QC 801 ·U65 no.22 c.2

MDAA Technical Memorandum NOS 22



PERFORMANCE EVALUATIONS OF THE ORBISPHERE LABORATORIES MODELS 2702 AND 2709 OXYGEN MEASURING SYSTEMS

Washington, D.C. June 1979



8

NOAR NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION

National Ocean Survey



NOAA TECHNICAL MEMORANDUMS

National Ocean Survey Series

Survey (NOS) provides charts and related information for the safe navigation of herce. The survey also furnishes other Earth science data--from geodetic, hydroc, geomagnetic, seismologic, gravimetric, and astronomic surveys or observations, measurements--to protect life and property and to meet the needs of engineering, 1, industrial, and defense interests.

NOAA Technical Memorandums NOS series facilitate rapid distribution of material that may be preliminary in nature and which may be published formally elsewhere at a later date. Publications 1 through 8 are in the former series, ESSA Technical Memoranda, Coast and Geodetic Survey Technical Memoranda (C&GSTM). Beginning with 9, publications are now part of the series, NOAA Technical Memorandums NOS.

Publications listed below are available from the National Technical Information Service (NTIS), U.S. Department of Commerce, Sills Bldg., 5285 Port Royal Road, Springfield, VA 22161. Price varies for paper copy; \$3.00 microfiche. Order by accession number (in parentheses) when given.

ESSA Technical Memoranda

- C&GSTM 1 Preliminary Measurements With a Laser Geodimeter. S. E. Smathers, G. B. Lesley, R. Tomlinson, and H. W. Boyne, November 1966. (PB-174-649)
- C&GSTM 2 Table of Meters to Fathoms for Selected Intervals. D. E. Westbrook, November 1966. (PB-174-655)
- C&GSTM 3 Electronic Positioning Systems for Surveyors. Angelo A. Ferrara, May 1967. (PB-175-604)
- C&GSTM 4 Specifications for Horizontal Control Marks. L. S. Baker, April 1968. (PB-179-343)
- C&GSTM 5 Measurement of Ocean Currents by Photogrammetric Methods. Everett H. Ramey, May 1968. (PB-179-083)
- C&GSTM 6 Preliminary Results of a Geophysical Study of Portions of the Juan de Fuca Ridge and Blanco Fracture Zone. William G. Melson, December 1969. (PB-189-226)
- C&GSTM 7 Error Study for Determination of Center of Mass of the Earth From Pageos Observations. K. R. Koch and H. H. Schmid, January 1970. (PB-190-982)
- C&GSTM 8 Performance Tests of Richardson-Type Current Meters: I. Tests 1 Through 7. R. L. Swanson and R. H. Kerley, January 1970. (PB-190-983)

NOAA Technical Memorandums

- NOS 9 The Earth's Gravity Field Represented by a Simple Layer Potential From Doppler Tracking of Satellites. Karl-Rudolf Koch and Bertold U. Witte, April 1971. (COM-71-00668)
- NOS 10 Evaluation of the Space Optic Monocomparator. Lawrence W. Fritz, June 1971. (COM-71-00768)
- NOS 11 Errors of Quadrature Connected With the Simple Layer Model of the Geopotential. Karl-Rudolf Koch, December 1971. (COM-72-10135)
- NOS 12 Trends and Variability of Yearly Mean Sea Level 1893-1971. Steacy D. Hicks, March 1973. (COM-73-10670)
- NOS 13 Trends and Variability of Yearly Mean Sea Level 1893-1972. Steacy D. Hicks and James E. Crosby, March 1974. (COM-74-11012)
- NOS 14 Some Features of the Dynamic Structure of a Deep Estuary. Michael Devine, April 1974. (COM-74-10885)
- NOS 15 An Average, Long-Period, Sea-Level Series for the United States. Steacy D. Hicks and James E. Crosby, September 1975. (COM-75-11463)

(Continued on inside back cover)

NOAA Technical Memorandum NOS 22

PERFORMANCE EVALUATIONS OF THE ORBISPHERE LABORATORIES MODELS 2702 AND 2709 OXYGEN MEASURING SYSTEMS

Jerald M. Peterson, Charles C. White, Barbara S. Pijanowski, and Gary K. Ward

Test and Evaluation Laboratory Washington, D.C. June 1979

CENTRAL LIBRARY 00T1 1981 N. O. A. A. S. Dept. of Commence

UNITED STATES DEPARTMENT OF COMMERCE Juanita M. Kreps, Secretary NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION Richard A. Frank, Administrator

81 2801

National Ocean Survey Allen L. Powell, Director



This NOAA Technical Memorandum does not constitute an endorsement of any commercial product or conclude any procurement action or intend to be an opinion beyond engineering or technical facts by the National Oceanic and Atmospheric Administration. Moreover, the fact that all instruments of any one class are not evaluated and reported upon is not a reflection on the quality of the instruments not tested.

No reference shall be made to the National Oceanic and Atmospheric Administration, or to this publication furnished by the National Oceanic and Atmospheric Administration, in any advertising or sales promotion which would indicate or imply that the National Oceanic and Atmospheric Administration approves, recommends, or endorses any proprietary product or proprietary material mentioned herein, or which has as its purpose an intent to cause directly or indirectly the advertised product to be used or purchased because of this National Oceanic and Atmospheric Administration.

CONTENTS

ABSTRACT	1
INTRODUCTION	1
TEST PROCEDURE AND RESULTS	2
Temperature	2
Dissolved Oxygen	3
Response Times	4
Environmental Effects	5
Power Supply Variation Effects	5
Long-Term Stability	6
GENERAL COMMENTS	6
ACKNOWLEDGMENT	6
APPENDIX A MANUFACTURER'S PERFORMANCE SPECIFICATIONS	10
APPENDIX B PERFORMANCE SUMMARY	11
APPENDIX C GLOSSARY	12

PERFORMANCE EVALUATIONS OF THE ORBISPHERE LABORATORIES MODELS 2702 AND 2709 OXYGEN MEASURING SYSTEMS

Jerald M. Peterson Charles C. White Barbara S. Pijanowski Gary K. Ward

Test and Evaluation Laboratory National Ocean Survey, NOAA Washington, D.C.

ABSTRACT: Test and evaluation results are reported for two portable oxygen and temperature measuring systems. System descriptions, manufacturer's specifications, and performance results are provided with associated figures and tables summarizing accuracy, precision, stability, and environmental effects.

INTRODUCTION

The Orbisphere Models 2702 and 2709 Oxygen Measuring Systems are all-solid-state instruments designed to measure temperature in the range of 0°C to 50°C and dissolved oxygen concentrations from 0 to 20 ppm (mg/l) and 0 to 30 ppm, respectively. The electronics section may be powered by any battery possessing a voltage from 5.5 to 10 volts. A 9-volt "transistor" battery will provide 180 days of continuous operation. The detector section uses the polarographic membrane technique with a gold cathode and silver anode. Thermistors are used to provide temperature compensation to correct for the nonlinearity of the oxygen membrane permeability curve versus temperature. The temperature compensation is automatic from 0°C to 45°C. The protected sensing head has a maximum diameter of 15 mm. It may be used

1

for measurements in NS 19 to NS 24 flasks fitted with special sleeves. The sensor has a built-in stirrer with a battery life of 8.6 hours of continuous use. A minimum of 4 minutes stabilization time is required when the plug-in sensing head is changed. The oxygen consumption is 0.1 μ g/hour-ppm.

The electronics section provides a constant predetermined voltage to the oxygen sensor. The dissolved oxygen (DO) signal is applied to a current-to-voltage converter which also contains the temperature compensating circuitry. This is followed by a chopper electrometer amplifier and output amplifier which feeds both the panel meter and analog recorder output. The total current drain is 250 μ A. The 2702 DO meter ranges are 0-2, 0-10, and 0-20 ppm. The 2709 DO meter ranges are 0-1, 0-3, 0-10, and 0-30 ppm.

The basic difference between the two instruments is that the Model 2709 uses a nonlinear galvanometer scale to give more precise temperature measurements than the 2702 model. The 2709 also has an improved oxygen sensor head. The 2702 and 2709 are shown in figures 1 and 2, respectively.

The manufacturer's performance specifications are summarized in appendix A.

TEST PROCEDURES AND RESULTS*

Temperature

The temperature accuracy and precision determinations were conducted in a nonmetallic, constant-temperature water bath. The temperature range for the Model 2702 evaluation was from 2°C to 40°C. The test range for the

*A performance summary is given in appendix B.

2

Model 2709 was from 0°C to 40°C. The bath temperature was determined with a platinum resistance thermometer in conjunction with a Mueller bridge having a combined accuracy of ± 0.002 °C or with a calibrated quartz thermometer having an accuracy of ± 0.02 °C.

The temperature calibration curves for both models are shown in figure 3. The worst cases of inaccuracy and imprecision for the Model 2702 were 2.44°C and ± 0.37 °C, respectively. For the Model 2709 the worst-case inaccuracy was 1.91°C* and the worst-case imprecision was ± 0.13 °C.

Dissolved Oxygen

The dissolved oxygen accuracy and precision data were obtained from instrument readings in a constant-temperature water bath in which the concentration of dissolved oxygen was established as follows. The water bath was saturated with a gas mixture of 0_2 and N₂ in a temperature cycle of 20°C, 10°C, 0°C, 20°C, 30°C, 40°C, and 20°C. This saturation process and temperature cycling was repeated two or more times in baths of 0-ppt and 35-ppt salinity. The artificial seawater was prepared from American Society for Testing and Materials (ASTM) Formula A sea salt at a temperature of 40°C. Three different gas mixtures (4, 8, and 21 percent 0_2 in N₂)⁺ were used to saturate the test bath that was temperature cycled to obtain a complete range of dissolved oxygen concentrations. Literature values for dissolved oxygen in saturated seawater as functions of temperature and

^{*}The 2709 had a 1.0°C offset over the entire temperature range. If corrected for the offset, the worst-case inaccuracy would be 0.91°C.

⁺Actual gas mixture oxygen concentrations were obtained to within ± 0.08 mole percent from analyses performed by the National Bureau of Standards.

salinity were obtained from Gilbert, et al. (1967)*. Water samples were also taken at each test point to be analyzed by the modified Winkler method and gas chromatographic techniques.

Figure 4 shows the freshwater dissolved oxygen calibration curves for the Model 2702 for the three gas mixtures. (The Model 2709 did not arrive until after the freshwater tests were completed and, therefore, was not tested for dissolved oxygen in freshwater.) The worst-case inaccuracy was 0.92 ppm (4 percent 0_2 mixture at 2°C), and the worst-case imprecision was ± 0.26 ppm (4 percent 0_2 at 20°C). Figure 5 presents the seawater (35-ppt salinity) dissolved oxygen calibration curves for both instruments. The worst-case inaccuracy for the Model 2702 in seawater was 0.50 ppm (4 percent 0_2 mixture at 0°C), and the worst-case imprecision was ± 0.50 ppm (21 percent 0_2 mixture at 20°C). For the Model 2709 in seawater the worst-case inaccuracy and imprecision were 0.60 ppm (4 percent 0_2 mixture at 0° C) and ± 0.10 ppm (4 percent 0_2 mixture at 10°C), respectively.

Response Times

The response times for each parameter (temperature and dissolved oxygen) were obtained by subjecting the sensor to a step change in measurand and monitoring the output on an analog recorder. The results of the 95 percent response tests are summarized in table 1. It should be noted that the temperature measuring thermistor and the two temperature compensating thermistors are thermally connected directly to the cathode of the detector, which results in faster temperature response times.

^{*}Gilbert, Pawley, and Park, 1967: Carpenter's oxygen solubility table and nomograph for seawater as a function of temperature and salinity. Oceanographic Society of Japan, 23 (5), p. 252-255.

Measurand	At 0°C	At 20°C	At 40°C
Dissolved oxygen	106	21	7
Temperature	124	132	140

Table 1.--Measured response times (seconds)*

Environmental Effects

To examine the effects of temperature and humidity variations on the electronics portion of the system, the sensor inputs were simulated and the electronics package was placed in an environmental chamber where the temperature was cycled from 10° C to 45° C. Two cycles were conducted at 25 percent relative humidity and one cycle at 85 percent relative humidity. The sensor-simulation circuitry was isolated from these temperature variations. The worst-case temperature error during the environmental evaluation was $\pm 1.9^{\circ}$ C for the Model 2709. The worst-case dissolved oxygen error was ± 0.9 ppm for the Model 2709. The Model 2702 was not tested for environmental effects, because the electronics circuitry is the same for both instruments.

Power Supply Variation Effects

A DC power supply was substituted for the instrument's internal battery, and the voltage was varied from the "normal fresh-battery" voltage down to 65 percent of the battery voltage. No detectable errors were observed in the outputs of either instrument.

^{*}Response time is herein defined as the time required for the system output to attain 95 percent of the asymptotic value when subjected to a step input. This 95 percent response time is three times the time constant $[(1-e^{-1})$ value] for a pure exponential response.

Long-Term Stability

The long-term stability tests were conducted for 24 days to determine the instrument's reliability for monitoring applications. For this test, the sensors were once again placed into the nonmettalic bath containing freshwater saturated with a gas mixture of 21 percent oxygen in nitrogen. The bath was resaturated, and readings recorded each day. Figure 6 depicts the dissolved oxygen error for each instrument as a function of time in days.

GENERAL COMMENTS

- The 2104.01 sensor head in the Model 2709 failed prior to the environmental testing and was replaced by the manufacturer.
- 2. The manual supplied with the instruments does not contain a system description and includes only a very brief circuit description. The manual does contain an excellent section on polarographic oxygen measurements, and the sections on operation, care and maintenance, and trouble-shooting are quite detailed. The manual also contains a parts list and circuit schematics.

ACKNOWLEDGMENT

The authors wish to acknowledge the dedicated efforts of Paul Eichelberger without whose expertise, perseverance, and attention to testing detail, the data in this report could not have been gathered.

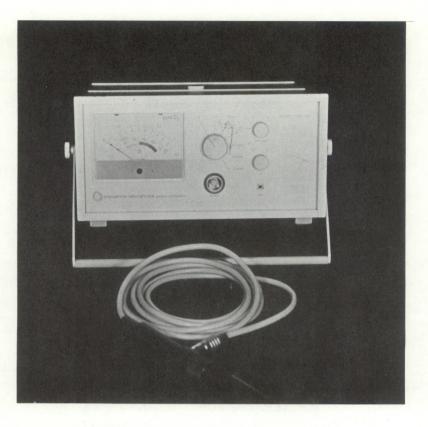


Figure 1.--Orbisphere model 2702 oxygen measuring system.

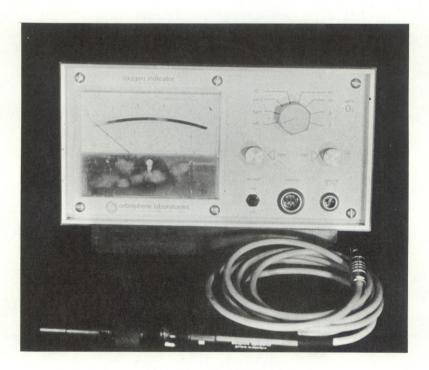


Figure 2.--Orbisphere model 2709 oxygen measuring system.

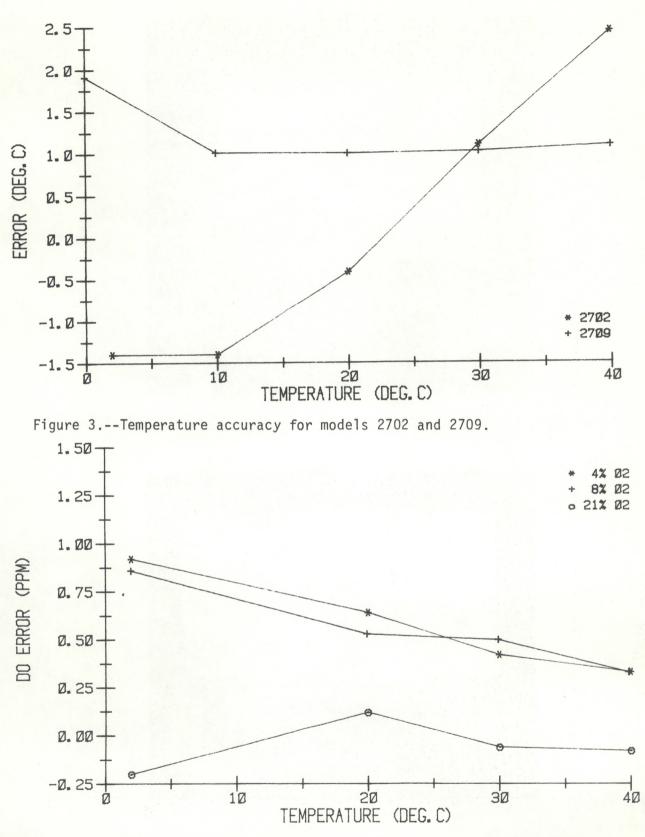
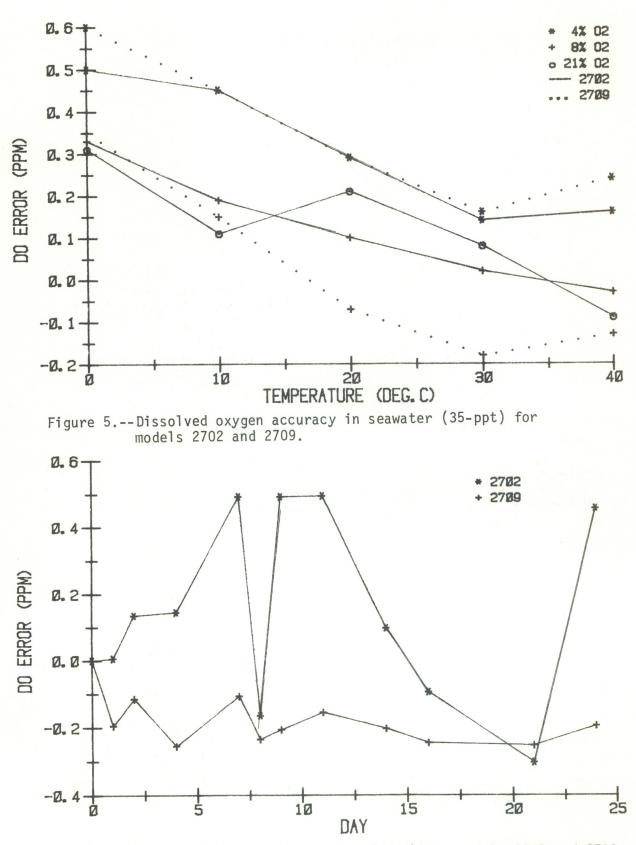
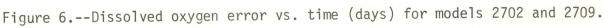


Figure 4.--Dissolved oxygen accuracy in freshwater for the model 2702.





APPENDIX A -- MANUFACTURER'S PERFORMANCE SPECIFICATIONS

Temperature

Range

Accuracy

Dissolved oxygen

Ranges

Accuracy

Response time

 0_2 consumption

Linearity

Temperature compensation

0°C to 50°C

+0.5°C

0 to 2, 0 to 10, 0 to 20 ppm

<u>+</u>1 percent when temperature of unknown sample is within <u>+</u>5°C of calibration temperature

10 s to reach 90 percent of true value

30 s to reach 99 percent of true value

0.1 µg/hour-ppm

+1 percent

0°C to 45°C

APPENDIX B -- PERFORMANCE SUMMARY*+

	2702	2709
Temperature		
Range tested	2°C to 40°C	0°C to 40°C
Accuracy	2.44°C	1.91°C**
Precision	<u>+</u> 0.37°C	<u>+</u> 0.13°C
Dissolved oxygen		
Range tested	1 to 14 ppm (mg/1)	1 to 14 ppm
Accuracy, freshwater	0.92 ppm	
Accuracy, seawater	0.50 ppm	0.60 ppm
Precision, freshwater	<u>+</u> 0.26 ppm	
Precision, seawater	<u>+</u> 0.50 ppm	<u>+</u> 0.19 ppm

*Abbreviated from the Test Procedures and Results and associated graphs. +All test results are worst-case values averaged from two or more cycles unless otherwise specified. **Includes a 1°C calibration offset

11

Measurand - A physical quantity, property, or condition which is measured.

Error - The algebraic difference between the indicated value and the true value of the measurand, usually expressed in percent of the full-scale output, somtimes expressed in percent of the output reading of the instrument.

Accuracy - The ratio of the error to the full-scale output (usually expressed as "within \pm ---- percent of full-scale output") or the ratio of the error to the output, expressed in percent. Accuracy may also be expressed in terms of units of measurand.

Precision (repeatability) - The ability of an instrument to reproduce output readings when the same measurand value is applied to it repeatedly, under the same conditions, and in the same direction. Precision is expressed as the maximum difference between output readings or as "within ---- percent of full-scale output." Three calibration cycles are used to determine precision unless otherwise specified.

Throughout this report, the values for errors, accuracies, and precisions are reported in terms of units of measurand. Accuracies are the average errors from the true value determined from two or more calibration cycles and are reported as + or - biases. Precisions are averages of the worst-case high and low values obtained with the same measurand input value under the same conditions over two or more calibration cycles unless otherwise noted. These precision averages are reported in measurand units as + (highest value - lowest value)/2.

(Continued from inside front cover)

- NOS 16 Deep Sea Tide and Current Observations in the Gulf of Alaska and Northeast Pacific. Carl A. Pearson, December 1975.
- NOS 17 Deep Sea Tide Observations Off the Southeastern United States. Carl A. Pearson, December 1975. (PB-250072)
- NOS 18 Performance Evaluation of Guildline Model 8400 Laboratory Salinometer. James E. Boyd, July 1976.
- NOS 19 Test Results on an Electromagnetic Current Sensor With an Open Design. David R. Crump, August 1976. (PB-260444)
- NOS 20 Test and Evaluation of the Interocean Systems, Inc. Model 500 CTD/Oxygen pH In-Situ Monitor System. Barbara S. Pijanowski, August 1976. (PB-260442)

NOS 21 National Ocean Survey Abstracts - 1976. October 1977, 20 pp. (PB-275293)



NOAA SCIENTIFIC AND TECHNICAL PUBLICATIONS

The National Oceanic and Atmospheric Administration was established as part of the Department of Commerce on October 3, 1970. The mission responsibilities of NOAA are to assess the socioeconomic impact of natural and technological changes in the environment and to monitor and predict the state of the solid Earth, the oceans and their living resources, the atmosphere, and the space environment of the Earth.

The major components of NOAA regularly produce various types of scientific and technical information in the following kinds of publications:

PROFESSIONAL PAPERS — Important definitive research results, major techniques, and special investigations.

CONTRACT AND GRANT REPORTS — Reports prepared by contractors or grantees under NOAA sponsorship.

ATLAS — Presentation of analyzed data generally in the form of maps showing distribution of rainfall, chemical and physical conditions of oceans and atmosphere, distribution of fishes and marine mammals, ionospheric conditions, etc. TECHNICAL SERVICE PUBLICATIONS — Reports containing data, observations, instructions, etc. A partial listing includes data serials; prediction and outlook periodicals; technical manuals, training papers, planning reports, and information serials; and miscellaneous technical publications.

TECHNICAL REPORTS — Journal quality with extensive details, mathematical developments, or data listings.

TECHNICAL MEMORANDUMS — Reports of preliminary, partial, or negative research or technology results, interim instructions, and the like.



Information on availability of NOAA publications can be obtained from:

ENVIRONMENTAL SCIENCE INFORMATION CENTER (D822) ENVIRONMENTAL DATA AND INFORMATION SERVICE NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION U.S. DEPARTMENT OF COMMERCE

> 6009 Executive Boulevard Rockville, MD 20852