NOAA Technical Memorandum NWS WR-132

ESTIMATES OF THE EFFECTS OF TERRAIN BLOCKING ON THE LOS ANGELES WSR-74C WEATHER RADAR

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Division, Western Region.

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## 1. INTRODUCTION

In the western United States weather radar antennas often must be placed at valley-floor locations bounded on one or more sides by mountainous terrain because of high cost of remoting and difficulty of maintenance. This reduces the effective range of the radar for precipitation detection and its capability to measure intensity to distances less than that limited by earth's curvature alone.

Pappas (1967) derived a simple geometric technique for estimating the height of the base of the radar beam due to the combined effects of the earth's curvature and partial blocking by nearby mountains. A.condensed version of his paper is given in the Appendix. This technique was developed for the Sacramento WSR-57 radar to assist users in understanding the radar's limitations and in interpneting observations. This same technique may also be applied to other radar systems and is presented here as an example for development of similar data to assist users in other areas in their evaluation of radar data.

## 1I. APPLICATION TO THE LOS ANGELES RADAR

The Los Angeles WSR-74C radar was installed in early 1978 on top of the Federal Building in west Los Angeles, California. This location is in an area adjacent to mountainous terrain. The Pappas technique was programmed in BASIC by B. W. Finke and run on a microcomputer for application to this radar's site. Table A is the program listing. An example of the output is presented in Table B. Result of plotting the entire output on a map of the area is presented in Figure 1. This provides an easy reference to refer to when determining areas of poor detection or when ascertaining capability of radar to see over particular drainages. Dotted lines represent heights to which storms must reach in order to be detected by the radar.

The map (Figure 1) shows extensive blocking in the west-through-north-through-east sector. (Almost total blocking over a small sector to the east-northeast caused by nearby high buildings is not included in Figure 1.) Less severe blocking occurs to the south and east-southeast. The heavily blocked area over the northern semicircle area will undoubtedly lessen the radar's effectiveness in assessing flash-flood potential over Santa Barbara and northern Ventura Counties, San Gabriel Mountains, northern San Bernardino Mountains, Antelope Valley, and Mojave Desert.

## 111. REFERENCE

Pappas, R. G., 1967: Derivation of Radar Horizons in Mountainous Terrain. NOAA Technical Memorandum NWS WR-22, National Weather Service, Western Region, Salt Lake City, Utah, 6.p.

## OK

LIST

```
A DIM K(100),HT(100), [(1\cup0),H(4) 100)
10 INPUT'NUMBER ')F rJINTS ALJNG BEARING';N
20 INPUT"bEARIVG(DEGS)";A
30 FOKI=1[JN
35 INPUT'KANGE,ELEVATI)N';r(1),T(1)
40 IF R(1)=<| THEN 6U
So NEXT
6# PRINT"INPIJT TERMINATED':PRIVI
65 STJP
100 0J「53,23
110 POKE 1233.53:PJKE1,241,54:NJLLG
12U FOR I=1TOSUU:U=1.5.9*I:NEXT
130 PRINTA
135 PRINTN
14\triangle FDRI=1TJI\triangleU:Q=15.4*I:NEXI
150 FOR [=1「JN
16: PKINTK(1)
174 PKLN[f(1)
180 NExT
185 Dur53.55
196 PJKE 1233,51:PJKE1241,503:NULLU
1y5 rRINF"TAPED':HKINT
20. 5A=\operatorname{ser}(5*0)
210 
22| FJR 1=1[JN
234 H[(I)=((R(I)/1.23)-SA)+2
240 OV S G.jF) 250,280
250 IF H[(I)>=T(I) THEV HM(1)=H[(I):GJTJE95
26*) K=(T(I)-HT(I))/R(I)
276 5=2
2%vjHM(I)=H[(I)+K*R(I)
2,0 IF HM, (I)<I(I) THEN 250
2YS NEXT
3GE IF(31ANDINP(255))=0 THEN 320
310 POKE1233,67:PJKE1241,66
32G PRINT"RADAK MJKIEJN FJR ";A;"DEGS":PRINT:PKINI
```



```
340 F.Jत I=1[J,N
350 PKlNTR(I),T(I),INT(HT(1)+.5),INT(HM(I)+.5)
364 vext
370 HJKE1233,51:rJKE 1241,56
360 EV!
OK
```

    Table A. Program Listing.
    RADAK MOKLEDN FOR 5 DEGS

| KANGE(MIS) | TRRV HGT | ECHJ ALT | IRKN MJD | E(H) ALI |
| :---: | :---: | :---: | :---: | :---: |
| 5 | 1000 | 401 | 1000 |  |
| 10 | 1100 | 255. | 1453 |  |
| 15 | 800 | 141 | 1739 |  |
| 20 | 3600 | 61 | 3600 |  |
| 25 | 2000 | 14 | 4438 |  |
| 30 | 4200 | 0 | 5308 |  |
| 40 | 4600 | 71 | 7149 |  |
| 50 | 3100 | 274 | 9121 |  |
| 60 | 6100 | 610 | 11226 |  |
| 70 | 6100 | 1078 | 13453 |  |
| 80 | 5600 | 1678 | 15833 |  |
| 90 | 8100 | 2410 | 18334 |  |
| 100 | 6600 | 3274 | 20968 |  |
| 110 | 9600 | 4270 | 23734 |  |
| 130 | 9600 | 6660 | 29562 |  |
| 150 | 11600 | 9578 | 35119 |  |
| 170 | 14384 | 13025 | 43105 |  |
| 190 | 12560 | 17001 | 50620 |  |

Table B. Program output for azimuth angle of $50^{\circ}$. For each range, the program lists the terrain height (TRRN HGT - input from a suitable topographic map); the radar beam-base height without consideration of terrain (ECHO ALT); and the radar beam-based height modified for terrain blocking (TRRN MOD ECHO ALT). Heights are in feet, range in nautical miles.


Figure 1. Effects of Terrain Blocking on Los Angeles WSR-74C Radar. Dotted lines represent heights to which storms must reach in order to be detected by the radar.

## APPENDIX

## Technique for Derivation of Earth's Curvature and Blocking Chart*

Hiser and Freseman (page 83, equation 40) give the maximum possible range between a radar and a target as limited only the radar horizon. This equation assumes standard propagation conditions and radar capability of target detection at this range.
(1) $R_{\text {hmax }}=1.23\left(\sqrt{h_{r}}+\sqrt{h_{f}}\right)$ nautical miles where $R_{\text {max }}$ is the range to the target, $h_{r}$ is the height of the radar antenna in feet, and $h_{t}$ is the height of the target in feet.

By solving for $h_{t}$ it is possibla to determine the minimum target height for interception of the radar beam at a given range:

$$
\text { (2) } h_{t}=\left(R_{\max } / 1.23-\sqrt{h_{r}}\right)^{2} \text {. }
$$

The computation of the minimum target height is complicated by the introduction of a mountain barrier or "block" in the radar beam. This is illustrated in Figure 1. : In Figure 1 the location of the radar is at Point. R. Point $H$ is where the radar beam is tangential to the earth, i.e., the horizon of the radar. A mountain or blocking barrier is introduced at Point E, with a height CE. It is desired to determine the height of the beam's case, $C^{\prime} E^{\prime}$, oyer Point $E^{\prime}$ after partial beam blocking by the mountain at $E$.

It can be seen that $B$ is the point at. which the base of the beam is intercepted by the mountain and BB' represents the extension of the beam's base if no blocking had occurred. Further, the stippled area represents the region below the radar horizon, and the hatched area the additional region blocked by the mountain at $E$. HBB' is the locus of $h_{+}$.

Since $R C B$ and RC' $B^{\prime}$ are triangles which are approximately similar,

$$
\frac{C B}{R H B} \approx \frac{C^{\prime} B^{\prime}}{R H B B^{\prime}} \text {, where } C B=C E-B E \text {, or the difference }
$$

between the elevation of the mountain and $h_{+}$computed for range to $E$. RHB is essentially the range to $E$, and $R H B B^{\prime}$ is the given range to $E^{\prime}$. Hence, $C^{\prime} B^{\prime}$ is easily evaluated, and when added to $B^{\prime} E^{\prime}$ (the value of $h+$ at Point E') gives the value of $C^{\prime} B^{\prime} E^{\prime}$, the minimum target height for penetration of the radar beam.

In cases where higher terrain is down range from the blocking mountain at, say, Point E', it is necessary to test whether or not it is higher than C'B'E'. It it is higher, a new proportionality must be set up based on the amount of further blocking caused by the peak at Point E'. If not,
*Pappas, 1967: Derivation of Radar Horizons in Mountainous Terrain, NOAA Technical Memorandum NWS WR-22.

## APPENDIX (Contlnuad)

the computations continue down range at intervals of 10 to 20 nautical miles.

The construction of the blocking charts was accomplished by tabulating terrain height data along azimuth radials from the radar at five-degree increments. Using an aeronautical chart showing 1000-foot contours, the crossing of each contour on the radials is noted with regard to its range. In the case of mountain peaks, the exact elevation is recorded. Starting with the first contour of elevation that is higher than the $h_{+}$value at that range, the "blocking" computation is begun and carried down range as explained above (with, of course, testing for additional down-range blocking by higher terrain and setting up new proportionalities if necessary). Values for CBE, C'B'E', C"B'E', etc., (or $h_{+}$if there is no terrain blocking) along each five degrees of azimuth are then plotted and isopleths drawn to obtain the final chart. The procedure is rather time-consuming and tedious, but certainly worth the effort. Once the computations get beyond about 100 nautical miles, they become fewer since blocking from terrain rarely occurs at those extended ranges. It should be pointed out that this technique could easily be programmed for a computer.

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Figure I. Beam Blocking Diagram.





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