.482 | 3.098 | 3.946 | 4.700 |
| 80-0160 | 0.884 | 0.983 | 1.076 | 1.156 | 1.352 | 1.512 | 1.957 | 2.334 | 2.875 | 3.434 |
| 80-0200 | 1.132 | 1.301 | 1.456 | 1.588 | 1.887 | 2.133 | 2.908 | 3.613 | 4.576 | 5.417 |
| 80-0220 | 4.803 | 5.980 | 7.091 | 8.096 | 10.662 | 12.871 | 19.437 | 25.308 | 33.476 | 41.048 |
| 80-0240 | 1.467 | 1.679 | 1.894 | 2.112 | 2.847 | 3.466 | 4.624 | 5.433 | 6.575 | 7.934 |
| 80-0260 | 0.978 | 1.124 | 1.259 | 1.375 | 1.644 | 1.864 | 2.539 | 3.144 | 3.942 | 4.602 |
| 80-0340 | 1.517 | 1.758 | 1.984 | 2.190 | 2.710 | 3.171 | 4.670 | 6.090 | 8.022 | 9.640 |
| 80-0425 | 1.468 | 1.775 | 2.054 | 2.285 | 2.797 | 3.187 | 4.241 | 5.103 | 6.306 | 7.519 |
| 80-0440 | 0.880 | 0.995 | 1.102 | 1.195 | 1.412 | 1.589 | 2.112 | 2.573 | 3.156 | 3.604 |
| 80-0460 | 1.432 | 1.770 | 2.065 | 2.269 | 2.577 | 2.798 | 3.612 | 4.389 | 5.559 | 6.781 |
| 80-0540 | 1.071 | 1.302 | 1.503 | 1.642 | 1.848 | 2.001 | 2.663 | 3.359 | 4.283 | 4.947 |
| 80-0560 | 1.563 | 1.830 | 2.068 | 2.253 | 2.609 | 2.877 | 3.713 | 4.449 | 5.532 | 6.677 |
| 80-0640 | 1.304 | 1.605 | 1.870 | 2.061 | 2.371 | 2.605 | 3.517 | 4.427 | 5.694 | 6.761 |
| 80-0780 | 1.357 | 1.727 | 2.050 | 2.277 | 2.626 | 2.877 | 3.787 | 4.647 | 5.900 | 7.128 |
| 80-0820 | 1.567 | 1.857 | 2.127 | 2.366 | 2.950 | 3.438 | 4.950 | 6.322 | 7.862 | 8.712 |
| 80-0860 | 1.603 | 1.892 | 2.146 | 2.328 | 2.623 | 2.844 | 3.717 | 4.592 | 5.785 | 6.739 |
| 80-0900 | 1.310 | 1.632 | 1.915 | 2.113 | 2.426 | 2.647 | 3.406 | 4.099 | 5.050 | 5.891 |
| 80-0920 | 3.479 | 4.186 | 4.811 | 5.273 | 6.099 | 6.667 | 8.255 | 9.539 | 11.262 | 12.888 |
| 80-0940 | 0.935 | 1.081 | 1.213 | 1.320 | 1.542 | 1.709 | 2.174 | 2.557 | 3.101 | 3.664 |
| 80-1020 | 0.946 | 1.152 | 1.337 | 1.482 | 1.768 | 1.988 | 2.694 | 3.329 | 4.221 | 5.056 |
| 80-1060 | 0.838 | 0.948 | 1.050 | 1.137 | 1.338 | 1.503 | 2.004 | 2.450 | 3.082 | 3.691 |
| 80-1100 | 0.948 | 1.040 | 1.128 | 1.211 | 1.438 | 1.636 | 2.188 | 2.666 | 3.331 | 3.965 |
| 80-1120 | 1.432 | 1.653 | 1.858 | 2.040 | 2.499 | 2.856 | 3.705 | 4.361 | 5.240 | 6.103 |
| 80-1140 | 1.903 | 2.229 | 2.522 | 2.752 | 3.209 | 3.554 | 4.613 | 5.539 | 6.787 | 7.890 |
| 80-1180 | 3.003 | 3.881 | 4.702 | 5.429 | 7.241 | 8.724 | 12.817 | 16.284 | 20.841 | 24.781 |
| 80-1220 | 1.280 | 1.460 | 1.633 | 1.794 | 2.229 | 2.605 | 3.650 | 4.552 | 5.757 | 6.813 |
| 80-1240 | 1.637 | 1.864 | 2.074 | 2.254 | 2.666 | 3.009 | 4.126 | 5.164 | 6.516 | 7.563 |
| 80-1280 | 1.018 | 1.222 | 1.406 | 1.548 | 1.822 | 2.034 | 2.742 | 3.397 | 4.357 | 5.327 |
| 80-1300 | 2.844 | 3.561 | 4.224 | 4.797 | 6.143 | 7.249 | 10.519 | 13.392 | 17.541 | 21.763 |
| 80-1320 | 1.037 | 1.091 | 1.146 | 1.203 | 1.387 | 1.572 | 2.139 | 2.680 | 3.481 | 4.285 |
| 80-1340 | 1.133 | 1.302 | 1.466 | 1.619 | 2.056 | 2.414 | 3.238 | 3.874 | 4.708 | 5.495 |
| 80-1360 | 1.068 | 1.343 | 1.589 | 1.779 | 2.143 | 2.417 | 3.295 | 4.080 | 5.163 | 6.144 |
| 80-1380 | 3.656 | 4.296 | 4.880 | 5.364 | 6.448 | 7.254 | 9.272 | 10.850 | 13.010 | 15.203 |
| 80-1400 | 1.459 | 1.656 | 1.834 | 1.977 | 2.269 | 2.495 | 3.184 | 3.789 | 4.687 | 5.659 |
| 80-1420 | 1.242 | 1.442 | 1.623 | 1.771 | 2.086 | 2.329 | 3.045 | 3.660 | 4.535 | 5.410 |
| 80-1440 | 1.190 | 1.379 | 1.566 | 1.749 | 2.300 | 2.796 | 4.155 | 5.336 | 6.769 | 7.781 |
| 80-1460 | 1.064 | 1.233 | 1.389 | 1.521 | 1.819 | 2.065 | 2.844 | 3.556 | 4.542 | 5.433 |
| 80-1480 | 1.109 | 1.327 | 1.527 | 1.692 | 2.053 | 2.341 | 3.258 | 4.090 | 5.172 | 6.027 |
| 80-1540 | 0.821 | 0.963 | 1.095 | 1.212 | 1.499 | 1.736 | 2.417 | 3.008 | 3.745 | 4.299 |
| 80-1740 | 0.950 | 1.032 | 1.116 | 1.202 | 1.480 | 1.742 | 2.430 | 3.021 | 3.825 | 4.560 |
| 80-1760 | 1.182 | 1.419 | 1.636 | 1.816 | 2.218 | 2.528 | 3.391 | 4.111 | 5.102 | 6.055 |
| 80-1900 | 1.086 | 1.267 | 1.432 | 1.567 | 1.859 | 2.087 | 2.759 | 3.341 | 4.126 | 4.827 |
| 80-1940 | 1.088 | 1.187 | 1.285 | 1.380 | 1.662 | 1.921 | 2.655 | 3.308 | 4.163 | 4.866 |
| 80-1980 | 0.913 | 1.049 | 1.172 | 1.270 | 1.464 | 1.618 | 2.145 | 2.640 | 3.299 | 3.827 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-7

| Station <br> ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $80-2000$ | 1.705 | 2.024 | 2.309 | 2.530 | 2.953 | 3.279 | 4.386 | 5.416 | 6.877 | 8.239 |
| $80-2040$ | 1.357 | 1.562 | 1.760 | 1.946 | 2.471 | 2.928 | 4.187 | 5.273 | 6.650 | 7.730 |
| $80-2080$ | 1.147 | 1.494 | 1.796 | 1.997 | 2.279 | 2.477 | 3.255 | 4.016 | 5.001 | 5.715 |
| $80-2120$ | 1.266 | 1.492 | 1.703 | 1.888 | 2.340 | 2.703 | 3.662 | 4.448 | 5.599 | 6.877 |
| $80-2140$ | 1.269 | 1.506 | 1.723 | 1.904 | 2.305 | 2.622 | 3.575 | 4.411 | 5.507 | 6.416 |
| $80-2160$ | 1.123 | 1.314 | 1.486 | 1.626 | 1.913 | 2.141 | 2.905 | 3.615 | 4.548 | 5.280 |
| $80-2320$ | 1.593 | 1.855 | 2.091 | 2.281 | 2.664 | 2.966 | 3.955 | 4.864 | 6.150 | 7.360 |
| $80-2340$ | 1.454 | 1.698 | 1.919 | 2.094 | 2.439 | 2.719 | 3.760 | 4.797 | 6.255 | 7.522 |
| $80-2380$ | 1.322 | 1.536 | 1.731 | 1.890 | 2.225 | 2.493 | 3.359 | 4.154 | 5.296 | 6.410 |
| $80-2440$ | 1.149 | 1.428 | 1.674 | 1.853 | 2.158 | 2.385 | 3.195 | 3.963 | 5.028 | 5.959 |
| $80-2560$ | 1.127 | 1.306 | 1.469 | 1.603 | 1.888 | 2.113 | 2.810 | 3.433 | 4.284 | 5.049 |
| $80-2620$ | 0.804 | 0.956 | 1.089 | 1.181 | 1.320 | 1.419 | 1.759 | 2.070 | 2.567 | 3.173 |
| $80-2640$ | 1.207 | 1.368 | 1.516 | 1.641 | 1.921 | 2.160 | 2.987 | 3.790 | 4.968 | 6.109 |
| $80-2700$ | 3.679 | 4.588 | 5.433 | 6.175 | 7.947 | 9.467 | 14.429 | 19.097 | 25.402 | 30.637 |
| $90-0001$ | 2.327 | 3.142 | 3.867 | 4.414 | 5.412 | 6.155 | 8.634 | 10.892 | 13.921 | 16.467 |

Table A.4.2. $\lambda_{2}$ moments.

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10-0208 | 0.297 | 0.373 | 0.438 | 0.481 | 0.542 | 0.582 | 0.714 | 0.829 | 1.014 | 1.251 |
| 10-0215 | 0.252 | 0.303 | 0.348 | 0.377 | 0.416 | 0.444 | 0.560 | 0.678 | 0.845 | 0.988 |
| 10-0236 | 0.265 | 0.324 | 0.375 | 0.408 | 0.452 | 0.480 | 0.575 | 0.658 | 0.776 | 0.893 |
| 10-0238 | 0.277 | 0.306 | 0.331 | 0.351 | 0.388 | 0.415 | 0.501 | 0.577 | 0.691 | 0.819 |
| 10-0240 | 0.433 | 0.607 | 0.761 | 0.876 | 1.083 | 1.229 | 1.646 | 1.987 | 2.496 | 3.078 |
| 10-0241 | 0.634 | 0.829 | 1.006 | 1.154 | 1.475 | 1.734 | 2.535 | 3.253 | 4.275 | 5.267 |
| 10-0946 | 0.498 | 0.578 | 0.652 | 0.714 | 0.855 | 0.965 | 1.259 | 1.500 | 1.842 | 2.203 |
| 10-0947 | 0.337 | 0.400 | 0.455 | 0.497 | 0.574 | 0.630 | 0.801 | 0.949 | 1.154 | 1.346 |
| 10-0948 | 0.280 | 0.347 | 0.406 | 0.445 | 0.500 | 0.538 | 0.681 | 0.818 | 1.011 | 1.186 |
| 10-0949 | 0.314 | 0.411 | 0.495 | 0.552 | 0.639 | 0.698 | 0.885 | 1.046 | 1.282 | 1.532 |
| 10-0950 | 0.368 | 0.467 | 0.553 | 0.608 | 0.676 | 0.723 | 0.905 | 1.081 | 1.354 | 1.655 |
| 10-0951 | 0.246 | 0.299 | 0.345 | 0.379 | 0.436 | 0.479 | 0.637 | 0.790 | 1.008 | 1.207 |
| 10-0952 | 0.324 | 0.399 | 0.464 | 0.506 | 0.563 | 0.602 | 0.750 | 0.892 | 1.113 | 1.358 |
| 10-0955 | 0.464 | 0.546 | 0.621 | 0.682 | 0.811 | 0.907 | 1.171 | 1.388 | 1.665 | 1.897 |
| 10-0956 | 0.867 | 1.052 | 1.214 | 1.334 | 1.532 | 1.686 | 2.332 | 3.006 | 3.844 | 4.361 |
| 10-0957 | 0.292 | 0.345 | 0.396 | 0.442 | 0.571 | 0.672 | 0.888 | 1.048 | 1.257 | 1.465 |
| 10-0958 | 0.273 | 0.322 | 0.365 | 0.398 | 0.462 | 0.510 | 0.678 | 0.835 | 1.046 | 1.218 |
| 10-0959 | 0.687 | 0.819 | 0.937 | 1.027 | 1.196 | 1.317 | 1.670 | 1.964 | 2.368 | 2.757 |
| 10-0961 | 0.169 | 0.188 | 0.206 | 0.221 | 0.255 | 0.281 | 0.349 | 0.403 | 0.482 | 0.571 |
| 10-0962 | 0.267 | 0.324 | 0.374 | 0.411 | 0.473 | 0.519 | 0.684 | 0.840 | 1.061 | 1.263 |
| 10-0964 | 0.746 | 0.933 | 1.102 | 1.238 | 1.520 | 1.737 | 2.443 | 3.084 | 3.782 | 4.136 |
| 10-0966 | 0.251 | 0.293 | 0.333 | 0.372 | 0.485 | 0.568 | 0.701 | 0.787 | 0.892 | 0.999 |
| 10-0967 | 0.415 | 0.489 | 0.558 | 0.615 | 0.745 | 0.843 | 1.088 | 1.281 | 1.536 | 1.775 |
| 10-0968 | 0.388 | 0.435 | 0.474 | 0.496 | 0.514 | 0.527 | 0.636 | 0.792 | 1.001 | 1.119 |
| 10-1002 | 0.274 | 0.313 | 0.350 | 0.384 | 0.474 | 0.547 | 0.723 | 0.862 | 1.054 | 1.251 |
| 10-1003 | 0.357 | 0.411 | 0.459 | 0.497 | 0.571 | 0.630 | 0.836 | 1.032 | 1.283 | 1.466 |
| 10-1037 | 0.878 | 1.154 | 1.400 | 1.586 | 1.920 | 2.182 | 3.232 | 4.301 | 5.551 | 6.219 |
| 10-1064 | 0.686 | 0.832 | 0.963 | 1.065 | 1.259 | 1.414 | 2.031 | 2.660 | 3.379 | 3.739 |
| 10-1094 | 0.240 | 0.304 | 0.360 | 0.402 | 0.477 | 0.531 | 0.705 | 0.858 | 1.084 | 1.324 |
| 10-1291 | 0.270 | 0.327 | 0.376 | 0.408 | 0.454 | 0.484 | 0.576 | 0.653 | 0.765 | 0.883 |
| 10-1444 | 0.239 | 0.289 | 0.334 | 0.366 | 0.420 | 0.460 | 0.608 | 0.750 | 0.962 | 1.175 |
| 10-1449 | 0.638 | 0.791 | 0.928 | 1.034 | 1.235 | 1.392 | 1.950 | 2.483 | 3.138 | 3.565 |
| 10-9909 | 0.245 | 0.309 | 0.366 | 0.409 | 0.489 | 0.549 | 0.744 | 0.920 | 1.166 | 1.392 |
| 21-0115 | 0.168 | 0.196 | 0.220 | 0.239 | 0.275 | 0.300 | 0.379 | 0.446 | 0.536 | 0.616 |
| 21-0160 | 0.275 | 0.344 | 0.405 | 0.449 | 0.520 | 0.575 | 0.806 | 1.047 | 1.351 | 1.544 |

NOAA Atlas 14 Volume 7 Version 2.0

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21-0163 | 0.310 | 0.369 | 0.420 | 0.457 | 0.521 | 0.568 | 0.739 | 0.902 | 1.130 | 1.336 |
| 21-0182 | 0.223 | 0.261 | 0.294 | 0.321 | 0.373 | 0.414 | 0.548 | 0.671 | 0.826 | 0.939 |
| 21-0200 | 0.179 | 0.200 | 0.218 | 0.233 | 0.261 | 0.282 | 0.354 | 0.420 | 0.500 | 0.554 |
| 21-0330 | 0.533 | 0.714 | 0.875 | 0.997 | 1.222 | 1.389 | 1.941 | 2.441 | 3.108 | 3.665 |
| 21-0402 | 0.155 | 0.175 | 0.194 | 0.211 | 0.257 | 0.295 | 0.385 | 0.457 | 0.549 | 0.629 |
| 21-0446 | 0.629 | 0.812 | 0.975 | 1.098 | 1.322 | 1.490 | 2.062 | 2.590 | 3.288 | 3.851 |
| 21-0468 | 0.295 | 0.335 | 0.371 | 0.400 | 0.458 | 0.504 | 0.665 | 0.818 | 0.997 | 1.102 |
| 21-0560 | 0.192 | 0.210 | 0.227 | 0.242 | 0.277 | 0.306 | 0.391 | 0.467 | 0.561 | 0.628 |
| 21-0630 | 0.274 | 0.315 | 0.350 | 0.376 | 0.420 | 0.449 | 0.527 | 0.589 | 0.677 | 0.775 |
| 21-0679 | 0.191 | 0.215 | 0.237 | 0.257 | 0.308 | 0.350 | 0.468 | 0.570 | 0.706 | 0.827 |
| 21-0685 | 0.200 | 0.240 | 0.276 | 0.300 | 0.338 | 0.364 | 0.450 | 0.525 | 0.618 | 0.684 |
| 21-0794 | 0.186 | 0.213 | 0.238 | 0.258 | 0.305 | 0.340 | 0.438 | 0.520 | 0.623 | 0.703 |
| 21-0805 | 0.234 | 0.270 | 0.303 | 0.328 | 0.377 | 0.412 | 0.518 | 0.609 | 0.717 | 0.790 |
| 21-0907 | 0.172 | 0.205 | 0.233 | 0.253 | 0.288 | 0.313 | 0.407 | 0.499 | 0.617 | 0.706 |
| 21-0935 | 0.338 | 0.382 | 0.421 | 0.453 | 0.516 | 0.562 | 0.684 | 0.782 | 0.917 | 1.053 |
| 21-1000 | 0.306 | 0.350 | 0.390 | 0.420 | 0.476 | 0.520 | 0.684 | 0.845 | 1.064 | 1.241 |
| 21-1033 | 0.193 | 0.222 | 0.248 | 0.270 | 0.317 | 0.352 | 0.438 | 0.505 | 0.585 | 0.646 |
| 21-1050 | 0.341 | 0.440 | 0.525 | 0.577 | 0.634 | 0.673 | 0.829 | 0.984 | 1.192 | 1.358 |
| 21-1070 | 0.130 | 0.150 | 0.168 | 0.185 | 0.232 | 0.268 | 0.338 | 0.387 | 0.449 | 0.509 |
| 21-1086 | 0.539 | 0.645 | 0.742 | 0.826 | 1.029 | 1.187 | 1.596 | 1.926 | 2.372 | 2.800 |
| 21-1300 | 0.166 | 0.202 | 0.234 | 0.257 | 0.292 | 0.316 | 0.404 | 0.485 | 0.593 | 0.679 |
| 21-1400 | 0.186 | 0.225 | 0.259 | 0.280 | 0.303 | 0.319 | 0.398 | 0.485 | 0.607 | 0.702 |
| 21-1440 | 0.252 | 0.309 | 0.359 | 0.394 | 0.447 | 0.484 | 0.618 | 0.743 | 0.923 | 1.094 |
| 21-2340 | 0.184 | 0.225 | 0.260 | 0.285 | 0.324 | 0.351 | 0.444 | 0.527 | 0.656 | 0.802 |
| 21-3245 | 0.226 | 0.305 | 0.373 | 0.410 | 0.442 | 0.460 | 0.535 | 0.604 | 0.708 | 0.817 |
| 21-3255 | 0.183 | 0.217 | 0.248 | 0.272 | 0.318 | 0.351 | 0.449 | 0.532 | 0.635 | 0.711 |
| 21-3298 | 0.560 | 0.714 | 0.851 | 0.952 | 1.127 | 1.257 | 1.701 | 2.112 | 2.663 | 3.119 |
| 21-3315 | 0.683 | 0.797 | 0.904 | 1.001 | 1.250 | 1.453 | 1.980 | 2.410 | 2.999 | 3.575 |
| 21-3672 | 0.184 | 0.230 | 0.270 | 0.298 | 0.341 | 0.372 | 0.486 | 0.593 | 0.728 | 0.819 |
| 21-4500 | 0.336 | 0.390 | 0.444 | 0.496 | 0.653 | 0.790 | 1.116 | 1.373 | 1.775 | 2.297 |
| 21-4920 | 0.296 | 0.339 | 0.382 | 0.424 | 0.557 | 0.674 | 0.942 | 1.150 | 1.471 | 1.881 |
| 21-5130 | 0.510 | 0.728 | 0.917 | 1.045 | 1.227 | 1.355 | 1.835 | 2.295 | 2.943 | 3.527 |
| 21-5248 | 0.431 | 0.490 | 0.545 | 0.595 | 0.724 | 0.825 | 1.051 | 1.221 | 1.446 | 1.666 |
| 21-5275 | 0.515 | 0.695 | 0.854 | 0.970 | 1.168 | 1.309 | 1.757 | 2.149 | 2.687 | 3.183 |
| 21-5384 | 0.420 | 0.579 | 0.719 | 0.821 | 1.001 | 1.122 | 1.455 | 1.720 | 2.085 | 2.450 |
| 21-6336 | 0.471 | 0.661 | 0.829 | 0.949 | 1.151 | 1.295 | 1.769 | 2.193 | 2.769 | 3.280 |
| 21-6420 | 0.630 | 0.753 | 0.869 | 0.973 | 1.239 | 1.459 | 2.051 | 2.546 | 3.219 | 3.847 |
| 21-6483 | 0.542 | 0.689 | 0.822 | 0.925 | 1.129 | 1.283 | 1.764 | 2.189 | 2.749 | 3.217 |
| 21-6488 | 0.744 | 0.935 | 1.106 | 1.242 | 1.517 | 1.721 | 2.316 | 2.819 | 3.473 | 4.024 |
| 21-6492 | 0.627 | 0.823 | 0.997 | 1.133 | 1.394 | 1.588 | 2.188 | 2.713 | 3.377 | 3.890 |
| 21-6493 | 0.699 | 0.892 | 1.065 | 1.201 | 1.472 | 1.672 | 2.252 | 2.742 | 3.386 | 3.949 |
| 21-7742 | 0.583 | 0.732 | 0.866 | 0.974 | 1.200 | 1.369 | 1.843 | 2.236 | 2.788 | 3.342 |
| 21-8036 | 0.433 | 0.541 | 0.637 | 0.713 | 0.862 | 0.976 | 1.338 | 1.662 | 2.108 | 2.512 |
| 21-8040 | 0.218 | 0.266 | 0.307 | 0.331 | 0.357 | 0.375 | 0.459 | 0.548 | 0.659 | 0.725 |
| 21-8041 | 0.258 | 0.324 | 0.379 | 0.413 | 0.448 | 0.471 | 0.563 | 0.650 | 0.771 | 0.875 |
| 21-8202 | 0.196 | 0.243 | 0.285 | 0.314 | 0.364 | 0.397 | 0.497 | 0.580 | 0.700 | 0.825 |
| 21-8250 | 0.298 | 0.349 | 0.397 | 0.441 | 0.558 | 0.654 | 0.896 | 1.092 | 1.358 | 1.615 |
| 21-8535 | 0.552 | 0.677 | 0.792 | 0.889 | 1.113 | 1.282 | 1.708 | 2.043 | 2.503 | 2.967 |
| 30-1100 | 0.364 | 0.414 | 0.457 | 0.483 | 0.513 | 0.534 | 0.641 | 0.762 | 0.930 | 1.056 |
| 30-1110 | 0.350 | 0.407 | 0.455 | 0.484 | 0.514 | 0.534 | 0.641 | 0.763 | 0.930 | 1.055 |
| 40-1220 | 0.373 | 0.410 | 0.443 | 0.465 | 0.494 | 0.516 | 0.634 | 0.773 | 0.968 | 1.114 |
| 40-1250 | 0.342 | 0.378 | 0.409 | 0.429 | 0.453 | 0.471 | 0.587 | 0.736 | 0.931 | 1.046 |
| 40-1300 | 0.166 | 0.181 | 0.194 | 0.206 | 0.228 | 0.248 | 0.322 | 0.397 | 0.509 | 0.616 |
| 40-1510 | 0.138 | 0.149 | 0.159 | 0.169 | 0.196 | 0.219 | 0.272 | 0.313 | 0.386 | 0.504 |
| 50-0026 | 0.550 | 0.598 | 0.642 | 0.677 | 0.747 | 0.809 | 1.082 | 1.392 | 1.850 | 2.256 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-9

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-0230 | 0.234 | 0.257 | 0.279 | 0.300 | 0.359 | 0.410 | 0.540 | 0.646 | 0.793 | 0.937 |
| 50-0243 | 0.722 | 0.918 | 1.092 | 1.220 | 1.444 | 1.614 | 2.258 | 2.889 | 3.664 | 4.155 |
| 50-0249 | 0.304 | 0.371 | 0.434 | 0.486 | 0.609 | 0.703 | 0.962 | 1.178 | 1.435 | 1.617 |
| 50-0280 | 0.375 | 0.406 | 0.435 | 0.462 | 0.536 | 0.597 | 0.751 | 0.876 | 1.043 | 1.199 |
| 50-0310 | 0.318 | 0.393 | 0.463 | 0.522 | 0.658 | 0.768 | 1.097 | 1.386 | 1.791 | 2.179 |
| 50-0332 | 0.298 | 0.358 | 0.412 | 0.455 | 0.540 | 0.603 | 0.797 | 0.965 | 1.179 | 1.349 |
| 50-0352 | 0.568 | 0.711 | 0.841 | 0.948 | 1.175 | 1.354 | 1.903 | 2.389 | 3.066 | 3.701 |
| 50-0363 | 0.613 | 0.769 | 0.912 | 1.033 | 1.306 | 1.529 | 2.204 | 2.805 | 3.708 | 4.697 |
| 50-0433 | 0.625 | 0.647 | 0.671 | 0.696 | 0.781 | 0.870 | 1.146 | 1.415 | 1.836 | 2.307 |
| 50-0452 | 0.795 | 0.920 | 1.036 | 1.136 | 1.375 | 1.565 | 2.081 | 2.508 | 3.097 | 3.668 |
| 50-0464 | 0.393 | 0.470 | 0.542 | 0.603 | 0.745 | 0.864 | 1.232 | 1.567 | 2.081 | 2.660 |
| 50-0522 | 0.781 | 0.978 | 1.158 | 1.308 | 1.631 | 1.902 | 2.878 | 3.839 | 5.119 | 6.103 |
| 50-0546 | 0.118 | 0.133 | 0.146 | 0.156 | 0.179 | 0.197 | 0.253 | 0.302 | 0.373 | 0.442 |
| 50-0558 | 0.209 | 0.247 | 0.279 | 0.299 | 0.323 | 0.338 | 0.400 | 0.460 | 0.538 | 0.598 |
| 50-0657 | 0.784 | 0.973 | 1.144 | 1.284 | 1.577 | 1.812 | 2.594 | 3.322 | 4.338 | 5.252 |
| 50-0676 | 0.596 | 0.734 | 0.859 | 0.962 | 1.187 | 1.367 | 1.934 | 2.446 | 3.164 | 3.831 |
| 50-0685 | 0.410 | 0.492 | 0.567 | 0.631 | 0.787 | 0.904 | 1.169 | 1.366 | 1.646 | 1.965 |
| 50-0707 | 0.255 | 0.293 | 0.328 | 0.354 | 0.401 | 0.437 | 0.565 | 0.687 | 0.846 | 0.966 |
| 50-0754 | 0.247 | 0.298 | 0.345 | 0.381 | 0.450 | 0.504 | 0.686 | 0.857 | 1.078 | 1.248 |
| 50-0761 | 0.228 | 0.256 | 0.283 | 0.310 | 0.387 | 0.452 | 0.604 | 0.723 | 0.887 | 1.057 |
| 50-0770 | 0.268 | 0.313 | 0.352 | 0.382 | 0.439 | 0.478 | 0.585 | 0.670 | 0.787 | 0.901 |
| 50-0788 | 0.586 | 0.740 | 0.886 | 1.019 | 1.384 | 1.651 | 2.120 | 2.426 | 2.871 | 3.470 |
| 50-0910 | 0.218 | 0.254 | 0.287 | 0.315 | 0.383 | 0.436 | 0.581 | 0.701 | 0.865 | 1.019 |
| 50-1201 | 0.603 | 0.706 | 0.811 | 0.916 | 1.253 | 1.561 | 2.332 | 2.973 | 3.811 | 4.541 |
| 50-1220 | 0.269 | 0.309 | 0.346 | 0.377 | 0.441 | 0.492 | 0.650 | 0.792 | 0.979 | 1.134 |
| 50-1230 | 0.145 | 0.167 | 0.186 | 0.200 | 0.223 | 0.240 | 0.307 | 0.375 | 0.479 | 0.587 |
| 50-1240 | 0.681 | 1.000 | 1.284 | 1.503 | 1.922 | 2.234 | 3.230 | 4.117 | 5.288 | 6.265 |
| 50-1243 | 0.317 | 0.375 | 0.426 | 0.462 | 0.519 | 0.561 | 0.719 | 0.873 | 1.104 | 1.339 |
| 50-1251 | 0.480 | 0.585 | 0.681 | 0.763 | 0.956 | 1.105 | 1.479 | 1.772 | 2.221 | 2.784 |
| 50-1269 | 0.453 | 0.531 | 0.602 | 0.662 | 0.794 | 0.906 | 1.276 | 1.626 | 2.152 | 2.703 |
| 50-1308 | 0.652 | 0.895 | 1.111 | 1.275 | 1.576 | 1.802 | 2.561 | 3.256 | 4.229 | 5.126 |
| 50-1312 | 0.249 | 0.328 | 0.396 | 0.442 | 0.505 | 0.549 | 0.708 | 0.858 | 1.055 | 1.213 |
| 50-1314 | 0.400 | 0.515 | 0.615 | 0.685 | 0.792 | 0.870 | 1.169 | 1.462 | 1.866 | 2.204 |
| 50-1318 | 0.338 | 0.429 | 0.510 | 0.574 | 0.701 | 0.797 | 1.098 | 1.365 | 1.725 | 2.041 |
| 50-1321 | 0.661 | 0.842 | 1.008 | 1.145 | 1.443 | 1.683 | 2.469 | 3.195 | 4.131 | 4.844 |
| 50-1325 | 0.321 | 0.401 | 0.472 | 0.529 | 0.648 | 0.733 | 0.955 | 1.132 | 1.345 | 1.508 |
| 50-1334 | 0.746 | 0.957 | 1.146 | 1.292 | 1.576 | 1.791 | 2.472 | 3.079 | 3.960 | 4.855 |
| 50-1466 | 0.227 | 0.268 | 0.305 | 0.332 | 0.378 | 0.412 | 0.540 | 0.664 | 0.821 | 0.932 |
| 50-1492 | 0.203 | 0.228 | 0.252 | 0.270 | 0.307 | 0.336 | 0.438 | 0.535 | 0.667 | 0.774 |
| 50-1574 | 0.298 | 0.371 | 0.435 | 0.477 | 0.539 | 0.580 | 0.712 | 0.824 | 0.994 | 1.184 |
| 50-1684 | 0.290 | 0.324 | 0.355 | 0.380 | 0.435 | 0.479 | 0.625 | 0.761 | 0.932 | 1.054 |
| 50-1763 | 0.635 | 0.819 | 0.982 | 1.099 | 1.293 | 1.430 | 1.864 | 2.240 | 2.816 | 3.488 |
| 50-1824 | 0.380 | 0.464 | 0.538 | 0.585 | 0.656 | 0.692 | 0.749 | 0.782 | 0.826 | 0.886 |
| 50-1926 | 0.494 | 0.630 | 0.750 | 0.839 | 1.001 | 1.113 | 1.427 | 1.681 | 2.040 | 2.415 |
| 50-1977 | 0.202 | 0.226 | 0.246 | 0.262 | 0.288 | 0.308 | 0.381 | 0.451 | 0.541 | 0.609 |
| 50-1987 | 0.243 | 0.293 | 0.337 | 0.364 | 0.394 | 0.415 | 0.516 | 0.629 | 0.779 | 0.885 |
| 50-2005 | 0.385 | 0.446 | 0.501 | 0.541 | 0.618 | 0.672 | 0.836 | 0.974 | 1.166 | 1.351 |
| 50-2102 | 0.403 | 0.473 | 0.537 | 0.591 | 0.716 | 0.812 | 1.068 | 1.278 | 1.560 | 1.827 |
| 50-2107 | 0.244 | 0.296 | 0.341 | 0.372 | 0.415 | 0.446 | 0.560 | 0.669 | 0.826 | 0.973 |
| 50-2112 | 0.251 | 0.304 | 0.351 | 0.382 | 0.426 | 0.458 | 0.579 | 0.698 | 0.870 | 1.031 |
| 50-2126 | 0.123 | 0.131 | 0.141 | 0.150 | 0.188 | 0.221 | 0.282 | 0.324 | 0.394 | 0.509 |
| 50-2144 | 0.581 | 0.720 | 0.843 | 0.938 | 1.119 | 1.249 | 1.639 | 1.971 | 2.375 | 2.670 |
| 50-2147 | 0.473 | 0.534 | 0.588 | 0.627 | 0.686 | 0.729 | 0.896 | 1.061 | 1.294 | 1.502 |
| 50-2156 | 0.285 | 0.308 | 0.328 | 0.344 | 0.374 | 0.397 | 0.475 | 0.547 | 0.643 | 0.723 |
| 50-2173 | 1.174 | 1.581 | 1.946 | 2.228 | 2.775 | 3.184 | 4.458 | 5.580 | 7.032 | 8.197 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-10

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-2177 | 0.845 | 1.109 | 1.346 | 1.533 | 1.908 | 2.191 | 3.048 | 3.793 | 4.803 | 5.713 |
| 50-2227 | 0.592 | 0.717 | 0.834 | 0.940 | 1.210 | 1.435 | 2.039 | 2.544 | 3.255 | 3.971 |
| 50-2247 | 0.203 | 0.238 | 0.269 | 0.293 | 0.337 | 0.371 | 0.498 | 0.622 | 0.797 | 0.953 |
| 50-2339 | 0.274 | 0.334 | 0.386 | 0.423 | 0.481 | 0.519 | 0.636 | 0.734 | 0.868 | 0.998 |
| 50-2350 | 0.274 | 0.320 | 0.362 | 0.393 | 0.453 | 0.496 | 0.617 | 0.717 | 0.855 | 0.988 |
| 50-2352 | 0.253 | 0.304 | 0.349 | 0.378 | 0.419 | 0.446 | 0.543 | 0.631 | 0.749 | 0.846 |
| 50-2457 | 0.260 | 0.332 | 0.396 | 0.441 | 0.511 | 0.563 | 0.762 | 0.958 | 1.229 | 1.460 |
| 50-2568 | 0.291 | 0.346 | 0.394 | 0.431 | 0.499 | 0.548 | 0.699 | 0.829 | 1.007 | 1.173 |
| 50-2587 | 0.601 | 0.777 | 0.933 | 1.052 | 1.278 | 1.438 | 1.890 | 2.260 | 2.745 | 3.174 |
| 50-2607 | 0.199 | 0.219 | 0.238 | 0.253 | 0.289 | 0.319 | 0.416 | 0.506 | 0.626 | 0.727 |
| 50-2707 | 0.270 | 0.342 | 0.404 | 0.441 | 0.481 | 0.508 | 0.631 | 0.760 | 0.944 | 1.101 |
| 50-2725 | 0.184 | 0.207 | 0.228 | 0.246 | 0.283 | 0.313 | 0.408 | 0.496 | 0.612 | 0.708 |
| 50-2730 | 0.266 | 0.303 | 0.336 | 0.362 | 0.412 | 0.452 | 0.592 | 0.728 | 0.914 | 1.074 |
| 50-2737 | 0.234 | 0.270 | 0.302 | 0.328 | 0.378 | 0.416 | 0.544 | 0.661 | 0.826 | 0.982 |
| 50-2770 | 0.569 | 0.749 | 0.910 | 1.036 | 1.286 | 1.470 | 2.004 | 2.454 | 3.036 | 3.527 |
| 50-2785 | 0.727 | 0.844 | 0.956 | 1.059 | 1.333 | 1.570 | 2.250 | 2.848 | 3.676 | 4.449 |
| 50-2820 | 0.250 | 0.285 | 0.317 | 0.344 | 0.405 | 0.454 | 0.604 | 0.738 | 0.916 | 1.070 |
| 50-2825 | 0.233 | 0.276 | 0.314 | 0.346 | 0.417 | 0.473 | 0.643 | 0.793 | 0.990 | 1.151 |
| 50-2952 | 0.290 | 0.340 | 0.384 | 0.416 | 0.474 | 0.517 | 0.653 | 0.775 | 0.952 | 1.135 |
| 50-2968 | 0.296 | 0.338 | 0.375 | 0.400 | 0.439 | 0.466 | 0.566 | 0.660 | 0.802 | 0.951 |
| 50-2988 | 0.293 | 0.346 | 0.393 | 0.431 | 0.509 | 0.569 | 0.745 | 0.896 | 1.128 | 1.406 |
| 50-3009 | 0.308 | 0.339 | 0.368 | 0.395 | 0.469 | 0.533 | 0.708 | 0.859 | 1.060 | 1.240 |
| 50-3072 | 0.384 | 0.458 | 0.527 | 0.585 | 0.718 | 0.829 | 1.190 | 1.526 | 1.979 | 2.356 |
| 50-3082 | 0.203 | 0.220 | 0.236 | 0.251 | 0.293 | 0.329 | 0.421 | 0.497 | 0.607 | 0.723 |
| 50-3085 | 0.230 | 0.278 | 0.321 | 0.356 | 0.426 | 0.481 | 0.649 | 0.798 | 1.008 | 1.209 |
| 50-3160 | 0.318 | 0.418 | 0.504 | 0.558 | 0.626 | 0.671 | 0.855 | 1.037 | 1.293 | 1.521 |
| 50-3163 | 0.264 | 0.292 | 0.318 | 0.343 | 0.415 | 0.477 | 0.642 | 0.782 | 0.964 | 1.120 |
| 50-3196 | 0.233 | 0.274 | 0.312 | 0.344 | 0.415 | 0.467 | 0.593 | 0.690 | 0.825 | 0.972 |
| 50-3198 | 0.392 | 0.492 | 0.581 | 0.650 | 0.782 | 0.886 | 1.262 | 1.627 | 2.134 | 2.569 |
| 50-3205 | 0.211 | 0.242 | 0.269 | 0.290 | 0.324 | 0.350 | 0.431 | 0.502 | 0.625 | 0.801 |
| 50-3212 | 0.226 | 0.246 | 0.264 | 0.280 | 0.317 | 0.351 | 0.478 | 0.609 | 0.790 | 0.935 |
| 50-3226 | 0.315 | 0.346 | 0.375 | 0.401 | 0.464 | 0.516 | 0.675 | 0.819 | 1.003 | 1.146 |
| 50-3275 | 0.295 | 0.365 | 0.426 | 0.468 | 0.528 | 0.570 | 0.727 | 0.876 | 1.085 | 1.270 |
| 50-3294 | 0.405 | 0.524 | 0.633 | 0.723 | 0.918 | 1.071 | 1.516 | 1.899 | 2.444 | 2.997 |
| 50-3299 | 0.353 | 0.416 | 0.473 | 0.515 | 0.590 | 0.646 | 0.850 | 1.044 | 1.323 | 1.585 |
| 50-3454 | 0.343 | 0.427 | 0.504 | 0.569 | 0.716 | 0.833 | 1.168 | 1.454 | 1.867 | 2.296 |
| 50-3465 | 0.215 | 0.239 | 0.260 | 0.276 | 0.306 | 0.330 | 0.409 | 0.483 | 0.589 | 0.688 |
| 50-3475 | 0.372 | 0.457 | 0.534 | 0.598 | 0.737 | 0.847 | 1.179 | 1.470 | 1.904 | 2.375 |
| 50-3490 | 0.609 | 0.770 | 0.917 | 1.038 | 1.302 | 1.502 | 2.044 | 2.488 | 3.099 | 3.698 |
| 50-3500 | 0.545 | 0.687 | 0.816 | 0.922 | 1.155 | 1.329 | 1.791 | 2.162 | 2.685 | 3.231 |
| 50-3504 | 0.596 | 0.724 | 0.842 | 0.940 | 1.163 | 1.335 | 1.799 | 2.181 | 2.713 | 3.249 |
| 50-3530 | 0.483 | 0.575 | 0.658 | 0.726 | 0.868 | 0.980 | 1.336 | 1.658 | 2.062 | 2.357 |
| 50-3573 | 0.518 | 0.640 | 0.746 | 0.816 | 0.910 | 0.975 | 1.241 | 1.506 | 1.865 | 2.151 |
| 50-3585 | 0.298 | 0.359 | 0.413 | 0.451 | 0.512 | 0.556 | 0.699 | 0.827 | 1.020 | 1.232 |
| 50-3605 | 0.634 | 0.774 | 0.906 | 1.025 | 1.328 | 1.591 | 2.420 | 3.187 | 4.200 | 5.010 |
| 50-3655 | 0.286 | 0.331 | 0.370 | 0.400 | 0.450 | 0.490 | 0.645 | 0.804 | 1.025 | 1.208 |
| 50-3665 | 0.312 | 0.362 | 0.406 | 0.442 | 0.515 | 0.574 | 0.772 | 0.958 | 1.214 | 1.436 |
| 50-3672 | 0.334 | 0.394 | 0.449 | 0.493 | 0.582 | 0.653 | 0.892 | 1.116 | 1.414 | 1.658 |
| 50-3682 | 0.302 | 0.345 | 0.385 | 0.417 | 0.481 | 0.533 | 0.721 | 0.905 | 1.147 | 1.327 |
| 50-3695 | 0.399 | 0.500 | 0.590 | 0.662 | 0.800 | 0.908 | 1.265 | 1.595 | 2.076 | 2.557 |
| 50-3720 | 0.388 | 0.432 | 0.471 | 0.500 | 0.551 | 0.591 | 0.763 | 0.946 | 1.203 | 1.411 |
| 50-3765 | 0.383 | 0.424 | 0.461 | 0.492 | 0.561 | 0.614 | 0.758 | 0.877 | 1.027 | 1.149 |
| 50-3905 | 0.344 | 0.419 | 0.486 | 0.534 | 0.614 | 0.674 | 0.901 | 1.122 | 1.411 | 1.625 |
| 50-3910 | 0.364 | 0.456 | 0.536 | 0.592 | 0.675 | 0.733 | 0.937 | 1.124 | 1.352 | 1.505 |
| 50-3933 | 0.381 | 0.473 | 0.555 | 0.616 | 0.725 | 0.805 | 1.071 | 1.312 | 1.628 | 1.884 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-11

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-4094 | 0.547 | 0.661 | 0.765 | 0.852 | 1.045 | 1.204 | 1.722 | 2.205 | 2.933 | 3.707 |
| 50-4100 | 0.376 | 0.449 | 0.516 | 0.572 | 0.701 | 0.807 | 1.132 | 1.423 | 1.876 | 2.407 |
| 50-4103 | 0.529 | 0.633 | 0.729 | 0.812 | 1.005 | 1.171 | 1.723 | 2.251 | 3.037 | 3.839 |
| 50-4155 | 0.387 | 0.463 | 0.534 | 0.596 | 0.755 | 0.885 | 1.239 | 1.537 | 1.925 | 2.258 |
| 50-4425 | 0.259 | 0.311 | 0.358 | 0.396 | 0.479 | 0.537 | 0.670 | 0.770 | 0.899 | 1.025 |
| 50-4546 | 0.366 | 0.419 | 0.467 | 0.506 | 0.590 | 0.652 | 0.809 | 0.932 | 1.092 | 1.236 |
| 50-4550 | 0.304 | 0.367 | 0.424 | 0.469 | 0.561 | 0.625 | 0.784 | 0.905 | 1.072 | 1.252 |
| 50-4555 | 0.380 | 0.482 | 0.570 | 0.630 | 0.718 | 0.780 | 1.018 | 1.249 | 1.543 | 1.752 |
| 50-4590 | 0.846 | 1.046 | 1.226 | 1.372 | 1.670 | 1.906 | 2.676 | 3.381 | 4.365 | 5.264 |
| 50-4621 | 0.295 | 0.377 | 0.450 | 0.501 | 0.589 | 0.648 | 0.812 | 0.942 | 1.154 | 1.455 |
| 50-4766 | 0.217 | 0.267 | 0.311 | 0.343 | 0.399 | 0.442 | 0.612 | 0.783 | 1.020 | 1.216 |
| 50-4812 | 0.395 | 0.510 | 0.610 | 0.681 | 0.789 | 0.870 | 1.191 | 1.516 | 1.973 | 2.363 |
| 50-4964 | 0.318 | 0.404 | 0.480 | 0.536 | 0.635 | 0.704 | 0.903 | 1.069 | 1.288 | 1.485 |
| 50-4988 | 0.520 | 0.662 | 0.786 | 0.867 | 0.973 | 1.048 | 1.362 | 1.682 | 2.148 | 2.574 |
| 50-4991 | 0.466 | 0.598 | 0.714 | 0.790 | 0.898 | 0.973 | 1.252 | 1.518 | 1.905 | 2.283 |
| 50-5076 | 0.173 | 0.212 | 0.246 | 0.272 | 0.321 | 0.359 | 0.486 | 0.605 | 0.765 | 0.898 |
| 50-5136 | 0.144 | 0.152 | 0.159 | 0.167 | 0.189 | 0.209 | 0.258 | 0.297 | 0.355 | 0.421 |
| 50-5318 | 0.267 | 0.310 | 0.348 | 0.375 | 0.418 | 0.449 | 0.564 | 0.674 | 0.837 | 1.000 |
| 50-5397 | 0.232 | 0.245 | 0.256 | 0.268 | 0.299 | 0.329 | 0.430 | 0.532 | 0.681 | 0.823 |
| 50-5454 | 0.669 | 0.919 | 1.146 | 1.331 | 1.713 | 2.034 | 3.300 | 4.608 | 6.266 | 7.349 |
| 50-5464 | 0.267 | 0.316 | 0.359 | 0.392 | 0.447 | 0.489 | 0.638 | 0.780 | 0.973 | 1.137 |
| 50-5499 | 0.363 | 0.430 | 0.494 | 0.552 | 0.699 | 0.823 | 1.176 | 1.483 | 1.891 | 2.241 |
| 50-5519 | 1.425 | 1.656 | 1.867 | 2.041 | 2.406 | 2.711 | 3.801 | 4.874 | 6.426 | 7.873 |
| 50-5534 | 0.223 | 0.258 | 0.291 | 0.318 | 0.381 | 0.430 | 0.554 | 0.653 | 0.802 | 0.985 |
| 50-5604 | 0.821 | 1.159 | 1.461 | 1.693 | 2.121 | 2.466 | 3.830 | 5.231 | 7.192 | 8.831 |
| 50-5607 | 0.275 | 0.359 | 0.434 | 0.496 | 0.624 | 0.722 | 1.008 | 1.252 | 1.595 | 1.933 |
| 50-5644 | 0.334 | 0.385 | 0.432 | 0.472 | 0.566 | 0.639 | 0.836 | 0.997 | 1.210 | 1.401 |
| 50-5733 | 0.241 | 0.281 | 0.317 | 0.344 | 0.394 | 0.433 | 0.570 | 0.700 | 0.876 | 1.022 |
| 50-5757 | 0.288 | 0.360 | 0.423 | 0.467 | 0.536 | 0.587 | 0.797 | 1.012 | 1.274 | 1.433 |
| 50-5769 | 0.236 | 0.263 | 0.289 | 0.311 | 0.367 | 0.415 | 0.554 | 0.676 | 0.858 | 1.053 |
| 50-5778 | 0.348 | 0.402 | 0.449 | 0.482 | 0.532 | 0.566 | 0.684 | 0.789 | 0.960 | 1.179 |
| 50-5810 | 0.248 | 0.299 | 0.345 | 0.382 | 0.458 | 0.517 | 0.709 | 0.886 | 1.088 | 1.204 |
| 50-5880 | 0.298 | 0.360 | 0.416 | 0.456 | 0.527 | 0.577 | 0.726 | 0.852 | 1.043 | 1.266 |
| 50-5881 | 0.287 | 0.317 | 0.346 | 0.372 | 0.436 | 0.491 | 0.652 | 0.794 | 0.999 | 1.203 |
| 50-5882 | 0.302 | 0.347 | 0.388 | 0.418 | 0.470 | 0.510 | 0.665 | 0.818 | 1.020 | 1.169 |
| 50-5894 | 0.535 | 0.639 | 0.732 | 0.808 | 0.973 | 1.093 | 1.396 | 1.636 | 1.933 | 2.179 |
| 50-5898 | 0.503 | 0.626 | 0.737 | 0.827 | 1.014 | 1.152 | 1.511 | 1.796 | 2.211 | 2.686 |
| 50-6058 | 0.285 | 0.332 | 0.375 | 0.411 | 0.494 | 0.560 | 0.753 | 0.919 | 1.138 | 1.326 |
| 50-6147 | 0.268 | 0.334 | 0.392 | 0.432 | 0.495 | 0.540 | 0.712 | 0.878 | 1.062 | 1.152 |
| 50-6270 | 0.252 | 0.277 | 0.301 | 0.321 | 0.367 | 0.405 | 0.526 | 0.638 | 0.805 | 0.983 |
| 50-6309 | 0.294 | 0.356 | 0.411 | 0.451 | 0.521 | 0.570 | 0.716 | 0.840 | 1.014 | 1.191 |
| 50-6441 | 0.330 | 0.377 | 0.420 | 0.455 | 0.528 | 0.585 | 0.753 | 0.898 | 1.094 | 1.271 |
| 50-6496 | 0.268 | 0.324 | 0.374 | 0.412 | 0.483 | 0.537 | 0.733 | 0.921 | 1.173 | 1.375 |
| 50-6562 | 0.644 | 0.835 | 1.009 | 1.152 | 1.453 | 1.702 | 2.584 | 3.443 | 4.560 | 5.386 |
| 50-6581 | 0.253 | 0.297 | 0.335 | 0.362 | 0.402 | 0.431 | 0.539 | 0.642 | 0.784 | 0.903 |
| 50-6586 | 0.294 | 0.331 | 0.365 | 0.392 | 0.446 | 0.489 | 0.648 | 0.804 | 1.004 | 1.144 |
| 50-6656 | 0.236 | 0.275 | 0.311 | 0.341 | 0.407 | 0.461 | 0.631 | 0.786 | 0.994 | 1.169 |
| 50-6727 | 0.257 | 0.301 | 0.338 | 0.360 | 0.379 | 0.392 | 0.480 | 0.592 | 0.755 | 0.879 |
| 50-6760 | 0.344 | 0.391 | 0.436 | 0.479 | 0.596 | 0.695 | 0.956 | 1.175 | 1.449 | 1.667 |
| 50-6853 | 0.535 | 0.695 | 0.834 | 0.929 | 1.067 | 1.164 | 1.518 | 1.851 | 2.323 | 2.759 |
| 50-6870 | 0.251 | 0.293 | 0.331 | 0.359 | 0.409 | 0.446 | 0.578 | 0.704 | 0.873 | 1.012 |
| 50-6875 | 0.405 | 0.456 | 0.502 | 0.542 | 0.636 | 0.708 | 0.899 | 1.054 | 1.260 | 1.446 |
| 50-7097 | 0.255 | 0.312 | 0.363 | 0.404 | 0.486 | 0.550 | 0.755 | 0.942 | 1.188 | 1.389 |
| 50-7105 | 0.219 | 0.255 | 0.289 | 0.319 | 0.391 | 0.451 | 0.623 | 0.774 | 0.962 | 1.104 |
| 50-7141 | 1.023 | 1.298 | 1.553 | 1.773 | 2.298 | 2.715 | 3.857 | 4.811 | 6.038 | 7.062 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-12

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-7251 | 0.646 | 0.762 | 0.873 | 0.979 | 1.284 | 1.545 | 2.201 | 2.735 | 3.483 | 4.244 |
| 50-7352 | 0.257 | 0.289 | 0.318 | 0.342 | 0.392 | 0.432 | 0.562 | 0.683 | 0.849 | 0.998 |
| 50-7365 | 0.292 | 0.349 | 0.399 | 0.434 | 0.488 | 0.529 | 0.709 | 0.901 | 1.163 | 1.362 |
| 50-7431 | 0.197 | 0.236 | 0.270 | 0.293 | 0.328 | 0.354 | 0.462 | 0.574 | 0.734 | 0.874 |
| 50-7442 | 0.144 | 0.183 | 0.219 | 0.251 | 0.332 | 0.390 | 0.512 | 0.600 | 0.694 | 0.756 |
| 50-7451 | 0.500 | 0.642 | 0.766 | 0.853 | 0.988 | 1.089 | 1.480 | 1.873 | 2.469 | 3.081 |
| 50-7494 | 0.582 | 0.789 | 0.975 | 1.119 | 1.396 | 1.610 | 2.352 | 3.050 | 3.885 | 4.403 |
| 50-7557 | 0.909 | 1.050 | 1.178 | 1.282 | 1.494 | 1.678 | 2.434 | 3.249 | 4.451 | 5.540 |
| 50-7570 | 0.270 | 0.337 | 0.396 | 0.437 | 0.500 | 0.545 | 0.702 | 0.849 | 1.050 | 1.223 |
| 50-7700 | 0.278 | 0.321 | 0.359 | 0.381 | 0.405 | 0.422 | 0.514 | 0.623 | 0.789 | 0.943 |
| 50-7738 | 0.588 | 0.771 | 0.936 | 1.072 | 1.352 | 1.590 | 2.532 | 3.512 | 4.822 | 5.788 |
| 50-7783 | 0.421 | 0.478 | 0.527 | 0.561 | 0.613 | 0.651 | 0.792 | 0.929 | 1.106 | 1.235 |
| 50-7854 | 0.686 | 0.833 | 0.967 | 1.074 | 1.289 | 1.468 | 2.149 | 2.843 | 3.787 | 4.533 |
| 50-7900 | 0.287 | 0.320 | 0.350 | 0.374 | 0.423 | 0.459 | 0.557 | 0.637 | 0.750 | 0.870 |
| 50-7977 | 0.276 | 0.343 | 0.402 | 0.443 | 0.509 | 0.552 | 0.678 | 0.782 | 0.917 | 1.035 |
| 50-8025 | 0.270 | 0.317 | 0.359 | 0.392 | 0.455 | 0.502 | 0.658 | 0.798 | 0.988 | 1.153 |
| 50-8054 | 0.256 | 0.293 | 0.328 | 0.360 | 0.446 | 0.515 | 0.686 | 0.822 | 0.994 | 1.140 |
| 50-8105 | 0.233 | 0.281 | 0.326 | 0.362 | 0.437 | 0.496 | 0.681 | 0.847 | 1.042 | 1.164 |
| 50-8118 | 0.193 | 0.233 | 0.270 | 0.300 | 0.366 | 0.418 | 0.572 | 0.706 | 0.894 | 1.074 |
| 50-8140 | 0.310 | 0.382 | 0.444 | 0.482 | 0.526 | 0.556 | 0.691 | 0.832 | 1.029 | 1.191 |
| 50-8183 | 0.392 | 0.480 | 0.562 | 0.634 | 0.815 | 0.949 | 1.229 | 1.431 | 1.693 | 1.954 |
| 50-8355 | 0.500 | 0.586 | 0.666 | 0.736 | 0.904 | 1.040 | 1.421 | 1.747 | 2.149 | 2.450 |
| 50-8371 | 0.877 | 1.056 | 1.217 | 1.341 | 1.571 | 1.754 | 2.474 | 3.207 | 4.113 | 4.681 |
| 50-8375 | 0.964 | 1.191 | 1.393 | 1.541 | 1.801 | 1.994 | 2.664 | 3.289 | 4.132 | 4.833 |
| 50-8377 | 0.828 | 0.953 | 1.066 | 1.157 | 1.339 | 1.481 | 1.960 | 2.404 | 2.945 | 3.303 |
| 50-8409 | 0.309 | 0.363 | 0.412 | 0.447 | 0.508 | 0.553 | 0.713 | 0.862 | 1.048 | 1.177 |
| 50-8419 | 0.417 | 0.468 | 0.516 | 0.559 | 0.668 | 0.758 | 0.992 | 1.185 | 1.462 | 1.756 |
| 50-8437 | 0.182 | 0.195 | 0.208 | 0.220 | 0.256 | 0.289 | 0.392 | 0.487 | 0.614 | 0.716 |
| 50-8494 | 0.615 | 0.725 | 0.826 | 0.911 | 1.098 | 1.255 | 1.812 | 2.356 | 3.085 | 3.656 |
| 50-8503 | 0.638 | 0.748 | 0.849 | 0.935 | 1.131 | 1.298 | 1.871 | 2.424 | 3.170 | 3.773 |
| 50-8512 | 0.510 | 0.595 | 0.669 | 0.714 | 0.764 | 0.801 | 1.019 | 1.290 | 1.683 | 1.992 |
| 50-8525 | 0.488 | 0.594 | 0.690 | 0.765 | 0.916 | 1.027 | 1.338 | 1.593 | 1.937 | 2.258 |
| 50-8536 | 0.416 | 0.505 | 0.583 | 0.643 | 0.756 | 0.836 | 1.063 | 1.250 | 1.513 | 1.782 |
| 50-8547 | 0.280 | 0.325 | 0.366 | 0.400 | 0.474 | 0.532 | 0.701 | 0.847 | 1.040 | 1.211 |
| 50-8584 | 0.853 | 1.130 | 1.383 | 1.594 | 2.062 | 2.429 | 3.454 | 4.313 | 5.654 | 7.321 |
| 50-8594 | 0.233 | 0.259 | 0.283 | 0.301 | 0.331 | 0.355 | 0.457 | 0.566 | 0.732 | 0.899 |
| 50-8625 | 0.211 | 0.244 | 0.273 | 0.297 | 0.348 | 0.388 | 0.509 | 0.616 | 0.780 | 0.973 |
| 50-8666 | 0.313 | 0.375 | 0.432 | 0.477 | 0.573 | 0.645 | 0.853 | 1.028 | 1.265 | 1.484 |
| 50-8811 | 0.332 | 0.390 | 0.440 | 0.476 | 0.531 | 0.572 | 0.721 | 0.864 | 1.081 | 1.305 |
| 50-8882 | 0.361 | 0.451 | 0.532 | 0.595 | 0.720 | 0.814 | 1.093 | 1.332 | 1.662 | 1.974 |
| 50-8915 | 0.286 | 0.348 | 0.403 | 0.441 | 0.499 | 0.540 | 0.688 | 0.828 | 1.023 | 1.196 |
| 50-8976 | 0.417 | 0.517 | 0.607 | 0.679 | 0.826 | 0.932 | 1.200 | 1.407 | 1.706 | 2.040 |
| 50-8987 | 0.461 | 0.501 | 0.536 | 0.563 | 0.613 | 0.649 | 0.762 | 0.862 | 0.991 | 1.098 |
| 50-9014 | 0.298 | 0.337 | 0.373 | 0.406 | 0.489 | 0.557 | 0.738 | 0.889 | 1.090 | 1.275 |
| 50-9035 | 0.221 | 0.261 | 0.298 | 0.328 | 0.393 | 0.443 | 0.581 | 0.696 | 0.872 | 1.088 |
| 50-9102 | 0.226 | 0.268 | 0.305 | 0.330 | 0.367 | 0.394 | 0.515 | 0.643 | 0.816 | 0.943 |
| 50-9121 | 0.490 | 0.629 | 0.755 | 0.859 | 1.084 | 1.260 | 1.789 | 2.253 | 2.852 | 3.336 |
| 50-9144 | 0.307 | 0.348 | 0.386 | 0.420 | 0.504 | 0.577 | 0.807 | 1.022 | 1.304 | 1.530 |
| 50-9249 | 0.262 | 0.315 | 0.363 | 0.401 | 0.476 | 0.535 | 0.742 | 0.938 | 1.198 | 1.404 |
| 50-9313 | 0.295 | 0.329 | 0.358 | 0.379 | 0.410 | 0.433 | 0.529 | 0.630 | 0.779 | 0.918 |
| 50-9385 | 0.300 | 0.342 | 0.378 | 0.401 | 0.426 | 0.444 | 0.512 | 0.579 | 0.679 | 0.779 |
| 50-9399 | 0.444 | 0.602 | 0.744 | 0.857 | 1.088 | 1.265 | 1.815 | 2.301 | 2.946 | 3.494 |
| 50-9410 | 0.537 | 0.635 | 0.725 | 0.801 | 0.975 | 1.104 | 1.409 | 1.640 | 1.967 | 2.333 |
| 50-9421 | 0.198 | 0.234 | 0.267 | 0.295 | 0.354 | 0.398 | 0.515 | 0.610 | 0.730 | 0.830 |
| 50-9460 | 0.812 | 0.978 | 1.128 | 1.245 | 1.478 | 1.657 | 2.253 | 2.800 | 3.497 | 4.018 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-13

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-9489 | 0.293 | 0.366 | 0.430 | 0.475 | 0.545 | 0.593 | 0.749 | 0.885 | 1.092 | 1.323 |
| 50-9511 | 0.527 | 0.651 | 0.759 | 0.832 | 0.935 | 1.009 | 1.303 | 1.595 | 2.027 | 2.447 |
| 50-9539 | 0.399 | 0.424 | 0.445 | 0.455 | 0.459 | 0.461 | 0.483 | 0.517 | 0.573 | 0.631 |
| 50-9564 | 0.232 | 0.275 | 0.313 | 0.342 | 0.398 | 0.442 | 0.608 | 0.773 | 0.996 | 1.171 |
| 50-9641 | 0.346 | 0.395 | 0.437 | 0.466 | 0.508 | 0.538 | 0.650 | 0.758 | 0.912 | 1.054 |
| 50-9686 | 0.460 | 0.640 | 0.799 | 0.914 | 1.114 | 1.254 | 1.671 | 2.020 | 2.532 | 3.085 |
| 50-9702 | 0.688 | 0.837 | 0.978 | 1.106 | 1.433 | 1.713 | 2.536 | 3.267 | 4.254 | 5.121 |
| 50-9739 | 0.237 | 0.286 | 0.330 | 0.363 | 0.420 | 0.465 | 0.626 | 0.782 | 0.998 | 1.183 |
| 50-9759 | 0.254 | 0.306 | 0.351 | 0.385 | 0.442 | 0.485 | 0.639 | 0.785 | 0.984 | 1.148 |
| 50-9765 | 0.259 | 0.325 | 0.384 | 0.427 | 0.504 | 0.559 | 0.744 | 0.910 | 1.129 | 1.306 |
| 50-9790 | 0.365 | 0.438 | 0.503 | 0.555 | 0.659 | 0.735 | 0.935 | 1.095 | 1.318 | 1.548 |
| 50-9793 | 0.262 | 0.311 | 0.355 | 0.388 | 0.449 | 0.491 | 0.602 | 0.689 | 0.808 | 0.929 |
| 50-9829 | 0.937 | 1.334 | 1.691 | 1.976 | 2.541 | 2.997 | 4.670 | 6.316 | 8.505 | 10.188 |
| 50-9861 | 0.385 | 0.448 | 0.506 | 0.552 | 0.645 | 0.714 | 0.907 | 1.067 | 1.283 | 1.485 |
| 50-9869 | 0.260 | 0.312 | 0.357 | 0.389 | 0.443 | 0.482 | 0.621 | 0.751 | 0.933 | 1.097 |
| 50-9883 | 0.432 | 0.459 | 0.486 | 0.512 | 0.584 | 0.651 | 0.864 | 1.067 | 1.358 | 1.629 |
| 50-9919 | 0.506 | 0.581 | 0.655 | 0.729 | 0.961 | 1.170 | 1.691 | 2.122 | 2.699 | 3.231 |
| 50-9930 | 0.692 | 0.841 | 0.978 | 1.095 | 1.362 | 1.584 | 2.313 | 2.995 | 3.863 | 4.497 |
| 50-9941 | 0.976 | 1.157 | 1.326 | 1.475 | 1.832 | 2.137 | 3.133 | 4.067 | 5.261 | 6.139 |
| 55-0064 | 0.636 | 0.798 | 0.943 | 1.057 | 1.278 | 1.450 | 2.050 | 2.618 | 3.334 | 3.841 |
| 55-0079 | 0.186 | 0.219 | 0.249 | 0.273 | 0.327 | 0.368 | 0.488 | 0.589 | 0.741 | 0.914 |
| 55-0080 | 0.462 | 0.565 | 0.661 | 0.745 | 0.950 | 1.120 | 1.620 | 2.059 | 2.629 | 3.095 |
| 55-0087 | 0.279 | 0.307 | 0.334 | 0.361 | 0.442 | 0.510 | 0.657 | 0.768 | 0.918 | 1.072 |
| 55-0096 | 0.254 | 0.277 | 0.299 | 0.321 | 0.390 | 0.451 | 0.597 | 0.715 | 0.873 | 1.027 |
| 55-0164 | 0.134 | 0.145 | 0.156 | 0.165 | 0.188 | 0.208 | 0.278 | 0.347 | 0.434 | 0.494 |
| 80-0100 | 0.381 | 0.417 | 0.450 | 0.478 | 0.537 | 0.586 | 0.752 | 0.910 | 1.124 | 1.304 |
| 80-0120 | 0.307 | 0.355 | 0.398 | 0.427 | 0.472 | 0.504 | 0.619 | 0.727 | 0.904 | 1.128 |
| 80-0140 | 0.231 | 0.253 | 0.272 | 0.289 | 0.328 | 0.361 | 0.477 | 0.589 | 0.735 | 0.841 |
| 80-0160 | 0.211 | 0.224 | 0.238 | 0.251 | 0.293 | 0.330 | 0.415 | 0.482 | 0.583 | 0.707 |
| 80-0200 | 0.247 | 0.273 | 0.297 | 0.318 | 0.365 | 0.403 | 0.524 | 0.634 | 0.780 | 0.898 |
| 80-0220 | 0.976 | 1.132 | 1.286 | 1.435 | 1.868 | 2.264 | 3.399 | 4.413 | 5.747 | 6.844 |
| 80-0240 | 0.297 | 0.327 | 0.359 | 0.393 | 0.519 | 0.628 | 0.815 | 0.941 | 1.118 | 1.328 |
| 80-0260 | 0.226 | 0.256 | 0.282 | 0.304 | 0.350 | 0.387 | 0.508 | 0.620 | 0.755 | 0.842 |
| 80-0340 | 0.258 | 0.302 | 0.340 | 0.368 | 0.410 | 0.443 | 0.590 | 0.752 | 0.979 | 1.164 |
| 80-0425 | 0.327 | 0.400 | 0.465 | 0.511 | 0.593 | 0.648 | 0.797 | 0.915 | 1.094 | 1.317 |
| 80-0440 | 0.215 | 0.234 | 0.251 | 0.267 | 0.310 | 0.345 | 0.437 | 0.511 | 0.607 | 0.687 |
| 80-0460 | 0.320 | 0.403 | 0.473 | 0.516 | 0.561 | 0.590 | 0.713 | 0.835 | 1.039 | 1.297 |
| 80-0540 | 0.196 | 0.236 | 0.272 | 0.299 | 0.345 | 0.380 | 0.520 | 0.658 | 0.809 | 0.875 |
| 80-0560 | 0.315 | 0.343 | 0.368 | 0.389 | 0.437 | 0.475 | 0.583 | 0.676 | 0.823 | 1.010 |
| 80-0640 | 0.284 | 0.326 | 0.362 | 0.387 | 0.426 | 0.456 | 0.606 | 0.780 | 1.020 | 1.199 |
| 80-0780 | 0.304 | 0.370 | 0.427 | 0.465 | 0.517 | 0.555 | 0.703 | 0.850 | 1.072 | 1.296 |
| 80-0820 | 0.299 | 0.343 | 0.383 | 0.415 | 0.479 | 0.530 | 0.710 | 0.881 | 1.097 | 1.248 |
| 80-0860 | 0.348 | 0.394 | 0.435 | 0.465 | 0.520 | 0.561 | 0.690 | 0.805 | 0.959 | 1.091 |
| 80-0900 | 0.282 | 0.343 | 0.397 | 0.434 | 0.492 | 0.528 | 0.620 | 0.689 | 0.786 | 0.893 |
| 80-0920 | 0.697 | 0.829 | 0.945 | 1.024 | 1.144 | 1.226 | 1.524 | 1.800 | 2.124 | 2.320 |
| 80-0940 | 0.227 | 0.249 | 0.270 | 0.288 | 0.331 | 0.364 | 0.445 | 0.509 | 0.600 | 0.702 |
| 80-1020 | 0.184 | 0.217 | 0.247 | 0.269 | 0.309 | 0.339 | 0.445 | 0.545 | 0.690 | 0.830 |
| 80-1060 | 0.210 | 0.226 | 0.242 | 0.258 | 0.301 | 0.338 | 0.430 | 0.504 | 0.614 | 0.738 |
| 80-1100 | 0.212 | 0.231 | 0.249 | 0.266 | 0.318 | 0.363 | 0.463 | 0.541 | 0.649 | 0.762 |
| 80-1120 | 0.330 | 0.365 | 0.398 | 0.430 | 0.525 | 0.598 | 0.736 | 0.831 | 0.961 | 1.108 |
| 80-1140 | 0.383 | 0.439 | 0.488 | 0.524 | 0.584 | 0.628 | 0.787 | 0.938 | 1.130 | 1.269 |
| 80-1180 | 0.503 | 0.627 | 0.742 | 0.841 | 1.070 | 1.257 | 1.820 | 2.318 | 2.964 | 3.484 |
| 80-1220 | 0.257 | 0.285 | 0.310 | 0.334 | 0.394 | 0.446 | 0.596 | 0.727 | 0.912 | 1.089 |
| 80-1240 | 0.372 | 0.421 | 0.466 | 0.503 | 0.584 | 0.650 | 0.883 | 1.107 | 1.367 | 1.511 |
| 80-1280 | 0.204 | 0.233 | 0.259 | 0.278 | 0.311 | 0.337 | 0.450 | 0.574 | 0.759 | 0.929 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-14

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $80-1300$ | 0.463 | 0.537 | 0.607 | 0.669 | 0.825 | 0.956 | 1.336 | 1.670 | 2.150 | 2.637 |
| $80-1320$ | 0.243 | 0.243 | 0.243 | 0.244 | 0.275 | 0.322 | 0.432 | 0.530 | 0.672 | 0.812 |
| $80-1340$ | 0.246 | 0.275 | 0.302 | 0.328 | 0.401 | 0.464 | 0.625 | 0.757 | 0.936 | 1.100 |
| $80-1360$ | 0.217 | 0.272 | 0.320 | 0.357 | 0.427 | 0.479 | 0.644 | 0.791 | 1.006 | 1.230 |
| $80-1380$ | 0.830 | 0.933 | 1.028 | 1.105 | 1.271 | 1.399 | 1.783 | 2.118 | 2.544 | 2.878 |
| $80-1400$ | 0.285 | 0.320 | 0.353 | 0.379 | 0.438 | 0.480 | 0.573 | 0.640 | 0.737 | 0.855 |
| $80-1420$ | 0.266 | 0.299 | 0.330 | 0.354 | 0.405 | 0.446 | 0.586 | 0.719 | 0.914 | 1.105 |
| $80-1440$ | 0.243 | 0.279 | 0.314 | 0.348 | 0.452 | 0.540 | 0.753 | 0.925 | 1.117 | 1.241 |
| $80-1460$ | 0.216 | 0.229 | 0.243 | 0.256 | 0.293 | 0.328 | 0.428 | 0.518 | 0.663 | 0.843 |
| $80-1480$ | 0.253 | 0.284 | 0.313 | 0.338 | 0.398 | 0.448 | 0.609 | 0.759 | 0.940 | 1.060 |
| $80-1540$ | 0.184 | 0.215 | 0.243 | 0.267 | 0.320 | 0.361 | 0.469 | 0.558 | 0.677 | 0.790 |
| $80-1740$ | 0.202 | 0.223 | 0.244 | 0.263 | 0.318 | 0.366 | 0.489 | 0.592 | 0.736 | 0.884 |
| $80-1760$ | 0.261 | 0.285 | 0.308 | 0.333 | 0.416 | 0.490 | 0.653 | 0.780 | 0.953 | 1.133 |
| $80-1900$ | 0.224 | 0.244 | 0.263 | 0.278 | 0.315 | 0.346 | 0.451 | 0.552 | 0.692 | 0.813 |
| $80-1940$ | 0.259 | 0.274 | 0.290 | 0.306 | 0.358 | 0.406 | 0.536 | 0.649 | 0.792 | 0.905 |
| $80-1980$ | 0.177 | 0.198 | 0.217 | 0.232 | 0.261 | 0.284 | 0.366 | 0.444 | 0.554 | 0.653 |
| $80-2000$ | 0.347 | 0.395 | 0.438 | 0.471 | 0.533 | 0.583 | 0.761 | 0.934 | 1.176 | 1.389 |
| $80-2040$ | 0.267 | 0.302 | 0.336 | 0.367 | 0.458 | 0.535 | 0.726 | 0.880 | 1.092 | 1.303 |
| $80-2080$ | 0.281 | 0.340 | 0.390 | 0.424 | 0.469 | 0.502 | 0.641 | 0.786 | 0.967 | 1.082 |
| $80-2120$ | 0.277 | 0.340 | 0.396 | 0.440 | 0.529 | 0.591 | 0.731 | 0.833 | 0.987 | 1.190 |
| $80-2140$ | 0.320 | 0.372 | 0.420 | 0.460 | 0.552 | 0.621 | 0.805 | 0.956 | 1.133 | 1.256 |
| $80-2160$ | 0.252 | 0.288 | 0.320 | 0.344 | 0.387 | 0.421 | 0.564 | 0.717 | 0.927 | 1.091 |
| $80-2320$ | 0.304 | 0.363 | 0.415 | 0.450 | 0.502 | 0.540 | 0.681 | 0.818 | 1.009 | 1.177 |
| $80-2340$ | 0.302 | 0.344 | 0.381 | 0.404 | 0.435 | 0.459 | 0.586 | 0.740 | 0.958 | 1.123 |
| $80-2380$ | 0.255 | 0.295 | 0.331 | 0.360 | 0.425 | 0.472 | 0.591 | 0.684 | 0.812 | 0.946 |
| $80-2440$ | 0.260 | 0.311 | 0.355 | 0.386 | 0.437 | 0.473 | 0.596 | 0.707 | 0.873 | 1.046 |
| $80-2560$ | 0.241 | 0.272 | 0.301 | 0.325 | 0.379 | 0.420 | 0.522 | 0.602 | 0.709 | 0.812 |
| $80-2620$ | 0.198 | 0.223 | 0.246 | 0.263 | 0.292 | 0.313 | 0.376 | 0.429 | 0.518 | 0.652 |
| $80-2640$ | 0.294 | 0.321 | 0.346 | 0.369 | 0.427 | 0.479 | 0.643 | 0.796 | 1.017 | 1.230 |
| $80-2700$ | 0.565 | 0.630 | 0.696 | 0.764 | 0.985 | 1.194 | 1.753 | 2.240 | 2.848 | 3.305 |
| $90-0001$ | 0.424 | 0.588 | 0.733 | 0.839 | 1.021 | 1.152 | 1.568 | 1.933 | 2.452 | 2.963 |
| 8 |  |  |  |  |  |  |  |  |  |  |

Table A.4.3. $\lambda_{3}$ moments.

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $10-0208$ | 0.096 | 0.114 | 0.129 | 0.140 | 0.164 | 0.177 | 0.194 | 0.205 | 0.216 | 0.229 |
| $10-0215$ | 0.070 | 0.082 | 0.093 | 0.100 | 0.114 | 0.122 | 0.134 | 0.141 | 0.152 | 0.168 |
| $10-0236$ | 0.054 | 0.063 | 0.071 | 0.078 | 0.100 | 0.113 | 0.118 | 0.120 | 0.123 | 0.129 |
| $10-0238$ | 0.060 | 0.062 | 0.063 | 0.065 | 0.071 | 0.075 | 0.077 | 0.079 | 0.080 | 0.082 |
| $10-0240$ | 0.110 | 0.124 | 0.138 | 0.152 | 0.203 | 0.244 | 0.300 | 0.333 | 0.387 | 0.478 |
| $10-0241$ | 0.130 | 0.161 | 0.189 | 0.213 | 0.274 | 0.316 | 0.396 | 0.452 | 0.503 | 0.528 |
| $10-0946$ | 0.125 | 0.129 | 0.135 | 0.142 | 0.185 | 0.220 | 0.236 | 0.244 | 0.256 | 0.286 |
| $10-0947$ | 0.087 | 0.095 | 0.101 | 0.105 | 0.109 | 0.110 | 0.112 | 0.113 | 0.115 | 0.120 |
| $10-0948$ | 0.070 | 0.077 | 0.082 | 0.085 | 0.089 | 0.090 | 0.092 | 0.093 | 0.094 | 0.098 |
| $10-0949$ | 0.069 | 0.076 | 0.083 | 0.090 | 0.110 | 0.123 | 0.136 | 0.144 | 0.149 | 0.151 |
| $10-0950$ | 0.092 | 0.092 | 0.092 | 0.092 | 0.102 | 0.116 | 0.136 | 0.150 | 0.165 | 0.174 |
| $10-0951$ | 0.050 | 0.056 | 0.062 | 0.066 | 0.072 | 0.077 | 0.093 | 0.109 | 0.123 | 0.127 |
| $10-0952$ | 0.078 | 0.079 | 0.080 | 0.082 | 0.093 | 0.104 | 0.118 | 0.127 | 0.138 | 0.151 |
| $10-0955$ | 0.102 | 0.107 | 0.113 | 0.120 | 0.148 | 0.172 | 0.206 | 0.228 | 0.254 | 0.280 |
| $10-0956$ | 0.200 | 0.213 | 0.230 | 0.250 | 0.355 | 0.450 | 0.566 | 0.638 | 0.720 | 0.800 |
| $10-0957$ | 0.100 | 0.104 | 0.107 | 0.110 | 0.119 | 0.125 | 0.130 | 0.132 | 0.135 | 0.140 |
| $10-0958$ | 0.075 | 0.089 | 0.101 | 0.109 | 0.122 | 0.129 | 0.145 | 0.155 | 0.169 | 0.183 |
| $10-0959$ | 0.159 | 0.166 | 0.173 | 0.180 | 0.207 | 0.230 | 0.268 | 0.294 | 0.330 | 0.379 |

NOAA Atlas 14 Volume 7 Version 2.0

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10-0961 | 0.035 | 0.040 | 0.044 | 0.047 | 0.054 | 0.057 | 0.059 | 0.060 | 0.062 | 0.066 |
| 10-0962 | 0.064 | 0.080 | 0.094 | 0.103 | 0.117 | 0.125 | 0.141 | 0.152 | 0.165 | 0.177 |
| 10-0964 | 0.203 | 0.230 | 0.254 | 0.274 | 0.313 | 0.346 | 0.478 | 0.615 | 0.766 | 0.831 |
| 10-0966 | 0.054 | 0.066 | 0.076 | 0.085 | 0.107 | 0.120 | 0.129 | 0.134 | 0.140 | 0.150 |
| 10-0967 | 0.110 | 0.125 | 0.139 | 0.149 | 0.170 | 0.180 | 0.189 | 0.194 | 0.200 | 0.211 |
| 10-0968 | 0.133 | 0.146 | 0.158 | 0.164 | 0.168 | 0.171 | 0.186 | 0.202 | 0.215 | 0.215 |
| 10-1002 | 0.090 | 0.101 | 0.110 | 0.117 | 0.130 | 0.136 | 0.144 | 0.148 | 0.155 | 0.169 |
| 10-1003 | 0.099 | 0.115 | 0.130 | 0.140 | 0.158 | 0.172 | 0.216 | 0.256 | 0.312 | 0.366 |
| 10-1037 | 0.265 | 0.318 | 0.367 | 0.411 | 0.521 | 0.602 | 0.773 | 0.896 | 1.045 | 1.176 |
| 10-1064 | 0.207 | 0.230 | 0.253 | 0.276 | 0.347 | 0.400 | 0.480 | 0.531 | 0.600 | 0.690 |
| 10-1094 | 0.051 | 0.071 | 0.089 | 0.100 | 0.115 | 0.124 | 0.148 | 0.166 | 0.186 | 0.200 |
| 10-1291 | 0.058 | 0.072 | 0.083 | 0.092 | 0.107 | 0.114 | 0.115 | 0.116 | 0.117 | 0.122 |
| 10-1444 | 0.072 | 0.081 | 0.090 | 0.096 | 0.109 | 0.118 | 0.147 | 0.172 | 0.203 | 0.226 |
| 10-1449 | 0.152 | 0.177 | 0.199 | 0.219 | 0.268 | 0.305 | 0.400 | 0.478 | 0.546 | 0.568 |
| 10-9909 | 0.053 | 0.063 | 0.071 | 0.076 | 0.086 | 0.091 | 0.102 | 0.109 | 0.118 | 0.126 |
| 21-0115 | 0.038 | 0.039 | 0.040 | 0.041 | 0.046 | 0.050 | 0.054 | 0.056 | 0.060 | 0.067 |
| 21-0160 | 0.064 | 0.071 | 0.079 | 0.085 | 0.103 | 0.114 | 0.130 | 0.139 | 0.150 | 0.160 |
| 21-0163 | 0.069 | 0.077 | 0.085 | 0.091 | 0.108 | 0.120 | 0.140 | 0.152 | 0.171 | 0.196 |
| 21-0182 | 0.034 | 0.041 | 0.048 | 0.053 | 0.064 | 0.070 | 0.075 | 0.077 | 0.080 | 0.084 |
| 21-0200 | 0.050 | 0.058 | 0.064 | 0.069 | 0.079 | 0.084 | 0.089 | 0.092 | 0.095 | 0.100 |
| 21-0330 | 0.125 | 0.160 | 0.190 | 0.211 | 0.243 | 0.261 | 0.296 | 0.319 | 0.351 | 0.391 |
| 21-0402 | 0.027 | 0.027 | 0.028 | 0.029 | 0.035 | 0.040 | 0.044 | 0.047 | 0.050 | 0.053 |
| 21-0446 | 0.145 | 0.174 | 0.203 | 0.232 | 0.331 | 0.400 | 0.458 | 0.488 | 0.530 | 0.600 |
| 21-0468 | 0.097 | 0.107 | 0.115 | 0.121 | 0.136 | 0.143 | 0.146 | 0.148 | 0.150 | 0.157 |
| 21-0560 | 0.041 | 0.042 | 0.042 | 0.043 | 0.045 | 0.046 | 0.048 | 0.050 | 0.052 | 0.055 |
| 21-0630 | 0.072 | 0.080 | 0.087 | 0.092 | 0.099 | 0.103 | 0.108 | 0.111 | 0.115 | 0.120 |
| 21-0679 | 0.050 | 0.053 | 0.056 | 0.059 | 0.072 | 0.080 | 0.083 | 0.084 | 0.085 | 0.088 |
| 21-0685 | 0.080 | 0.088 | 0.095 | 0.100 | 0.107 | 0.110 | 0.115 | 0.118 | 0.120 | 0.121 |
| 21-0794 | 0.043 | 0.049 | 0.054 | 0.057 | 0.064 | 0.067 | 0.072 | 0.074 | 0.077 | 0.080 |
| 21-0805 | 0.092 | 0.096 | 0.100 | 0.103 | 0.114 | 0.120 | 0.124 | 0.126 | 0.127 | 0.128 |
| 21-0907 | 0.043 | 0.047 | 0.050 | 0.053 | 0.061 | 0.066 | 0.074 | 0.077 | 0.084 | 0.098 |
| 21-0935 | 0.151 | 0.165 | 0.178 | 0.185 | 0.194 | 0.198 | 0.198 | 0.198 | 0.198 | 0.198 |
| 21-1000 | 0.089 | 0.096 | 0.102 | 0.106 | 0.115 | 0.120 | 0.130 | 0.137 | 0.145 | 0.151 |
| 21-1033 | 0.036 | 0.038 | 0.040 | 0.042 | 0.050 | 0.055 | 0.055 | 0.054 | 0.054 | 0.056 |
| 21-1050 | 0.066 | 0.083 | 0.097 | 0.105 | 0.115 | 0.118 | 0.120 | 0.120 | 0.121 | 0.121 |
| 21-1070 | 0.030 | 0.032 | 0.034 | 0.035 | 0.038 | 0.039 | 0.041 | 0.041 | 0.042 | 0.043 |
| 21-1086 | 0.108 | 0.133 | 0.156 | 0.173 | 0.210 | 0.231 | 0.257 | 0.275 | 0.284 | 0.284 |
| 21-1300 | 0.040 | 0.043 | 0.047 | 0.050 | 0.061 | 0.069 | 0.076 | 0.079 | 0.086 | 0.103 |
| 21-1400 | 0.045 | 0.052 | 0.059 | 0.064 | 0.074 | 0.080 | 0.087 | 0.091 | 0.098 | 0.114 |
| 21-1440 | 0.068 | 0.076 | 0.082 | 0.085 | 0.089 | 0.090 | 0.091 | 0.091 | 0.091 | 0.091 |
| 21-2340 | 0.060 | 0.068 | 0.075 | 0.081 | 0.098 | 0.108 | 0.111 | 0.113 | 0.115 | 0.117 |
| 21-3245 | 0.053 | 0.064 | 0.074 | 0.080 | 0.087 | 0.090 | 0.099 | 0.106 | 0.112 | 0.115 |
| 21-3255 | 0.041 | 0.043 | 0.045 | 0.047 | 0.053 | 0.058 | 0.062 | 0.064 | 0.067 | 0.070 |
| 21-3298 | 0.110 | 0.128 | 0.145 | 0.160 | 0.201 | 0.228 | 0.274 | 0.303 | 0.336 | 0.363 |
| 21-3315 | 0.209 | 0.229 | 0.248 | 0.264 | 0.300 | 0.329 | 0.418 | 0.497 | 0.573 | 0.600 |
| 21-3672 | 0.041 | 0.053 | 0.064 | 0.070 | 0.077 | 0.080 | 0.084 | 0.086 | 0.088 | 0.090 |
| 21-4500 | 0.067 | 0.078 | 0.087 | 0.096 | 0.124 | 0.142 | 0.165 | 0.177 | 0.198 | 0.240 |
| 21-4920 | 0.085 | 0.102 | 0.117 | 0.130 | 0.161 | 0.180 | 0.206 | 0.221 | 0.240 | 0.263 |
| 21-5130 | 0.117 | 0.144 | 0.167 | 0.184 | 0.214 | 0.229 | 0.251 | 0.264 | 0.280 | 0.301 |
| 21-5248 | 0.120 | 0.130 | 0.139 | 0.146 | 0.159 | 0.169 | 0.196 | 0.219 | 0.247 | 0.266 |
| 21-5275 | 0.110 | 0.133 | 0.154 | 0.170 | 0.204 | 0.225 | 0.270 | 0.302 | 0.330 | 0.341 |
| 21-5384 | 0.120 | 0.149 | 0.175 | 0.193 | 0.227 | 0.247 | 0.280 | 0.302 | 0.320 | 0.329 |
| 21-6336 | 0.130 | 0.195 | 0.250 | 0.280 | 0.307 | 0.320 | 0.345 | 0.361 | 0.380 | 0.400 |
| 21-6420 | 0.127 | 0.156 | 0.182 | 0.204 | 0.253 | 0.283 | 0.332 | 0.366 | 0.385 | 0.385 |
| 21-6483 | 0.095 | 0.121 | 0.145 | 0.163 | 0.198 | 0.222 | 0.276 | 0.315 | 0.372 | 0.441 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-16

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21-6488 | 0.123 | 0.161 | 0.193 | 0.209 | 0.219 | 0.226 | 0.293 | 0.389 | 0.473 | 0.473 |
| 21-6492 | 0.104 | 0.137 | 0.166 | 0.191 | 0.246 | 0.283 | 0.362 | 0.422 | 0.460 | 0.460 |
| 21-6493 | 0.156 | 0.182 | 0.207 | 0.230 | 0.296 | 0.340 | 0.393 | 0.424 | 0.460 | 0.500 |
| 21-7742 | 0.130 | 0.175 | 0.215 | 0.241 | 0.281 | 0.300 | 0.323 | 0.337 | 0.350 | 0.362 |
| 21-8036 | 0.094 | 0.110 | 0.123 | 0.133 | 0.150 | 0.160 | 0.188 | 0.208 | 0.243 | 0.300 |
| 21-8040 | 0.053 | 0.065 | 0.076 | 0.082 | 0.091 | 0.095 | 0.105 | 0.111 | 0.120 | 0.130 |
| 21-8041 | 0.054 | 0.058 | 0.062 | 0.065 | 0.074 | 0.080 | 0.087 | 0.092 | 0.096 | 0.100 |
| 21-8202 | 0.037 | 0.043 | 0.049 | 0.054 | 0.070 | 0.080 | 0.088 | 0.092 | 0.096 | 0.100 |
| 21-8250 | 0.045 | 0.058 | 0.068 | 0.075 | 0.083 | 0.089 | 0.121 | 0.157 | 0.198 | 0.212 |
| 21-8535 | 0.117 | 0.139 | 0.157 | 0.169 | 0.184 | 0.193 | 0.214 | 0.230 | 0.247 | 0.259 |
| 30-1100 | 0.124 | 0.139 | 0.152 | 0.160 | 0.169 | 0.173 | 0.180 | 0.184 | 0.190 | 0.200 |
| 30-1110 | 0.104 | 0.116 | 0.127 | 0.135 | 0.149 | 0.156 | 0.163 | 0.166 | 0.171 | 0.178 |
| 40-1220 | 0.127 | 0.138 | 0.147 | 0.154 | 0.163 | 0.168 | 0.174 | 0.178 | 0.180 | 0.180 |
| 40-1250 | 0.117 | 0.127 | 0.136 | 0.142 | 0.149 | 0.153 | 0.164 | 0.173 | 0.180 | 0.181 |
| 40-1300 | 0.035 | 0.042 | 0.047 | 0.050 | 0.052 | 0.053 | 0.053 | 0.053 | 0.053 | 0.053 |
| 40-1510 | 0.020 | 0.022 | 0.024 | 0.026 | 0.030 | 0.033 | 0.041 | 0.047 | 0.054 | 0.060 |
| 50-0026 | 0.106 | 0.111 | 0.117 | 0.122 | 0.138 | 0.150 | 0.167 | 0.178 | 0.192 | 0.214 |
| 50-0230 | 0.066 | 0.074 | 0.081 | 0.085 | 0.088 | 0.089 | 0.098 | 0.109 | 0.130 | 0.160 |
| 50-0243 | 0.132 | 0.156 | 0.179 | 0.200 | 0.255 | 0.300 | 0.424 | 0.530 | 0.640 | 0.696 |
| 50-0249 | 0.064 | 0.080 | 0.094 | 0.106 | 0.129 | 0.145 | 0.186 | 0.218 | 0.251 | 0.270 |
| 50-0280 | 0.070 | 0.089 | 0.106 | 0.115 | 0.124 | 0.128 | 0.134 | 0.137 | 0.142 | 0.150 |
| 50-0310 | 0.047 | 0.068 | 0.085 | 0.097 | 0.116 | 0.125 | 0.143 | 0.154 | 0.168 | 0.180 |
| 50-0332 | 0.073 | 0.101 | 0.124 | 0.135 | 0.141 | 0.144 | 0.152 | 0.158 | 0.165 | 0.170 |
| 50-0352 | 0.097 | 0.157 | 0.211 | 0.250 | 0.326 | 0.370 | 0.446 | 0.495 | 0.550 | 0.600 |
| 50-0363 | 0.115 | 0.137 | 0.155 | 0.164 | 0.170 | 0.174 | 0.203 | 0.242 | 0.312 | 0.398 |
| 50-0433 | 0.112 | 0.121 | 0.129 | 0.135 | 0.150 | 0.159 | 0.177 | 0.188 | 0.200 | 0.208 |
| 50-0452 | 0.176 | 0.198 | 0.217 | 0.230 | 0.249 | 0.260 | 0.287 | 0.305 | 0.336 | 0.386 |
| 50-0464 | 0.083 | 0.090 | 0.097 | 0.101 | 0.108 | 0.113 | 0.140 | 0.172 | 0.226 | 0.291 |
| 50-0522 | 0.075 | 0.111 | 0.141 | 0.159 | 0.179 | 0.191 | 0.232 | 0.266 | 0.312 | 0.353 |
| 50-0546 | 0.035 | 0.038 | 0.040 | 0.042 | 0.045 | 0.047 | 0.056 | 0.064 | 0.074 | 0.080 |
| 50-0558 | 0.074 | 0.082 | 0.090 | 0.096 | 0.108 | 0.115 | 0.128 | 0.137 | 0.145 | 0.150 |
| 50-0657 | 0.154 | 0.193 | 0.227 | 0.253 | 0.305 | 0.336 | 0.398 | 0.444 | 0.472 | 0.472 |
| 50-0676 | 0.089 | 0.121 | 0.148 | 0.165 | 0.189 | 0.200 | 0.217 | 0.228 | 0.234 | 0.219 |
| 50-0685 | 0.099 | 0.128 | 0.154 | 0.172 | 0.205 | 0.222 | 0.245 | 0.258 | 0.271 | 0.280 |
| 50-0707 | 0.054 | 0.062 | 0.070 | 0.077 | 0.092 | 0.100 | 0.105 | 0.107 | 0.110 | 0.115 |
| 50-0754 | 0.080 | 0.088 | 0.095 | 0.100 | 0.111 | 0.120 | 0.146 | 0.169 | 0.195 | 0.210 |
| 50-0761 | 0.075 | 0.085 | 0.094 | 0.100 | 0.112 | 0.120 | 0.136 | 0.148 | 0.160 | 0.168 |
| 50-0770 | 0.055 | 0.063 | 0.071 | 0.076 | 0.085 | 0.090 | 0.098 | 0.103 | 0.108 | 0.112 |
| 50-0788 | 0.090 | 0.117 | 0.142 | 0.166 | 0.239 | 0.285 | 0.316 | 0.331 | 0.350 | 0.380 |
| 50-0910 | 0.046 | 0.049 | 0.052 | 0.056 | 0.071 | 0.082 | 0.097 | 0.105 | 0.117 | 0.131 |
| 50-1201 | 0.111 | 0.126 | 0.138 | 0.146 | 0.156 | 0.162 | 0.175 | 0.185 | 0.191 | 0.191 |
| 50-1220 | 0.058 | 0.073 | 0.086 | 0.095 | 0.108 | 0.115 | 0.123 | 0.128 | 0.131 | 0.131 |
| 50-1230 | 0.027 | 0.028 | 0.028 | 0.028 | 0.029 | 0.031 | 0.036 | 0.042 | 0.050 | 0.058 |
| 50-1240 | 0.108 | 0.133 | 0.157 | 0.179 | 0.244 | 0.303 | 0.478 | 0.638 | 0.854 | 1.041 |
| 50-1243 | 0.105 | 0.107 | 0.108 | 0.109 | 0.110 | 0.110 | 0.113 | 0.115 | 0.119 | 0.121 |
| 50-1251 | 0.097 | 0.104 | 0.109 | 0.113 | 0.119 | 0.123 | 0.143 | 0.163 | 0.190 | 0.209 |
| 50-1269 | 0.089 | 0.097 | 0.105 | 0.113 | 0.141 | 0.160 | 0.181 | 0.194 | 0.206 | 0.216 |
| 50-1308 | 0.152 | 0.191 | 0.226 | 0.258 | 0.343 | 0.400 | 0.486 | 0.541 | 0.600 | 0.650 |
| 50-1312 | 0.060 | 0.068 | 0.077 | 0.084 | 0.106 | 0.120 | 0.136 | 0.145 | 0.157 | 0.174 |
| 50-1314 | 0.077 | 0.106 | 0.131 | 0.147 | 0.168 | 0.181 | 0.211 | 0.232 | 0.263 | 0.300 |
| 50-1318 | 0.067 | 0.081 | 0.093 | 0.100 | 0.108 | 0.114 | 0.148 | 0.188 | 0.237 | 0.262 |
| 50-1321 | 0.152 | 0.189 | 0.222 | 0.247 | 0.295 | 0.330 | 0.427 | 0.506 | 0.632 | 0.798 |
| 50-1325 | 0.072 | 0.095 | 0.116 | 0.133 | 0.169 | 0.190 | 0.211 | 0.222 | 0.235 | 0.249 |
| 50-1334 | 0.168 | 0.222 | 0.268 | 0.295 | 0.322 | 0.340 | 0.436 | 0.543 | 0.650 | 0.680 |
| 50-1466 | 0.059 | 0.071 | 0.082 | 0.090 | 0.105 | 0.115 | 0.136 | 0.150 | 0.165 | 0.173 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-17

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-1492 | 0.034 | 0.042 | 0.049 | 0.053 | 0.060 | 0.064 | 0.073 | 0.080 | 0.087 | 0.090 |
| 50-1574 | 0.077 | 0.087 | 0.096 | 0.100 | 0.104 | 0.105 | 0.107 | 0.108 | 0.110 | 0.116 |
| 50-1684 | 0.077 | 0.092 | 0.106 | 0.116 | 0.134 | 0.148 | 0.188 | 0.223 | 0.267 | 0.300 |
| 50-1763 | 0.114 | 0.130 | 0.144 | 0.154 | 0.167 | 0.176 | 0.203 | 0.225 | 0.255 | 0.280 |
| 50-1824 | 0.120 | 0.150 | 0.176 | 0.190 | 0.204 | 0.210 | 0.218 | 0.223 | 0.225 | 0.225 |
| 50-1926 | 0.129 | 0.137 | 0.144 | 0.152 | 0.180 | 0.200 | 0.222 | 0.234 | 0.250 | 0.273 |
| 50-1977 | 0.042 | 0.050 | 0.056 | 0.061 | 0.068 | 0.073 | 0.084 | 0.092 | 0.099 | 0.100 |
| 50-1987 | 0.069 | 0.082 | 0.092 | 0.098 | 0.105 | 0.108 | 0.121 | 0.133 | 0.143 | 0.146 |
| 50-2005 | 0.109 | 0.131 | 0.149 | 0.160 | 0.172 | 0.178 | 0.191 | 0.201 | 0.214 | 0.230 |
| 50-2102 | 0.090 | 0.107 | 0.123 | 0.137 | 0.169 | 0.191 | 0.230 | 0.255 | 0.285 | 0.311 |
| 50-2107 | 0.076 | 0.088 | 0.098 | 0.106 | 0.119 | 0.127 | 0.141 | 0.151 | 0.160 | 0.165 |
| 50-2112 | 0.068 | 0.070 | 0.073 | 0.076 | 0.094 | 0.110 | 0.129 | 0.141 | 0.155 | 0.168 |
| 50-2126 | 0.026 | 0.028 | 0.030 | 0.032 | 0.039 | 0.043 | 0.043 | 0.044 | 0.044 | 0.045 |
| 50-2144 | 0.136 | 0.141 | 0.147 | 0.153 | 0.178 | 0.204 | 0.292 | 0.382 | 0.463 | 0.480 |
| 50-2147 | 0.114 | 0.124 | 0.132 | 0.140 | 0.162 | 0.177 | 0.191 | 0.199 | 0.210 | 0.227 |
| 50-2156 | 0.070 | 0.075 | 0.079 | 0.082 | 0.085 | 0.087 | 0.090 | 0.092 | 0.095 | 0.100 |
| 50-2173 | 0.254 | 0.329 | 0.397 | 0.452 | 0.578 | 0.659 | 0.798 | 0.883 | 1.015 | 1.218 |
| 50-2177 | 0.178 | 0.227 | 0.272 | 0.309 | 0.395 | 0.457 | 0.612 | 0.734 | 0.850 | 0.900 |
| 50-2227 | 0.107 | 0.134 | 0.159 | 0.180 | 0.231 | 0.262 | 0.308 | 0.339 | 0.356 | 0.356 |
| 50-2247 | 0.044 | 0.044 | 0.045 | 0.046 | 0.047 | 0.048 | 0.052 | 0.055 | 0.061 | 0.071 |
| 50-2339 | 0.058 | 0.070 | 0.080 | 0.087 | 0.101 | 0.108 | 0.115 | 0.119 | 0.126 | 0.142 |
| 50-2350 | 0.058 | 0.071 | 0.082 | 0.091 | 0.112 | 0.122 | 0.124 | 0.126 | 0.127 | 0.131 |
| 50-2352 | 0.054 | 0.061 | 0.067 | 0.072 | 0.087 | 0.095 | 0.100 | 0.102 | 0.105 | 0.110 |
| 50-2457 | 0.110 | 0.127 | 0.142 | 0.151 | 0.162 | 0.167 | 0.181 | 0.191 | 0.198 | 0.199 |
| 50-2568 | 0.062 | 0.066 | 0.070 | 0.073 | 0.080 | 0.086 | 0.097 | 0.104 | 0.117 | 0.136 |
| 50-2587 | 0.150 | 0.189 | 0.222 | 0.244 | 0.275 | 0.292 | 0.333 | 0.361 | 0.397 | 0.431 |
| 50-2607 | 0.040 | 0.045 | 0.050 | 0.053 | 0.058 | 0.060 | 0.062 | 0.064 | 0.065 | 0.065 |
| 50-2707 | 0.089 | 0.108 | 0.124 | 0.135 | 0.152 | 0.160 | 0.174 | 0.182 | 0.190 | 0.195 |
| 50-2725 | 0.040 | 0.041 | 0.043 | 0.044 | 0.050 | 0.054 | 0.057 | 0.059 | 0.061 | 0.063 |
| 50-2730 | 0.045 | 0.051 | 0.057 | 0.060 | 0.063 | 0.064 | 0.070 | 0.076 | 0.082 | 0.086 |
| 50-2737 | 0.038 | 0.042 | 0.046 | 0.049 | 0.055 | 0.058 | 0.066 | 0.070 | 0.077 | 0.088 |
| 50-2770 | 0.132 | 0.176 | 0.214 | 0.243 | 0.297 | 0.327 | 0.368 | 0.390 | 0.426 | 0.494 |
| 50-2785 | 0.173 | 0.206 | 0.234 | 0.249 | 0.260 | 0.267 | 0.293 | 0.318 | 0.361 | 0.422 |
| 50-2820 | 0.064 | 0.080 | 0.093 | 0.100 | 0.107 | 0.110 | 0.115 | 0.119 | 0.123 | 0.128 |
| 50-2825 | 0.049 | 0.055 | 0.060 | 0.065 | 0.075 | 0.082 | 0.097 | 0.108 | 0.124 | 0.145 |
| 50-2952 | 0.045 | 0.048 | 0.050 | 0.052 | 0.056 | 0.058 | 0.064 | 0.068 | 0.073 | 0.078 |
| 50-2968 | 0.079 | 0.088 | 0.096 | 0.103 | 0.116 | 0.123 | 0.133 | 0.140 | 0.146 | 0.150 |
| 50-2988 | 0.054 | 0.056 | 0.058 | 0.060 | 0.065 | 0.068 | 0.073 | 0.076 | 0.080 | 0.086 |
| 50-3009 | 0.060 | 0.061 | 0.061 | 0.062 | 0.064 | 0.065 | 0.068 | 0.069 | 0.072 | 0.076 |
| 50-3072 | 0.070 | 0.104 | 0.133 | 0.153 | 0.182 | 0.200 | 0.253 | 0.295 | 0.350 | 0.400 |
| 50-3082 | 0.051 | 0.054 | 0.057 | 0.060 | 0.071 | 0.078 | 0.085 | 0.088 | 0.093 | 0.104 |
| 50-3085 | 0.056 | 0.059 | 0.062 | 0.064 | 0.068 | 0.071 | 0.078 | 0.083 | 0.088 | 0.090 |
| 50-3160 | 0.092 | 0.106 | 0.119 | 0.128 | 0.144 | 0.154 | 0.175 | 0.190 | 0.206 | 0.218 |
| 50-3163 | 0.049 | 0.059 | 0.067 | 0.073 | 0.084 | 0.090 | 0.095 | 0.098 | 0.102 | 0.109 |
| 50-3196 | 0.050 | 0.061 | 0.070 | 0.076 | 0.085 | 0.089 | 0.096 | 0.100 | 0.105 | 0.113 |
| 50-3198 | 0.076 | 0.081 | 0.085 | 0.087 | 0.088 | 0.089 | 0.102 | 0.124 | 0.157 | 0.182 |
| 50-3205 | 0.050 | 0.051 | 0.051 | 0.052 | 0.054 | 0.055 | 0.056 | 0.057 | 0.058 | 0.060 |
| 50-3212 | 0.068 | 0.073 | 0.077 | 0.080 | 0.086 | 0.090 | 0.095 | 0.097 | 0.101 | 0.109 |
| 50-3226 | 0.054 | 0.064 | 0.072 | 0.079 | 0.098 | 0.110 | 0.133 | 0.150 | 0.164 | 0.170 |
| 50-3275 | 0.100 | 0.113 | 0.125 | 0.134 | 0.152 | 0.161 | 0.166 | 0.168 | 0.170 | 0.171 |
| 50-3294 | 0.082 | 0.094 | 0.104 | 0.111 | 0.121 | 0.126 | 0.133 | 0.137 | 0.144 | 0.159 |
| 50-3299 | 0.077 | 0.094 | 0.109 | 0.120 | 0.140 | 0.151 | 0.164 | 0.172 | 0.177 | 0.179 |
| 50-3454 | 0.076 | 0.087 | 0.098 | 0.109 | 0.140 | 0.161 | 0.188 | 0.205 | 0.218 | 0.223 |
| 50-3465 | 0.040 | 0.041 | 0.042 | 0.043 | 0.046 | 0.048 | 0.049 | 0.049 | 0.050 | 0.052 |
| 50-3475 | 0.074 | 0.077 | 0.081 | 0.085 | 0.100 | 0.110 | 0.114 | 0.116 | 0.118 | 0.120 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-18

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-3490 | 0.134 | 0.159 | 0.181 | 0.198 | 0.231 | 0.253 | 0.304 | 0.339 | 0.403 | 0.526 |
| 50-3500 | 0.120 | 0.142 | 0.161 | 0.176 | 0.205 | 0.224 | 0.268 | 0.299 | 0.349 | 0.425 |
| 50-3504 | 0.127 | 0.150 | 0.170 | 0.184 | 0.204 | 0.217 | 0.253 | 0.281 | 0.326 | 0.386 |
| 50-3530 | 0.113 | 0.145 | 0.172 | 0.189 | 0.208 | 0.221 | 0.290 | 0.368 | 0.453 | 0.485 |
| 50-3573 | 0.158 | 0.174 | 0.189 | 0.200 | 0.222 | 0.236 | 0.256 | 0.269 | 0.288 | 0.320 |
| 50-3585 | 0.073 | 0.087 | 0.100 | 0.107 | 0.113 | 0.117 | 0.130 | 0.141 | 0.157 | 0.171 |
| 50-3605 | 0.059 | 0.089 | 0.115 | 0.130 | 0.142 | 0.150 | 0.179 | 0.206 | 0.255 | 0.332 |
| 50-3655 | 0.069 | 0.087 | 0.102 | 0.110 | 0.117 | 0.120 | 0.126 | 0.130 | 0.135 | 0.141 |
| 50-3665 | 0.075 | 0.094 | 0.111 | 0.122 | 0.140 | 0.152 | 0.195 | 0.236 | 0.279 | 0.300 |
| 50-3672 | 0.079 | 0.101 | 0.121 | 0.137 | 0.175 | 0.200 | 0.244 | 0.274 | 0.305 | 0.327 |
| 50-3682 | 0.073 | 0.089 | 0.104 | 0.115 | 0.137 | 0.153 | 0.188 | 0.215 | 0.254 | 0.304 |
| 50-3695 | 0.083 | 0.095 | 0.105 | 0.109 | 0.110 | 0.111 | 0.112 | 0.114 | 0.117 | 0.138 |
| 50-3720 | 0.102 | 0.110 | 0.117 | 0.122 | 0.130 | 0.136 | 0.149 | 0.158 | 0.171 | 0.185 |
| 50-3765 | 0.106 | 0.115 | 0.124 | 0.130 | 0.142 | 0.150 | 0.163 | 0.171 | 0.184 | 0.203 |
| 50-3905 | 0.063 | 0.089 | 0.111 | 0.123 | 0.135 | 0.142 | 0.166 | 0.186 | 0.219 | 0.261 |
| 50-3910 | 0.106 | 0.130 | 0.152 | 0.166 | 0.188 | 0.200 | 0.225 | 0.241 | 0.262 | 0.284 |
| 50-3933 | 0.072 | 0.100 | 0.124 | 0.140 | 0.167 | 0.182 | 0.210 | 0.227 | 0.255 | 0.300 |
| 50-4094 | 0.106 | 0.111 | 0.117 | 0.124 | 0.151 | 0.175 | 0.212 | 0.238 | 0.269 | 0.300 |
| 50-4100 | 0.091 | 0.103 | 0.114 | 0.125 | 0.154 | 0.175 | 0.208 | 0.229 | 0.253 | 0.276 |
| 50-4103 | 0.150 | 0.175 | 0.198 | 0.220 | 0.281 | 0.330 | 0.452 | 0.550 | 0.650 | 0.700 |
| 50-4155 | 0.052 | 0.070 | 0.085 | 0.094 | 0.105 | 0.110 | 0.118 | 0.122 | 0.130 | 0.148 |
| 50-4425 | 0.055 | 0.069 | 0.082 | 0.089 | 0.100 | 0.105 | 0.109 | 0.112 | 0.114 | 0.116 |
| 50-4546 | 0.094 | 0.099 | 0.103 | 0.106 | 0.112 | 0.115 | 0.117 | 0.118 | 0.120 | 0.123 |
| 50-4550 | 0.090 | 0.107 | 0.122 | 0.130 | 0.137 | 0.140 | 0.143 | 0.145 | 0.146 | 0.115 |
| 50-4555 | 0.062 | 0.088 | 0.111 | 0.128 | 0.162 | 0.182 | 0.215 | 0.236 | 0.261 | 0.288 |
| 50-4590 | 0.170 | 0.249 | 0.317 | 0.362 | 0.436 | 0.470 | 0.498 | 0.511 | 0.527 | 0.547 |
| 50-4621 | 0.084 | 0.103 | 0.119 | 0.130 | 0.147 | 0.157 | 0.180 | 0.197 | 0.216 | 0.229 |
| 50-4766 | 0.046 | 0.062 | 0.077 | 0.089 | 0.114 | 0.130 | 0.156 | 0.174 | 0.190 | 0.200 |
| 50-4812 | 0.096 | 0.108 | 0.119 | 0.128 | 0.147 | 0.158 | 0.169 | 0.175 | 0.184 | 0.200 |
| 50-4964 | 0.074 | 0.101 | 0.124 | 0.142 | 0.178 | 0.200 | 0.238 | 0.262 | 0.290 | 0.315 |
| 50-4988 | 0.140 | 0.152 | 0.163 | 0.170 | 0.183 | 0.190 | 0.206 | 0.215 | 0.230 | 0.250 |
| 50-4991 | 0.113 | 0.129 | 0.142 | 0.151 | 0.164 | 0.171 | 0.183 | 0.190 | 0.200 | 0.216 |
| 50-5076 | 0.035 | 0.041 | 0.046 | 0.051 | 0.065 | 0.075 | 0.092 | 0.104 | 0.116 | 0.125 |
| 50-5136 | 0.031 | 0.033 | 0.034 | 0.036 | 0.039 | 0.041 | 0.044 | 0.047 | 0.050 | 0.054 |
| 50-5318 | 0.085 | 0.092 | 0.098 | 0.103 | 0.114 | 0.122 | 0.136 | 0.146 | 0.158 | 0.168 |
| 50-5397 | 0.049 | 0.050 | 0.051 | 0.052 | 0.056 | 0.058 | 0.060 | 0.061 | 0.062 | 0.064 |
| 50-5454 | 0.130 | 0.140 | 0.151 | 0.163 | 0.203 | 0.243 | 0.360 | 0.468 | 0.600 | 0.690 |
| 50-5464 | 0.056 | 0.061 | 0.066 | 0.069 | 0.073 | 0.075 | 0.078 | 0.079 | 0.082 | 0.085 |
| 50-5499 | 0.069 | 0.076 | 0.084 | 0.091 | 0.119 | 0.140 | 0.165 | 0.180 | 0.200 | 0.229 |
| 50-5519 | 0.214 | 0.224 | 0.236 | 0.250 | 0.315 | 0.370 | 0.434 | 0.475 | 0.510 | 0.530 |
| 50-5534 | 0.058 | 0.063 | 0.069 | 0.074 | 0.086 | 0.095 | 0.111 | 0.121 | 0.133 | 0.143 |
| 50-5604 | 0.190 | 0.201 | 0.218 | 0.238 | 0.367 | 0.497 | 0.693 | 0.827 | 0.977 | 1.100 |
| 50-5607 | 0.072 | 0.087 | 0.101 | 0.114 | 0.153 | 0.184 | 0.258 | 0.317 | 0.370 | 0.389 |
| 50-5644 | 0.087 | 0.096 | 0.104 | 0.111 | 0.123 | 0.132 | 0.161 | 0.187 | 0.215 | 0.232 |
| 50-5733 | 0.046 | 0.049 | 0.052 | 0.055 | 0.063 | 0.069 | 0.080 | 0.088 | 0.096 | 0.100 |
| 50-5757 | 0.036 | 0.047 | 0.056 | 0.064 | 0.082 | 0.095 | 0.128 | 0.155 | 0.179 | 0.186 |
| 50-5769 | 0.030 | 0.031 | 0.031 | 0.032 | 0.034 | 0.036 | 0.036 | 0.037 | 0.037 | 0.038 |
| 50-5778 | 0.077 | 0.079 | 0.081 | 0.083 | 0.091 | 0.098 | 0.105 | 0.108 | 0.113 | 0.122 |
| 50-5810 | 0.051 | 0.059 | 0.066 | 0.073 | 0.089 | 0.100 | 0.124 | 0.142 | 0.160 | 0.170 |
| 50-5880 | 0.080 | 0.082 | 0.083 | 0.085 | 0.091 | 0.096 | 0.100 | 0.102 | 0.105 | 0.110 |
| 50-5881 | 0.080 | 0.078 | 0.077 | 0.077 | 0.081 | 0.089 | 0.106 | 0.122 | 0.144 | 0.161 |
| 50-5882 | 0.057 | 0.061 | 0.064 | 0.066 | 0.072 | 0.076 | 0.084 | 0.090 | 0.100 | 0.125 |
| 50-5894 | 0.130 | 0.132 | 0.134 | 0.137 | 0.156 | 0.178 | 0.232 | 0.280 | 0.334 | 0.366 |
| 50-5898 | 0.107 | 0.130 | 0.149 | 0.161 | 0.177 | 0.187 | 0.212 | 0.229 | 0.265 | 0.359 |
| 50-6058 | 0.063 | 0.070 | 0.075 | 0.078 | 0.076 | 0.075 | 0.089 | 0.117 | 0.144 | 0.144 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-19

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-6147 | 0.045 | 0.056 | 0.065 | 0.072 | 0.086 | 0.096 | 0.112 | 0.122 | 0.136 | 0.152 |
| 50-6270 | 0.046 | 0.044 | 0.042 | 0.041 | 0.042 | 0.042 | 0.044 | 0.048 | 0.050 | 0.050 |
| 50-6309 | 0.095 | 0.114 | 0.131 | 0.143 | 0.164 | 0.177 | 0.201 | 0.217 | 0.239 | 0.271 |
| 50-6441 | 0.081 | 0.093 | 0.102 | 0.109 | 0.120 | 0.127 | 0.146 | 0.160 | 0.184 | 0.221 |
| 50-6496 | 0.054 | 0.060 | 0.066 | 0.073 | 0.096 | 0.112 | 0.132 | 0.145 | 0.156 | 0.160 |
| 50-6562 | 0.086 | 0.095 | 0.106 | 0.118 | 0.161 | 0.210 | 0.373 | 0.541 | 0.768 | 0.942 |
| 50-6581 | 0.072 | 0.084 | 0.095 | 0.102 | 0.114 | 0.120 | 0.130 | 0.136 | 0.144 | 0.156 |
| 50-6586 | 0.080 | 0.083 | 0.087 | 0.090 | 0.102 | 0.110 | 0.121 | 0.127 | 0.134 | 0.142 |
| 50-6656 | 0.064 | 0.069 | 0.074 | 0.079 | 0.092 | 0.100 | 0.107 | 0.111 | 0.114 | 0.118 |
| 50-6727 | 0.062 | 0.065 | 0.067 | 0.069 | 0.077 | 0.082 | 0.086 | 0.088 | 0.090 | 0.092 |
| 50-6760 | 0.081 | 0.086 | 0.091 | 0.097 | 0.122 | 0.144 | 0.178 | 0.201 | 0.226 | 0.243 |
| 50-6853 | 0.139 | 0.152 | 0.163 | 0.172 | 0.190 | 0.200 | 0.209 | 0.213 | 0.220 | 0.240 |
| 50-6870 | 0.048 | 0.058 | 0.066 | 0.072 | 0.082 | 0.087 | 0.092 | 0.095 | 0.100 | 0.110 |
| 50-6875 | 0.120 | 0.128 | 0.135 | 0.140 | 0.146 | 0.150 | 0.164 | 0.176 | 0.190 | 0.200 |
| 50-7097 | 0.067 | 0.074 | 0.080 | 0.086 | 0.104 | 0.118 | 0.154 | 0.183 | 0.214 | 0.234 |
| 50-7105 | 0.057 | 0.060 | 0.062 | 0.065 | 0.076 | 0.086 | 0.114 | 0.138 | 0.163 | 0.173 |
| 50-7141 | 0.232 | 0.307 | 0.370 | 0.399 | 0.410 | 0.416 | 0.453 | 0.497 | 0.575 | 0.683 |
| 50-7251 | 0.120 | 0.140 | 0.158 | 0.166 | 0.167 | 0.168 | 0.188 | 0.223 | 0.269 | 0.288 |
| 50-7352 | 0.050 | 0.058 | 0.065 | 0.071 | 0.089 | 0.100 | 0.109 | 0.113 | 0.120 | 0.136 |
| 50-7365 | 0.067 | 0.087 | 0.105 | 0.117 | 0.137 | 0.148 | 0.167 | 0.180 | 0.195 | 0.209 |
| 50-7431 | 0.035 | 0.048 | 0.059 | 0.065 | 0.070 | 0.073 | 0.086 | 0.100 | 0.117 | 0.129 |
| 50-7442 | 0.050 | 0.057 | 0.064 | 0.070 | 0.082 | 0.090 | 0.105 | 0.115 | 0.125 | 0.130 |
| 50-7451 | 0.099 | 0.111 | 0.121 | 0.128 | 0.140 | 0.147 | 0.164 | 0.176 | 0.191 | 0.203 |
| 50-7494 | 0.142 | 0.177 | 0.210 | 0.240 | 0.318 | 0.382 | 0.551 | 0.694 | 0.840 | 0.910 |
| 50-7557 | 0.120 | 0.133 | 0.146 | 0.160 | 0.213 | 0.250 | 0.280 | 0.296 | 0.316 | 0.342 |
| 50-7570 | 0.055 | 0.082 | 0.105 | 0.119 | 0.134 | 0.141 | 0.148 | 0.152 | 0.156 | 0.161 |
| 50-7700 | 0.063 | 0.074 | 0.084 | 0.090 | 0.097 | 0.100 | 0.104 | 0.106 | 0.110 | 0.120 |
| 50-7738 | 0.120 | 0.125 | 0.132 | 0.140 | 0.180 | 0.223 | 0.325 | 0.412 | 0.513 | 0.580 |
| 50-7783 | 0.150 | 0.179 | 0.203 | 0.220 | 0.246 | 0.260 | 0.286 | 0.304 | 0.320 | 0.330 |
| 50-7854 | 0.127 | 0.141 | 0.154 | 0.166 | 0.196 | 0.220 | 0.283 | 0.337 | 0.381 | 0.390 |
| 50-7900 | 0.078 | 0.084 | 0.089 | 0.093 | 0.098 | 0.102 | 0.106 | 0.109 | 0.114 | 0.128 |
| 50-7977 | 0.063 | 0.082 | 0.098 | 0.109 | 0.128 | 0.137 | 0.139 | 0.139 | 0.141 | 0.147 |
| 50-8025 | 0.059 | 0.075 | 0.090 | 0.099 | 0.111 | 0.117 | 0.125 | 0.130 | 0.133 | 0.133 |
| 50-8054 | 0.063 | 0.065 | 0.068 | 0.071 | 0.085 | 0.097 | 0.114 | 0.125 | 0.139 | 0.152 |
| 50-8105 | 0.052 | 0.059 | 0.066 | 0.071 | 0.080 | 0.087 | 0.100 | 0.109 | 0.122 | 0.137 |
| 50-8118 | 0.035 | 0.047 | 0.057 | 0.065 | 0.083 | 0.093 | 0.101 | 0.104 | 0.110 | 0.120 |
| 50-8140 | 0.087 | 0.102 | 0.116 | 0.127 | 0.150 | 0.164 | 0.183 | 0.195 | 0.207 | 0.216 |
| 50-8183 | 0.068 | 0.107 | 0.142 | 0.163 | 0.194 | 0.210 | 0.239 | 0.257 | 0.281 | 0.312 |
| 50-8355 | 0.121 | 0.152 | 0.179 | 0.197 | 0.225 | 0.244 | 0.314 | 0.381 | 0.471 | 0.547 |
| 50-8371 | 0.300 | 0.364 | 0.421 | 0.465 | 0.548 | 0.602 | 0.729 | 0.823 | 0.935 | 1.027 |
| 50-8375 | 0.256 | 0.289 | 0.319 | 0.347 | 0.420 | 0.476 | 0.607 | 0.709 | 0.827 | 0.915 |
| 50-8377 | 0.221 | 0.230 | 0.238 | 0.246 | 0.264 | 0.282 | 0.369 | 0.473 | 0.597 | 0.657 |
| 50-8409 | 0.046 | 0.067 | 0.085 | 0.095 | 0.108 | 0.114 | 0.120 | 0.124 | 0.126 | 0.126 |
| 50-8419 | 0.124 | 0.130 | 0.136 | 0.141 | 0.156 | 0.165 | 0.173 | 0.177 | 0.180 | 0.182 |
| 50-8437 | 0.029 | 0.031 | 0.034 | 0.035 | 0.039 | 0.041 | 0.047 | 0.051 | 0.055 | 0.055 |
| 50-8494 | 0.076 | 0.091 | 0.103 | 0.112 | 0.128 | 0.137 | 0.153 | 0.161 | 0.178 | 0.218 |
| 50-8503 | 0.069 | 0.087 | 0.103 | 0.115 | 0.137 | 0.151 | 0.178 | 0.196 | 0.220 | 0.246 |
| 50-8512 | 0.119 | 0.123 | 0.126 | 0.130 | 0.141 | 0.150 | 0.162 | 0.170 | 0.181 | 0.200 |
| 50-8525 | 0.108 | 0.123 | 0.136 | 0.146 | 0.163 | 0.173 | 0.199 | 0.217 | 0.252 | 0.321 |
| 50-8536 | 0.133 | 0.152 | 0.169 | 0.177 | 0.181 | 0.183 | 0.188 | 0.192 | 0.197 | 0.200 |
| 50-8547 | 0.045 | 0.056 | 0.067 | 0.075 | 0.097 | 0.110 | 0.128 | 0.139 | 0.148 | 0.152 |
| 50-8584 | 0.161 | 0.198 | 0.230 | 0.251 | 0.280 | 0.298 | 0.352 | 0.395 | 0.446 | 0.483 |
| 50-8594 | 0.038 | 0.038 | 0.039 | 0.039 | 0.040 | 0.041 | 0.043 | 0.043 | 0.045 | 0.046 |
| 50-8625 | 0.048 | 0.052 | 0.056 | 0.059 | 0.067 | 0.072 | 0.080 | 0.084 | 0.090 | 0.097 |
| 50-8666 | 0.070 | 0.077 | 0.083 | 0.089 | 0.109 | 0.120 | 0.120 | 0.120 | 0.121 | 0.121 |

NOAA Atlas 14 Volume 7 Version 2.0
A. $4-20$

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50-8811 | 0.060 | 0.068 | 0.075 | 0.080 | 0.092 | 0.098 | 0.102 | 0.103 | 0.105 | 0.106 |
| 50-8882 | 0.083 | 0.121 | 0.154 | 0.172 | 0.186 | 0.192 | 0.206 | 0.215 | 0.229 | 0.257 |
| 50-8915 | 0.060 | 0.069 | 0.077 | 0.084 | 0.101 | 0.110 | 0.115 | 0.117 | 0.120 | 0.125 |
| 50-8976 | 0.114 | 0.142 | 0.166 | 0.180 | 0.198 | 0.206 | 0.223 | 0.232 | 0.248 | 0.272 |
| 50-8987 | 0.110 | 0.128 | 0.144 | 0.155 | 0.172 | 0.181 | 0.205 | 0.222 | 0.240 | 0.250 |
| 50-9014 | 0.075 | 0.088 | 0.100 | 0.110 | 0.134 | 0.150 | 0.176 | 0.194 | 0.210 | 0.220 |
| 50-9035 | 0.043 | 0.044 | 0.045 | 0.047 | 0.051 | 0.054 | 0.058 | 0.060 | 0.064 | 0.077 |
| 50-9102 | 0.045 | 0.050 | 0.056 | 0.060 | 0.074 | 0.082 | 0.090 | 0.095 | 0.100 | 0.108 |
| 50-9121 | 0.088 | 0.102 | 0.115 | 0.126 | 0.154 | 0.170 | 0.183 | 0.190 | 0.200 | 0.220 |
| 50-9144 | 0.077 | 0.092 | 0.105 | 0.115 | 0.130 | 0.141 | 0.196 | 0.257 | 0.313 | 0.322 |
| 50-9249 | 0.049 | 0.066 | 0.080 | 0.090 | 0.102 | 0.110 | 0.133 | 0.153 | 0.170 | 0.176 |
| 50-9313 | 0.057 | 0.061 | 0.065 | 0.067 | 0.073 | 0.078 | 0.095 | 0.111 | 0.129 | 0.137 |
| 50-9385 | 0.078 | 0.080 | 0.081 | 0.082 | 0.082 | 0.082 | 0.082 | 0.083 | 0.084 | 0.085 |
| 50-9399 | 0.082 | 0.110 | 0.136 | 0.153 | 0.179 | 0.197 | 0.286 | 0.381 | 0.456 | 0.456 |
| 50-9410 | 0.117 | 0.132 | 0.146 | 0.159 | 0.198 | 0.224 | 0.255 | 0.273 | 0.296 | 0.328 |
| 50-9421 | 0.037 | 0.046 | 0.054 | 0.060 | 0.080 | 0.090 | 0.093 | 0.095 | 0.097 | 0.101 |
| 50-9460 | 0.210 | 0.266 | 0.313 | 0.343 | 0.380 | 0.405 | 0.525 | 0.653 | 0.798 | 0.865 |
| 50-9489 | 0.088 | 0.101 | 0.112 | 0.121 | 0.144 | 0.156 | 0.168 | 0.174 | 0.180 | 0.185 |
| 50-9511 | 0.100 | 0.107 | 0.113 | 0.120 | 0.145 | 0.163 | 0.180 | 0.190 | 0.200 | 0.210 |
| 50-9539 | 0.107 | 0.107 | 0.108 | 0.108 | 0.109 | 0.109 | 0.110 | 0.110 | 0.110 | 0.110 |
| 50-9564 | 0.061 | 0.065 | 0.068 | 0.070 | 0.077 | 0.083 | 0.095 | 0.105 | 0.115 | 0.120 |
| 50-9641 | 0.088 | 0.099 | 0.108 | 0.114 | 0.125 | 0.131 | 0.139 | 0.144 | 0.150 | 0.157 |
| 50-9686 | 0.102 | 0.123 | 0.142 | 0.159 | 0.207 | 0.238 | 0.275 | 0.296 | 0.326 | 0.374 |
| 50-9702 | 0.125 | 0.156 | 0.185 | 0.210 | 0.277 | 0.317 | 0.356 | 0.380 | 0.395 | 0.400 |
| 50-9739 | 0.054 | 0.061 | 0.068 | 0.074 | 0.089 | 0.100 | 0.117 | 0.129 | 0.141 | 0.151 |
| 50-9759 | 0.047 | 0.060 | 0.072 | 0.079 | 0.089 | 0.095 | 0.105 | 0.111 | 0.118 | 0.123 |
| 50-9765 | 0.060 | 0.072 | 0.083 | 0.091 | 0.108 | 0.117 | 0.126 | 0.132 | 0.137 | 0.141 |
| 50-9790 | 0.073 | 0.097 | 0.117 | 0.129 | 0.143 | 0.151 | 0.168 | 0.179 | 0.195 | 0.214 |
| 50-9793 | 0.053 | 0.067 | 0.079 | 0.088 | 0.106 | 0.115 | 0.118 | 0.118 | 0.120 | 0.124 |
| 50-9829 | 0.137 | 0.159 | 0.182 | 0.206 | 0.288 | 0.365 | 0.566 | 0.741 | 0.900 | 0.950 |
| 50-9861 | 0.086 | 0.103 | 0.117 | 0.127 | 0.141 | 0.148 | 0.158 | 0.163 | 0.170 | 0.180 |
| 50-9869 | 0.063 | 0.077 | 0.090 | 0.097 | 0.105 | 0.110 | 0.123 | 0.133 | 0.145 | 0.154 |
| 50-9883 | 0.085 | 0.086 | 0.088 | 0.089 | 0.094 | 0.097 | 0.100 | 0.102 | 0.104 | 0.105 |
| 50-9919 | 0.088 | 0.099 | 0.109 | 0.114 | 0.115 | 0.115 | 0.118 | 0.122 | 0.129 | 0.137 |
| 50-9930 | 0.123 | 0.157 | 0.189 | 0.218 | 0.297 | 0.356 | 0.471 | 0.553 | 0.653 | 0.747 |
| 50-9941 | 0.167 | 0.200 | 0.231 | 0.255 | 0.301 | 0.340 | 0.506 | 0.686 | 0.946 | 1.165 |
| 55-0064 | 0.100 | 0.143 | 0.182 | 0.210 | 0.267 | 0.300 | 0.359 | 0.398 | 0.436 | 0.459 |
| 55-0079 | 0.028 | 0.033 | 0.037 | 0.041 | 0.049 | 0.055 | 0.076 | 0.096 | 0.124 | 0.151 |
| 55-0080 | 0.098 | 0.125 | 0.149 | 0.171 | 0.226 | 0.266 | 0.351 | 0.418 | 0.460 | 0.460 |
| 55-0087 | 0.055 | 0.072 | 0.086 | 0.095 | 0.106 | 0.111 | 0.120 | 0.126 | 0.129 | 0.129 |
| 55-0096 | 0.051 | 0.064 | 0.075 | 0.083 | 0.097 | 0.103 | 0.111 | 0.116 | 0.118 | 0.118 |
| 55-0164 | 0.024 | 0.028 | 0.031 | 0.033 | 0.037 | 0.040 | 0.045 | 0.048 | 0.050 | 0.050 |
| 80-0100 | 0.126 | 0.128 | 0.130 | 0.133 | 0.144 | 0.152 | 0.165 | 0.173 | 0.182 | 0.188 |
| 80-0120 | 0.074 | 0.080 | 0.086 | 0.091 | 0.103 | 0.110 | 0.112 | 0.113 | 0.115 | 0.120 |
| 80-0140 | 0.052 | 0.058 | 0.064 | 0.069 | 0.080 | 0.088 | 0.104 | 0.116 | 0.127 | 0.133 |
| 80-0160 | 0.043 | 0.050 | 0.055 | 0.058 | 0.061 | 0.062 | 0.069 | 0.076 | 0.087 | 0.096 |
| 80-0200 | 0.053 | 0.056 | 0.059 | 0.062 | 0.073 | 0.081 | 0.093 | 0.100 | 0.110 | 0.120 |
| 80-0220 | 0.229 | 0.247 | 0.267 | 0.289 | 0.374 | 0.454 | 0.607 | 0.714 | 0.903 | 1.232 |
| 80-0240 | 0.064 | 0.082 | 0.098 | 0.110 | 0.133 | 0.145 | 0.154 | 0.158 | 0.167 | 0.189 |
| 80-0260 | 0.050 | 0.063 | 0.074 | 0.081 | 0.092 | 0.099 | 0.120 | 0.139 | 0.152 | 0.152 |
| 80-0340 | 0.053 | 0.063 | 0.072 | 0.076 | 0.080 | 0.082 | 0.084 | 0.086 | 0.088 | 0.094 |
| 80-0425 | 0.095 | 0.113 | 0.128 | 0.136 | 0.143 | 0.147 | 0.156 | 0.163 | 0.168 | 0.170 |
| 80-0440 | 0.041 | 0.046 | 0.049 | 0.052 | 0.057 | 0.061 | 0.068 | 0.072 | 0.078 | 0.084 |
| 80-0460 | 0.091 | 0.109 | 0.124 | 0.134 | 0.152 | 0.163 | 0.190 | 0.211 | 0.234 | 0.252 |
| 80-0540 | 0.025 | 0.029 | 0.033 | 0.036 | 0.046 | 0.053 | 0.060 | 0.063 | 0.071 | 0.098 |

NOAA Atlas 14 Volume 7 Version 2.0
A.4-21

| Station ID | 1day | 2day | 3day | 4day | 7day | 10day | 20day | 30day | 45day | 60day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80-0560 | 0.050 | 0.053 | 0.056 | 0.058 | 0.062 | 0.064 | 0.067 | 0.069 | 0.072 | 0.079 |
| 80-0640 | 0.090 | 0.097 | 0.103 | 0.107 | 0.114 | 0.118 | 0.126 | 0.131 | 0.139 | 0.151 |
| 80-0780 | 0.063 | 0.072 | 0.079 | 0.083 | 0.086 | 0.087 | 0.089 | 0.090 | 0.092 | 0.095 |
| 80-0820 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 | 0.060 |
| 80-0860 | 0.076 | 0.077 | 0.079 | 0.082 | 0.097 | 0.109 | 0.116 | 0.119 | 0.123 | 0.132 |
| 80-0900 | 0.057 | 0.074 | 0.088 | 0.097 | 0.109 | 0.114 | 0.116 | 0.116 | 0.118 | 0.119 |
| 80-0920 | 0.126 | 0.141 | 0.155 | 0.168 | 0.202 | 0.230 | 0.305 | 0.367 | 0.439 | 0.486 |
| 80-0940 | 0.043 | 0.048 | 0.052 | 0.055 | 0.059 | 0.062 | 0.067 | 0.070 | 0.075 | 0.086 |
| 80-1020 | 0.048 | 0.059 | 0.069 | 0.076 | 0.089 | 0.096 | 0.111 | 0.121 | 0.133 | 0.143 |
| 80-1060 | 0.049 | 0.051 | 0.053 | 0.055 | 0.059 | 0.061 | 0.066 | 0.069 | 0.072 | 0.073 |
| 80-1100 | 0.038 | 0.044 | 0.049 | 0.053 | 0.064 | 0.072 | 0.085 | 0.093 | 0.104 | 0.120 |
| 80-1120 | 0.082 | 0.098 | 0.113 | 0.123 | 0.138 | 0.147 | 0.167 | 0.182 | 0.200 | 0.218 |
| 80-1140 | 0.098 | 0.107 | 0.116 | 0.123 | 0.137 | 0.148 | 0.174 | 0.194 | 0.223 | 0.256 |
| 80-1180 | 0.087 | 0.103 | 0.117 | 0.126 | 0.137 | 0.143 | 0.154 | 0.161 | 0.173 | 0.200 |
| 80-1220 | 0.045 | 0.049 | 0.053 | 0.055 | 0.059 | 0.062 | 0.072 | 0.081 | 0.093 | 0.106 |
| 80-1240 | 0.072 | 0.080 | 0.088 | 0.095 | 0.121 | 0.138 | 0.150 | 0.158 | 0.162 | 0.162 |
| 80-1280 | 0.052 | 0.057 | 0.062 | 0.064 | 0.070 | 0.072 | 0.074 | 0.074 | 0.076 | 0.080 |
| 80-1300 | 0.071 | 0.087 | 0.100 | 0.105 | 0.102 | 0.098 | 0.102 | 0.111 | 0.131 | 0.178 |
| 80-1320 | 0.058 | 0.067 | 0.074 | 0.080 | 0.093 | 0.100 | 0.109 | 0.113 | 0.120 | 0.130 |
| 80-1340 | 0.060 | 0.076 | 0.090 | 0.100 | 0.119 | 0.130 | 0.152 | 0.168 | 0.180 | 0.183 |
| 80-1360 | 0.031 | 0.034 | 0.038 | 0.041 | 0.050 | 0.059 | 0.089 | 0.118 | 0.157 | 0.185 |
| 80-1380 | 0.226 | 0.232 | 0.238 | 0.244 | 0.261 | 0.279 | 0.346 | 0.420 | 0.515 | 0.578 |
| 80-1400 | 0.050 | 0.054 | 0.057 | 0.060 | 0.066 | 0.070 | 0.074 | 0.076 | 0.080 | 0.088 |
| 80-1420 | 0.057 | 0.066 | 0.074 | 0.081 | 0.099 | 0.110 | 0.126 | 0.136 | 0.147 | 0.157 |
| 80-1440 | 0.054 | 0.058 | 0.063 | 0.068 | 0.088 | 0.105 | 0.135 | 0.157 | 0.171 | 0.171 |
| 80-1460 | 0.040 | 0.041 | 0.042 | 0.042 | 0.043 | 0.043 | 0.043 | 0.044 | 0.044 | 0.044 |
| 80-1480 | 0.081 | 0.092 | 0.101 | 0.107 | 0.116 | 0.122 | 0.143 | 0.163 | 0.187 | 0.205 |
| 80-1540 | 0.051 | 0.060 | 0.068 | 0.073 | 0.084 | 0.090 | 0.099 | 0.104 | 0.111 | 0.119 |
| 80-1740 | 0.038 | 0.044 | 0.049 | 0.054 | 0.067 | 0.077 | 0.093 | 0.103 | 0.120 | 0.153 |
| 80-1760 | 0.079 | 0.086 | 0.093 | 0.099 | 0.114 | 0.124 | 0.140 | 0.149 | 0.166 | 0.201 |
| 80-1900 | 0.051 | 0.052 | 0.053 | 0.054 | 0.057 | 0.060 | 0.069 | 0.078 | 0.090 | 0.100 |
| 80-1940 | 0.070 | 0.075 | 0.081 | 0.085 | 0.097 | 0.105 | 0.113 | 0.117 | 0.122 | 0.129 |
| 80-1980 | 0.033 | 0.036 | 0.039 | 0.041 | 0.052 | 0.059 | 0.065 | 0.068 | 0.072 | 0.078 |
| 80-2000 | 0.075 | 0.088 | 0.100 | 0.109 | 0.126 | 0.136 | 0.147 | 0.154 | 0.158 | 0.158 |
| 80-2040 | 0.061 | 0.069 | 0.077 | 0.085 | 0.110 | 0.131 | 0.170 | 0.199 | 0.223 | 0.233 |
| 80-2080 | 0.082 | 0.086 | 0.089 | 0.092 | 0.099 | 0.104 | 0.113 | 0.118 | 0.123 | 0.125 |
| 80-2120 | 0.073 | 0.086 | 0.097 | 0.106 | 0.125 | 0.136 | 0.146 | 0.151 | 0.159 | 0.171 |
| 80-2140 | 0.112 | 0.125 | 0.137 | 0.144 | 0.154 | 0.158 | 0.163 | 0.166 | 0.170 | 0.180 |
| 80-2160 | 0.056 | 0.061 | 0.065 | 0.070 | 0.086 | 0.100 | 0.132 | 0.158 | 0.180 | 0.186 |
| 80-2320 | 0.065 | 0.076 | 0.085 | 0.090 | 0.097 | 0.100 | 0.104 | 0.106 | 0.110 | 0.120 |
| 80-2340 | 0.076 | 0.081 | 0.084 | 0.087 | 0.091 | 0.093 | 0.094 | 0.094 | 0.095 | 0.100 |
| 80-2380 | 0.055 | 0.069 | 0.082 | 0.090 | 0.104 | 0.110 | 0.115 | 0.116 | 0.120 | 0.130 |
| 80-2440 | 0.056 | 0.058 | 0.059 | 0.060 | 0.062 | 0.064 | 0.071 | 0.079 | 0.090 | 0.100 |
| 80-2560 | 0.051 | 0.056 | 0.061 | 0.065 | 0.075 | 0.080 | 0.087 | 0.090 | 0.095 | 0.104 |
| 80-2620 | 0.042 | 0.045 | 0.047 | 0.050 | 0.058 | 0.063 | 0.067 | 0.070 | 0.072 | 0.072 |
| 80-2640 | 0.077 | 0.080 | 0.082 | 0.084 | 0.092 | 0.099 | 0.116 | 0.131 | 0.151 | 0.169 |
| 80-2700 | 0.094 | 0.100 | 0.106 | 0.110 | 0.117 | 0.120 | 0.122 | 0.122 | 0.123 | 0.129 |
| 90-0001 | 0.103 | 0.147 | 0.186 | 0.216 | 0.277 | 0.319 | 0.430 | 0.520 | 0.606 | 0.644 |

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# Final Report <br> Production of Precipitation Frequency Grids for Alaska Using a Specifically Optimized PRISM System 

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## 1. Project Goal

The Hydrometeorological Design Studies Center (HDSC) within the Office of Hydrologic Development of NOAA's National Weather Service is updating precipitation frequency estimates for Alaska. In order to complete the spatial interpolation of point estimates, HDSC requires spatially interpolated grids of MAM (Mean Annual Maximum) precipitation. The contractor, the PRISM Climate Group at Oregon State University (OSU), was tasked with producing a series of grids for precipitation frequency estimation using an optimized system based on the Parameter-elevation Regressions on Independent Slopes Model (PRISM) and HDSC-calculated point estimates for the state of Alaska.

## 2. Background

HDSC used L-moment based regional frequency analysis approach to estimate precipitation frequencies. In this approach, the mean of the underlying precipitation frequency distribution is estimated at point locations with a sufficient history of observations. The form of the distribution and its parameters are estimated regionally. Once the form of the distribution has been selected and its parameters have been estimated, precipitation frequency estimates can be computed from grids of the MAM. The grids that are the subject of this report are spatially interpolated grids of the point estimates of the MAM for various precipitation durations. The point estimates of the MAM were provided by HDSC. HDSC selected an appropriate precipitation frequency distribution along with regionally estimated parameters and used this information with the grids of the MAM to derive grids of precipitation frequency estimates.

The PRISM Climate Group has previously performed similar work to produce spatially interpolated MAM grids for updates of precipitation frequency estimates in the Semiarid Southwest United States, the Ohio River Basin and Surrounding States, Puerto Rico/US Virgin Islands, Hawaiian Islands and Alaska study areas.

## 3. Report

This report describes tasks performed to produce draft mean annual maximum (MAM) grids for 15 precipitation durations: $1,2,3,6$, and 12 hours; and $1,2,3,4,7,10,20,30,45$, and 60 days for AK. The tasks described were not necessarily performed in the order described, nor were they performed just once. The process was dynamic and had numerous feedbacks.

### 3.1. Adapting the PRISM system

The PRISM modeling system was adapted for use in this project after a small investigation was performed for the Semiarid Southwest United States, and subsequently used in the Ohio River Basin and Surrounding States, Puerto Rico/Virgin Islands, Hawaiian Islands, and Alaska study areas. This investigation and adaptation procedure is summarized below.

PRISM is a knowledge-based system that uses point data, a digital elevation model (DEM), and many other geographic data sets to generate gridded estimates of climatic parameters (Daly et al. 1994, 2002, $2003,2006,2008)$ at monthly to daily time scales. Originally developed for precipitation estimation, PRISM has been generalized and applied successfully to temperature, among other parameters. PRISM has been used extensively to map precipitation, dew point, and minimum and maximum temperature over the United States, Canada, China, and other countries. Details on PRISM formulation can be found in Daly et al. (2002, 2003, 2008), which are available from http://prism.oregonstate.edu/docs/.

Adapting the PRISM system for mapping precipitation frequencies required an approach slightly different than the standard modeling procedure. The amount of station data available to HDSC for precipitation frequency was much less than that available for high-quality precipitation maps, such as the peer-reviewed PRISM 1971-2000 mean precipitation maps (Daly et al. 2008). Data sources suitable for long-term mean precipitation but not for precipitation frequency included snow courses, short-term COOP stations, remote storage gauges, and others. In addition, data for precipitation durations of less than 24 hours were available from hourly precipitation stations only. This meant that mapping precipitation frequency using HDSC stations would sacrifice a significant amount of the spatial detail present in the 1971-2000 mean precipitation maps.

A pilot project to identify ways of capturing more spatial detail in the precipitation frequency maps was undertaken. Early tests showed that mean annual precipitation (MAP) was an excellent predictor of precipitation frequency in a local area, much better than elevation, which is typically used as the underlying, gridded predictor variable in PRISM applications. In these initial tests, the DEM, the predictor grid in PRISM, was replaced by the official USDA digital map of MAP for the lower 48 states (USDA-NRCS 1998, Daly et al. 2000). Detailed information on the creation of the USDA PRISM precipitation grids is available from Daly and Johnson (1999). MAP was found to have superior predictive capability over the DEM for locations in the southwestern US. The relationships between MAP and precipitation frequency were strong because many of the effects of various physiographic features on mean precipitation patterns had already been incorporated into the MAP grid from PRISM. Preliminary PRISM maps of 2-year and 100-year, 24-hour precipitation were made for the Semiarid Southwest and compared to hand-drawn HDSC maps of the same statistics. Differences were minimal, and mostly related to differences in station data used.

Further investigation found that the square-root transformation of MAP produced somewhat more linear, tighter and cleaner regression functions, and hence, more stable predictions, than the untransformed values; this transformation was incorporated into subsequent model applications. Squareroot MAP was a good local predictor of not only longer-duration precipitation frequency statistics, but for short-duration statistics, as well. Therefore, it was determined that a modified PRISM system that used square-root MAP as the predictive grid was suitable for producing high-quality precipitation frequency maps for this project.

For this study, an updated official USDA grid of MAP for AK (1971-2000 average) was used (Figure 1). This grid was developed under funding from the USDOI National Park Service (Daly et al. 2009).

### 3.2. PRISM configuration and operation for Alaska

In general, PRISM interpolation consists of a local moving-window regression function between a predictor grid and station values of the element to be interpolated. The regression function is guided by an encoded knowledge base and inference engine (Daly et al., 2002, 2008). This knowledge base/inference engine is a series of rules, decisions and calculations that set weights for the station data points entering the regression function. In general, a weighting function contains knowledge about an important relationship between the climate field and a geographic or meteorological factor. The inference engine sets values for input parameters by using default values, or it may use the regression function to infer grid cell-specific parameter settings for the situation at hand. PRISM acquires knowledge through assimilation of station data, spatial data sets such as MAP and others, and a control file containing parameter settings.

The other center of knowledge and inference is that of the user. The user accesses literature, previously published maps, spatial data sets, and a graphical user interface to guide the model application. One of the most important roles of the user is to form expectations for the modeled climatic patterns, i.e., what is deemed "reasonable." Based on knowledgeable expectations, the user selects the station weighting algorithms to be used and determines whether any parameters should be changed from their default values. Through the graphical user interface, the user can click on any grid cell, run the model with a given set of algorithms and parameter settings, view the results graphically, and access a traceback of the decisions and calculations leading to the model prediction.

For each grid cell, the moving-window regression function for MAM vs. MAP took the form MAM value $=\beta_{1} * \operatorname{sqrt}(\mathrm{MAP})+\beta_{0}$
where $\beta_{l}$ is the slope and $\beta_{0}$ is the intercept of the regression equation, and MAP is the grid cell value of mean annual precipitation.

Upon entering the regression function, each station was assigned a weight that is based on several factors. For PRISM MAP mapping (used as the predictor grid in this study), the combined weight of a station was a function of distance, elevation, cluster, vertical layer, topographic facet, coastal proximity, and effective terrain weights, respectively. A full discussion of the general PRISM station weighting functions is available from Daly et al. (2008).

Given that the MAP grid incorporated detailed information about the complex spatial patterns of precipitation, only a subset of these weighting functions was needed for this study. For Alaska, the combined weight of a station was a function of distance and clustering, respectively. A station is downweighted when it is relatively from the target grid cell, or when it is clustered with other stations (which can lead to over-representation).

The moving-window regression function was populated by station data provided by the HDSC. A PRISM GUI snapshot of the moving-window relationship between MAP and 24-hour MAM in southern Alaska is shown in Figure 2.

There were relatively few stations with data for durations of 12 hours or less from which to perform the interpolation. In addition, it was clear that the spatial patterns of durations of 12 hours or less could be very different than those of durations of 24 hours or more. This issue was encountered in a previous study for Puerto Rico. During that study the following procedure was developed, and adopted here:
(1) Convert available $\leq 12$-hour station values to an MAM/24-hr MAM ratio (termed R24) by dividing by the 24 -hour values;
(2) using the station R24 data in (1), interpolate R24 values for each $\leq 12$-hour duration using PRISM;
(3) using bi-linear interpolation from the cells in the R24 grids from (2), estimate R24 at the location of each station having data for $\geq 24$-hour durations only;
(4) multiply the estimated R24 values from (3) by the 24 -hour value at each $\geq 24$-hour station to obtain estimated $\leq 12$-hour values;
(5) append the estimated stations from (4) to the $\leq 12$-hour station list to generate a station list that matches the density of that for $\geq 24$ hours; and
(6) interpolate MAM values for $\leq 12$-hour durations with PRISM, using MAP as the predictor grid.

The interpolation of R24 values using PRISM (step 2 above) is normally performed with PRISM in inverse-distance weighting (IDW) mode. However, in Alaska, a lack of station data and strong spatial gradients in R24 made it difficult for the IDW parameterization to produce an adequate field of in R24 values, especially along coastal areas in southern Alaska. R24 values are typically lower along the coast than inland. Coastal areas receive high total precipitation amounts, but intensities at short durations, as a proportion of the 24-hour values, are less than in the drier, inland areas.

Experimentation with more sophisticated parameterizations of PRISM showed that there was a useful relationship between MAP and R24 that could be used to add skill to the R24 interpolation process. Further testing indicated that the cube root of the MAP provided the most linear fit. Therefore, the moving-window regression function for R24 vs. MAP took the form

$$
\begin{equation*}
\mathrm{R} 24=\beta_{1} *(\mathrm{MAP})^{1 / 3}+\beta_{0} \tag{2}
\end{equation*}
$$

A PRISM GUI snapshot of a moving-window relationship between cube root MAP and 12-hour R24 in southern Alaska is shown in Figure 3.

Relevant PRISM parameters for applications to 60-minute R24 and 24-hour MAM statistics are listed in Tables 1 and 2, respectively. Further explanations of these parameters and associated equations are available in Daly et al. $(2002,2008)$.

The values of radius of influence $(R)$, the minimum number of total $\left(s_{t}\right)$ stations required in the regression were based on information from user assessment via the PRISM graphical user interface, and on a jackknife cross-validation exercise, in which each station was deleted from the data set one at a time, a prediction made in its absence, and mean absolute error statistics compiled (see Results section).

The input parameter that changed readily among the various durations was the default slope ( $\beta_{I d}$ ) of the regression function. Slopes are expressed in units that are normalized by the average observed value of the precipitation in the regression data set for the target cell. Evidence gathered during PRISM model development indicates that this method of expression is relatively stable in both space and time (Daly et al. 1994).

Bounds are put on the slopes to minimize unreasonable slopes that might occasionally be generated due to local station data patterns; if the slope is out of bounds and cannot be brought within bounds by the PRISM outlier deletion algorithm, the default slope is invoked (Daly et al., 2002). The maximum slope bound was set to a uniformly high value of 30.0 , to accommodate a large range of valid slopes. Lower slope bounds were generally not needed to handle extreme values, because values were within reasonable ranges. The exception was the shortest durations, where slightly negative slopes occasionally occurred; these were accommodated by setting the lower slope bound slightly below zero (Table 3). Slope default values were based on PRISM diagnostics that provided information on the distribution of slopes across the modeling region. The default value was set to approximate the average regression slope calculated by PRISM. For these applications, default slopes typically increased with increasing duration (Table 3). In general, the longer the duration, the larger the slope. This is primarily a result of higher precipitation amounts at the longer durations, and the tendency for longer-duration MAM statistics to bear a stronger and steeper relationship with MAP than shorter-duration statistics.

### 3.3. Preparation and review of draft grids

Draft grids for the 60 -minute, 24 -hour and 10 -day durations were produced and made available to HDSC for evaluation. All of the necessary station data were provided by HDSC. The process began with a careful scrutiny of the station data and PRISM behavior. A version of PRISM which predicts for stations locations in the absence of each station (termed jackknifing) was run, and stations that were difficult for PRISM to predict for were identified, and sent to HDSC for review. HDSC removed the stations, NOAA Atlas 14 Volume 6 Version 2.0
modified their values, or determined that the stations were accurate as-is. This process was performed iteratively, until an acceptable station data set was produced. The draft PRISM grids were subsequently completed and submitted to HDSC for review.

### 3.4. Final grids

Having found the revised draft grids acceptable, HDSC requested that grids for all durations be completed. Before delivering the final grids to HDSC, the PRISM Climate Group checked them for internal consistency. In other words, the value of the MAM at each grid point for each duration must be greater than the value for shorter durations at the same grid point. If an inconsistency of this nature occurs, the current convention is to start with the 24 duration as a baseline, and set longer durations to slightly higher values and shorter durations to slightly lower values. Small consistency adjustments were needed at a few scattered locations around the state. Most were in remote areas, but two were at station locations, revealing inconsistencies in the station values. The data were corrected and the model re-run.

The final delivered grids inherited the spatial resolution of the latest 1971-2000 PRISM mean annual precipitation grids for Alaska, which is 30 arc-seconds ( $\sim 800$ meters). The grid cell units are in $\mathrm{mm}^{*} 100$. Final MAM grids delivered to HDSC are as follows:

> 60 -minute
> 2 -hour
> 3-hour
> 6-hour
> 12-hour
> 24 -hour
> 48 -hour
> 3 -day
> 4-day
> 7 -day
> 10-day
> 20-day
> 30-day
> 45-day
> 60-day

Total: 15

### 3.5. Performance evaluation

PRISM cross-validation statistics for 60-minute/24-hour MAM ratio and the 60-minute, 24 -hour, 10 -day, and 60-day MAM intensities were compiled and summarized in Table 4. These errors were estimated using an omit-one jackknife method, where each station is omitted from the data set, estimated in its absence, then replaced. Since the 60 -minute/ 24 -hour MAM ratio was expressed as a percent, the percent bias and mean absolute error are the given as the bias and MAE in the original percent units (not as a percentage of the percent).

For the 60 -minute/ 24 -hour MAM ratio, the overall bias was less than one percent and the mean absolute error (MAE) about 3 percent. For the 60 -minute, 24 -hour, 10 -day, and 60 -day MAM intensities, biases were about 2 percent. MAEs for the 60 -munite, 24 -hour, 10 -day, and 60 -day durations were mostly in the $10-11$ percent range. Given that so few stations are available in Alaska, and that crossvalidation errors can be calculated only at stations, there is little doubt that the true interpolation errors in many parts of the state are higher than those shown in Table 4.

Table 1. Values of relevant PRISM parameters for interpolation of 60 -minute/24-hour mean annual maximum ratio (60-minute R24) for Alaska. See Daly et al. (2002) for details on PRISM parameters.

| Name | Description | Value |
| :---: | :---: | :---: |
| Regression Function |  |  |
| $R$ | Radius of influence | 10 km* |
| $s_{t}$ | Minimum number of total stations desired in regression | 10 stations |
| $\beta_{1 m}$ | Minimum valid regression slope | $-1.5{ }^{+}$ |
| $\beta_{1 x}$ | Maximum valid regression slope | $0.0^{+}$ |
| $\beta_{1 d}$ | Default valid regression slope | $-0.05^{+}$ |
| Distance Weighting |  |  |
| $A$ | Distance weighting exponent | 2.0 |
| $F_{d}$ | Importance factor for distance weighting | 0.5 |
| $D_{m}$ | Minimum allowable distance | 0.0 km |
| Elevation Weighting |  |  |
| $B$ | MAP weighting exponent | 1.0 |
| $F_{z}$ | Importance factor for MAP weighting | 0.5 |
| $\Delta z_{m}$ | Minimum station-grid cell MAP difference below which MAP weighting is maximum | 10\% of MAP |
| $\Delta z_{x}$ | Maximum station-grid cell MAP difference above which MAP weight is minimal | $50 \%$ of MAP upwards, $20 \%$ downwards |

* Expands to encompass minimum number of total stations desired in regression $\left(s_{t}\right)$.
${ }^{+}$Slopes are expressed in units that are normalized by the average observed value of the precipitation in the regression data set for the target cell. Units here are $1 /\left[\operatorname{cuberoot}(\mathrm{MAP}(\mathrm{mm}))^{*} 1000\right]$.

Table 2. Values of relevant PRISM parameters for modeling of 24-hour mean annual maximum statistics for Alaska. See Daly et al. (2002) for details on PRISM parameters.

| Name | Description | Value |
| :---: | :---: | :---: |
| Regression Function |  |  |
| $R$ | Radius of influence | 10 km * |
| $s_{t}$ | Minimum number of total stations desired in regression | 45 stations |
| $\beta_{\text {lm }}$ | Minimum valid regression slope | $0.0^{+}$ |
| $\beta_{l x}$ | Maximum valid regression slope | $30.0^{+}$ |
| $\beta_{1 d}$ | Default valid regression slope | $2.8{ }^{+}$ |
| Distance Weighting |  |  |
| A | Distance weighting exponent | 2.0 |
| $F_{d}$ | Importance factor for distance weighting | 1.0 |
| $D_{m}$ | Minimum allowable distance | 0.0 km |
| Elevation Weighting |  |  |
| $B$ | Elevation weighting exponent | 0.0 |
| $F_{z}$ | Importance factor for elev weighting | 0.0 |
| $\Delta z_{m}$ | Minimum station-grid cell elev difference below which MAP weighting is maximum | NA |
| $\Delta z_{x}$ | Maximum station-grid cell elevation difference above which station is given minimal weighting | 50 m upwards, 5000 m downwards |

[^0]Table 3. Values of PRISM slope parameters for modeling of MAM statistics for Alaska for all durations. For durations of 12 hours and below, station data were expressed as the ratio of the given duration's MAM value to the 24-hour MAM value, and interpolated; this was followed by an interpolation of the actual MAM values. See text for details. See Table 1 for definitions of parameters.

|  | Alaska |  |  |
| :--- | :---: | :---: | :---: |
| Duration | $\boldsymbol{\beta}_{\boldsymbol{1 m}}$ | $\boldsymbol{\beta}_{\boldsymbol{1} \boldsymbol{x}}$ | $\boldsymbol{\beta}_{\boldsymbol{l d}}$ |
| 1h/24h ratio | -1.5 | 0.0 | -0.05 |
| 2h/24h ratio | -1.5 | 0.0 | -0.05 |
| 3h/24h ratio | -1.5 | 0.0 | -0.05 |
| 6h/24h ratio | -1.5 | 0.0 | -0.05 |
| 12h/24h ratio | -1.5 | 0.0 | -0.05 |
|  |  |  |  |
| 1 hour MAM | -0.5 | 30.0 | 2.3 |
| 2 hour MAM | -0.5 | 30.0 | 2.3 |
| 3 hour MAM | -0.3 | 30.0 | 2.4 |
| 6 hour MAM | -0.2 | 30.0 | 2.5 |
| 12 hour MAM | 0.0 | 30.0 | 2.7 |
| 24 hour MAM | 0.0 | 30.0 | 2.8 |
| 48 hour MAM | 0.0 | 30.0 | 3.0 |
| 3 day MAM | 0.0 | 30.0 | 3.1 |
| 4 day MAM | 0.0 | 30.0 | 3.2 |
| 7 day MAM | 0.0 | 30.0 | 3.6 |
| 10 day MAM | 0.0 | 30.0 | 3.8 |
| 20 day MAM | 0.0 | 30.0 | 4.2 |
| 30 day MAM | 0.0 | 30.0 | 4.5 |
| 45 day MAM | 0.0 | 30.0 | 4.6 |
| 60 day MAM | 0.0 | 30.0 | 4.8 |

Table 4. PRISM cross-validation errors for 60-minute/24-hour MAM ratio and 24-hour, 10-day, and 60-day MAM applications to Alaska. Since the 60 -minute/ 24 -hour MAM ratio was expressed as a percent, the percent bias and mean absolute error are the given as the bias and MAE in the original percent units (not as a percentage of the percent).

| Statistic | $\mathbf{N}$ | \% Bias | \% MAE |
| :--- | :---: | :---: | :---: |
| 60-min/24-hr MAM ratio | 123 | 0.13 | 3.15 |
| 60-minute MAM | 353 | 1.62 | 10.31 |
| 24-hour MAM | 353 | 1.95 | 9.86 |
| 10-day MAM | 352 | 2.28 | 11.20 |
| 60-day MAM | 352 | 2.11 | 10.92 |



Figure 1. PRISM 1971-2000 mean annual precipitation (MAP) grid for Alaska.


Figure 2. PRISM GUI snapshot of the moving-window weighted regression between the square root of mean annual precipitation and 24 -hour mean annual maximum precipitation (MAM) in south-central Alaska. Regression is for the pixel marked with the black "+". Stations are shown with a white "+".


Figure 3. PRISM GUI snapshot of the moving-window weighted regression between the cube root of mean annual precipitation and 12-hour R24 (ratio of 12-hour to 24-hour MAM, expressed in percent) in south-central Alaska. Regression is for the pixel marked with the black "+". Stations are shown with a red "+".

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## Appendix A. 6 Peer review comments and responses

A peer review of preliminary results for the Alaska precipitation frequency project was carried out during a four week period starting on August 2, 2011. The request for review was sent via email to the over 600 members of the HDSC list-server from all over the United States and other interested parties in Alaska. Potential reviewers were asked to evaluate the reasonableness of point precipitation frequency estimates as well as their spatial patterns. The review included the following items:

1. List of all stations used in the analysis. The list included information on station name, state, name of agency that provided data, assigned station ID, latitude, longitude, elevation, and period of record. It also showed information if the station was merged with another station, if the station was co-located with another station with a different ID, and if metadata at the station were changed.
2. List of all stations that were received by HDSC, but not considered in analysis. This list contained stations that were not used, either because there was another station with a longer period of record nearby, station data were not reliable, or the station period of record was not long enough and it was not a candidate for merging with any nearby station.
3. Spatially-interpolated estimates of mean annual maxima for 60 -minute, 24 -hour and 10 -day durations.
4. Spatially-interpolated precipitation frequency estimates for 60 -minute, 24 -hour and 10 -day durations and for 2 -year and 100 -year ARIs.
5. At-station depth-duration-frequency curves for 60 -minute to 10 -day durations and for 2-year to 100 -year average recurrence intervals (ARI).
Four reviews were received. All reviewers' comments and HDSC's responses are shown below.
The comments and their respective HDSC responses have been divided in four categories:
6. Station metadata;
7. At-station precipitation frequency estimates;
8. Precipitation frequency grids/maps;
9. Additional and supplementary information.

## 1. Comments pertaining to station metadata

1.1 List of stations used in analysis: elevation of Chistochina appears to be in error - reads 180 and should be 1800 .

HDSC response: Elevation of Chistochina station was changed to 1800 feet.

## 2. Comments pertaining to at-station precipitation frequency estimates

2.1 Station Amchitka is labeled Attuhitka on the DDF curve. As an aside, this station also has surprisingly low rainfall compared to nearby Aleutian stations.

HDSC response: The station name in our records is Amchitka and was mislabeled on the curve for the peer review. Annual maximum series at Amchitka station were revisited and a decision
was made not to use this station's data in the analysis. The station's period of record was relatively short with long spans of missing data. The station recorded data during relatively dry periods causing estimates to be much lower than corresponding estimates at nearby stations.
2.2 Why are so many fewer stations shown on the 2 -yr 60-minute map, when all stations have data for 2 -yr 1-hr on the frequency curves?

HDSC response: On the 60-minute map we showed only locations of stations that have measurements at hourly durations (stations recording at 15-minute and/or 1-hour intervals). The contour lines on the map were created from gridded PDS-based precipitation frequency estimates that were obtained through spatial interpolation of at-station precipitation frequency estimates. These gridded hourly estimates were used to display depth-duration-frequency curves at each station.
2.3 Short duration precip maxima in Interior Alaska are completely a function of summer convection. It is therefore somewhat disconcerting to see that hourly precipitation data from a number of SNOTEL sites (e.g. MSOA2, EAGA2, MTRA2) equipped with tipping bucket gauges were not used in the construction of the products.

HDSC response: During the initial quality control effort, it was decided to exclude stations from hourly SNOTEL dataset due to their short periods of record and significant number of missing data. In addition, aggregated amounts at 24-hour duration were frequently considerably lower than corresponding 1-day amounts obtained from co-located daily SNOTEL stations. However, after further review of the dataset that was prompted by this comment, a decision was made to include two hourly SNOTEL stations that have reasonable records relative to their co-located daily stations.

## 3. Comments pertaining to precipitation frequency grids/maps

3.1 I reviewed approximately 40 at-station frequency estimates (Kenai Peninsula, Seward Peninsula, Fairbanks Area and North Slope of Alaska) and the estimates appear to match my local knowledge and seem to be representative. The frequency contour maps seem reasonable and the spatial distribution matches my limited local knowledge of the entire state. The two extreme locations in SE Alaska are interesting considering that there are no station data within the extreme isopluvials. These two areas seem to match up with similar areas shown in HR. No. 54.

HDSC response: Estimates in areas with no stations were developed through spatial interpolation of at-station estimates using hybrid statistical-geographic techniques for mapping climate (described in Section 4.8 of this document) and are influenced, among other factors, by terrain.
3.2 Smoothing and interpolation generally appear consistent with measurements and terrain. There are a few places where isolines are drawn around isolated stations, because the station measurements are higher/lower than the surrounding interpolated areas. These would indicate islands of higher/lower rainfall where there isn't enough data to determine that this is really true. I only list the ones below that do not have an apparent terrain influence that would support showing them as different than the surrounding area.

- Willow West - this station is shown as an "island" on the 2-yr/24-hr map, despite not having any apparent topographic isolation from surrounding areas. The isoline ( 2 inches) seems to be right at the $2-\mathrm{yr} / 24 \mathrm{hr}$ estimate for the station.
- Holy Cross and Cape Romanzof on the 10 -day MAM map both are in their own "islands" without apparent topographic reasons
- On 2-year 10-day map, there are separate "islands" around Gulkana and Gakona, while the curves suggest that the isoline might be drawn around Gulkana, Gakona, and Klawasi to distinguish that area of lower precip.

HDSC response: A single contour line around an isolated station can occur frequently and is typically of little concern. Although it may appear from a cartographic map that an at-station estimate is much higher/lower than surrounding estimates, when the actual gridded estimates that were used to create the map are compared, the differences are typically minor. However, there can be cases where at-station estimates are very different from nearby interpolated values (resulting in several contour lines around a station); an effort was made to scrutinize such cases. After the peer review, an alternative interpolation technique was developed for this project area to address the inability of the interpolation technique used in the peer review (and in previous studies) to produce spatial patterns in line with expected climatological patterns, especially for ARIs of 100-years or more and in areas with very few stations (see Section 4.8 for more details). Therefore, estimates in areas surrounding the locations singled out in this comment have changed. The resulting spatial patterns were improved.
3.3 It looks to me like the maximum one hour precip in Interior Alaska are too low. In the area of maximum convection (Yukon-Tanana uplands), two year return period amounts should at least 0.50 inches and 10 year returns should be something near or a little below one inch. This seems to be supported on the "MEAN ANNUAL MAXIMUM PRECIPITATION FOR 60-MINUTES DURATION" map that shows a number "bulleyes" near stations that were used in the analysis.

HDSC response: Please see response to comment 3.2. As a result of the updated interpolation approach, estimates across interior Alaska changed and are more in line with expectations. Mean annual maximum (MAM) estimates for hourly durations were adjusted at locations where they appeared to be low, but the range of MAMs in this area remains the same ( 0.40 to 0.50 inches), which is consistent with observed data.
3.4 The map of isopluvials with 100 year return period seems much too low over some portions of the uplands north and west of Fairbanks, though here the "bullseyes" seem to be on the low side. It is meteorologically unreasonable that the 100 return period of one hour precip would be higher over the Tanana Flats, south of Fairbanks, than over the higher terrain to the north.

HDSC response: After the peer review, several unreliable stations in this region with short records were deleted. The new estimates are more in-line with expectations.

## 4. Comments pertaining to additional and supplementary information

4.1 Suggestion I have would be to add a column to the "Gages not used" table explaining why some gages were excluded from analysis. For most locations the reasons are obvious (not a long
enough period of record or duplicate gage). But some locations, such as the Fort Greeley/Allen A gage (70-2670), were unclear as to why they were excluded.

HDSC response: In Section 4.4 of this document we provide a description of the screening process and why stations may not be used in the frequency analysis; we do not provide information on individual stations not retained. Hourly station 70-2670 was deleted because the station was missing about $97 \%$ of the precipitation observations during its period of record.
4.2 It would be useful for future planning purposes to include a flag in the 'Stations Not Included' data file that describes why a station was not used in the analysis (reliability, proximity, short record, etc.). This could aid in coordinating future precipitation data collection throughout the state.

HDSC response: Please see response to comment 4.1; this suggestion will be considered for future peer reviews.
4.3. Suggest selectively including intermediate isopluvials in the Central, Western and Northern portions of the state to add more detail to these areas.

HDSC response: We purposefully keep the contour intervals on cartographic maps constant. Please keep in mind that cartographic maps were created to serve only as visual aids. Users are advised to take advantage of the PFDS interface or the underlying ASCII grids for obtaining precipitation frequency estimates. Additionally, a user can contour the grids specifically for their area of interest.
4.4 Suggest that a temporal analysis (similar to HI Atlas 14 update) and comparison to previous precipitation estimates be included in the final report.

HDSC response: The temporal analysis and comparison of new and previous estimates are not part of the peer review process, but are included in the final publication. The temporal analysis is described in the Appendix A.7, and temporal distributions are available from the PFDS web page when any point is selected in the project area. The comparison of updated and previous estimates (from Technical Paper No. 47) is available in Section 7.

## Appendix A. 7 Temporal distributions of heavy precipitation

## 1. Introduction

Temporal distributions of precipitation amounts exceeding precipitation frequency estimates for the 2-year recurrence interval are provided for $6-, 12-, 24-$, and 96 -hour durations. The temporal distributions are expressed in probability terms as cumulative percentages of precipitation totals at various time steps. To provide detailed information on the varying temporal distributions, separate temporal distributions were also derived for four precipitation cases defined by the duration quartile in which the greatest percentage of the total precipitation occurred. To increase sample sizes, stations from the Arctic, Interior, West Coast and Southwest Interior climate regions were grouped in the Northern Region and Southwest Islands, Cook Inlet, and South/Southeast Coast regions into the Southern Region (see Section 4.1 and Figure 4.1.2).

## 2. Methodology and results

The methodology used to produce the temporal distributions is similar to the one developed by Huff (1967) except in the definition of precipitation cases. In accordance with the way a precipitation case ('event') was defined for the precipitation frequency analysis, a precipitation case for the temporal distribution analysis was computed as the total accumulation over a specific duration (6-, 12-, 24-, or 96-hours). As a result, it may contain parts of one or more storms. Because of that, temporal distribution curves presented here may be different from corresponding temporal distribution curves obtained from the analysis of single storms.

Also, precipitation cases for this project always start with precipitation but do not necessarily end with precipitation, resulting in potentially more front-loaded cases when compared with distributions derived from the single storm approach. Cases were selected from all events of a given duration that exceeded the 2 -year average recurrence interval at each station. Table A.7.1 shows the total number of precipitation cases and number of cases in each quartile for each region and duration.

For each precipitation case, cumulative precipitation amounts were converted into percentages of the total precipitation amount at one hour time increments. All cases for a specific duration were then combined and probabilities of occurrence of precipitation totals were computed at each hour. The temporal distribution curves for nine deciles ( $10 \%$ to $90 \%$ ) were smoothed using linear programming method (Bonta and Rao, 1988) and plotted in the same graph. Figure A.7.1 shows as an example of temporal distribution curves computed from all cases for the four selected durations for the Southern Region; time steps were converted into percentages of durations for easier comparison.

The cases were further divided into four categories by the quartile in which the greatest percentage of the total precipitation occurred. Table A.7.1 shows the numbers and proportion of precipitation cases used to derive the temporal distributions in each quartile. Unlike the cases of 12-, 24-, and 96-hour durations in which the number of data points can be equally divided by four, the cases of 6-hour duration contain only six data points and they cannot be evenly distributed into four quartiles. Therefore, in this analysis, for the 6 -hour duration, the first quartile contains precipitation cases where the most precipitation occurred in the first hour, the second quartile contains precipitation cases where the most precipitation occurred in the second and third hours, the third quartile contains precipitation cases where the most precipitation occurred in the fourth hour, and the fourth quartile contains precipitation cases where the most precipitation occurred in the fifth and sixth hours. This uneven distribution affects the number of cases contained in each quartile for the 6 -hour duration. Figures A.7.2 through A.7.5 show the Southern Region's temporal distribution curves for the four quartile cases for 6 -hour, 12 -hour, 24 -hour and 96 -hour durations, respectively.

Table A.7.1. Total number of precipitation cases and number (and percent) of cases in each quartile for selected durations for each climate region.

| Duration | Region | All cases | First- <br> quartile <br> cases | Second- <br> quartile <br> cases | Third- <br> quartile <br> cases | Fourth- <br> quartile <br> cases |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Northern Region | 785 | $273(35 \%)$ | $247(31 \%)$ | $186(24 \%)$ | $79(10 \%)$ |
|  | Southern Region | 363 | $60(16 \%)$ | $130(36 \%)$ | $101(28 \%)$ | $72(20 \%)$ |
| $\mathbf{1 2}$-hour | Northern Region | 825 | $292(36 \%)$ | $233(28 \%)$ | $200(24 \%)$ | $100(12 \%)$ |
|  | Southern Region | 391 | $69(18 \%)$ | $133(34 \%)$ | $129(33 \%)$ | $60(15 \%)$ |
| 24-hour | Northern Region | 680 | $242(36 \%)$ | $186(27 \%)$ | $153(22 \%)$ | $99(15 \%)$ |
|  | Southern Region | 324 | $53(16 \%)$ | $113(35 \%)$ | $109(34 \%)$ | $49(15 \%)$ |
| 96-hour | Northern Region | 688 | $299(43 \%)$ | $145(21 \%)$ | $129(19 \%)$ | $115(17 \%)$ |
|  | Southern Region | 301 | $114(38 \%)$ | $64(21 \%)$ | $54(18 \%)$ | $69(23 \%)$ |

From the Precipitation Frequency Data Server, regional temporal distribution data are available in a tabular form for a selected location under the 'Supplementary information' tab or through the temporal distribution web page (http://hdsc.nws.noaa.gov/hdsc/pfds/pfds temporal.html). For 6-, 12- and 24-hour durations, temporal distribution data are provided in 0.5 -hour increments and for 96 -hour duration in hourly increments.

## 3. Interpretation

Figure A.7.1 shows as an example the temporal distribution curves of all precipitation cases in the Southern Region for the 6 -, 12-, 24 -, and 96 -hour durations. Time steps were converted into percentages of total durations for easier comparison. Figures A.7.2 through A.7.5 show temporal distribution curves for first-, second-, third-, and fourth-quartile cases for 6-hour, 12-hour, 24-hour and 96 -hour durations, respectively. First-quartile plots show temporal distribution curves for cases where the greatest percentage of the total precipitation fell during the first quarter of the duration (e.g., the first 3 hours of a 12 -hour duration). The second, third, and fourth quartile plots are similarly for cases where the most precipitation fell in the second, third, or fourth quarter of the duration.

The temporal distribution curves represent the averages of many cases and illustrate the temporal distribution patterns with $10 \%$ to $90 \%$ occurrence probabilities in $10 \%$ increments. For example, the $10 \%$ curve in any figure indicates that $10 \%$ of the corresponding precipitation cases had distributions that fell above and to the left of the curve. Similarly, $10 \%$ of the cases had temporal distribution falling to the right and below the $90 \%$ curve. The $50 \%$ curve represents the median temporal distribution.

The following is an example of how to interpret the results using the figure (a) in the upper left panel of Figure A. 7.4 for 24 -hour first-quartile cases in the Southern Region.

- In $10 \%$ of the first-quartile cases, $50 \%$ of the total precipitation fell in the first 4.3 hours ( $18 \%$ of duration) and $90 \%$ of the total precipitation fell by 10.7 hours ( $44.8 \%$ of duration).
- A median case of this type will drop half of the precipitation ( $50 \%$ on the $y$-axis) in approximately 8.1 hours.
- In $90 \%$ of the cases, $50 \%$ of the total precipitation fell by 12.4 hours ( $52 \%$ of duration) and $90 \%$ of precipitation fell by 22.3 hours ( $94 \%$ of duration).
Temporal distribution curves are provided in order to show the range of possibilities. Care should be taken in the interpretation and use of temporal distribution curves. For example, the use of different temporal distribution data in hydrologic models may result in very different peak flow estimates. Therefore, they should be selected and used in a way to reflect users' objectives.


Figure A.7.1. Temporal distribution curves for the Southern Region all cases for: a) 6-hour, b) 12-hour, c) 24 -hour, and d) 96 -hour durations.


Figure A.7.2. 6-hour temporal distribution curves for the Southern Region: a) first-quartile, b) secondquartile, c) third-quartile, and d) fourth-quartile cases.


Figure A.7.3. 12-hour temporal distribution curves for the Southern Region: a) first-quartile, b) secondquartile, c) third-quartile, and d) fourth-quartile cases.


Figure A.7.4. 24-hour temporal distribution curves for the Southern Region: a) first-quartile, b) secondquartile, c) third-quartile, and d) fourth-quartile cases.


Figure A.7.5. 96-hour temporal distribution curves for the Southern Region: a) first-quartile, b) secondquartile, third-quartile, and d) fourth-quartile cases.

## Appendix A. 8 Seasonality

## 1. Introduction

To portray the seasonality of extreme precipitation throughout the project area, annual maxima that exceeded precipitation frequency estimates (quantiles) with selected annual exceedance probabilities (AEPs) for chosen durations were examined for the Northern and Southern climate regions described in Section 4.1. Graphs showing the monthly variation of the exceedances for a region are provided for each location in the project area via the Precipitation Frequency Data Server (PFDS) at http://hdsc.nws.noaa.gov/hdsc/pfds/. For a selected location, seasonal exceedance graphs can be viewed by selecting 'V. Seasonality analysis' of the 'Supplementary information' tab on the output page.

## 2. Method

Separate seasonal exceedance graphs were created for the Northern and Southern climate regions. They show the percentage of annual maxima for a given duration from all stations in a region that exceeded corresponding precipitation frequency estimates at selected AEP levels in each month. Results are provided for unconstrained 60 -minute, 24-hour, 2-day, and 10-day durations and for AEPs of $1 / 2,1 / 5,1 / 10,1 / 25,1 / 50$, and $1 / 100$.

To prepare the graphs, first, the number of annual maxima exceeding the precipitation frequency estimate at a station for a given AEP was tabulated for each duration. Those numbers were then combined for all stations in a given region, sorted by month, normalized by the total number of data years in the region, and finally plotted via the PFDS.

## 3. Results

The exceedance graphs for a selected location (see an example for a location in the Northern Region in Figure A.8.1) indicate percent of annual maxima exceeding the quantiles with selected AEPs for various durations. The percentages are based on regional statistics. On average, $1 \%$ of annual maxima for a given duration in a year (i.e., the sum of percentages of all twelve months) are expected to exceed the $1 / 100 \mathrm{AEP}$ quantile, $4 \%$ is expected to exceed the $1 / 25 \mathrm{AEP}$ quantile, etc.

Note that seasonality graphs are not intended to be used to derive seasonal precipitation frequency estimates.


Figure A.8.1. Example of seasonal exceedance graphs for the Northern climate region for the: a) 60minute, b) 24-hour, c) 2-day, and d) 10-day durations.

## Glossary

(All definitions are given relative to precipitation frequency analyses in NOAA Atlas 14 Volume 7)

ANNUAL EXCEEDANCE PROBABILITY (AEP) - The probability associated with exceeding a given amount in any given year once or more than once; the inverse of AEP provides a measure of the average time between years (and not events) in which a particular value is exceeded at least once; the term is associated with analysis of annual maximum series (see also AVERAGE RECCURENCE INTERVAL).

ANNUAL MAXIMUM SERIES (AMS) - Time series of the largest precipitation amounts in a continuous 12 -month period (calendar or water year) for a specified duration at a given station.

ASCII GRID - Grid format with a 6 -line header, which provides location and size of the grid and precedes the actual grid data. The grid is written as a series of rows, which contain one ASCII integer or floating point value per column in the grid. The first element of the grid corresponds to the upper-left corner of the grid.
AVERAGE RECURRENCE INTERVAL (ARI; a.k.a. RETURN PERIOD, AVERAGE RETURN PERIOD) - Average time between cases of a particular precipitation magnitude for a specified duration and at a given location; the term is associated with the analysis of partial duration series. However, ARI is frequently calculated as the inverse of AEP for the annual maximum series; in this case it represents the average period between years in which a given precipitation magnitude is exceeded at least once.

CASCADE, RESIDUAL ADD-BACK (CRAB) - The HDSC-developed spatial interpolation procedure for deriving grids of precipitation frequency estimates from grids of mean annual maxima and point precipitation frequency estimates for a given duration.
CONSTRAINED OBSERVATION - A precipitation measurement or observation bound by clock hours and occurring in regular intervals. This observation requires conversion to an unconstrained value (see UNCONSTRAINED OBSERVATION) because maximum 60-minute or 24-hour amounts seldom fall within a single hourly or daily observation period.

## DATA YEARS - See RECORD LENGTH.

DEPTH-DURATION-FREQUENCY (DDF) CURVE - Graphical depiction of precipitation frequency estimates in terms of depth, duration and frequency (ARI or AEP).

DISTRIBUTION FUNCTION (CUMULATIVE DISTRIBUTION FUNCTION) - Mathematical description that completely describes frequency distribution of a random variable, here precipitation. Distribution functions commonly used to describe precipitation data include 3parameter distributions such as Generalized Extreme Value (GEV), Generalized Normal, Generalized Pareto, Generalized Logistic and Pearson type III, the 4-parameter Kappa distribution, and the 5-parameter Wakeby distribution.

FEDERAL GEOGRAPHIC DATA COMMITTEE (FGDC) COMPLIANT METADATA - A document that describes the content, quality, condition, and other characteristics of data and follows the guidelines set forth by the FGDC; metadata is "data about data."

FREQUENCY - General term for specifying the average recurrence interval or annual exceedance probability associated with specific precipitation magnitude for a given duration.
FREQUENCY ANALYSIS - Process of derivation of a mathematical model that represents the relationship between precipitation magnitudes and their frequencies.

FREQUENCY ESTIMATE - Precipitation magnitude associated with specific average recurrence interval or annual exceedance probability for a given duration.
HEAVY PRECIPITATION - Precipitation with an average recurrence interval roughly between 1 year and 1,000 years for a given duration.

INTENSITY-DURATION-FREQUENCY (IDF) CURVE - Graphical depiction of precipitation frequency estimates in terms of intensity, duration and frequency.

INTERNAL CONSISTENCY - Term used to describe the required behavior of the precipitation frequency estimates from one duration to the next or from one frequency to the next. For instance, it is required that the 100-year 3-hour precipitation frequency estimates be greater than (or at least equal to) corresponding 100-year 2-hour estimates.

L-MOMENTS - L-moments are summary statistics for probability distributions and data samples. They are analogous to ordinary moments, providing measures of location, dispersion, skewness, kurtosis, and other aspects of the shape of probability distributions or data samples, but are computed from linear combinations of the ordered data values (hence the prefix L).

MEAN ANNUAL PRECIPITATION (MAP) - The average precipitation for a year (usually calendar) based on the whole period of record or for a selected period (usually 30 year period such as 1971-2000).

PARTIAL DURATION SERIES (PDS) - Time series that includes all precipitation amounts for a specified duration at a given station above a pre-defined threshold regardless of year; it can include more than one event in any particular year.

PRECIPITATION FREQUENCY DATA SERVER (PFDS) - The on-line portal for all NOAA Atlas 14 deliverables, documentation, and information; http://hdsc.nws.noaa.gov/hdsc/pfds/.

PARAMETER-ELEVATION REGRESSIONS ON INDEPENDENT SLOPES MODEL (PRISM) Hybrid statistical-geographic approach to mapping climate data developed by Oregon State University's PRISM Climate Group.

QUANTILE - Generic term to indicate the precipitation frequency estimate associated with either ARI or AEP.

RECORD LENGTH - Number of years in which enough precipitation data existed to extract meaningful annual maxima in a station's period of record (or data years).

UNCONSTRAINED OBSERVATION - A precipitation measurement or observation for a defined duration. However the observation is not made at a specific repeating time, rather the duration is a moveable window through time.

WATER YEAR - Any 12-month period, usually selected to begin and end during a relatively dry season. In NOAA Atlas 14 Volume 7, it is defined as the calendar year (January 1 to December 31).

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[^0]:    * Expands to encompass minimum number of total stations desired in regression $\left(s_{t}\right)$.
    ${ }^{+}$Slopes are expressed in units that are normalized by the average observed value of the precipitation in the regression data set for the target cell. Units here are $1 /\left[\operatorname{sqrt}(\operatorname{MAP}(\mathrm{mm}))^{*} 1000\right]$.

