# Long-Term Studies of Particulate Flux On and Near the Juan de Fuca Ridge 

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#### Abstract

Sequentially sampling sediment traps were deployed in the region of the Cleft segment of the Juan de Fuca Ridge from 1984 to 1991 to gain a better understanding of the vertical flux of particles from hydrothermal plumes. Most traps collected ten sequential subsamples spanning a total deployment time of nearly a year. Data from four of the moorings (V18, V24, V26, and V43) were binned and averaged by trap depth to estimate the mean total flux from above and below the hydrothermal plume. Total flux in traps above 2100 m was $25.6 \pm 44.6 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; below 2100 m the mean flux was $30.4 \pm 37.1 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. The flux of hydrothermal particles enriched in Fe, Mn, P, V, S, and Cu at North Cleft moorings near Monolith and Pipe Organ vents showed a greater increase as a function of depth than did the total flux. Flux of these elements was 2 to 5 times greater below the plume than above but their combined flux was not great enough to account for the total flux increase at the bottommost traps. A combination of hydrothermal input and resuspended sediments may account for the near-bottom flux increase. Total and elemental fluxes generally increased at all depths during the spring and fall surface plankton blooms. Typical fluxes during non-bloom periods were 10 to $25 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$, while peak fluxes during blooms were generally 40 to $150 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. Al, Si, P, Fe, and Mn fluxes increased by factors of 3 to 9 during bloom periods. Microscopic examination of trap samples indicated that organic aggregates were a common constituent. We suggest that organic aggregates produced in the euphotic zone account for the increase in hydrothermal sedimentation following surface blooms because these aggregates scavenge hydrothermal particles from the plume during the vertical descent and transport them to the seafloor.


## 1. Introduction

Seafloor hydrothermal venting on the Juan de Fuca Ridge (JDFR) has been observed, measured, and documented over the last several years by many investigators. Initial research and discovery was reported by Delaney et al. (1981), Normark et al. (1983), and Lupton et al. (1985).

Pacific Marine Environmental Laboratory (PMEL) began broad-based scientific investigations of hydrothermal venting on and near the JDFR in 1984. The JDFR is located approximately 500 km off the northwestern coast of the United States between the Blanco and Sovanco fracture zones (Fig. 1). One area of research PMEL has concentrated on has been the elucidation of the chemical and physical nature of the hydrothermal plumes associated with active seafloor vents. This study focused on hydrothermal plumes on the Cleft segment (Fig. 1), one of the most hydrothermally active tectonic segments on the JDFR (Baker and Hammond, 1992). High velocity ( $\sim 0.1$ to $\sim 1.0 \mathrm{~m} \mathrm{~s}^{-1}$ ) hot water, rich with dissolved minerals, discharges from deep-sea hot springs and produces clouds of fine-grained sulfide and sulfate precipitates. Edifices formed by the precipitated sulfides and sulfates

[^0]

Figure 1: (Top) Bathymetry ( 100 m contour interval) and locations of sediment trap moorings. (Bottom) Location of Cleft segment on the Juan de Fuca Ridge. Note that the grey shaded area of the bathymetric map denotes the walls of the ridge with the axial valley between.


Figure 2: CTDT transect of hydrothermal temperature $\left({ }^{\circ} \mathrm{C}\right)$ anomalies along the Cleft segment axial valley during summer 1990.
are commonly called black and white smokers, respectively. Hydrothermal particulates vented at Cleft segment of the JDFR characteristically include sphalerite, pyrite, sulfur, pyrrhotite, barite, cubanite, Fe oxyhydroxides, and chalcopyrite (Feely et al., 1987). The elemental composition of the common minerals includes $\mathrm{Cr}, \mathrm{Cu}, \mathrm{Zn}, \mathrm{Mn}, \mathrm{Fe}, \mathrm{Al}, \mathrm{Si}, \mathrm{S}$, and P. The hot discharge mixes with ambient seawater and rises to a level of neutral buoyancy (Fig. 2) where the water and entrained particles are dispersed by the regional flow.

Two principal discharge areas are known on the Cleft segment. The south Cleft site is centered near $44^{\circ} 41^{\prime} \mathrm{N}$ and was discovered in 1981 (Normark et al., 1983). The north Cleft site is centered near $44^{\circ} 57^{\prime} \mathrm{N}$ and was discovered in 1986 (Baker et al., 1987). PMEL has been mapping the plume at south Cleft since 1984 (Baker et al., 1985; Baker and Massoth, 1986; Baker, 1994; Feely et al., 1994; Massoth et al., 1994). Since 1986 our surveys extended to, and in most cases concentrated on, plumes associated with north Cleft vent fields (Baker, 1994). Plume mapping was accomplished by towing a CTD and beam transmissometer (CTDT) in a saw-tooth pattern through the bottom 400-800 m of water so that continuous measurements of hydrography and light attenuation were made. These up-down tows (Tow-yos) were conducted along and across axis; thus it was possible to produce a threedimensional representation of the hydrothermal plume. Although there is interannual variation of the hydrothermal temperature and attenuation signals (both spatially and in magnitude), typically the Cleft hydrothermal plume temperature and attenuation anomaly maxima were about $100 \pm 50$ meters above bottom (mab). The maximum plume rise height is typically
$\sim 200 \mathrm{~m}$ at south Cleft and $\sim 300 \mathrm{~m}$ at north Cleft (Baker, 1994). Plumes emanating from the Cleft segment tend to be entrained by regional flow along the strike of the axial valley from north to south and spread several kilometers east and west of the axial valley (Baker et al., 1985; Cannon et al., 1991).

This study was initiated to answer several questions regarding the vertical flux of particles within and above the hydrothermal plume. Specifically, the research had the following objectives:

1. To determine the vertical mass flux (VMF) of hydrothermal particulates at JDFR hydrothermal plume sites,
2. To characterize the chemical and physical nature of the hydrothermal plume particulates,
3. To determine whether there is a periodicity associated with the vertical flux of hydrothermal plume particles, and if so,
4. To determine what mechanisms regulate the periodicity.

Sequentially sampling sediment traps (Baker and Milburn, 1983) on taut wire moorings were placed above, within, and beneath the hydrothermal plumes at Cleft segment for periods of days to months to determine the VMF of the plume particles. Mooring deployment data is listed in Table 1.

Moorings were located within the axial valley and on the outer and inner flanks of the Cleft Segment; off-axis deployments were placed both east and west of the ridge (Fig. 1).

## 2. Methods

### 2.1 Predeployment Preparations

Sequentially sampling traps, which collect up to 10 samples per deployment at predetermined time intervals, were used in this study (Fig. 3). The traps have a teflon funnel $(\sim 0.2$ by 0.5 m$)$ which feeds into the opening of the sample jars. The plate into which the sample jars fit contains 11 holes to accommodate 10 sample jars and a blank space which is open to the funnel during deployment and recovery; such a configuration prevents the brine solution in the jars (see next paragraph) from washing out during deployment and recovery. This plate and sample jars comprise a carrousel which rotates via an attachment to a motor/timer. The funnel, sample jar carrousel, and motor/timer are housed within a 1.0 by 0.20 m PVC tube; the sample jars are 3.2 by 22.2 cm acrylic cylinders of $\sim 200 \mathrm{ml}$ capacity. Subsurface moorings fitted with acoustic releases were employed in all cases.

Prior to deployment the sample jars are filled with a dense brine to prevent the diffusion of preservative (formalin) from the sample jars when they are open to the funnel. A preservative is required to kill biota which alter the collected particulates (Knauer et al., 1984; Wakeham et al., 1993). Because our sediment trap collections were to be analyzed for metalliferous

## PMEL Sequentially Sampling Sediment Trap



Figure 3: Diagram of sequentially sampling sediment trap used in this study. The vane orients the sediment trap upstream of the mooring line which attaches to the top and bottom of the vane gimbal (rearward of the two gimbal pivots shown).
precipitates, a careful cleaning procedure was carried out on the sediment trap brine/preservative solution to ensure freedom from contamination. A bed of Chelex-100 was first cleaned by rinsing it with 1 NHCl , adding several rinses of particle free water and adjusting it to pH 8 with 1 N NaOH . The sea water and formalin to be used as the sediment trap fill solution was then put through the Chelex-100 bed using slightly positive pressure. The salinity of the solution was then adjusted to approximately 85 ppt and enough $\mathrm{CaCl}_{2}$ was added $\left(0.76 \mathrm{~g} \mathrm{l}^{-1}\right)$ to saturate the solution with calcium to prevent calcareous particulates from premature dissolution. The reagents used were Merck Suprapur®.

### 2.2 Deployment and Collection Strategies

Sediment traps were moored at several depths to determine the vertical flux of particles: (a) in ambient water above the hydrothermal plume; (b) at several locations within the hydrothermal plumes ( $\sim 100 \mathrm{~m}$ above bottom), (c) close beneath the plume core, and (d) near bottom.

Several different experiments were conducted to observe vertical flux over short-term (hours to days) and long-term (year-long) periods. Most collections were long term to obtain continuous flux data over a year; a few shortterm deployments were conducted to observe high-frequency flux trends.

### 2.3 Sample Storage

Recovered samples were retained in the sediment trap collection jars and stored in refrigerated picnic coolers in the cold box of the ship and then transferred to laboratory cold boxes until processing could begin. In some cases (Mooring V43) the supernate was sampled immediately upon trap recovery. Prior to processing, samples of the supernate of the sampling jars were collected for salinity, nutrient, and metal analyses.

### 2.4 Vertical Mass Flux Determination

Sediment trap samples were prefiltered through acid cleaned ( 24 hrs in 6 N HCl bath) 406 mm mesh polyethylene screen to eliminate swimmers (see Knauer et al., 1984; Wakeham et al., 1993). During the first several years subsamples were produced with a Folsom splitter; in subsequent years with a Walker splitter (Tennant et al., 1987) to provide more aliquots. The Folsom splitter is a binary splitter; if more than two aliquots are required, the initial ones must be resplit. As many as ten aliquots are provided with the Walker splitter. In almost all cases at least two aliquots were produced for vertical flux measurements and elemental analyses. Mass determinations were done by vacuum filtering a known fraction of the sample through preweighed $47 \mathrm{~mm} 0.4 \mu \mathrm{~m}$ pore Nuclepore membranes that were subsequently dried and reweighed. Vertical mass flux (VMF) $\left(\mathrm{mg} \mathrm{m}^{-2}\right.$ day $\left.^{-1}\right)$ was calculated from the following relationship:

$$
\begin{aligned}
\mathrm{m} & =\text { Measured mass of cylinder contents }(\mathrm{mg}) \\
\mathrm{a} & =\text { Collection area of the sediment trap }\left(\mathrm{m}^{2}\right) \\
\mathrm{t} & =\text { Collection period (days) } \\
\mathrm{VMF} & =\mathrm{m} / \mathrm{ta}
\end{aligned}
$$

The Si concentrations in the supernates of the sampling jars after recovery indicated the opal had dissolved into the sampling jar solution between collection and processing. We were able to approximate the amount of this loss in some cases. When possible (during the processing of the V34 mooring samples only), the VMF was corrected by adding back to the VMF value the amount of Si which we determined had dissolved. This method for accounting for the sample loss due to dissolution into the brine solution is described below.

### 2.5 Microscopic Examination

Several samples of each sediment trap were given a cursory microscopic examination under a Wild dissecting microscope $(120 \times-1000 \times)$ to obtain an impression of the nature of the particles.

### 2.6 Biogenic Silica Determination

Beginning in 1988, we measured opal concentrations in sediment trap samples to evaluate the role that sinking surface diatoms might play in mediating the vertical flux of particles from the hydrothermal plumes. The sample from the mass flux filter was used for the silica analysis after the mass analysis was completed. A hot NaOH extraction (Krausse et al., 1983; Paasche, 1973) was used for the analysis.

### 2.7 Elemental Flux

### 2.7.1 Particle Flux

The total elemental fluxes were calculated from concentrations of the elements in the sediment trap samples as well as the amounts of elements remobilized during deployment, storage, and processing. Particles from some of the sample aliquots produced during splitting were analyzed for several hydrothermal elements by X-ray primary and secondary emission spectrometry using a Kevex Model 8000-770 X-ray energy spectrometer with a rhodium Xray source and Zr , Se , and Co secondary targets. A nondestructive thin film technique was used (Feely et al., 1991). The aliquot of the sediment trap particles allotted to elemental analysis was carefully concentrated, ground, and loaded onto $37-\mathrm{mm}$ filters with the appropriate loading mass ( $250-400 \mu \mathrm{~g}$ ). The split of sediment trap material allotted to metal determination was first centrifuged in $250-\mathrm{ml}$ wide-mouth centrifuge bottles at 7500 RPM. After sampling the splitting solution, most of the remaining splitting solution was removed by vacuum suction. The sediment trap particles were resuspended in the small volume of remaining liquid and transferred to a $15-\mathrm{ml}$ conical centrifuge tube. After centrifuging at 15,000 RPM, the splitting solution was removed by vacuum suction and the slurry containing the particles was
transferred to a $2.5-\mathrm{ml}$ acrylic ball-mill vial. The particles and the accompanying splitting solution, which contained salt, were freeze dried. A $5-\mathrm{mm}$ acrylic ball was added to the ball-mill vial and the mixture of particles and salt was ground for 15 min . Based on the mass of particles obtained from the mass flux split, all or a fraction of the dried ground particles was transferred to a $2-\mathrm{ml}$ spectrophotometer cuvette. After adding 1.9 ml of distilled water and resuspending the particles, the absorbance of the suspension was measured at 750 nm . Based on an empirical calibration curve, the mass of the particles contained in the cuvette was estimated. Depending on the results of this calculation, all or a portion of the volume in the cuvette was pipetted into 30 ml of pH 8 water overlying an acid-cleaned, pre-weighed, $37-\mathrm{mm}$, $0.4-\mu \mathrm{m}$ polycarbonate filter. This slurry was then vacuum filtered, and the filter was rinsed with pH 8 water. The fluxes of elements that were associated with the analyzed particles were calculated by multiplying the mass fraction of each element in the particles ( mg of element/per mg of suspended matter) by the VMF.

### 2.7.2 Remobilized Flux

Metals on particles can be remobilized (a) into the supernate of the collection jar during deployment, (b) into the supernate of the jar during storage between recovery and splitting, (c) into the diluted splitting aliquots between the splitting of and processing on split aliquots, and (d) during the centrifuging of the splitting aliquot, freeze-drying, grinding, and resuspending the particles onto the final filters. The variable manner in which each of the four sets of recovered samples was processed dictated that the remobilized flux be calculated differently for each sample set (Appendix Table A1).

Analyses of some solutions needed to accurately calculate the remobilized flux were not performed because of budgetary or sample storage limitations. The instances in which the remobilized fluxes could not be determined because of missing data are noted.
2.7.2.1 Remobilization During Deployment and Storage. In general, the salinity of the supernate in the recovered sample jar was considerably less than the salinity of the fill solution, but higher than the salinity of open ocean water. This observation indicated that a considerable volume of the fill solution added to the collection jars before deployment was replaced by ambient seawater. Given the salinity of the supernate in a sampling jar upon recovery $\left(S_{s u}\right)$, the salinity of the fill solution $\left(S_{f}\right)$ and the salinity of the ambient water at the depth of the trap $\left(S_{a}\right)$, the fraction of ambient seawater present in the sampling jars at recovery $\left(F r_{a}\right)$ and the fraction of fill solution present in the sampling jars at recovery $\left(F r_{f}\right)$ can be calculated using the conservation of volume:

$$
\begin{equation*}
F r_{a}+F r_{f}=1 \tag{1}
\end{equation*}
$$

and salt:

$$
\begin{equation*}
S_{s u}=\left(F r_{a} * S_{a}\right)+\left(F r_{f} * S_{f}\right) \tag{2}
\end{equation*}
$$

Combining equations 1 and 2 , the fraction of ambient water in the sampling jars $\left(F r_{a}\right)$ can be calculated as:

$$
\begin{equation*}
F r_{a}=\left(S_{f}-S_{s u}\right) /\left(S_{f}-S_{a}\right) \tag{3}
\end{equation*}
$$

$F r_{f}$ can be calculated by difference using eq. 1. The excess elemental concentration of Si and P that was generated from the remobilization from the particles ( $C_{e x}$ ) can be calculated using the following mass balance:

$$
\begin{equation*}
C_{e x}=C_{s u}-\left[\left(F r_{f} * C_{f}\right)+\left(F r_{a} * C_{a}\right)\right] \tag{4}
\end{equation*}
$$

where $C_{s u}$ is the measured elemental concentration in the supernate in the full sampling jars, $C_{f}$ is the elemental concentration of the fill solution, and $C_{a}$ is the elemental concentration of seawater at depth obtained from field data (Appendix Table A2a-d).

In the case in which the supernate is sampled at recovery, the elemental flux attributable to remobilization in the supernate solution ( $R F_{s u}$ ) during deployment is calculated as:

$$
\begin{equation*}
R f_{s u}=\left(C_{e x} * V_{s u}\right) /(A * t) \tag{5}
\end{equation*}
$$

where $V_{s u}$ is the volume of the sampling jar ( 0.18 l ), $A$ is the area of the trap opening $\left(0.0314 \mathrm{~m}^{2}\right)$ and $t$ is the time during which the sampling jar was collecting material. Equation 5 can be used to calculate remobilization during both deployment and storage only when the full volume of original supernate in the jar is first sampled at some time after recovery, i.e., just prior to splitting of traps from moorings V23, V26, and V34 ( $R f_{s u}$ in Appendix Table 1). We have assumed that the Fe and Mn concentration in the fill solution, which was pre-extracted, and in seawater at the depth of the sediment trap were low compared to the Fe and Mn concentrations found in the supernate solution. Therefore, we assume that all Fe and Mn in the sampling jar supernates originated from the particles (i.e., $\mathrm{Mn}_{s u}=\mathrm{Mn}_{e x}$ ), and that the fluxes of Fe and Mn attributable to remobilization in the supernate solution $\left(R F_{s u}\right)$ can be calculated according to equation 5 .

The salinity and nutrient data from the supernate can also provide additional information used for quality control purposes. In some cases in which there was significant replacement of the fill solution in the collection jars by ambient seawater, the excess Si and P concentrations calculated from eq. 4 $\left(C_{e x}\right)$ were negative. Si and P must have been stripped from the supernate by the particles, if all the assumptions on which eqs. 1-4 were based are correct. While adsorption of P onto Fe-rich particles in the collection jars is plausible, significant amounts of Si are unlikely to precipitate. The inorganic N data provides the answer to this dilemma. If total inorganic N is lower than that expected from the replacement of the fill solution by deep ocean water and is in the form of nitrate, then the seawater that replaced the fill solution must have been surface water. If the seals between the jar and the rotating plate or the seal between the stationary plate and the rotating plate were leaking, low-nutrient surface water could have leaked into the collection jar during recovery. This set of conditions is especially plausible if an upside-down trap
is bobbing in and out of the water right before being brought onboard. If the aqueous contents of the collection jar are exchanging with surface water, then sediment particles could also have escaped from the collection jar and the total and elemental fluxes from this collection jar should be scrutinized for errors. If the total inorganic nitrogen is low and in the form of ammonia, then denitrification could also be responsible for the low inorganic nitrogen concentration. The chemical form of the inorganic nitrogen can also be used to assess whether the degree of Fe and Mn remobilization is consistent with the progression of reactions for organic matter remobilization (Froelich et al., 1979). The reduction of Fe and Mn oxides on the particles should only occur after all the nitrate has been converted to ammonia.

In contrast to moorings V23, V26, and V34, the four traps on mooring V43 were sampled immediately after recovery for salinity, nutrients, and metals. The remobilization $\left(R F_{s u}\right)$ in the full supernate volume during only the time of deployment can be calculated using eqs. 1-5. The samples were then stored in a reduced volume $(\sim 70 \mathrm{ml})$ at $4^{\circ} \mathrm{C}$ for 10 weeks. Before splitting, the volume of supernate $\left(V_{2}\right)$ was measured and additional supernate samples were collected. This supernate sample was analyzed for Fe and Mn concentrations $\left(C_{2}\right)$, but was not analyzed for Si or P . The changes in Fe and Mn concentrations of supernates $\left(C_{2}-C_{s u}\right)$ during the 10-week storage period were used to calculate a separate storage remobilization term $\left(R F_{s t}\right)$ in the reduced storage volume.

$$
\begin{equation*}
R f_{s t}=\left[\left(C_{2}-C_{s u}\right) * V_{2}\right] /(A * t) . \tag{6}
\end{equation*}
$$

2.7.2.2 Remobilization During Storage in the Diluted Splitting Solution and Resuspension. A preliminary experiment on the remobilization of elements during storage in the splitting solution and during processing was conducted on four samples from mooring V24. After the particles had been stored in the diluted splitting solution aliquot for 18 months, the particles were processed as described above, and the splitting solution aliquots were sampled and analyzed. The amounts of $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn in excess of that expected from dilution of the original supernate were calculated, and compared to the amounts remaining on the particles. In this experiment, less than $2 \%$ of the total Mn fluxes and less than $1 \%$ of the total Fe fluxes were found to have been remobilized over the 18 -month period in which the particles were in contact with the diluted splitting solution aliquot. In contrast, between $4 \%$ and $12 \%$ of the total Si fluxes were remobilized in the splitting solution. The amount of P remobilized in the splitting solutions ranged between $1 \%$ and $58 \%$ of the total P fluxes. Unless P remobilization can be calculated during storage in splitting solution, caution is suggested when interpreting P fluxes. Less than $2 \%$ of the mass of $\mathrm{Si}, \mathrm{P}, \mathrm{V}, \mathrm{Fe}$, and Mn of the particles was remobilized during the process of freeze drying, grinding, and resuspending onto filters.

The determinations of salinity, Si , and P in the splitting solutions from mooring V34 collected in August 1991 (Appendix Table A2c) allowed calculations of remobilization while the particles were in the splitting solution $\left(R F_{\text {spl }}\right)$. The total volumes of liquid in all fractions of the split fractions
( $V_{s p l}$ ) were measured. The splitting solutions allotted to element analysis were sampled after the initial centrifugation. The ratio of the salinity in the splitting solution $\left(S_{s p l}\right)$ to the salinity in the supernate $\left(S_{s u}\right)$ allows calculation of dilution by the splitting process. Excess elemental concentration $\left(C_{e x-s p l}\right)$ in the splitting solution not attributable to dilution of the supernate is calculated as follows:

$$
\begin{equation*}
C_{e x-s p l}=C_{s p l}-\left[\left(S_{s p l} / S_{s u}\right) * C_{s u}\right] \tag{7}
\end{equation*}
$$

where $C_{s p l}$ is the elemental concentration in the split. The flux attributable to dissolution during storage in the splitting solution $\left(R F_{s p l}\right)$ is calculated as follows:

$$
\begin{equation*}
R F_{s p l}=\left(C_{e x-s p l} * V_{s p l}\right) /(A * t) \tag{8}
\end{equation*}
$$

2.7.2.3 Mooring V23. The supernates of the full collection jars were sampled 17 months after recovery and analyzed. Equations $1-5$ were used to calculate $\mathrm{Si}, \mathrm{P}, \mathrm{Mn}$, and Fe remobilization (Appendix Table A3) during both deployment and storage $\left(R F_{s u}\right.$ in Appendix Table A1). The salinities of the supernates ( $38.7-47.6 \mathrm{ppt}$ ) were low compared to the salinity of the fill solution added to the traps before deployment ( 88.3 ppt ). These calculations indicated that the liquid in the sampling jars at recovery contained between $76 \%$ and $92 \%$ ambient seawater. Eight of the nine concentrations of Si and $P$ in the supernate solutions (Appendix Table A2a) were higher than the concentrations of fill solution, which were obtained from sampling jars that were not opened at depth due to malfunctions. There were measurable amounts of Mn in all nine sampling jars and measurable Fe concentrations in supernates from two sampling jars. The lower amounts of nitrate in the sampling jars compared to the fill solutions suggest that nitrate was the dominant electron acceptor for organic matter oxidation.

The samples of the splitting solutions taken after 19 months of storage were not analyzed. Therefore, the extent of remobilization of $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn while the particles were stored in the splitting solution is not known.
2.7.2.4 Mooring V26. The supernates of the full collection jars were sampled 7.5 months after recovery and analyzed (Appendix Table A2b). Equations 1-5 were used to calculate $\mathrm{Si}, \mathrm{P}, \mathrm{Mn}$, and Fe remobilization (Appendix Table A3) during both deployment and storage $\left(R F_{s u}\right.$ in Appendix Table A1). Because of limited amounts of supernate, not all sampling jars were sampled for salinity. For missing salinity data, the average value of the available salinity data from the appropriate trap was used. Like the trap on mooring V23, the extent of replacement of the fill solution ranged between $77 \%$ and $96 \%$. The lower amounts of nitrate in the sampling jars compared to the fill solution suggest that nitrate was the electron acceptor for organic matter oxidation.

The samples of the splitting solutions taken after storage of 6 months were not analyzed. Therefore, the extent of remobilization of $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn while the particles were stored in the splitting solution is not known.
2.7.2.5 Mooring V34. The supernates of the full collection jars were sampled 7.5 weeks after recovery and analyzed (Appendix Table A2c). Equations $1-5$ were used to calculate $\mathrm{Si}, \mathrm{P}, \mathrm{Mn}$, and Fe remobilization (Appendix

Table 3c) during both deployment and storage ( $R F_{\text {su }}$ in Appendix Table 1). The salinity data from sampling jars from this mooring were generally between 45 and 60 ppt (Appendix Table A2c), which indicated that an average of $35 \%$ of the fill solution was replaced by ambient waters. In this set of traps, the lesser degree of replacement of fill solution by ambient seawater is consistent with the shorter collection time. Moderate amounts of Fe and Mn were found in the supernate. The nutrient data suggest that oxygen was the electron acceptor for organic matter remobilization in all sampling jars on mooring V34. This observation is consistent with the short collection time and the immediate recovery of the mooring.

The determinations of salinity, Si , and P in the splitting solutions (Appendix Table A2c) allowed calculations of remobilization while the particles were stored in the splitting solution $\left(R F_{\text {spl }}\right.$ in Appendix Table A1) for 10 months. The amount of Si remobilized in the splitting solution averaged $75 \%$ of the total remobilized Si flux, and ranged between $30 \%$ and $100 \%$ of the remobilized Si flux. The amounts of P remobilized in splitting solution were low and highly variable.
2.7.2.6 Mooring V43. Supernates in the full collection jars for traps on mooring V43 were sampled immediately after recovery. Remobilization of Si, $\mathrm{P}, \mathrm{Mn}$, and Fe during deployment only ( $R F_{s u}$ in Appendix Table 1) was calculated using the salinity, nutrients, and metal data (Appendix Table A2d) and eqs. $1-5$. The remaining supernate ( $\sim 70 \mathrm{ml}$ ) was stored for 3 months and analyzed immediately before processing. Equation 6 was used to calculate remobilization during storage ( $R F_{s t}$ in Appendix Table A1) for only this set of traps on mooring V43. The low nitrate, high ammonia (not presented), and the high Fe and Mn concentrations in the supernate of sampling jars 1 and 4 of the trap at 2150 m on mooring 43 indicate that Fe and Mn were the electron acceptors for organic matter remobilization. In these two cylinders, the remobilized Mn flux was greater than $90 \%$ of the total Mn flux. For all other sampling jars from traps on mooring V43, oxygen appeared to be the electron acceptor for organic matter remobilization. The Fe and Mn remobilized flux listed in Appendix Table A3 includes remobilization during both deployment and storage. Unfortunately, the samples collected from the supernate in contact with the particles during storage were not analyzed for nutrients. Therefore, only the Si and P remobilized flux during deployment $\left(R F_{s u}\right)$ is reflected in Appendix Table A3.

Within 2 days, the splitting solutions allotted to the determination of metals were centrifuged and freeze dried. Under these circumstances, it is unlikely that any particulate $\mathrm{Si}, \mathrm{P}, \mathrm{Mn}$, or Fe were remobilized into the splitting solution.

### 2.8 Current Velocity Measurements

Aanderaa current meters were deployed on all moorings. These data are available at PMEL.


## Year

Figure 4: Vertical mass flux as a function of time at mooring V5.

## 3. Results

Compilations of total VMF and elemental fluxes are given in Tables 2-6. Below we summarize the results on a yearly basis.

### 3.11984 (V1, V4, V5)

VMF (Table 2) was measured at three on-axis locations (moorings V1, V4, and V5) at south Cleft during the 1984 field season. The original data from V1 and V4 have been lost but the mean flux from the single sediment trap at 2178 m on V4 was $110 \pm 40 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ for 102 -day samples (Baker et al., 1985).

The VMF at mooring V5 (Fig. 4) trended from high in June to low in September 1984 and increased with increasing depth. Mean flux at 1858 m and 2338 m was 37 and $111 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$, respectively. The spike observed during the fourth collection period is anomalous.

## $3.2 \quad 1985$

### 3.2.1 (V7) 3.5-Day Collections; On-Axis

Mooring V7 sediment traps (Fig. 5) collected particles at south Cleft from 7 June to 12 July 1985, in 3.5-day intervals, at approximately mid-axis of the Cleft Segment, at $2195 \mathrm{~m}, 2230 \mathrm{~m}$, and 2245 m . The three traps were located from directly below the top of the hydrothermal plume to 5 mab. Two



Figure 5: Vertical mass flux as a function of time at moorings V7 and V8.
additional traps at 1950 m and 2240 m malfunctioned. Of the functioning traps, the mean VMF was similar at the three depths (33, 30, and 29 mg $\mathrm{m}^{-2}$ day $^{-1}$ ). In general, the sedimentation rate was unvaried throughout the collection period at all depths except for the two spikes observed at 2195 m .

### 3.2.2 (V8) 30-Day Collections; Off-Axis

Mooring V8 was located approximately 14 km due west of the south Cleft vent field in 2250 m of water from 8 June 1985 to 22 August 1986. Of the four moored sediment traps (at $1348 \mathrm{~m}, 1698 \mathrm{~m}, 1948 \mathrm{~m}$, and 2230 m ) only one operated properly; the others stopped at various times in the normal rotational sequence which was set to be completed by 4 April 1986. In general, the flux appeared similar at all depths except at 1948 m and increased gradually to a peak during January 1986 (Fig. 5).

## $3.3 \quad 1986$

During 1986-1987, four moorings were deployed; two were on-axis (V10: short term experiment, V12) and two were off-axis (V9, V11).


Figure 6: Vertical mass flux as a function of time at moorings V9, V11, and V12.

### 3.3.1 (V9, V11, V12) 30-Day Collections; Off- and On-Axis

3.3.1.1 Off-Axis. Mooring V9 was moored off axis $\sim 11 \mathrm{~km}$ NNW of the south Cleft vents; each sample was a 30 -day interval. Sediment traps were placed at $1850 \mathrm{~m}, 2205 \mathrm{~m}$, and 2405 m . Results (Fig. 6) show that VMF was sharply increased during late fall--arly winter 1986 and again during the following spring. Flux magnitudes were similar at all three depths except that the VMF was somewhat lower during the first three collection intervals at 1850 m .

Mooring V11 was located $\sim 10 \mathrm{~km}$ due east of the south Cleft site and had one sediment trap at $2200 \mathrm{~m}(50 \mathrm{mab})$. Sedimentation maxima of about $150 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ during late summer and the following spring were apparent (Fig. 6).
3.3.1.2 On-Axis. Mooring V12 held two sediment traps at 2152 m and 2227 m and was moored in the axial valley at south Cleft. The VMF at


Figure 7: Vertical mass flux as a function of time at mooring V10.
both depths trended similarly and the VMF temporal variation was similar to V9 and V11 (Fig. 6). The magnitude of the VMF at both depths was considerably elevated ( $150-250 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) during the fall-winter of 1986 compared to the rest of the year.

### 3.3.2 (V10) 16-Hour Collections; On-Axis

A 7-day mooring (16-hour collection intervals), V10, was deployed at south Cleft segment. The VMF was about 10 to $50 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ throughout August 1986, the higher fluxes occurring at the deepest trap. It is noteworthy that the VMF at V12 was 3 to 4 times higher during the same time while being located only about 1 km distant (see Figs. 6-7).

## $3.4 \quad 1987$

Five moorings were deployed between mid-July 1987 and mid-May 1988; V17 was moored off-axis about 45 km northwest of the south Cleft site, V18 in the region of the 1986 megaplume discovery (Baker et al., 1987), and V19 at south Cleft. In addition, moorings V16 and V20 were deployed off-axis and at the megaplume site, respectively. Trap failures occurred during/after
the fourth cycle at 2250 m at V17 and at 2248 m at V19. Thus, the last data point in both cases represents an integrated VMF, i.e., when the traps malfunctioned, the sequencing was stopped so that sedimentation continued only into one cylinder for the duration of the deployment. Thus the daily VMF was determined by dividing by the number of days each of the terminal cylinders were open. Trap failures also occurred on V16 and V20, rendering no usable samples from either mooring.

### 3.4.1 (V17) 30-Day Collections; Off-Axis

Mooring V17 was off-axis about 45 km northwest of the south Cleft site and had sediment traps at $1500 \mathrm{~m}, 2100 \mathrm{~m}$, and 2500 m . The sediment traps had 30 -day collection periods. Sedimentation rates (Fig. 8) were relatively low, steady, and similar during the first seven collection periods, then increased from less than $20 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ to 150 to $250 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$.

### 3.4.2 (V18) 30-Day Collections; Megaplume I Site

Mooring V18 was deployed at the 1986 megaplume site from July 1987 to May 1988 with sediment traps at $1500 \mathrm{~m}, 2100 \mathrm{~m}$, and 2285 m . The temporal and quantitative VMF variations observed (Fig. 8) were very similar to those observed at both V17 and V19.

### 3.4.3 (V19) 30-Day Collections; South Cleft Site

Mooring V19, deployed at south Cleft, had sediment traps at 2000 m and 2245 m , the former of which failed after mid-November.

### 3.51988

Two moorings, V23 and V24, were deployed in the mid-axial valley, near the sites of megaplumes I and II, respectively (see Baker et al., 1989). Collections were made from mid-June 1988 to mid-May 1989. Subsamples were collected in 30-day intervals. Opal analyses were done on all of the 1988 samples (Table 2).

### 3.5.1 (V23) 30-Day Collections; Megaplume I Site

3.5.1.1 VMF. Of four sediment traps on mooring V23, only the 2050 m trap produced usable samples for determination of VMF and opal concentrations (Fig. 9). Traps at $1850 \mathrm{~m}, 2125 \mathrm{~m}$, and 2195 m malfunctioned. The measured VMF of the first subsample (mid-July to mid-August 1988) at 2050 m was anomalously high ( $526 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) and was not plotted. Otherwise the particle flux trend was uniformly low from throughout the year and then increased sharply the following spring.
3.5.1.2 Opal. The contribution to the VMF from opal particles was about $20 \%$ by weight and except for the low opal concentration during August-September ( $2.3 \%$ ), was fairly consistent; the highest concentration (30\%) was observed during the January-February 1989 interval.


Figure 8: Vertical mass flux as a function of time at moorings V17, V18, and V19.



Figure 9: Top to bottom: vertical mass flux and \% opal at mooring V23, and vertical mass flux and \% opal at V24 as a function of time.
3.5.1.3 Elemental Fluxes. The V23 samples were analyzed to determine the flux of several elements associated with hydrothermal systems including $\mathrm{Fe}, \mathrm{P}, \mathrm{Mn}, \mathrm{Zn}, \mathrm{S}, \mathrm{Cu}$, and Cr .

The corrected flux of the elements (Table 3) analyzed are shown in Fig. 10 as a function of time. A plot of the total VMF is at the top of each panel for comparison. Several of the elements (Fe, S, $\mathrm{Zn}, \mathrm{Cr}$, and Si ) exhibited temporal signatures very similar to that exhibited by the total VMF, i.e., very low sedimentation rates during the first six to seven collection periods with a sharp increase during the spring months of 1989 . The Cu and P flux was highly variable throughout the year with a sharp spring increase; the Mn flux was highest in late summer 1988, decreasing steadily until late winter 1989 and then increasing sharply during the spring.

### 3.5.2 (V24) 30-Day Collections; Megaplume II Site

3.5.2.1 VMF. Mooring V24 had sediment traps at $1850 \mathrm{~m}, 2100 \mathrm{~m}$, 2175 m , and 2245 m . Several VMF subsamples were not reported; the tenth sample from the 2100 m trap was lost; the fourth through ninth samples of the 2175 m trap were unusable; the ninth and tenth 2245 m samples were absent due to trap malfunction. The VMF trend (Fig. 9) was similar to that at V23: low ( 2 to $30 \mathrm{mg} \mathrm{m}^{-2}$ day ${ }^{-1}$ ), uniform sedimentation rate from mid-July 1988 through February and at 1850 m and 2245 m , well into March 1989. The VMF was highest ( $\sim 150 \mathrm{~m}^{-2}$ day $^{-1}$ at 1850 m and 2100 m ) from March to April 1989.
3.5.2.2 Opal. Opal concentrations were greatest at $1850 \mathrm{~m}, 2100 \mathrm{~m}$, and 2245 m (Fig. 9) during mid-October to mid-November 1988 and the opal concentrations at those depths were similar throughout the first 7 months. Opal concentrations were lowest ( $1 \%$ and $4 \%$ ) at 1850 m and 2100 m when VMF was greatest during the April-May collection periods. Opal flux at 2175 m was considerably less than at the other three depths during the first three collection periods.

### 3.61989

Two moorings, V25 and V26, were deployed in 1989 at the northern and middle part of Cleft segment, respectively, each collecting 33-day subsamples. Samples from 1848 m and 2050 m were analyzed for a suite of elements associated with hydrothermal vent fluid.

### 3.6.1 (V25) 33-Day Collections; Megaplume II Site

Mooring V25 had sediment traps at $1848 \mathrm{~m}, 2100 \mathrm{~m}, 2175 \mathrm{~m}$, and 2245 m . The two upper traps malfunctioned after four and three collection periods, respectively. While functioning, the VMF into these traps was similar (Fig. 11) and ranged between 5 and $11 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. VMF at 2175 m and 2245 m was uniform and low until April 1990 when it increased to 433 and $83 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$, respectively, and then decreased to $6.5 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ by July-August 1990 at the 2245 m trap.


Figure 10a: Mean elemental flux ( $\mathrm{Zn}, \mathrm{Fe}, \mathrm{Cu}$, and Cr ) and total flux as a function of time at the 2050 m trap on mooring V23.


Figure 10b: Mean elemental flux (Al, Mn, Si, S, and P) and total flux as a function of time at the 2050 m trap on mooring V23.


Figure 11: Vertical mass flux as a function of time at moorings V25 and V26.

### 3.6.2 (V26) 33-Day Collections; North Cleft

Mooring V26 had sediment traps at $1848 \mathrm{~m}, 2050 \mathrm{~m}, 2125 \mathrm{~m}$, and 2195 m . Each trap collected nine 33 -day subsamples; the tenth was lost because the traps were retrieved prematurely. The fourth through sixth samples of the 2125 m trap had insufficient mass for VMF determination.
3.6.2.1 VMF. The VMF at V26 trended similarly to that at V25 (Fig. 11) on an annual basis. The August 1989 to April 1990 VMF generally ranged between about 10 and $25 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ at the three lower traps. The VMF at the 1848 m trap was less, generally between 2 and 20 $\mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. The peak sedimentation rate ( $\sim 100-160 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) in all but the 2125 m trap occurred during April-May 1990. The peak rate at the $2125 \mathrm{~m} \operatorname{trap}\left(\sim 140 \mathrm{mg} \mathrm{m}^{-2}\right.$ day $^{-1}$ ) occurred about a month later, by
which time sedimentation at the other traps had fallen to between 2 and 50 $\mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$.
3.6.2.2 Elemental Fluxes. Samples from 1848 m and 2050 m were available for elemental analysis (Table 3). The elemental temporal flux variations at mooring V26 are shown in Figure 12a and 12b. In general the temporal pattern of elemental flux mimicked the total VMF pattern, i.e., it was relatively low midsummer with increases during the fall and during the spring of the nearly year-long collection period. At plume depth ( 2050 m ), notably sharp spring flux increases were observed by Fe ( 0.02 to $1.31 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ), $\mathrm{Mn}\left(0.008\right.$ to $0.155 \mathrm{mg} \mathrm{m}^{-2}$ day $\left.^{-1}\right)$, $\mathrm{S}\left(0.092-1.442 \mathrm{mg} \mathrm{m}^{-2}\right.$ day $\left.^{-1}\right)$, and Zn ( $0.0007-0.0382 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ).

### 3.71990

During the 1990 field season, long-term and short-term VMF experiments were done. In the short-term experiment, 11 moorings holding a total of 20 sediment traps which collected subsamples every 6 days were deployed in a grid on the north end of Cleft segment (Fig. 1). These short-term moorings were recovered about 3 days prior to the deployment of the long-term mooring (V43) that held four sediment traps which subsampled every 27 days. Moorings V43 was placed in the same locations as was the short-term mooring V34, i.e., mid-axis approximately 2.8 km southwest of Pipe Organ vent (Embley et al., 1991). Relatively complete data sets of elemental flux (uninterrupted, multi-depth) from both long- and short-term experiments were acquired during the 1990-1991 deployments. Consequently these data were examined more thoroughly than the elemental flux data from moorings V23 and V26.

### 3.7.1 (V43) 27-Day Collections; North Cleft

3.7.1.1 VMF. Mooring V43 had sediment traps at $1800 \mathrm{~m}, 2050 \mathrm{~m}$, 2150 m , and 2250 m (Table 2). VMF was measured from 28 September 1990 to 26 June 1991. The VMF trended similarly and was of similar magnitudes at all depths (Fig. 13). The trend was notably different from past years because of an increase in VMF during late fall to the early winter months of 1990. The late fall increase in VMF was remarkably similar at all four depths; from shallow to deep the VMF measured $44,45,56$, and $51 \mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$. The spring 1991 increase in VMF measured 80, 51, 77, and 87 mg $\mathrm{m}^{-2}$ day $^{-1}$, shallow to deep. Nominal background flux was about 10 to 20 $\mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$ and ranged from about 2 to $27 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$.
3.7.1.2 Elemental Fluxes. Four traps on mooring V43 were recovered on 10 June 1991. An aliquot of the solids of each cylinder from each of the four long-term traps was analyzed for elemental composition (including Al, P, Si, Ca, V, Cr, Mn, Fe, Cu, and Zn) by X-ray spectrometry (Table 4).

Hydrothermal particle flux vs. depth. Depth profiles of elemental flux (Fig. 14) show that $\mathrm{Fe}, \mathrm{Mn}, \mathrm{Cu}, \mathrm{P}, \mathrm{Al}$, and V have increased flux at 2050 m and below compared with fluxes at the $1800 \mathrm{~m} . \mathrm{Cu}$ flux increased about fourfold between the 1800 m and 2250 m trap, Mn increased fivefold,


Figure 12a: Elemental ( $\mathrm{Mn}, \mathrm{Cu}, \mathrm{Zn}, \mathrm{Cr}$, and Fe ) and total flux as a function of time at mooring V26.


Figure 12b: Elemental (S, $\mathrm{Si}, \mathrm{Al}$, and P ) and total flux as a function of time at mooring V26.


Figure 13: Vertical mass flux as a function of time at mooring V43.

V flux nearly doubled between 1800 m and 2250 m , P flux increased more than 4 times from the 2050 m trap to the 2250 m trap, and the 2150 m Fe flux was about 30 times higher than at the 1800 m trap.

Hydrothermal particle flux vs. time. The magnitude of elemental fluxes at the 2150 m and 2250 m depths varied considerably throughout the year and trended similarly to the total VMF (Fig. 15). In all cases at the two deepest traps, the flux of $\mathrm{Al}, \mathrm{Si}, \mathrm{P}, \mathrm{Fe}, \mathrm{Mn}$, and V increased considerably above background in late fall to early winter 1990 and again during the spring months of 1991. Elemental fluxes at the 1800 m and 2050 m traps tended to be considerably smaller in most cases.

Al - Background particulate Al flux was about $0.1-0.3 \mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$ during late summer 1990 and mid-winter 1990-1991 at all depths. Lower particulate Al flux trends were measured at the 1800 m and 2050 m depths and higher fluxes tended to occur at 2150 m and 2250 m with a few exceptions. The lowest particulate Al flux $\left(\sim 0.1 \mathrm{mg} \mathrm{m}^{-2}\right.$ day $\left.^{-1}\right)$ was measured at the 2250 m trap during the fall of 1990 and at the 2050 m and 2250 m traps during early summer 1991. Highest particulate aluminum fluxes were recorded at the 2150 m and 2250 m traps ( $\sim 0.4-0.6 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) during the late fall and spring peak flux periods.


Figure 14: Elemental flux as a function of depth at mooring V43. Error bars denote one standard deviation.


Figure 15: Elemental flux as a function of time at mooring V43.
$\mathbf{S i}$ - Particulate Si flux was lowest throughout the year at $2250 \mathrm{~m}(\sim 1-$ $3 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ). A maximum in particulate Si flux was measured during late fall 1990 at 2150 m . During spring 1991 Si fluxes were particularly elevated ( $\sim 18 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) at 1800 m and 2150 m .
$\mathbf{P}$ - Particulate P flux was lowest throughout the year in the upper three traps which collected about $0.05 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ or less except for the 2150 m trap which collected about $0.1 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ during one collection period late in 1990 . The 2250 m trap collected substantially more particulate $P$, especially during the late fall and spring when $P$ fluxes of 0.15 to 0.18 mg $\mathrm{m}^{-2}$ day $^{-1}$ were recorded.

Fe - These fluxes were generally low in the upper traps at 1800 m and $2050 \mathrm{~m}\left(\leq 0.3 \mathrm{mg} \mathrm{m}^{-2}\right.$ day $\left.^{-1}\right)$ compared to the flux at the lower two traps and did not follow a noticeable trend. Fe flux at 2150 m was much higher throughout the year than at shallower depths and trended similarly to total VMF. The Fe flux at 2150 m ranged from about 0.2 to $>0.5 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ with maxima in late fall 1990 and spring 1991. Fe flux at 2250 m trended somewhat differently than at 2150 m . The maximum flux $\left(>0.5 \mathrm{mg} \mathrm{m}^{-2}\right.$ day ${ }^{-1}$ ) occurred 2 months earlier than at 2150 m and periods of relatively low flux alternated with periods of higher flux on a bi-monthly mode except during spring 1991. The spring 1991 maximum in particulate Fe flux was delayed by one interval relative to the 2150 m trap.

Mn - Particulate Mn flux was uniformly low ( $<0.02 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) at the 1800 m and 2050 m traps compared to the 2150 m and 2250 m traps. The Mn flux at 2150 m was relatively uniform throughout the year and ranged from about $0.03-0.1 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. At 2250 m the Mn flux was elevated compared to that at 2050 m but generally a bit lower than at 2150 m except for a dramatic increase during the spring of 1991 when it increased from a nominal background of about $0.05 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ to more than $0.15 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$.

V - Flux of particulate V trended similarly to the total VMF throughout the year. It was lowest in the upper traps ( $\sim .0005-.002 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) and greatest ( $0.003-0.004 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ) during fall-early winter of 1990 at 2250 m .

### 3.7.2 (V32-V42) 6-Day Collections; North Cleft

3.7.2.1 VMF. The short-term experiment commenced mid-July and ended mid-September 1990. The moorings were placed in a grid over and around the north Cleft vent field (Fig. 1) such that five of the moorings (V34, V35, V38, V39, and V41) were located in the axial valley near Monolith and Pipe Organ vents. The other six moorings were located as much as $\sim 8 \mathrm{~km}$ to the east and west of the axial valley. Three of the sediment traps, V32/2250 m, V34/2150 m (one of two replicate traps), and V38/2050 m, malfunctioned and returned no samples. All samples were measured for total VMF and opal concentration (Table 5).

The mean VMF measured in the axial valley was $\sim 36 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; the mean of the other traps was $\sim 26 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. In all cases $62 \% \pm 10 \%$ of the VMF was attributable to opal (Figs. 16-18). The peak sedimentation
rate occurred during August, during which the VMF increased from $\sim 20$ to $\sim 50-60 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ in nearly all the traps and opal concentrations varied much the same as the VMF. On the other hand, the 2150 m trap on V34 collected much higher VMF, $110-140 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$, and a much lower opal contribution, $5 \%-40 \%$ ( $80 \%$ in the first subsample).
3.7.2.2 Elemental Fluxes. Samples from mooring V34 only were analyzed for hydrothermal elemental concentrations. The corrected fluxes are found in Table 6. The average elemental flux during the 60 -day deployment was much higher in general than the average during the year-long deployment (see Figs. 15 and 19). Fe flux, for example, ranged from about 0.5 mg $\mathrm{m}^{-2}$ day $^{-1}$ at 2050 m to nearly $5 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ at 2250 during the 60 -day experiment. During the year-long deployment the Fe flux did not exceed $0.9 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. The flux of $\mathrm{Fe}, \mathrm{Cu}, \mathrm{P}, \mathrm{Mn}$, and V were also considerably greater during the short-term experiment. While the elemental flux magnitude was greater during the short-term experiment, the flux/depth pattern was similar to that observed during the year-long deployment (Fig. 20).

Several elemental fluxes did mimic to some extent the total VMF variation pattern. The total VMF was in excess of $150 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ during the first collection period at 2150 m . The $\mathrm{Al}, \mathrm{Si}, \mathrm{Fe}, \mathrm{Mn}, \mathrm{V}, \mathrm{Cr}$, and S fluxes at 2150 m were notably high during the first collection period. By the second collection period the fluxes of these elements decreased significantly, in some cases to as little as one third of the original level, which was in general maintained throughout the duration of the experiment. The flux level of these elements at 2050 m and 2250 m were in general about the same as the 2150 m background level. The V, Cr, and Fe fluxes at 2150 m exhibited a secondary maximum during the sixth collection period while $S$ and Fe fluxes exhibited secondary peaks during the same time span but at 2250 m . The S flux increased more than 4 times during the sixth collection interval at 2250 m . The flux of $\mathrm{Mn}, \mathrm{Zn}$, and P were variable. In general the elemental flux at 2050 m was much lower than at deeper depths.

## 4. Discussion

### 4.1 Total Vertical Mass Flux

### 4.1.1 Depth Variations

Several past investigations using sediment traps have found that particle flux as a function of depth is variable and that quantities measured can be a result of varying sources and mechanisms (Rowe and Gardner, 1979; Martin and Knauer, 1983; Gardner et al., 1985; Walsh et al., 1988; Dymond and Roth, 1988; Feely et al., 1994). The major sources of settling particles in the ocean include organic detritus generated in the euphotic zone, airborne (dust and pollen primarily), hydrothermal, and resuspended sediments from the seafloor. The bulk of the surface source is organic carbon, $\mathrm{CaCO}_{3}$, and opal, a large fraction of which does not reach the seabed because of dissolution and other recycling processes. Consequently, sediment trap catchment by a vertical regime of moored traps decreases with depth unless there are


Figure 16: Vertical mass flux (open circles) and \% opal (closed circles) as a function of time at moorings V32, V33, V34, and V35.





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Figure 17: Vertical mass flux (open circles) and \% opal (closed circles) as a function of time at mooring V36, V37, and V38.


Figure 18: Vertical mass flux (open circles) and \% opal (closed circles) as a function of time at mooring V39, V40, V41, and V42.


Figure 19: Elemental flux as a function of time at mooring V34.


Figure 20: Elemental flux as a function of depth at mooring V34. Error bars denote one standard deviation.
additional particle sources to the deeper traps, e.g., hydrothermal input and/or resuspension of seabed material.

One of the primary strategies employed in this study was locating sediment traps above the plume, within the plume, and below the plume in an attempt to quantify the input of hydrothermal particles. Figure 21 is a comparison of the mean total flux at those depths. Data from only four moorings (V18, V24, V26, and V43) were used because they were the only ones with enough data to compare interdepth flux variations in a statistically valid manner, i.e., they were on-axis moorings that had nearly complete data sets (eight or more consecutive subsamples) from at least two of the depth regimes. Data from these moorings were selected for comparison such that subsamples from any given depth must have a corresponding subsample at a comparison depth. If subsamples from any deployment were missing critical subsamples, the data from that trap would not be used. Critical subsamples are those that were collected during spring bloom and mid-winter months, and are so designated because these times are probably the most critical in terms of regulating the amount of sedimentation into the sediment traps (see discussion below). The mean VMF measured at $<2100 \mathrm{~m}$ traps was $25.6 \pm$ $44.6 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; at $>2100 \mathrm{~m}$ the VMF was $30.4 \pm 37.1 \mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$. Of the sediment trap samples collected only V43 had elemental data that corresponds to the above flux data. From the V43 data set (Table 4) it is clear that although there is a considerable increase in both Fe and S with increasing trap depth, the input of hydrothermally derived particles cannot account for more than $5 \%$ of the increased flux below 2100 m . It is possible that the increase of VMF with depth is a combination of hydrothermal and resuspended sediments. Although we do not have direct evidence of resuspended sediments, near-bottom Aanderaa current meter data from previous deployment periods (Cannon et al., 1991) in the axial valley have measured bottom current velocities $\geq 7 \mathrm{~cm} \mathrm{sec}{ }^{-1} 36 \%$ and $53 \%$ of the time during the periods that VMF exceeded $100 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. Southard et al. (1971) and Lonsdale and Southard (1974) have shown that current speeds of $7-10 \mathrm{~cm}$ $\mathrm{sec}^{-1}$ are required for resuspension of calcareous ooze.

### 4.1.2 Short-Term Temporal Variations-1990 Experiments

From 1990 to 1991 there were two separate deployment periods. During the first period, from mid-July to mid-September 1990, 6-day subsamples (60-day total) were collected at 11 mooring sites (V32-V42) at North Cleft. The second deployment period went from late September (1990) to late June (1991) during which 27-day subsamples were collected.

During the 1990 short-term experiment, total sedimentation rate increased significantly at most sediment trap locations and at several depths midway through the collection period (Figs. 16-18). VMF increased from $\sim 20$ to $\sim 60 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ during the July segment of the collection period. Fifteen of seventeen traps deployed showed this trend. We have no firm explanation for the cause of this increase. Summer bottom currents were apparently not vigorous enough to cause resuspension. Nor were the flux increases due to increased sedimentation of hydrothermal particles and/or


Figure 21: Mean VMF from traps located above the hydrothermal plume ( $<2100 \mathrm{~m}$ ) and traps within and below the plume. The data is from moorings V18, V24, V26, and V43. The overall above-plume mean VMF $=25.6 \pm 44.6 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; from within and below the plume, overall mean $\mathrm{VMF}=30.4 \pm 37.1 \mathrm{mg} \mathrm{m}^{-2}$ day ${ }^{-1}$. The dotted horizontal line indicates the nominal depth of the top of the hydrothermal plume at Cleft segment.
opal, as increases in those species were proportional to those of the total VMF.

### 4.2 Hydrothermal Flux

Hydrothermal elemental concentrations were measured in samples from V23, V26, V34, and V43. Most of the following discussion pertains to the flux at V34 (short term) and V43 (long term) because they had the most comprehensive depth coverage.

### 4.2.1 Elemental Flux vs. Time

In general the elemental fluxes measured at V23 (Figs. 10a, b) and V26 (Figs. 12a, b) mimic the total VMF: relatively low and unchanged during midsummer and midwinter with increases during fall and more sharply during spring months.

The elemental flux during the 1990 short-term deployment period at V34 showed two temporal trends (Fig. 19). One trend is the elevated flux of nearly all the measured elements and the total VMF during the first 6-day collection, but only at the 2150 m trap. We have no explanation for this observation and it is possibly the result of a trap malfunction. The other trend was a flux increase of several of the elements after the fourth collection period that peaked during the sixth or seventh collection periods. The flux of Mn and P did not follow the trend and exhibited a rather variable pattern.

Temporal variations in the elemental flux at V43 from 1990 to 1991 (Fig. 15) were consistent within the group of elements analyzed and the temporal flux pattern exhibited is similar to that of the total VMF temporal pattern. In all cases the flux was greatest during the spring and a secondary flux increase generally occurred in the fall. A similar particle flux study at Endeavour segment of the JDFR (Dymond and Roth, 1988) found the greatest hydrothermal elemental fluxes in the fall and slightly smaller fluxes during the spring.

### 4.2.2 Elemental Flux vs. Depth

Short-term elemental flux variations as a function of depth were noted at V34 (S, Fe, Mn, Zn, Cu, P, Cr, and V) (Fig. 20) and long-term variations at V43 (P, Fe, Al, Cu, Mn, and V) (Fig. 14). In general, elemental fluxes increased progressively with depth but in some cases the maximum flux occurred above the bottom trap. For example, during the short-term experiment at V34 the $\mathrm{S}, \mathrm{P}$, and V flux maxima were at 2150 m and during the long-term deployment the maximum Fe flux occurred at 2150 m and the maximum Cu flux was at 2050 m . The increase of elemental flux with depth was considerably greater during the short-term than long-term collection period, i.e., elemental background flux was similar for the most part during both collection periods, but the flux at the bottom traps was quite different. For example, the elemental bottom flux of Mn was twice as high, S was twice as high, Fe was 15 times higher, Cu was 100 times higher, and Zn was 4 times higher. In the discussion above it was pointed out that there was a general increase in total VMF midway through the short-term collection period at most depths and it is clear from Fig. 20 that the mean total VMF is considerably greater in the lower two traps than in the 2050 m trap. It is possible that sinking organic aggregates resulting from a surface bloom entrapped a relative abundance of hydrothermal particles during this time period. This explanation is discussed more thoroughly below under Seasonal Variation (Section 4.3).

The data from the long-term collection is also notably different from elemental fluxes measured at the Endeavour segment of the Juan de Fuca Ridge (Dymond and Roth, 1988) (Table 7). The Cu flux at the 2100 m trap at Endeavour was nearly 1000 times greater than the deep trap on V43; V, Zn, Fe, and Mn were about 500, 100, 30, and 2 times higher at the Endeavour deep trap. Feely et al. (1994) reported that Fe flux near Monolith vent on North Cleft was only $2 \%$ of that reported by the Dymond and Roth (1988) study. The large differences between the elemental fluxes reported at North

Cleft and Endeavour segments is likely caused principally by differences in the relative locations of vent sources and traps, but also by the total flux of hydrothermal particles discharged at each site, the differences in concentrations of elements in vent fluids at the different sites, and differences in bottom current velocities and trajectories.

The flux of $\mathrm{Fe}, \mathrm{Cu}, \mathrm{Mn}$, and V was greatest at mid- and below-plume depths at both V34 and V43. These elements are highly enriched in vent fluids or are scavenged from the ambient seawater by hydrothermal particles (Feely et al., 1994; Dymond and Roth, 1988). These observations (moorings V34 and V43) were made about 3 km from the nearest known vent (Pipe Organ). Resuspension of previously sedimented hydrothermal material may also account for higher fluxes of these elements caught in the 2250 m trap. In the study at Endeavour Ridge it was estimated that between $19 \%$ ( Ba ) and $43 \%(\mathrm{~V})$ of the flux of specified hydrothermal elements resulted from resuspension (Dymond and Roth, 1988). Current meter measurements from moorings V34, V35, and V38, however, suggest current velocities too weak for resuspension during the 1990 short-term experiment.

### 4.2.3 Hydrothermal Fe

In an attempt to further assess the hydrothermal component of particle flux at the study area, we analyzed Fe flux data from V34 and V43 to evaluate how much Fe in the sediment traps was from hydrothermal input. Nonhydrothermal background particles collected at the Juan de Fuca (Feely et al., 1992) and Gorda (Feely et al., 1998) Ridges were subsequently analyzed for a suite of elemental concentrations including Fe and Al . The $\mathrm{Fe} / \mathrm{Al}$ ratio was 0.43 at JDFR, and 0.34 and 0.42 at the Gorda Ridge during cruises Great 1 and Great 3, respectively. We used the mean (0.397) of these three data sets to assess hydrothermal Fe enrichment. We proceeded by assuming that any Fe in the sediment traps in excess of this mean value of 0.397 (on a molar basis) was due to hydrothermal enrichment of Fe (see Karlin and Lyle, 1986). On this basis we determined approximate proportions of terrestrial and hydrothermal Fe flux trapped at moorings V34 and V43 (Fig. 22). Accordingly, our calculations indicate that approximately $35 \%, 83 \%$, and $90 \%$ of the Fe flux at $2050 \mathrm{~m}, 2150 \mathrm{~m}$, and 2250 m , respectively, at V34 is hydrothermally generated. It is also clear that the uppermost trap at 2050 m was well into the hydrothermal plume based on the amount of hydrothermal Fe in the trap. The proportion of hydrothermal to terrestrial Fe at V43 traps is less than that at V34, i.e., the traps at $1800 \mathrm{~m}, 2050 \mathrm{~m}, 2150 \mathrm{~m}$, and 2250 m , respectively, had about $1 \%, 38 \%, 54 \%$, and $57 \%$ hydrothermal Fe . The enrichment of these elements in the sediment trap samples from within and below the plume is confirmation that hydrothermal precipitates were captured in sediment traps within the plume. That $1 \%$ of the Fe at 1800 m was denoted as hydrothermal is probably a result of the manner that we used to define the background $\mathrm{Fe} / \mathrm{Al}$ ratio. Plots of elemental enrichment with depth at mooring V43 (Fig. 14) indicate that hydrothermal enrichment begins beneath 1800 m .


Figure 22: Fe flux partitioned into that having terrestrial and hydrothermal origins at moorings V34 and V43. Flux magnitudes represent the mean Fe flux of the entire sediment trap at the various depths shown.


Figure 23: Particle flux from four depth bins from the time series data. Grey bars show approximate timing of the spring bloom (Perry et al., 1989).

### 4.3 Seasonal Variation

Between 1987 and 1991 several mooring arrays were deployed at north Cleft that were located closely enough together from year to year to construct coherent time series plots of the VMF at those sites. In general, except in cases of malfunction, all the data represent 27 - to 33-day collections or nearly a year's worth of data per trap. Several depth horizons are used to show representative flux patterns from throughout the lower water column. The data used to construct the VMF plots were from moorings V18, V23, V24, V25, V26, and V43 (Fig. 23). The periodicity of seasonal phytoplankton blooms off Oregon-Washington and the mechanisms and forces governing the onset and duration of such occurrences have been summarized and reported by Anderson (1964) and Perry et al. (1989).

The background VMF throughout the time series study at the selected mooring sites at all depths was about $10-25 \mathrm{mg} \mathrm{m}^{-2}$ day ${ }^{-1}$. The relatively steady sedimentation rate is seen to change abruptly in bursts of increased sedimentation during the spring months every year and, to a lesser degree, during the fall months of some years. The most dramatic increase was mea-
sured during the spring of 1990 at the $2150-2175 \mathrm{~m}$ depth horizon when the VMF increased to over $400 \mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$. Other VMF spring peak magnitudes were $\sim 290 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ at the $1500-1800$ depth, $\sim 150 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ at the $1500-1800 \mathrm{~m}$ depth and $\sim 80 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ at the $2245-2285 \mathrm{~m}$ depth during 1988, 1989, and 1991, respectively. Fall peaks of about 40-60 $\mathrm{mg} \mathrm{m}{ }^{-2}$ day $^{-1}$ appeared during most years of this study. The highest fall peak, about $60 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$, was observed at all depths during 1990.

Many researchers (Deuser and Ross, 1980; Deuser et al., 1981; Honjo, 1982; Smith and Baldwin, 1984; Billet et al., 1983; Lampitt, 1985; Wefer et al., 1988; Deuser, 1986, 1987; Dymond and Roth, 1988) have documented that the annual cycle of primary production is responsible for seasonally regulated pulses of particles to the ocean floor. Surface biogenic material in our samples was routinely inspected under a Wild microscope immediately after filtration. Items that commonly dominated the samples included foraminifera, radiolarians, silicious spicules, diatom tests, and fecal pellets. All of the above-mentioned biogenic parts and pieces were commonly embedded in an amorphous organic matrix (marine snow). These observations support the hypothesis that such macro-aggregates (Shanks and Trent, 1980; Alldredge, 1979; Silver and Alldredge, 1981; Wakeham et al., 1993) and fecal pellets (Turner and Ferrante, 1979 and references therein) provide effective mechanisms for the transfer of particles from the sea surface to the sea floor. Export of materials from the sea surface begins with the aggregation of sinking planktonic carcasses, diatomaceous mucous nets (Smetacek, 1985), fecal pellets, other particulates, and amorphous organic material. The remains of such material were readily identifiable, especially in the spring samples, because of the high concentrations of biogenic components. Such aggregates may provide an effective mechanism for removing the mineral precipitates from hydrothermal plumes as the aggregates sink through them. This mechanism is likely to be especially pronounced during the heavy flux of spring bloom detritus. The results of the total VMF time series analysis and the elemental flux data clearly indicate that both total and hydrothermal elemental particle flux maxima coincided closely in most cases, with the timing of spring phytoplankton blooms (Figs. 15 and 23). We frequently observed secondary fall and early-winter pulses of sedimentation which we presume are mediated by fall plankton blooms. Studies by Lund (1957) and Denny and Walsh (1979) indicated that sinking diatoms carried surface Pb and Zn to the bottom, and others have speculated that such aggregates would scavenge fecal pellets and fine particles (Small et al., 1989; Honjo, 1980; Nozaki et al., 1987; Bishop et al., 1977; Bacon et al., 1985) during descent and sediment them to the bottom. In light of these studies and our observations it is reasonable that sedimentation of hydrothermal particles to the bottom is implemented by such organic aggregates.

This hypothesis is supported by the seasonal pattern of elements with a strong hydrothermal source (e.g., Fe, Mn, P, V, Cu). The sedimentation of these elements consistently showed strong increases during the spring and fall bloom periods (Figs. 10, 12, 15). Moreover, the flux increase from shallow to deep traps was also greatest during the blooms, an increase not seen in the total VMF (Fig. 15). This difference confirms that these elements do
not primarily originate in the overlying surface waters but are scavenged out of the hydrothermal plume by bloom-produced biogenic material.

Thus, a pattern emerges from these data which suggests that there is a predictable periodicity to the vertical flux of hydrothermal plume particles and the periodicity appears to be strongly linked to the annual cycles of total VMF, which in turn appears to reflect the annual cycles of primary production in the overlying surface waters. The coincidence of the timing of maximum total flux and maximum hydrothermal flux presents a reasonable argument for seasonal pulses of surface biogenic matter mediating the vertical flux of hydrothermal particulates from the plume to the sea floor. It is possible that the surface aggregates trap and continue to agglomerate with the plume particles as they sink through it, thereby removing them to the bottom.

### 4.4 Opal

During microscopic examination of samples from the 1990 short-term traps it was noticed that opal fragments (diatom and radiolarian) were ubiquitous and especially abundant. These observations prompted us to quantify the opal concentration in as many samples as possible. Opal comprised $62 \pm$ $10 \%$ of the VMF in the 1990 samples. The opal contribution to the 1988 1989 samples (moorings V23, V24) was $\sim 17 \%$; the Endeavor Ridge samples of the Dymond and Roth study (1988) contained $\sim 31 \%$ opal. The 1990 summer opal concentrations were likely high because they coincided with a diatom and radiolarians bloom that typically occurs during July-August in the northeast Pacific (Takahashi, 1986, 1987). Our opal concentration intercomparisons are made with reservation because collection periods were not similar in all cases.

## 5. Summary

Sediment traps were deployed on subsurface moorings on and about the Juan de Fuca Ridge, generally within 300 m of the bottom, for the purpose of learning more about the vertical flux of particulates near regions of hydrothermal venting and especially the vertical settling of particles from vent generated plumes. During each successful sediment trap deployment period, ten sequential subsamples were collected. Deployment periods lasted from days to nearly a year. The study was conducted continuously from 1984 to 1991 ; samples were analyzed in all cases for mass and in several cases for a suite of elements including those that are enriched in seawater from hydrothermal venting, and biogenic silica. A summary of the findings of the study include:

1. The mean total VMF (binned data) for on-axis samples from north and south Cleft segment, from 1984-1991, from $<2100 \mathrm{~m}$ was $25.3 \pm$ $20.8 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; at depths from 2100 m to 2150 m the mean was $37.3 \pm 35.0 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$; at depths $>2150 \mathrm{~m}$ the mean was 44.8 $\pm 45.9 \mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$. The mean flux at the bottom depth bin is
1.8 times greater than in the uppermost depth bin; the difference is significant ( $95 \%$ C.I.). Current meter records suggest that resuspension was at least partially responsible for the increased bottom flux.
2. Elemental analysis of particulates from moorings V34 and V43 shows that elemental flux was generally 2 to 5 times greater below the hydrothermal plume at the JDFR as above the plume. In the case of hydrothermal Fe at V43 the enrichment was more than a hundredfold. In addition, the enrichment of $\mathrm{Mn}, \mathrm{Cu}$, and V in our bottommost traps was confirmation that hydrothermal particles are sedimented to the seafloor within 3 km of Pipe Organ Vent.
3. The measured VMF demonstrated a strong seasonal signal as a result of surface phytoplankton blooms. Vertical mass flux increased several hundredfold in some years following the surface bloom. Furthermore, temporal variations of elemental flux was found to trend similarly to the total VMF trends. Increased elemental flux was especially pronounced during the annual spring plankton bloom.
4. Microscopic examination of our samples indicated that organic aggregates comprise a major portion of the vertical particulate flux and they may be responsible for removing hydrothermal particles from the plume, especially following the spring bloom when the rain of surface debris to the seafloor is at a maximum.

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## Tables

Table 1: Sediment trap moorings: location and deployment data.

| Mooring designation | Latitude | Longitude | Collection days/ cylinder | Deployment dates | Trap depths |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V1 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 5/85-5/86 | 2030 |
| V4 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 5/84-6/84 | 2178 |
| V5 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 6/84-9/84 | 1858,2056,2258,2338 |
| V7 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 3.5 | 6/85-7/85 | $\begin{aligned} & 1950,2195,2230, \\ & 2240,2245 \end{aligned}$ |
| V8 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 6/85-4/86 | $\begin{aligned} & 1348,1698,1948, \\ & 2150,2230 \end{aligned}$ |
| V9 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 8/86-6/87 | 1805,2205,2405 |
| V10 | $44^{\circ} 41.42^{\prime} \mathrm{N}$ | $130^{\circ} 21.52^{\prime} \mathrm{W}$ | 1 | 6/86 | 2154,2204,2229 |
| V11 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 8/86-6/87 | 2200 |
| V12 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 8/86-6/87 | 2152,2202,2227 |
| V17 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 7/87-5/88 | 1500,2100,2500 |
| V18 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 7/87-5/88 | 1500,2100,2285 |
| V19 | $44^{\circ} 41.3^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 30 | 7/87-5/88 | 2000,2245 |
| V20 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 9/87 | 1655,2155,2205,2225 |
| V23 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 7/88-5/89 | 1850,2050,2125,2195 |
| V24 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 7/88-5/89 | 1850,2100,2175,2245 |
| V25 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 8/89-7/90 | 1848,2100,2175,2245 |
| V26 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 8/89-7/90 | $\begin{aligned} & 1848,2050,2125,2195 \\ & 2195 \end{aligned}$ |
| V32 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 1800,2250 |
| V33 | $44^{\circ} 56.0^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2150 |
| V34 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2050,2150,2150,2285 |
| V35 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2150 |
| V36 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4{ }^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 1500,1800,1800,2250 |
| V37 | $44^{\circ} 57.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.6^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2200 |
| V38 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 13.1^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2050,2150 |
| V39 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4{ }^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2200 |
| V40 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2200 |
| V41 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2050,2150 |
| V42 | $44^{\circ} 53.3^{\prime} \mathrm{N}$ | $130^{\circ} 18.5^{\prime} \mathrm{W}$ | 6 | 7/90-9/90 | 2200 |
| V43 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 9/90-6/91 | 1800,2050,2150,2250 |

Table 2: Total VMF and biogenic opal concentrations (when analyzed) from mooring V1 to V26

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{gathered} \text { Mean flux } \\ \pm 1 \text { std dev } \end{gathered}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V1/28-1 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime}$ W | 35 | 1984.400 | 2030 | 100 |  |  |  |  |
| V1/28-2 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.496 | 2030 | 100 |  |  |  |  |
| V1/28-3 | $44^{\circ} 38.6{ }^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.592 | 2030 | 100 |  |  |  |  |
| V1/28-4 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.688 | 2030 | 100 |  |  |  |  |
| V1/28-5 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.784 | 2030 | 100 |  |  |  |  |
| V1/28-6 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.880 | 2030 | 100 |  |  |  |  |
| V1/28-7 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1984.975 | 2030 | 100 |  |  |  |  |
| V1/28-8 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1985.071 | 2030 | 100 |  |  |  |  |
| V1/28-9 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1985.167 | 2030 | 100 |  |  |  |  |
| V1/28-10 | $44^{\circ} 38.6^{\prime} \mathrm{N}$ | $130^{\circ} 24.1^{\prime} \mathrm{W}$ | 35 | 1985.263 | 2030 | 100 |  |  |  |  |
| V4/33-1 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.400 | 2178 | 60 |  |  | $110 \pm 40$ |  |
| V4/33-2 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.406 | 2178 | 60 |  |  |  |  |
| V4/33-3 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.411 | 2178 | 60 |  |  |  |  |
| V4/33-4 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.416 | 2178 | 60 |  |  |  |  |
| V4/33-5 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.422 | 2178 | 60 |  |  |  |  |
| V4/33-6 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.427 | 2178 | 60 |  |  |  |  |
| V4/33-7 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.433 | 2178 | 60 |  |  |  |  |
| V4/33-8 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.438 | 2178 | 60 |  |  |  |  |
| V4/33-9 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.444 | 2178 | 60 |  |  |  |  |
| V4/33-10 | $44^{\circ} 40.9^{\prime} \mathrm{N}$ | $130^{\circ} 21.6^{\prime} \mathrm{W}$ | 2 | 1984.449 | 2178 | 60 |  |  |  |  |
| V5/30-1 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.400 | 1858 | 500 | 0.0 | 0.0 | $37.4 \pm 33$ |  |
| V5/30-2 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.427 | 1858 | 500 | 34.4 | 105.7 |  |  |
| V5/30-3 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.455 | 1858 | 500 | 21.4 | 65.7 |  |  |
| V5/30-4 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.482 | 1858 | 500 | 11.6 | 35.6 |  |  |
| V5/30-5 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.510 | 1858 | 500 | 16.0 | 49.2 |  |  |
| V5/30-6 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.537 | 1858 | 500 | 5.1 | 15.6 |  |  |
| V5/30-7 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.564 | 1858 | 500 | 4.4 | 13.4 |  |  |
| V5/30-8 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.592 | 1858 | 500 | 12.0 | 37.0 |  |  |
| V5/30-9 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.619 | 1858 | 500 | 2.8 | 8.6 |  |  |
| V5/30-10 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.647 | 1858 | 500 | 1.6 | 4.8 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1 \mathrm{std}$ dev | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V5/35-1 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.400 | 2056 | 301 | 0.0 | 0.0 | $40 \pm 33$ |  |
| V5/35-2 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.427 | 2056 | 301 | 23.9 | 73.6 |  |  |
| V5/35-3 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.455 | 2056 | 301 | 27.6 | 84.8 |  |  |
| V5/35-4 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.482 | 2056 | 301 | 17.1 | 52.5 |  |  |
| V5/35-5 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.510 | 2056 | 301 | 26.9 | 82.8 |  |  |
| V5/35-6 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.537 | 2056 | 301 | 7.2 | 22.3 |  |  |
| V5/35-7 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.564 | 2056 | 301 | 5.2 | 16.1 |  |  |
| V5/35-8 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.592 | 2056 | 301 | 4.4 | 13.5 |  |  |
| V5/35-9 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.619 | 2056 | 301 | 2.5 | 7.8 |  |  |
| V5/35-10 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.647 | 2056 | 301 | 1.6 | 5.0 |  |  |
| V5/27-1 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.400 | 2258 | 100 | 0.0 | 0.0 | $80.7 \pm 78$ |  |
| V5/27-2 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.427 | 2258 | 100 | 39.6 | 121.7 |  |  |
| V5/27-3 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.455 | 2258 | 100 | 40.4 | 124.4 |  |  |
| V5/27-4 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.482 | 2258 | 100 | 27.4 | 84.3 |  |  |
| V5/27-5 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.510 | 2258 | 100 | 83.0 | 255.5 |  |  |
| V5/27-6 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.537 | 2258 | 100 | 15.1 | 46.5 |  |  |
| V5/27-7 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.564 | 2258 | 100 | 9.6 | 29.4 |  |  |
| V5/27-8 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.592 | 2258 | 100 | 9.6 | 29.5 |  |  |
| V5/27-9 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.619 | 2258 | 100 | 7.0 | 21.5 |  |  |
| V5/27-10 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.647 | 2258 | 100 | 4.2 | 12.8 |  |  |
| V5/25-1 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.400 | 2338 | 20 |  |  |  |  |
| V5/25-2 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.427 | 2338 | 20 | 54.0 | 166.1 | $110.8 \pm 67$ |  |
| V5/25-3 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.455 | 2338 | 20 | 61.4 | 188.9 |  |  |
| V5/25-4 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.482 | 2338 | 20 | 57.7 | 177.4 |  |  |
| V5/25-5 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.510 | 2338 | 20 | 0.0 | 0.0 |  |  |
| V5/25-6 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.537 | 2338 | 20 | 37.9 | 116.6 |  |  |
| V5/25-7 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.564 | 2338 | 20 | 22.3 | 68.5 |  |  |
| V5/25-8 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.592 | 2338 | 20 | 25.2 | 77.6 |  |  |
| V5/25-9 | $44^{\circ} 38.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.619 | 2338 | 20 | 16.2 | 49.8 |  |  |
| V5/25-10 | $44^{\circ} 38.8^{\prime} \mathrm{N}$ | $130^{\circ} 25.9^{\prime} \mathrm{W}$ | 10 | 1984.647 | 2338 | 20 | 13.2 | 40.6 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1$ std dev | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V7/6-1 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.445 | 2195 | 55 | 1.0 | 9.2 | $33.7 \pm 27$ |  |
| V7/6-2 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.455 | 2195 | 55 | 1.5 | 13.8 |  |  |
| V7/6-3 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.464 | 2195 | 55 | 6.5 | 58.7 |  |  |
| V7/6-4 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.474 | 2195 | 55 | 1.5 | 14.0 |  |  |
| V7/6-5 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.484 | 2195 | 55 | 1.3 | 11.7 |  |  |
| V7/6-6 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.493 | 2195 | 55 | 1.6 | 14.2 |  |  |
| V7/6-7 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.503 | 2195 | 55 | 9.6 | 87.2 |  |  |
| V7/6-8 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.512 | 2195 | 55 | 3.2 | 28.8 |  |  |
| V7/6-9 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.522 | 2195 | 55 | 3.7 | 33.8 |  |  |
| V7/6-10 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.532 | 2195 | 55 | 7.3 | 66.1 |  |  |
| V7/15-1 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.445 | 2230 | 20 | 1.8 | 16.5 | $28.0 \pm 13$ |  |
| V7/15-2 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.455 | 2230 | 20 | 2.0 | 18.1 |  |  |
| V7/15-3 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.464 | 2230 | 20 | 3.3 | 29.7 |  |  |
| V7/15-4 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.474 | 2230 | 20 | 2.2 | 20.4 |  |  |
| V7/15-5 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.484 | 2230 | 20 | 2.5 | 22.9 |  |  |
| V7/15-6 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.493 | 2230 | 20 | 1.7 | 15.7 |  |  |
| V7/15-7 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.503 | 2230 | 20 | 2.5 | 22.4 |  |  |
| V7/15-8 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.512 | 2230 | 20 | 5.1 | 46.3 |  |  |
| V7/15-9 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.522 | 2230 | 20 | 4.2 | 37.9 |  |  |
| V7/15-10 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.532 | 2230 | 20 | 5.7 | 52.0 |  |  |
| V7/29-1 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.445 | 2245 | 5 | 1.3 | 12.0 | $32.4 \pm 16$ |  |
| V7/29-2 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.455 | 2245 | 5 | 3.1 | 28.2 |  |  |
| V7/29-3 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.465 | 2245 | 5 | 2.7 | 24.6 |  |  |
| V7/29-4 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.474 | 2245 | 5 | 2.6 | 23.4 |  |  |
| V7/29-5 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.484 | 2245 | 5 | 2.6 | 23.8 |  |  |
| V7/29-6 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.493 | 2245 | 5 | 3.9 | 35.7 |  |  |
| V7/29-7 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.503 | 2245 | 5 | 3.2 | 29.4 |  |  |
| V7/29-8 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.513 | 2245 | 5 | 4.2 | 38.3 |  |  |
| V7/29-9 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.522 | 2245 | 5 | 7.8 | 70.6 |  |  |
| V7/29-10 | $44^{\circ} 41.7^{\prime} \mathrm{N}$ | $130^{\circ} 22.7^{\prime} \mathrm{W}$ | 4 | 1985.532 | 2245 | 5 | 4.1 | 37.6 |  |  |

Table 2: (continued)

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \operatorname{std} \mathrm{dev} \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V8/30-1 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.521 | 1348 | 902 | 49.5 | 50.9 | $46.1 \pm 26$ |  |
| V8/30-2 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.603 | 1348 | 902 | 21.7 | 22.3 |  |  |
| V8/30-3 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.685 | 1348 | 902 | 23.6 | 24.2 |  |  |
| V8/30-4 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.768 | 1348 | 902 | 40.7 | 41.8 |  |  |
| V8/30-5 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.850 | 1348 | 902 | 50.2 | 51.7 |  |  |
| V8/30-6 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.932 | 1348 | 902 | 59.3 | 60.9 |  |  |
| V8/30-7 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.014 | 1348 | 902 | 83.3 | 85.6 |  |  |
| V8/30-8 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.096 | 1348 | 902 | 21.1 | 21.7 |  |  |
| V8/30-9 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.179 | 1348 | 902 | 15.7 | 16.2 |  |  |
| V8/30-10* | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 170 | 1986.643 | 1348 | 902 | 474.6 | 86.4 |  |  |
| V8/31-1 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.521 | 1698 | 552 | 25.1 | 25.8 | $42.5 \pm 31$ |  |
| V8/31-2 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.603 | 1698 | 552 | 16.4 | 16.8 |  |  |
| V8/31-3 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.685 | 1698 | 552 | 19.5 | 20.4 |  |  |
| V8/31-4 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.768 | 1698 | 552 | 51.7 | 53.2 |  |  |
| V8/31-5 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.850 | 1698 | 552 | 44.6 | 45.9 |  |  |
| V8/31-6 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.932 | 1698 | 552 | 50.6 | 52.0 |  |  |
| V8/31-7 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.014 | 1698 | 552 | 116.4 | 119.7 |  |  |
| V8/31-8 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.096 | 1698 | 552 | 18.7 | 19.2 |  |  |
| V8/31-9 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.179 | 1698 | 552 | 13.3 | 13.7 |  |  |
| V8/31-10 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.261 | 1698 | 552 | 56.2 | 57.8 |  |  |
| V8/32-1 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.521 | 1948 | 302 | 3.2 | 3.3 | $12.6 \pm 8.3$ |  |
| V8/32-2 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.603 | 1948 | 302 | 26.1 | 26.9 |  |  |
| V8/32-3 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.685 | 1948 | 302 | 7.7 | 7.9 |  |  |
| V8/32-4 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.768 | 1948 | 302 | 9.4 | 9.6 |  |  |
| V8/32-5 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.850 | 1948 | 302 | 10.8 | 11.1 |  |  |
| V8/32-6* | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 290 | 1986.259 | 1948 | 302 | 16.7 | 16.7 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1$ std dev | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V8/33-1 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.521 | 2150 | 100 | 17.9 | 18.4 |  |  |
| V8/33-2 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.603 | 2150 | 100 | 16.6 | 17.1 |  |  |
| V8/33-3 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.685 | 2150 | 100 | 17.3 | 17.8 |  |  |
| V8/33-4 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 350 | 1986.643 | 2150 | 100 | 57.3 | 57.3 |  |  |
| V8/36-1 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.521 | 2230 | 20 | 83.7 | 86.1 | $52.7 \pm 29$ |  |
| V8/36-2 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.603 | 2230 | 20 | 21.7 | 22.3 |  |  |
| V8/36-3 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.685 | 2230 | 20 | 14.2 | 14.6 |  |  |
| V8/36-4 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.768 | 2230 | 20 | 28.8 | 29.6 |  |  |
| V8/36-5 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.850 | 2230 | 20 | 44.8 | 46.1 |  |  |
| V8/36-6 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1985.932 | 2230 | 20 | 57.9 | 59.6 |  |  |
| V8/36-7 | $44^{\circ} 42.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.014 | 2230 | 20 | 89.4 | 91.9 |  |  |
| V8/36-8 | $44^{\circ} 42.0^{\prime} \mathrm{N}$ | $130^{\circ} 35.3^{\prime} \mathrm{W}$ | 30 | 1986.643 | 2230 | 20 | 519.9 | 72.0 |  |  |
| V9/12-1 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.712 | 1805 | 800 | 25.3 | 25.3 | $28.8 \pm 37$ |  |
| V9/12-2 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.794 | 1805 | 800 | 14.8 | 14.8 |  |  |
| V9/12-3 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.877 | 1805 | 800 | 4.6 | 4.6 |  |  |
| V9/12-4 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.959 | 1805 | 800 | 9.6 | 9.6 |  |  |
| V9/12-5 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.041 | 1805 | 800 |  |  |  |  |
| V9/12-6 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.123 | 1805 | 800 | 4.2 | 4.2 |  |  |
| V9/12-7 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.205 | 1805 | 800 | 4.2 | 4.2 |  |  |
| V9/12-8 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.288 | 1805 | 800 | 51.2 | 51.2 |  |  |
| V9/12-9 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.370 | 1805 | 800 | 119.9 | 119.9 |  |  |
| V9/12-10 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.452 | 1805 | 800 | 25.5 | 25.5 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \text { std dev } \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V9/13-1 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.712 | 2205 | 400 | 53.1 | 56.4 | $51.1 \pm 35$ |  |
| V9/13-2 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.794 | 2205 | 400 | 48.8 | 51.8 |  |  |
| V9/13-3 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.877 | 2205 | 400 | 90.5 | 96.1 |  |  |
| V9/13-4 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.959 | 2205 | 400 | 22.2 | 23.6 |  |  |
| V9/13-5 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.041 | 2205 | 400 | 8.1 | 8.6 |  |  |
| V9/13-6 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.123 | 2205 | 400 | 14.4 | 15.3 |  |  |
| V9/13-7 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.205 | 2205 | 400 | 31.6 | 33.6 |  |  |
| V9/13-8 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.288 | 2205 | 400 | 58.7 | 62.4 |  |  |
| V9/13-9 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.370 | 2205 | 400 | 105.2 | 111.7 |  |  |
| V9/13-10 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.452 | 2205 | 400 |  |  |  |  |
| V9/14-1 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.712 | 2405 | 200 | 63.9 | 67.9 |  |  |
| V9/14-2 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.794 | 2405 | 200 | 46.6 | 49.5 |  |  |
| V9/14-3 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.877 | 2405 | 200 | 56.8 | 60.4 |  |  |
| V9/14-4 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1986.959 | 2405 | 200 | 8.0 | 8.5 |  |  |
| V9/14-5 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.041 | 2405 | 200 |  |  |  |  |
| V9/14-6 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.123 | 2405 | 200 |  |  |  |  |
| V9/14-7 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.205 | 2405 | 200 |  |  |  |  |
| V9/14-8 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.288 | 2405 | 200 |  |  |  |  |
| V9/14-9 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.370 | 2405 | 200 |  |  |  |  |
| V9/14-10 | $44^{\circ} 47.7^{\prime} \mathrm{N}$ | $130^{\circ} 24.5^{\prime} \mathrm{W}$ | 30 | 1987.452 | 2405 | 200 |  |  |  |  |
| V11/25-1 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1986.729 | 2200 | 50 | 158.1 | 167.8 | $64.7 \pm 55$ |  |
| V11/25-2 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1986.811 | 2200 | 50 | 82.6 | 87.7 |  |  |
| V11/25-3 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1986.893 | 2200 | 50 | 81.5 | 86.6 |  |  |
| V11/25-4 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1986.975 | 2200 | 50 | 31.6 | 33.5 |  |  |
| V11/25-5 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.058 | 2200 | 50 | 8.4 | 8.9 |  |  |
| V11/25-6 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.140 | 2200 | 50 | 26.7 | 28.3 |  |  |
| V11/25-7 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.222 | 2200 | 50 | 6.8 | 7.2 |  |  |
| V11/25-8 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.304 | 2200 | 50 | 134.5 | 142.8 |  |  |
| V11/25-9 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.386 | 2200 | 50 | 42.0 | 44.6 |  |  |
| V11/25-10 | $44^{\circ} 41.05^{\prime} \mathrm{N}$ | $130^{\circ} 13.91^{\prime} \mathrm{W}$ | 30 | 1987.469 | 2200 | 50 | 37.5 | 39.8 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | $\begin{gathered} \text { Depth } \\ (\mathrm{m}) \\ \hline \end{gathered}$ | mab | Mass (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \mathrm{std} \mathrm{dev} \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V12/16-1 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0{ }^{\prime} \mathrm{W}$ | 30 | 1986.729 | 2152 | 100 | 165.0 | 175.2 | $73.0 \pm 68$ |  |
| V12/16-2 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.811 | 2152 | 100 | 140.5 | 149.2 |  |  |
| V12/16-3 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.893 | 2152 | 100 | 75.9 | 80.6 |  |  |
| V12/16-4 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.975 | 2152 | 100 | 143.2 | 152.0 |  |  |
| V12/16-5 | $44^{\circ} 41.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.058 | 2152 | 100 | 18.4 | 19.6 |  |  |
| V12/16-6 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.140 | 2152 | 100 | 18.6 | 19.8 |  |  |
| V12/16-7 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.222 | 2152 | 100 | 5.1 | 4.5 |  |  |
| V12/16-8 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.304 | 2152 | 100 | 29.0 | 30.8 |  |  |
| V12/16-9 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.386 | 2152 | 100 | 25.8 | 27.4 |  |  |
| V12/16-10 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.469 | 2152 | 100 |  |  |  |  |
| V12/18-1 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.729 | 2227 | 25 | 206.3 | 219.1 | $110 \pm 68$ |  |
| V12/18-2 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.811 | 2227 | 25 | 158.3 | 168.1 |  |  |
| V12/18-3 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.893 | 2227 | 25 | 108.7 | 115.5 |  |  |
| V12/18-4 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1986.975 | 2227 | 25 | 201.0 | 213.4 |  |  |
| V12/18-5 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.058 | 2227 | 25 | 69.9 | 74.3 |  |  |
| V12/18-6 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.140 | 2227 | 25 | 53.7 | 57.1 |  |  |
| V12/18-7 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.222 | 2227 | 25 | 34.8 | 37.0 |  |  |
| V12/18-8 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.304 | 2227 | 25 | 87.3 | 92.7 |  |  |
| V12/18-9 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.386 | 2227 | 25 | 67.8 | 72.0 |  |  |
| V12/18-10 | $44^{\circ} 41.4^{\prime} \mathrm{N}$ | $130^{\circ} 21.0^{\prime} \mathrm{W}$ | 30 | 1987.469 | 2227 | 25 | 44.8 | 47.6 |  |  |
| V17/7-1 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.548 | 1500 | 1350 | 15.3 | 16.3 | $36.7 \pm 51$ |  |
| V17/7-2 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.630 | 1500 | 1350 | 8.8 | 9.4 |  |  |
| V17/7-3 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.712 | 1500 | 1350 | 8.0 | 8.5 |  |  |
| V17/7-4 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.795 | 1500 | 1350 | 14.3 | 15.1 |  |  |
| V17/7-5 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.877 | 1500 | 1350 | 16.1 | 17.1 |  |  |
| V17/7-6 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.959 | 1500 | 1350 | 3.3 | 3.5 |  |  |
| V17/7-7 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.041 | 1500 | 1350 | 5.9 | 6.2 |  |  |
| V17/7-8 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.123 | 1500 | 1350 | 66.9 | 71.0 |  |  |
| V17/7-9 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.205 | 1500 | 1350 | 157.8 | 167.5 |  |  |
| V17/7-10 | $44^{\circ} 59.1^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.288 | 1500 | 1350 | 49.7 | 52.7 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{gathered} \text { Mean flux } \\ \pm 1 \mathrm{std} \mathrm{dev} \\ \hline \end{gathered}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V17/6-1 | $44^{\circ} 59.1{ }^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.548 | 2100 | 750 | 21.6 | 22.9 | $31.4 \pm 77$ |  |
| V17/6-2 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.630 | 2100 | 750 | 13.5 | 14.3 |  |  |
| V17/6-3 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.712 | 2100 | 750 | 10.8 | 11.5 |  |  |
| V17/6-4 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.795 | 2100 | 750 | 5.4 | 5.7 |  |  |
| V17/6-5 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.877 | 2100 | 750 | 1.6 | 1.7 |  |  |
| V17/6-6 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.959 | 2100 | 750 | 0.3 | 0.3 |  |  |
| V17/6-7 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.041 | 2100 | 750 | 0.4 | 0.4 |  |  |
| V17/6-8 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.123 | 2100 | 750 | 0.3 | 0.3 |  |  |
| V17/6-9 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.206 | 2100 | 750 | 234.7 | 249.1 |  |  |
| V17/6-10 | $44^{\circ} 59.1{ }^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.288 | 2100 | 750 | 6.8 | 7.2 |  |  |
| V17/11-1 | $44^{\circ} 59.1{ }^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.548 | 2500 | 350 | 17.7 | 18.7 |  |  |
| V17/11-2 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.630 | 2500 | 350 | 9.1 | 9.7 |  |  |
| V17/11-3 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.712 | 2500 | 350 | 4.8 | 5.1 |  |  |
| V17/11-4 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1987.795 | 2500 | 350 | 2.6 | 2.8 |  |  |
| V17/11-5 | $44^{\circ} 59.11^{\prime} \mathrm{N}$ | $130^{\circ} 59.5^{\prime} \mathrm{W}$ | 30 | 1988.288 | 2500 | 350 | 210.0 | 44.6 |  |  |
| V18/15-1 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.548 | 1500 | 800 | 13.2 | 14.0 | $42.2 \pm 86$ |  |
| V18/15-2 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.630 | 1500 | 800 | 7.4 | 7.9 |  |  |
| V18/15-3 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.712 | 1500 | 800 | 4.8 | 5.1 |  |  |
| V18/15-4 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.795 | 1500 | 800 | 7.0 | 7.4 |  |  |
| V18/15-5 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.877 | 1500 | 800 | 7.7 | 8.2 |  |  |
| V18/15-6 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.959 | 1500 | 800 | 1.9 | 4.0 |  |  |
| V18/15-7 | $44^{\circ} 53.44^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1988.041 | 1500 | 800 | 8.7 | 18.5 |  |  |
| V18/15-8 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1988.123 | 1500 | 800 | 23.5 | 25.0 |  |  |
| V18/15-9 | $44^{\circ} 53.44^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1988.206 | 1500 | 800 | 268.8 | 285.4 |  |  |
| V18/15-10 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1988.288 | 1500 | 800 | 43.6 | 46.3 |  |  |
| V18/26-1 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.548 | 2100 | 200 | 16.2 | 17.2 |  |  |
| V18/26-2 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.630 | 2100 | 200 | 7.2 | 7.7 |  |  |
| V18/26-3 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1987.712 | 2100 | 200 | 6.3 | 6.7 |  |  |
| V18/26-4 | $44^{\circ} 53.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 15.6^{\prime} \mathrm{W}$ | 30 | 1988.288 | 2100 | 200 |  |  |  |  |

Table 2: (continued).
$\left.\begin{array}{lccccccccc}\hline \text { Mooring ID } & \text { Latitude } & \text { Longitude } & \begin{array}{c}\text { Collection period } \\ \text { (days) }\end{array} & \begin{array}{c}\text { Completion date }\end{array} & \begin{array}{c}\text { Depth } \\ (\mathrm{m})\end{array} & \begin{array}{c}\text { Mass } \\ \text { mab }\end{array} & \begin{array}{c}\text { VMF } \\ (\mathrm{g})\end{array} & \begin{array}{c}\text { Mean flux } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right)\end{array} \\ \hline 1 \mathrm{std} \text { dev }\end{array} \quad \begin{array}{c}\text { \% Opal }\end{array}\right]$
Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{gathered} \text { Mean flux } \\ \pm 1 \text { std dev } \end{gathered}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V20/30-1 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 1655 | 600 | 1.8 |  | 29.2 |  |
| V20/30(2-9) | $44^{\circ} 59.5{ }^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 1655 | 600 |  |  |  |  |
| V20/30-2 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.690 | 1655 | 600 |  |  |  |  |
| V20/30-3 | $44^{\circ} 59.5{ }^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.696 | 1655 | 600 |  |  |  |  |
| V20/30-4 | $44^{\circ} 59.5{ }^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.701 | 1655 | 600 |  |  |  |  |
| V20/30-5 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.707 | 1655 | 600 |  |  |  |  |
| V20/30-6 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.712 | 1655 | 600 |  |  |  |  |
| V20/30-7 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.718 | 1655 | 600 |  |  |  |  |
| V20/30-8 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.723 | 1655 | 600 |  |  |  |  |
| V20/30-9 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.729 | 1655 | 600 |  |  |  |  |
| V20/30-10 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.734 | 1655 | 600 |  |  |  |  |
| V20/31-1 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2155 | 100 | 9.7 |  | 154.2 |  |
| V20/31(2-9) | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2155 | 100 |  |  |  |  |
| V20/31-2 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.690 | 2155 | 100 |  |  |  |  |
| V20/31-3 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.696 | 2155 | 100 |  |  |  |  |
| V20/31-4 | $44^{\circ} 59.5{ }^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.701 | 2155 | 100 |  |  |  |  |
| V20/31-5 | $44^{\circ} 59.5{ }^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.707 | 2155 | 100 |  |  |  |  |
| V20/31-6 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.712 | 2155 | 100 |  |  |  |  |
| V20/31-7 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.718 | 2155 | 100 |  |  |  |  |
| V20/31-8 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.723 | 2155 | 100 |  |  |  |  |
| V20/31-9 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.729 | 2155 | 100 |  |  |  |  |
| V20/31-10 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.734 | 2155 | 100 |  |  |  |  |
| V20/32-1 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2205 | 50 | 10.2 |  | 161.7 |  |
| V20/32(2-9) | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2205 | 50 |  |  |  |  |
| V20/32-2 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.690 | 2205 | 50 |  |  |  |  |
| V20/32-3 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.696 | 2205 | 50 |  |  |  |  |
| V20/32-4 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.701 | 2205 | 50 |  |  |  |  |
| V20/32-5 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.707 | 2205 | 50 |  |  |  |  |
| V20/32-6 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.712 | 2205 | 50 |  |  |  |  |
| V20/32-7 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.718 | 2205 | 50 |  |  |  |  |
| V20/32-8 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.723 | 2205 | 50 |  |  |  |  |
| V20/32-9 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.729 | 2205 | 50 |  |  |  |  |
| V20/32-10 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.734 | 2205 | 50 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth (m) | mab | Mass <br> (g) | $\begin{gathered} \hline \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \text { std dev } \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V20/33-1 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2225 | 25 | 7.5 |  | 118.7 |  |
| V20/33(2-9) | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.685 | 2225 | 25 |  |  |  |  |
| V20/33-2 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.690 | 2225 | 25 |  |  |  |  |
| V20/33-3 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.696 | 2225 | 25 |  |  |  |  |
| V20/33-4 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.701 | 2225 | 25 |  |  |  |  |
| V20/33-5 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.707 | 2225 | 25 |  |  |  |  |
| V20/33-6 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.712 | 2225 | 25 |  |  |  |  |
| V20/33-7 | $44^{\circ} 59.5^{\prime} \mathrm{Nv}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.718 | 2225 | 25 |  |  |  |  |
| V20/33-8 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.723 | 2225 | 25 |  |  |  |  |
| V20/33-9 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.729 | 2225 | 25 |  |  |  |  |
| V20/33-10 | $44^{\circ} 59.5^{\prime} \mathrm{N}$ | $130^{\circ} 11.4^{\prime} \mathrm{W}$ | 2 | 1987.734 | 2225 | 25 |  |  |  |  |
| V23/13-1 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.633 | 2050 | 175 | 526.0 |  |  |  |
| V23/13-2 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.715 | 2050 | 175 | 4.0 | 4.1 | $16.1 \pm 27$ | 17.1 |
| V23/13-3 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.797 | 2050 | 175 | 4.5 | 4.7 |  | 2.3 |
| V23/13-4 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.880 | 2050 | 175 | 5.6 | 5.7 |  | 18.3 |
| V23/13-5 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.962 | 2050 | 175 | 5.2 | 5.3 |  | 19.3 |
| V23/13-6 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.044 | 2050 | 175 | 1.9 | 2.0 |  | 25.9 |
| V23/13-7 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.126 | 2050 | 175 | 2.6 | 2.7 |  | 14.3 |
| V23/13-8 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.208 | 2050 | 175 | 7.8 | 8.1 |  | 29.8 |
| V23/13-9 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.291 | 2050 | 175 | 82.6 | 85.0 |  | 17.7 |
| V23/13-10 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.373 | 2050 | 175 | 27.1 | 27.8 |  | 16.8 |
| V23/14-1 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.633 | 2125 | 100 | 6.5 | 6.7 |  | 15.9 |
| V23/14-2 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.715 | 2125 | 100 | 7.0 | 7.3 |  | 15.2 |
| V23/14-3 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.797 | 2125 | 100 |  |  |  |  |
| V23/14-4 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.880 | 2125 | 100 |  |  |  |  |
| V23/14-5 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.962 | 2125 | 100 |  |  |  |  |
| V23/14-6 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.044 | 2125 | 100 |  |  |  |  |
| V23/14-7 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.126 | 2125 | 100 |  |  |  |  |
| V23/14-8 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.208 | 2125 | 100 |  |  |  |  |
| V23/14-9 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.291 | 2125 | 100 |  |  |  |  |
| V23/14-10 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.373 | 2125 | 100 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \text { std dev } \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V23/16-1 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.633 | 2195 | 30 | 1.8 | 1.8 |  | 15.9 |
| V23/16-2 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.715 | 2195 | 30 |  |  |  | 15.2 |
| V23/16-3 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.797 | 2195 | 30 |  |  |  |  |
| V23/16-4 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.880 | 2195 | 30 |  |  |  |  |
| V23/16-5 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1988.962 | 2195 | 30 |  |  |  |  |
| V23/16-6 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.044 | 2195 | 30 |  |  |  |  |
| V23/16-7 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.126 | 2195 | 30 |  |  |  |  |
| V23/16-8 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.208 | 2195 | 30 |  |  |  |  |
| V23/16-9 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.291 | 2195 | 30 |  |  |  |  |
| V23/16-10 | $44^{\circ} 48.14^{\prime} \mathrm{N}$ | $130^{\circ} 18.38^{\prime} \mathrm{W}$ | 30 | 1989.373 | 2195 | 30 |  |  |  |  |
| V24/17-1 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.630 | 1850 | 425 | 3.0 | 3.1 | $35.4 \pm 60$ | 10.4 |
| V24/17-2 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.712 | 1850 | 425 | 6.6 | 6.8 |  | 12.2 |
| V24/17-3 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.795 | 1850 | 425 | 10.8 | 11.1 |  |  |
| V24/17-4 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.877 | 1850 | 425 | 15.6 | 16.1 |  | 40.0 |
| V24/17-5 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.959 | 1850 | 425 | 4.4 | 4.5 |  | 31.3 |
| V24/17-6 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.041 | 1850 | 425 | 2.1 | 2.2 |  | 16.5 |
| V24/17-7 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.123 | 1850 | 425 | 4.8 | 4.9 |  | 13.0 |
| V24/17-8 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.205 | 1850 | 425 | 7.8 | 8.1 |  | 14.6 |
| V24/17-9 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.288 | 1850 | 425 | 155.6 | 160.1 |  | 4.5 |
| V24/17-10 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.370 | 1850 | 425 | 133.1 | 137.0 |  | 5.0 |
| V24/18-1 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.630 | 2100 | 175 | 3.7 | 3.9 | $23.7 \pm 46.9$ | 16.1 |
| V24/18-2 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.712 | 2100 | 175 | 3.6 | 3.7 |  | 10.3 |
| V24/18-3 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.795 | 2100 | 175 | 7.4 | 7.6 |  | 27.9 |
| V24/18-4 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.877 | 2100 | 175 | 12.4 | 12.7 |  | 33.5 |
| V24/18-5 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.959 | 2100 | 175 | 5.1 | 5.3 |  | 14.7 |
| V24/18-6 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.041 | 2100 | 175 | 1.7 | 1.8 |  | 12.6 |
| V24/18-7 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.123 | 2100 | 175 | 2.9 | 3.0 |  | 20.7 |
| V24/18-8 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.205 | 2100 | 175 | 28.4 | 29.2 |  | 3.3 |
| $\mathrm{V} 24 / 18-9$ | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.288 | 2100 | 175 | 142.5 | 146.7 |  | 1.0 |
| V24/18-10 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.370 | 2100 | 175 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1$ std dev | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V24/25-1 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.630 | 2175 | 100 | 3.3 | 3.4 |  | 10.2 |
| V24/25-2 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.712 | 2175 | 100 | 2.9 | 3.0 |  | 9.3 |
| V24/25-3 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.795 | 2175 | 100 | 3.3 | 3.4 |  | 4.0 |
| V24/25-4 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.877 | 2175 | 100 |  |  |  |  |
| V24/25-5 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.959 | 2175 | 100 |  |  |  |  |
| V24/25-6 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.041 | 2175 | 100 |  |  |  |  |
| V24/25-7 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.123 | 2175 | 100 |  |  |  |  |
| V24/25-8 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.205 | 2175 | 100 |  |  |  |  |
| V24/25-9 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.288 | 2175 | 100 |  |  |  |  |
| V24/25-10 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.370 | 2175 | 100 | 25.3 | 26.0 |  | 2.9 |
| V24/31-1 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.630 | 2245 | 30 | 9.6 | 9.9 | $17.8 \pm 6.3$ | 12.2 |
| V24/31-2 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.712 | 2245 | 30 | 18.6 | 19.1 |  | 10.4 |
| V24/31-3 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.795 | 2245 | 30 | 19.8 | 20.4 |  | 16.3 |
| V24/31-4 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.877 | 2245 | 30 | 26.7 | 27.5 |  | 35.6 |
| V24/31-5 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1988.959 | 2245 | 30 | 11.1 | 11.4 |  | 19.4 |
| V24/31-6 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.041 | 2245 | 30 | 12.3 | 12.7 |  | 21.6 |
| V24/31-7 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.123 | 2245 | 30 | 17.0 | 17.5 |  | 11.9 |
| V24/31-8 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.205 | 2245 | 30 | 23.6 | 24.2 |  | 27.1 |
| V24/31-9 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.288 | 2245 | 30 |  |  |  |  |
| V24/31-10 | $45^{\circ} 09.99^{\prime} \mathrm{N}$ | $130^{\circ} 10.17^{\prime} \mathrm{W}$ | 30 | 1989.370 | 2245 | 30 |  |  |  |  |
| V25/7-1 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.622 | 1848 | 427 | 4.8 | 5.4 | $10.3 \pm 4.4$ |  |
| V25/7-2 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.712 | 1848 | 427 | 11.0 | 12.5 |  |  |
| V25/7-3 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.803 | 1848 | 427 | 13.6 | 15.3 |  |  |
| V25/7-4 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.893 | 1848 | 427 | 7.0 | 8.0 |  |  |
| V25/7-5 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.984 | 1848 | 427 |  |  |  |  |
| V25/7-6 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.074 | 1848 | 427 |  |  |  |  |
| V25/7-7 | $45^{\circ} 06.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.164 | 1848 | 427 |  |  |  |  |
| V25/7-8 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.255 | 1848 | 427 |  |  |  |  |
| V25/7-9 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.345 | 1848 | 427 |  |  |  |  |
| V25/7-10 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.436 | 1848 | 427 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1$ std dev | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V25/11-1 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.622 | 2100 | 175 | 4.8 | 5.5 |  |  |
| V25/11-2 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.712 | 2100 | 175 | 9.9 | 11.2 |  |  |
| V25/11-3 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.803 | 2100 | 175 | 9.5 | 10.7 |  |  |
| V25/11-4 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.893 | 2100 | 175 |  |  |  |  |
| V25/11-5 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.984 | 2100 | 175 |  |  |  |  |
| V25/11-6 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.074 | 2100 | 175 |  |  |  |  |
| V25/11-7 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.164 | 2100 | 175 |  |  |  |  |
| V25/11-8 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.255 | 2100 | 175 |  |  |  |  |
| V25/11-9 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.345 | 2100 | 175 |  |  |  |  |
| V25/11-10 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.436 | 2100 | 175 |  |  |  |  |
| V25/15-1 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.622 | 2175 | 100 | 2.7 | 3.0 | $60.0 \pm 140$ |  |
| V25/15-2 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.712 | 2175 | 100 | 12.6 | 14.2 |  |  |
| V25/15-3 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.803 | 2175 | 100 | 26.2 | 29.5 |  |  |
| V25/15-4 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.893 | 2175 | 100 | 15.4 | 17.4 |  |  |
| V25/15-5 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.984 | 2175 | 100 | 6.7 | 7.6 |  |  |
| V25/15-6 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.074 | 2175 | 100 | 4.3 | 4.8 |  |  |
| V25/15-7 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.164 | 2175 | 100 | 10.0 | 11.3 |  |  |
| V25/15-8 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.255 | 2175 | 100 | 384.1 | 433.5 |  |  |
| V25/15-9 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.345 | 2175 | 100 | 16.3 | 18.4 |  |  |
| V25/15-10 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.436 | 2175 | 100 |  |  |  |  |
| V25/27-1 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.622 | 2245 | 30 | 3.4 | 3.8 | $20.7 \pm 25.7$ |  |
| V25/27-2 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.712 | 2245 | 30 | 11.1 | 12.5 |  |  |
| V25/27-3 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.803 | 2245 | 30 | 4.2 | 4.8 |  |  |
| V25/27-4 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.893 | 2245 | 30 | 15.0 | 16.9 |  |  |
| V25/27-5 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1989.984 | 2245 | 30 | 7.3 | 8.2 |  |  |
| V25/27-6 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.074 | 2245 | 30 | 4.1 | 4.7 |  |  |
| V25/27-7 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.164 | 2245 | 30 | 15.2 | 17.2 |  |  |
| V25/27-8 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.255 | 2245 | 30 | 73.3 | 82.8 |  |  |
| V25/27-9 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.345 | 2245 | 30 | 44.1 | 49.8 |  |  |
| V25/27-10 | $45^{\circ} 06.0^{\prime} \mathrm{N}$ | $130^{\circ} 10.0^{\prime} \mathrm{W}$ | 33 | 1990.436 | 2245 | 30 | 5.8 | 6.5 |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | $\begin{gathered} \text { Depth } \\ (\mathrm{m}) \end{gathered}$ | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \text { std dev } \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V26/30-1 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.707 | 1848 | 377 | 4.1 | 4.6 | $21.1 \pm 36$ |  |
| V26/30-2 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.797 | 1848 | 377 | 10.5 | 11.9 |  |  |
| V26/30-3 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.888 | 1848 | 377 | 17.8 | 20.0 |  |  |
| V26/30-4 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.978 | 1848 | 377 | 2.2 | 2.4 |  |  |
| V26/30-5 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.069 | 1848 | 377 | 2.1 | 2.4 |  |  |
| V26/30-6 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.159 | 1848 | 377 | 0.8 | 0.9 |  |  |
| V26/30-7 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.250 | 1848 | 377 | 18.8 | 21.2 |  |  |
| V26/30-8 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.340 | 1848 | 377 | 102.2 | 115.3 |  |  |
| V26/30-9 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.430 | 1848 | 377 | 9.6 | 10.8 |  |  |
| V26/30-10 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.521 | 1848 | 377 |  |  |  |  |
| V26/32-1 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.707 | 2050 | 175 | 13.4 | 15.1 | $27.9 \pm 45$ |  |
| V26/32-2 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.797 | 2050 | 175 | 10.4 | 11.7 |  |  |
| V26/32-3 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.888 | 2050 | 175 | 19.4 | 21.8 |  |  |
| V26/32-4 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.978 | 2050 | 175 | 16.1 | 18.2 |  |  |
| V26/32-5 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.069 | 2050 | 175 | 2.0 | 2.3 |  |  |
| V26/32-6 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.159 | 2050 | 175 | 7.3 | 8.2 |  |  |
| V26/32-7 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.250 | 2050 | 175 | 22.1 | 25.0 |  |  |
| V26/32-8 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.340 | 2050 | 175 | 130.3 | 147.1 |  |  |
| V26/32-9 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.430 | 2050 | 175 | 1.5 | 1.7 |  |  |
| V26/32-10 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.521 | 2050 | 175 |  |  |  |  |
| V26/33-1 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.707 | 2125 | 100 | 10.5 | 11.8 | $55.5 \pm 54$ |  |
| V26/33-2 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.797 | 2125 | 100 | 18.7 | 21.1 |  |  |
| V26/33-3 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.888 | 2125 | 100 | 4.7 | 5.3 |  |  |
| V26/33-4 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.978 | 2125 | 100 |  |  |  |  |
| V26/33-5 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.069 | 2125 | 100 |  |  |  |  |
| V26/33-6 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.159 | 2125 | 100 |  |  |  |  |
| V26/33-7 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.250 | 2125 | 100 | 55.7 | 62.9 |  |  |
| V26/33-8 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.340 | 2125 | 100 | 75.8 | 85.5 |  |  |
| V26/33-9 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.430 | 2125 | 100 | 129.6 | 146.3 |  |  |
| V26/33-10 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.521 | 2125 | 100 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period (days) | Completion date | Depth <br> (m) | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Mean flux $\pm 1 \mathrm{std} \mathrm{dev}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V26/36-1 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.707 | 2195 | 30 | 16.8 | 19.0 | $37.0 \pm 46$ |  |
| V26/36-2 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.797 | 2195 | 30 | 20.7 | 23.3 |  |  |
| V26/36-3 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.888 | 2195 | 30 | 21.3 | 24.1 |  |  |
| V26/36-4 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1989.978 | 2195 | 30 | 26.9 | 30.4 |  |  |
| V26/36-5 | $44^{\circ} 48.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.069 | 2195 | 30 | 12.9 | 14.5 |  |  |
| V26/36-6 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.159 | 2195 | 30 | 1.5 | 1.6 |  |  |
| V26/36-7 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.250 | 2195 | 30 | 14.1 | 15.9 |  |  |
| V26/36-8 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.340 | 2195 | 30 | 137.3 | 155.0 |  |  |
| V26/36-9 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.430 | 2195 | 30 | 43.9 | 49.5 |  |  |
| V26/36-10 | $44^{\circ} 48.0^{\prime} \mathrm{N}$ | $130^{\circ} 18.8^{\prime} \mathrm{W}$ | 33 | 1990.521 | 2195 | 30 |  |  |  |  |
| V43/17-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.743 | 1800 | 490 | 16.9 | 19.3 | $30.5 \pm 25$ |  |
| V43/17-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.817 | 1800 | 490 | 23.7 | 27.1 |  |  |
| V43/17-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.890 | 1800 | 490 | 38.5 | 44.0 |  |  |
| V43/17-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.965 | 1800 | 490 | 7.6 | 8.6 |  |  |
| V43/17-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.039 | 1800 | 490 | 15.0 | 17.1 |  |  |
| V43/17-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.112 | 1800 | 490 | 10.5 | 12.0 |  |  |
| V43/17-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.187 | 1800 | 490 | 69.4 | 79.3 |  |  |
| V43/17-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.261 | 1800 | 490 | 51.5 | 58.9 |  |  |
| V43/17-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.335 | 1800 | 490 | 7.4 | 8.5 |  |  |
| V43/17-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.408 | 1800 | 490 |  |  |  |  |
| V43/30-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.743 | 2050 | 240 | 20.9 | 23.9 | $21.0 \pm 17.5$ |  |
| V43/30-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.817 | 2050 | 240 | 15.5 | 17.7 |  |  |
| V43/30-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.890 | 2050 | 240 | 38.9 | 44.5 |  |  |
| V43/30-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.965 | 2050 | 240 | 5.6 | 6.4 |  |  |
| V43/30-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.039 | 2050 | 240 | 7.0 | 8.0 |  |  |
| V43/30-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.112 | 2050 | 240 | . 2 | 7.0 |  |  |
| V43/30-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.187 | 2050 | 240 | 44.3 | 50.6 |  |  |
| V43/30-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.261 | 2050 | 240 | 25.5 | 29.1 |  |  |
| V43/30-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.335 | 2050 | 240 | 1.9 | 2.2 |  |  |
| V43/30-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.408 | 2050 | 240 |  |  |  |  |

Table 2: (continued).

| Mooring ID | Latitude | Longitude | Collection period $\qquad$ | Completion date | $\begin{gathered} \text { Depth } \\ (\mathrm{m}) \end{gathered}$ | mab | Mass <br> (g) | $\begin{gathered} \text { VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | $\begin{aligned} & \text { Mean flux } \\ & \pm 1 \text { std dev } \end{aligned}$ | \% Opal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V43/33-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.743 | 2150 | 140 | 18.8 | 21.5 | $30.1 \pm 24.6$ |  |
| V43/33-2 | $44^{\circ} 56.3{ }^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.817 | 2150 | 140 | 16.9 | 19.3 |  |  |
| V43/33-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.890 | 2150 | 140 | 48.9 | 55.9 |  |  |
| V43/33-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.965 | 2150 | 140 | 7.9 | 9.0 |  |  |
| V43/33-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.039 | 2150 | 140 | 18.7 | 21.4 |  |  |
| V43/33-6 | $44^{\circ} 56.3{ }^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.112 | 2150 | 140 | 8.7 | 10.0 |  |  |
| V43/33-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.187 | 2150 | 140 | 67.4 | 77.1 |  |  |
| V43/33-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.261 | 2150 | 140 | 43.0 | 49.1 |  |  |
| V43/33-9 | $44^{\circ} 56.3{ }^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.335 | 2150 | 140 | 6.9 | 7.8 |  |  |
| V43/33-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.408 | 2150 | 140 |  |  |  |  |
| V43/34-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.743 | 2250 | 40 | 18.1 | 20.7 | $31.8 \pm 25$ |  |
| V43/34-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.817 | 2250 | 40 | 17.4 | 19.9 |  |  |
| V43/34-3 | $44^{\circ} 56.3{ }^{\prime} \mathrm{N}$ | $130^{\circ} 14.7{ }^{\prime} \mathrm{W}$ | 27 | 1990.890 | 2250 | 40 | 44.5 | 50.9 |  |  |
| V43/34-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1990.965 | 2250 | 40 | 10.4 | 11.9 |  |  |
| V43/34-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.039 | 2250 | 40 | 17.4 | 19.9 |  |  |
| V43/34-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.112 | 2250 | 40 | 11.8 | 13.5 |  |  |
| V43/34-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7{ }^{\prime} \mathrm{W}$ | 27 | 1991.187 | 2250 | 40 | 75.9 | 86.8 |  |  |
| V43/34-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.261 | 2250 | 40 | 40.0 | 45.7 |  |  |
| V43/34-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.335 | 2250 | 40 | 15.0 | 17.2 |  |  |
| V43/34-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 27 | 1991.408 | 2250 | 40 |  |  |  |  |

Table 3: Elemental fluxes from moorings V23 and V26.

| Mooring/ | Completion | Corr. VMF | Al flux | Corr. <br> Sl flux | Corr. <br> P flux | S flux | Corr. <br> Mn flux | Corr. <br> Fe flux | Cu flux | Zn flux | Cr flux |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sed. Trap | date | ( $\mathrm{mg} / \mathrm{m}^{2} /$ day) |  |  |  |  |  |  |  |  |  |
| V23/2050m | 1988.715 | 4.3384 | 0.080 | 0.56 | 0.030 | 0.031 | 0.095 | 0.086 | 0.00005 | 0.0016 | 0.0005 |
| V23/2050m | 1988.797 | 5.5715 | 0.060 | 1.43 | 0.008 | 0.036 | 0.049 | 0.068 | 0.00022 | 0.0010 | 0.0004 |
| V23/2050m | 1988.880 | 6.1902 | 0.080 | 1.09 | 0.037 | 0.052 | 0.033 | 0.105 | 0.00012 | 0.0014 | 0.0005 |
| V23/2050m | 1988.962 | 5.9759 | 0.060 | 1.14 | 0.034 | 0.033 | 0.024 | 0.082 | 0 | 0.0016 | 0.0005 |
| V23/2050m | 1989.044 | 2.2312 | 0.050 | 0.57 | -0.002 | 0.020 | 0.018 | 0.044 | 0.00006 | 0.0010 | 0.0003 |
| V23/2050m | 1989.126 | 2.7996 | 0.080 | 0.43 | 0.030 | 0.146 | 0.011 | 0.067 | 0.00059 | 0.0013 | 0.0005 |
| V23/2050m | 1989.208 | 8.8760 | 0.300 | 2.66 | 0.004 | 0.060 | 0.012 | 0.175 | 0 | 0.0023 | 0.0006 |
| V23/2050m | 1989.291 | 86.576 | 0.580 | 13.05 | 0.086 | 0.892 | 0.064 | 0.408 | 0.00043 | 0.0224 | 0.0024 |
| V23/2050m | 1989.373 | 28.884 | 0.320 | 3.83 | 0.029 | 0.147 | 0.025 | 0.286 | 0 | 0.0059 | 0.0017 |
| V26/1848m | 1989.707 | 5.0100 | 0.095 | 0.94 | 0.015 | 0.064 | 0.007 | 0.085 | 0.00001 | 0.0017 | 0.0002 |
| V26/1848m | 1989.797 | 14.220 | 0.130 | 3.44 | 0.083 | 0.144 | 0.008 | 0.078 | 0 | 0.0072 | 0.0003 |
| V26/1848m | 1989.888 | 23.850 | 0.230 | 6.35 | 0.105 | 0.222 | 0.013 | 0.135 | 0.00048 | 0.0068 | 0.0006 |
| V26/1848m | 1989.978 | 4.4400 | 0.140 | 2.62 | 0.011 | 0.046 | 0.002 | 0.021 | 0.00015 | 0.0023 | 0.0001 |
| V26/1848m | 1990.069 | 3.1600 | 0.001 | 1.00 | 0.025 | 0.018 | 0.000 | 0.005 | 0 | 0.0004 | 0.0000 |
| V26/1848m | 1990.159 | 1.0100 | 0.001 | 0.15 | 0.080 | 0.005 | 0.000 | 0.008 | 0.00001 | 0.0003 | 0.0000 |
| V26/1848m | 1990.250 | 24.490 | 0.430 | 5.87 | 0.108 | 0.452 | 0.103 | 0.594 | 0.00146 | 0.0133 | 0.0011 |
| V26/1848m | 1990.340 | 119.72 | 0.520 | 24.89 | 0.191 | 1.049 | 0.050 | 0.461 | 0.00519 | 0.0227 | 0.0016 |
| V26/1848m | 1990.430 | 13.800 | 0.095 | 4.45 | 0.028 | 0.113 | 0.007 | 0.052 | 0.00005 | 0.0040 | 0.0003 |
| V26/2050m | 1989.707 | 16.580 | 0.260 | 3.32 | 0.124 | 0.148 | 0.079 | 1.855 | 0.00214 | 0.0183 | 0.0031 |
| V26/2050m | 1989.797 | 13.880 | 0.142 | 3.33 | 0.099 | 0.124 | 0.035 | 0.874 | 0.00151 | 0.0100 | 0.0014 |
| V26/2050m | 1989.888 | 25.680 | 0.211 | 5.88 | 0.132 | 0.194 | 0.048 | 0.761 | 0.00218 | 0.0123 | 0.0015 |
| V26/2050m | 1989.978 | 21.740 | 0.127 | 7.64 | 0.037 | 0.160 | 0.017 | 0.174 | 0.00075 | 0.0082 | 0.0004 |
| V26/2050m | 1990.069 | 2.8900 | 0.015 | 1.09 | 0.026 | 0.019 | 0.003 | 0.022 | 0.00008 | 0.0007 | 0.0001 |
| V26/2050m | 1990.159 | 9.6800 | 0.071 | 2.35 | 0.036 | 0.092 | 0.008 | 0.149 | 0.00057 | 0.0055 | 0.0005 |
| V26/2050m | 1990.250 | 28.110 | 0.347 | 6.56 | 0.117 | 0.247 | 0.066 | 0.627 | 0.00183 | 0.0077 | 0.0016 |
| V26/2050m | 1990.340 | 151.59 | 0.706 | 27.48 | 0.199 | 1.442 | 0.155 | 1.313 | 0 | 0.0382 | 0.0044 |
| V26/2050m | 1990.430 | 2.8500 | 0.003 | 1.29 | 0.021 | 0.008 | 0.001 | 0.005 | 0 | 0.0002 | 0.0000 |

Table 4: Elemental fluxes from mooring V43.

| Sample | Dec. | Depth. | VMF | Al | Si | P | S | Cr | Mn | Fe | Cu | Zn | Ca | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | date | (m) | (mg/m ${ }^{2} /$ day $)$ |  |  |  |  |  |  |  |  |  |  |  |
| V43-17-1 | 1990.743 | 1800.0 | 19.276 | 0.093274 | 2.3728 | 0.026 | 0.082923 | 0.00041737 | 0.0059884 | 0.0662 | 0.0000 | 0.010586 | 3.1229 | 0.00056 |
| V43-17-2 | 1990.817 | 1800.0 | 27.089 | 0.11044 | 4.4330 | 0.177 | 0.20247 | 0.00062708 | 0.0073350 | 0.0728 | 0.0000 | 0.0090833 | 0.97524 | 0.00078 |
| V43-17-3 | 1990.891 | 1800.0 | 43.962 | 0.29649 | 11.886 | 0.065 | 0.31046 | 0.0014098 | 0.014217 | 0.2122 | 0.0000 | 0.015667 | 1.1431 | 0.00168 |
| V43-17-4 | 1990.965 | 1800.0 | 8.641 | 0.10474 | 2.3310 | 0.022 | 0.093388 | 0.00028935 | 0.0079352 | 0.0814 | 0.00051264 | 0.0040579 | 0.057039 | 0.00032 |
| V43-17-5 | 1991.039 | 1800.0 | 17.104 | 0.11999 | 4.9319 | 0.048 | 0.11882 | 0.00042287 | 0.0062528 | 0.0852 | 0.0000 | 0.0055604 | 0.14199 | 0.00042 |
| V43-17-6 | 1991.113 | 1800.0 | 12.016 | 0.096923 | 2.6550 | 0.022 | 0.093273 | 0.00048407 | 0.0077881 | 0.0707 | 0.00038534 | 0.0051410 | 0.28841 | 0.00029 |
| V43-17-7 | 1991.187 | 1800.0 | 79.299 | 0.33798 | 16.440 | 0.051 | 0.44787 | 0.0020988 | 0.025807 | 0.2957 | 0.0000 | 0.017315 | 9.0405 | 0.00185 |
| V43-17-8 | 1991.261 | 1800.0 | 58.900 | 0.36138 | 11.352 | 0.028 | 0.29738 | 0.0020670 | 0.022354 | 0.2656 | 0.0000 | 0.014012 | 6.3023 | 0.00198 |
| V43-17-9 | 1991.335 | 1800.0 | 8.512 | 0.074460 | 1.4318 | 0.000 | 0.10975 | 0.00023719 | 0.0011679 | 0.0483 | $5.1440 \mathrm{e}-05$ | 0.0024114 | 0.46819 | 0.00033 |
| V43-30-1 | 1990.743 | 2050.0 | 23.851 | 0.13093 | 2.7000 | 0.028 | 0.095576 | 0.0016756 | 0.017725 | 0.3203 | 0.00096789 | 0.0088862 | 5.1058 | 0.00099 |
| V43-30-2 | 1990.817 | 2050.0 | 17.690 | 0.11158 | 3.0704 | 0.037 | 0.16480 | 0.0013366 | 0.012812 | 0.2086 | 0.00046550 | 0.0081679 | 1.5217 | 0.00072 |
| V43-30-3 | 1990.891 | 2050.0 | 44.499 | 0.25322 | 8.0562 | 0.050 | 0.26235 | 0.0026221 | 0.023625 | 0.0547 | 0.0068841 | 0.013884 | 0.93458 | 0.00125 |
| V43-30-4 | 1990.965 | 2050.0 | 6.422 | 0.057421 | 0.87582 | 0.019 | 0.064616 | 0.00042833 | 0.0098061 | 0.0979 | 0.0013437 | 0.0046171 | 0.043697 | 0.00037 |
| V43-30-5 | 1991.039 | 2050.0 | 7.965 | 0.085789 | 2.2757 | 0.019 | 0.075494 | 0.00056250 | 0.012620 | 0.1275 | 0.00035945 | 0.0030730 | 0.044635 | 0.00039 |
| V43-30-6 | 1991.113 | 2050.0 | 7.046 | 0.087383 | 2.1193 | 0.014 | 0.076652 | 0.00047780 | 0.010403 | 0.1078 | 0.00033081 | 0.0026906 | 0.050049 | 0.00033 |
| V43-30-7 | 1991.187 | 2050.0 | 50.624 | 0.21632 | 10.146 |  | 0.32212 | 0.0025717 | 0.024667 | 0.2616 | 0.0000 | 0.0094313 | 6.3280 | 0.00123 |
| V43-30-8 | 1991.261 | 2050.0 | 29.108 | 0.19110 | 5.7148 | 0.023 | 0.17354 | 0.0026424 | 0.018343 | 0.1945 | 0.00011665 | 0.0092694 | 3.2313 | 0.00109 |
| V43-30-9 | 1991.335 | 2050.0 | 2.201 | 0.027377 | 0.39334 | 0.013 | 0.019789 | 0.00019584 | 0.0026274 | 0.0297 | 0.0000 | 0.0013498 | 0.018711 | 0.00010 |
| V43-33-1 | 1990.743 | 2150.0 | 21.458 | 0.15927 | 2.6277 | 0.040 | 0.13057 | 0.00096144 | 0.0027774 | 0.4500 | 0.00031382 | 0.0075077 | 1.7012 | 0.00108 |
| V43-33-2 | 1990.817 | 2150.0 | 19.306 | 0.11375 | 2.5874 | 0.039 | 0.10955 | 0.00081749 | 0.026719 | 0.4322 | $4.5727 \mathrm{e}-05$ | 0.010090 | 0.86904 | 0.00126 |
| V43-33-3 | 1990.891 | 2150.0 | 55.917 | 0.61527 | 20.284 | 0.128 | 0.55503 | 0.0022057 | 0.097427 | 0.8689 | 0.00043428 | 0.014811 | 1.7337 | 0.00296 |
| V43-33-4 | 1990.965 | 2150.0 | 8.979 | 0.13766 | 2.0088 | 0.048 | 0.13628 | 0.00059143 | 0.0014423 | 0.2534 | 0.00090537 | 0.0029864 | 0.060293 | 0.00073 |
| V43-33-5 | 1991.039 | 2150.0 | 21.423 | 0.24222 | 6.3807 | 0.036 | 0.15399 | 0.0010412 | 0.045854 | 0.3811 | 0.00011836 | 0.0092814 | 0.49284 | 0.00091 |
| V43-33-6 | 1991.113 | 2150.0 | 9.960 | 0.14829 | 2.7945 | 0.024 | 0.089292 | 0.00063676 | 0.026485 | 0.2535 | 0.00027929 | 0.0063219 | 0.17929 | 0.00063 |
| V43-33-7 | 1991.187 | 2150.0 | 77.068 | 0.43091 | 15.277 | 0.039 | 0.35533 | 0.0033818 | 0.079558 | 0.7697 | 0.0000 | 0.014378 | 8.0932 | 0.00247 |
| V43-33-8 | 1991.261 | 2150.0 | 49.090 | 0.35259 | 8.5465 | 0.018 | 0.21115 | 0.0017301 | 0.052350 | 0.4382 | 0.00079923 | 0.015540 | 6.1370 | 0.00174 |
| V43-33-9 | 1991.335 | 2150.0 | 7.847 | 0.083291 | 0.91069 |  | 0.063359 | 0.00096272 | 0.010800 | 0.1219 | $3.8103 \mathrm{e}-06$ | 0.0042893 | 1.4674 | 0.00035 |
| V43-34-1 | 1990.743 | 2250.0 | 20.654 | 0.20674 | 1.4803 | 0.075 | 0.30804 | 0.00043415 | 0.051892 | 0.6631 | 0.00018607 | 0.0066157 | 0.15506 | 0.00364 |
| V43-34-2 | 1990.817 | 2250.0 | 19.847 | 0.021840 | 0.087362 | 0.085 | 0.20848 | 0.0000 | 0.0031768 | 0.0772 | 0.0012906 | 0.0054998 | 0.10523 | 0.00000 |
| V43-34-3 | 1990.891 | 2250.0 | 50.902 | 0.44800 | 2.6065 | 0.185 | 0.69745 | 0.0000 | 0.050756 | 0.5977 | 0.0000 | 0.0085527 | 0.32073 | 0.00402 |
| V43-34-4 | 1990.965 | 2250.0 | 11.872 | 0.064141 | 0.31714 | 0.105 | 0.098587 | 0.0000 | 0.014622 | 0.1762 | 0.0000 | 0.0038722 | 0.11284 | 0.00069 |
| V43-34-5 | 1991.039 | 2250.0 | 19.863 | 0.19471 | 1.3014 | 0.053 | 0.19073 | 0.00027815 | 0.056167 | 0.4505 | 0.00049670 | 0.0041127 | 0.10331 | 0.00123 |
| V43-34-6 | 1991.113 | 2250.0 | 13.463 | 0.11717 | 0.79596 | 0.039 | 0.13603 | 0.0000 | 0.033764 | 0.2639 | $5.3872 \mathrm{e}-05$ | 0.0016431 | 0.082155 | 0.00096 |
| V43-34-7 | 1991.187 | 2250.0 | 86.773 | 0.22561 | 1.9090 | 0.169 | 1.0673 | 0.0000 | 0.014231 | 0.2793 | 0.0015619 | 0.077490 | 0.35578 | 0.00174 |
| V43-34-8 | 1991.261 | 2250.0 | 45.678 | 0.32434 | 2.3297 | 0.077 | 0.55731 | 0.0000 | 0.18058 | 0.4463 | 0.0000 | 0.0085880 | 0.25125 | 0.00123 |
| V43-34-9 | 1991.335 | 2250.0 | 17.182 | 0.020627 | 0.12204 | 0.045 | 0.15126 | 0.0000 | 0.0025268 | 0.0347 | 0.0000 | 0.0010313 | 0.077350 | 0.00000 |

Table 5: Total VMF and biogenic opal concentrations from moorings V32-V42.

| Mooring <br> ID | Latitude | Longitude | Coll. intvl. (days) | $\begin{gathered} \text { Compl. } \\ \text { date } \end{gathered}$ | $\begin{gathered} \text { Depth } \\ (\mathrm{m}) \end{gathered}$ | MAB | $\begin{gathered} \hline \text { Total mass } \\ (\mathrm{mg}) \end{gathered}$ | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | Opal free VMF $\left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right)$ | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V32/12-1 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 1800.0 | 695 | 1.550 | 0.613 | 7.9679 | 3.151 | 60.457 | 22.600 |
| V32/12-2 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 1800.0 | 695 |  | 1.429 | 17.340 | 7.352 | 57.602 |  |
| V32/12-3 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 1800.0 | 695 |  | 3.196 | 38.572 | 16.435 | 57.390 |  |
| V32/12-4 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 1800.0 | 695 |  | 2.458 | 32.283 | 12.641 | 60.843 |  |
| V32/12-5 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 1800.0 | 695 |  | 2.610 | 36.561 | 13.424 | 63.283 |  |
| V32/12-6 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 1800.0 | 695 |  | 3.022 | 33.383 | 15.541 | 53.447 |  |
| V32/12-7 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 1800.0 | 695 |  | 0.587 | 13.094 | 3.019 | 76.943 |  |
| V32/12-8 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 1800.0 | 695 |  | 1.435 | 25.707 | 7.383 | 71.278 |  |
| V32/12-9 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 1800.0 | 695 |  | 0.887 | 15.424 | 4.561 | 70.429 |  |
| V32/12-10 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 1800.0 | 695 |  | 0.390 | 5.6966 | 2.004 | 64.824 |  |
| V32/24-1 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2250.0 | 245 |  |  |  |  |  | 0.0000 |
| V32/24-2 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-3 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-4 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-5 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-6 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-7 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-8 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-9 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2250.0 | 245 |  |  |  |  |  |  |
| V32/24-10 | $44^{\circ} 54.4{ }^{\prime} \mathrm{N}$ | $130^{\circ} 07.8^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2250.0 | 245 |  |  |  |  |  |  |
| V33/26-1 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2150.0 | 120 |  | 0.599 | 6.1941 | 3.083 | 50.227 | 19.700 |
| V33/26-2 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2150.0 | 120 |  | 0.897 | 11.703 | 4.615 | 60.561 |  |
| V33/26-3 | $44^{\circ} 56.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2150.0 | 120 |  | 1.193 | 15.526 | 6.135 | 60.486 |  |
| V33/26-4 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2150.0 | 120 |  | 0.757 | 10.208 | 3.895 | 61.845 |  |
| V33/26-5 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2150.0 | 120 |  | 2.831 | 33.087 | 14.561 | 55.992 |  |
| V33/26-6 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2150.0 | 120 |  | 1.647 | 28.180 | 8.472 | 69.937 |  |
| V33/26-7 | $44^{\circ} 56.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2150.0 | 120 |  | 2.408 | 30.973 | 12.384 | 60.017 |  |
| V33/26-8 | $44^{\circ} 56.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2150.0 | 120 |  | 1.179 | 20.094 | 6.063 | 69.826 |  |
| V33/26-9 | $44^{\circ} 56.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2150.0 | 120 |  | 0.941 | 12.551 | 4.840 | 61.438 |  |
| V33/26-10 | $44^{\circ} 56.00^{\prime} \mathrm{N}$ | $130^{\circ} 12.35^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2150.0 |  |  | 2.891 | 28.662 | 14.868 | 48.128 |  |

Table 5: (continued).

| Mooring ID | Latitude | Longitude | Coll. intvl. (days) | Compl. date | Depth <br> (m) | MAB | Total mass (mg) | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Opal free VMF $\left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right)$ | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V34/15-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2050.0 | 243 |  | 0.875 | 18.043 | 4.500 | 75.062 | 28.600 |
| V34/15-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2050.0 | 243 |  | 0.956 | 15.136 | 4.915 | 67.526 |  |
| V34/15-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2050.0 | 243 |  | 2.123 | 27.845 | 10.917 | 60.793 |  |
| V34/15-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2050.0 | 243 |  | 1.597 | 31.829 | 8.214 | 74.192 |  |
| V34/15-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2050.0 | 243 |  | 3.035 | 50.240 | 15.607 | 68.934 |  |
| V34/15-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2050.0 | 243 |  | 3.416 | 52.462 | 17.568 | 66.513 |  |
| V34/15-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2050.0 | 243 |  | 1.315 | 31.725 | 6.766 | 78.673 |  |
| V34/15-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2050.0 | 243 |  | 1.505 | 32.417 | 7.741 | 76.121 |  |
| V34/15-9 | $44^{\circ} 56.3 \mathrm{Nv}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2050.0 | 243 |  | 0.833 | 19.817 | 4.283 | 78.388 |  |
| V34/15-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2050.0 | 243 |  | 0.438 | 6.8148 | 2.252 | 66.954 |  |
| V34/30-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2150.0 | 143 |  | 6.701 | 149.480 | 34.464 | 76.944 | 51.600 |
| V34/30-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2150.0 | 143 |  | 2.656 | 34.147 | 13.659 | 59.999 |  |
| V34/30-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2150.0 | 143 |  | 1.724 | 24.591 | 8.869 | 63.934 |  |
| V34/30-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2150.0 | 143 |  | 2.812 | 43.982 | 14.461 | 67.121 |  |
| V34/30-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2150.0 | 143 |  | 3.890 | 60.465 | 20.005 | 66.914 |  |
| V34/30-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2150.0 | 143 |  | 3.666 | 72.828 | 18.857 | 74.108 |  |
| V34/30-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2150.0 | 143 |  | 2.611 | 52.482 | 13.429 | 74.412 |  |
| V34/30-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2150.0 | 143 |  | 1.926 | 33.515 | 9.906 | 70.443 |  |
| V34/30-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2150.0 | 143 |  | 0.716 | 16.409 | 3.683 | 77.557 |  |
| V34/30-10 | $44^{\circ} 56.3 \mathrm{Nv}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2150.0 | 143 |  | 2.191 | 27.934 | 11.269 | 59.659 |  |
| V34/20-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2150.0 | 143 |  |  |  |  |  | 0.0000 |
| V34/20-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2150.0 | 143 |  |  |  |  |  |  |
| V34/20-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2150.0 | 143 |  |  |  |  |  |  |

Table 5: (continued).

| Mooring ID | Latitude | Longitude | Coll. intvl. (days) | Compl. date | Depth <br> (m) | MAB | Total mass (mg) | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Opal free VMF $\left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right)$ | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V34/27-1 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2285.0 | 5.00 |  | 2.403 | 26.938 | 12.361 | 54.112 | 42.200 |
| V34/27-2 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2285.0 | 5.00 |  | 1.534 | 22.769 | 7.892 | 65.341 |  |
| V34/27-3 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2285.0 | 5.00 |  | 2.492 | 30.607 | 12.819 | 58.117 |  |
| V34/27-4 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2285.0 | 5.00 |  | 2.949 | 34.616 | 15.169 | 56.179 |  |
| V34/27-5 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2285.0 | 5.00 |  | 5.016 | 70.266 | 25.798 | 63.285 |  |
| V34/27-6 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2285.0 | 5.00 |  | 5.160 | 75.860 | 26.542 | 65.012 |  |
| V34/27-7 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2285.0 | 5.00 |  | 4.633 | 51.682 | 23.829 | 53.893 |  |
| V34/27-8 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2285.0 | 5.00 |  | 4.108 | 60.578 | 21.130 | 65.119 |  |
| V34/27-9 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2285.0 | 5.00 |  | 2.191 | 28.507 | 11.268 | 60.472 |  |
| V34/27-10 | $44^{\circ} 56.3^{\prime} \mathrm{N}$ | $130^{\circ} 14.7^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2285.0 | 5.00 |  | 2.184 | 20.111 | 11.230 | 44.159 |  |
| V35/11-1 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2150.0 | 18.0 |  | 2.612 | 26.682 | 13.436 | 49.643 | 41.200 |
| V35/11-2 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2150.0 | 18.0 |  | 2.759 | 28.396 | 14.188 | 50.035 |  |
| V35/11-3 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2150.0 | 18.0 |  | 3.206 | 30.432 | 16.491 | 45.812 |  |
| V35/11-4 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2150.0 | 18.0 |  | 3.829 | 40.307 | 19.692 | 51.145 |  |
| V35/11-5 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2150.0 | 18.0 |  | 6.626 | 69.084 | 34.080 | 50.669 |  |
| V35/11-6 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2150.0 | 18.0 |  | 7.140 | 79.011 | 36.723 | 53.522 |  |
| V35/11-7 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2150.0 | 18.0 |  | 3.107 | 40.351 | 15.979 | 60.401 |  |
| V35/11-8 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2150.0 | 18.0 |  | 4.158 | 43.519 | 21.385 | 50.860 |  |
| V35/11-9 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2150.0 | 18.0 |  | 2.808 | 26.764 | 14.440 | 46.047 |  |
| V35/11-10 | $44^{\circ} 56.7^{\prime} \mathrm{N}$ | $130^{\circ} 15.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2150.0 | 18.0 |  | 3.455 | 26.963 | 17.769 | 34.098 |  |
| V36/29-1 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 1500.0 | 955 |  | 1.345 | 17.793 | 6.920 | 61.110 | 30.000 |
| V36/29-2 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 1500.0 | 955 |  | 1.192 | 21.118 | 6.133 | 70.960 |  |
| V36/29-3 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 1500.0 | 955 |  | 3.167 | 41.304 | 16.289 | 60.563 |  |
| V36/29-4 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 1500.0 | 955 |  | 4.413 | 55.759 | 22.696 | 59.296 |  |
| V36/29-5 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 1500.0 | 955 |  | 2.188 | 38.512 | 11.256 | 70.773 |  |
| V36/29-6 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 1500.0 | 955 |  | 0.881 | 19.100 | 4.534 | 76.263 |  |
| V36/29-7 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 1500.0 | 955 |  | 1.733 | 33.622 | 8.912 | 73.493 |  |
| V36/29-8 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 1500.0 | 955 |  | 1.273 | 18.819 | 6.547 | 65.210 |  |
| V36/29-9 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 1500.0 | 955 |  | 2.138 | 23.611 | 10.996 | 53.429 |  |
| V36/29-10 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 1500.0 | 955 |  |  |  |  |  |  |

Table 5: (continued).

| Mooring ID | Latitude | Longitude | Coll. intvl. (days) | Compl. date | Depth <br> (m) | MAB | Total mass (mg) | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Opal free VMF ( $\mathrm{mg} / \mathrm{m}^{2} /$ day) | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V36/32-1 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 1800.0 | 655 |  |  |  |  |  |  |
| V36/32-2 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 1800.0 | 655 |  |  |  |  |  |  |
| V36/32-3 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 1800.0 | 655 |  |  | 9.4825 |  |  |  |
| V36/32-4 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 1800.0 | 655 |  | 1.272 | 22.151 | 6.544 | 70.459 |  |
| V36/32-5 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 1800.0 | 655 |  | 0.992 | 20.783 | 5.102 | 75.453 |  |
| V36/32-6 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 1800.0 | 655 |  | 0.683 | 16.061 | 3.515 | 78.116 |  |
| V36/32-7 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 1800.0 | 655 |  | 0.327 | 8.7762 | 1.684 | 80.815 |  |
| V36/32-8 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 1800.0 | 655 |  | 0.000 | 7.9764 | 0.000 | 100.00 |  |
| V36/32-9 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 1800.0 | 655 |  |  |  |  |  |  |
| V36/32-10 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 1800.0 | 655 |  |  |  |  |  |  |
| V36/33-1 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 1800.0 | 655 |  | 2.224 | 26.308 | 11.437 | 56.525 | 17.600 |
| V36/33-2 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 1800.0 | 655 |  |  |  |  |  |  |
| V36/33-3 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 1800.0 | 655 |  | 1.298 | 22.885 | 6.675 | 70.833 |  |
| V36/33-4 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 1800.0 | 655 |  | 0.928 | 12.315 | 4.774 | 61.238 |  |
| V36/33-5 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 1800.0 | 655 |  | 2.757 | 38.086 | 14.179 | 62.772 |  |
| V36/33-6 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 1800.0 | 655 |  | 0.401 | 10.380 | 2.064 | 80.120 |  |
| V36/33-7 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 1800.0 | 655 |  | 1.205 | 22.407 | 6.196 | 72.346 |  |
| V36/33-8 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 1800.0 | 655 |  | 0.504 | 10.356 | 2.592 | 74.969 |  |
| V36/33-9 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 1800.0 | 655 |  | 0.394 | 7.0874 | 2.026 | 71.410 |  |
| V36/33-10 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 1800.0 | 655 |  | 1.204 | 8.5772 | 6.194 | 27.788 |  |
| V36/36-1 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2250.0 | 205 |  |  |  |  |  |  |
| V36/36-2 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2250.0 | 205 |  | 1.356 | 21.318 | 6.974 | 67.287 |  |
| V36/36-3 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2250.0 | 205 |  | 3.280 | 53.176 | 16.872 | 68.271 |  |
| V36/36-4 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2250.0 | 205 |  | 2.869 | 56.961 | 14.753 | 74.099 |  |
| V36/36-5 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2250.0 | 205 |  | 2.810 | 53.144 | 14.454 | 72.803 |  |
| V36/36-6 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2250.0 | 205 |  | 2.219 | 36.266 | 11.414 | 68.527 |  |
| V36/36-7 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2250.0 | 205 |  | 2.706 | 47.311 | 13.915 | 70.587 |  |
| V36/36-8 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2250.0 | 205 |  | 2.294 | 44.797 | 11.797 | 73.665 |  |
| V36/36-9 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2250.0 | 205 |  | 2.121 | 33.026 | 10.911 | 66.964 |  |
| V36/36-10 | $44^{\circ} 57.7^{\prime} \mathrm{N}$ | $130^{\circ} 20.4^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2250.0 | 205 |  | 1.636 | 26.507 | 8.413 | 68.263 |  |

Table 5: (continued).

| $\begin{gathered} \hline \text { Mooring } \\ \text { ID } \\ \hline \end{gathered}$ | Latitude | Longitude | Coll. intvl. (days) | $\begin{gathered} \text { Compl. } \\ \text { date } \end{gathered}$ | $\begin{gathered} \text { Depth } \\ (\mathrm{m}) \end{gathered}$ | MAB | $\begin{gathered} \hline \text { Total mass } \\ (\mathrm{mg}) \end{gathered}$ | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \\ \hline \end{gathered}$ | Opal free VMF ( $\mathrm{mg} / \mathrm{m}^{2} /$ day ) | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V37/6-1 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.66^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2200.0 | 175 |  | 1.968 | 18.275 | 10.124 | 44.601 | 28.800 |
| V37/6-2 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2200.0 | 175 |  | 1.707 | 20.326 | 8.779 | 56.810 |  |
| V37/6-3 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2200.0 | 175 |  | 1.885 | 23.124 | 9.693 | 58.081 |  |
| V37/6-4 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2200.0 | 175 |  | 2.752 | 30.731 | 14.155 | 53.941 |  |
| V37/6-5 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2200.0 | 175 |  | 6.007 | 58.440 | 30.898 | 47.130 |  |
| V37/6-6 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2200.0 | 175 |  | 2.676 | 38.830 | 13.764 | 64.553 |  |
| V37/6-7 | $44^{\circ} 57.00^{\prime} \mathrm{N}$ | $130^{\circ} 10.6{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2200.0 | 175 |  | 2.480 | 37.143 | 12.758 | 65.65 |  |
| V37/6-8 | $44^{\circ} 57.00^{\prime} \mathrm{N}$ | $130^{\circ} 10.6^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2200.0 | 175 |  | 0.860 | 15.023 | 4.425 | 70.549 |  |
| V37/6-9 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2200.0 | 175 |  | 1.342 | 17.034 | 6.900 | 59.491 |  |
| V37/6-10 | $44^{\circ} 57.0{ }^{\prime} \mathrm{N}$ | $130^{\circ} 10.6^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2200.0 | 175 |  |  |  |  |  |  |
| V38/18-1 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-2 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-3 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-4 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.11^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-5 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-6 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-7 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-8 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-9 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/18-10 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2050.0 | 232 |  |  |  |  |  |  |
| V38/34-1 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2150.0 | 132 |  | 1.643 | 21.297 | 8.449 | 60.325 | 32.600 |
| V38/34-2 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2150.0 | 132 |  | 1.929 | 19.653 | 9.923 | 49.506 |  |
| V38/34-3 | $44^{\circ} 58.8{ }^{\prime} \mathrm{N}$ | $130^{\circ} 13.1^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2150.0 | 132 |  | 4.165 | 34.823 | 21.423 | 38.482 |  |
| V38/34-4 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.11^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2150.0 | 132 |  | 2.147 | 20.636 | 11.045 | 46.477 |  |
| V38/34-5 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2150.0 | 132 |  | 5.887 | 61.081 | 30.280 | 50.425 |  |
| V38/34-6 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2150.0 | 132 |  | 5.138 | 60.007 | 26.428 | 55.959 |  |
| V38/34-7 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2150.0 | 132 |  | 1.902 | 30.895 | 9.783 | 68.334 |  |
| V38/34-8 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2150.0 | 132 |  | 2.094 | 29.776 | 10.768 | 63.838 |  |
| V38/34-9 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2150.0 | 132 |  | 0.724 | 15.207 | 3.723 | 75.520 |  |
| V38/34-10 | $44^{\circ} 58.88^{\prime} \mathrm{N}$ | $130^{\circ} 13.1{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2150.0 | 132 |  | 0.347 | 5.4523 | 1.784 | 67.276 |  |

Table 5: (continued).

| Mooring ID $\qquad$ | Latitude | Longitude | Coll. intvl. (days) | Compl. date | Depth <br> (m) | MAB | Total mass (mg) | Opal free mass (g) | $\begin{gathered} \text { Total VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ | Opal free VMF $\left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right)$ | \% opal | $\begin{gathered} \text { Mean VMF } \\ \left(\mathrm{mg} / \mathrm{m}^{2} / \text { day }\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V39/17-1 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2200.0 | 85.0 |  | 1.443 | 16.466 | 7.420 | 54.939 | 29.900 |
| V39/17-2 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2200.0 | 85.0 |  | 2.044 | 22.718 | 10.512 | 53.729 |  |
| V39/17-3 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2200.0 | 85.0 |  | 2.201 | 23.469 | 11.320 | 51.766 |  |
| V39/17-4 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2200.0 | 85.0 |  | 1.807 | 20.683 | 9.295 | 55.060 |  |
| V39/17-5 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2200.0 | 85.0 |  | 2.270 | 35.752 | 11.677 | 67.338 |  |
| V39/17-6 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2200.0 | 85.0 |  | 4.010 | 54.759 | 20.624 | 62.337 |  |
| V39/17-7 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2200.0 | 85.0 |  | 2.050 | 32.300 | 10.544 | 67.356 |  |
| V39/17-8 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2200.0 | 85.0 |  | 4.906 | 56.386 | 25.235 | 55.246 |  |
| V39/17-9 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2200.0 | 85.0 |  | 2.168 | 30.296 | 11.151 | 63.194 |  |
| V39/17-10 | $44^{\circ} 58.8^{\prime} \mathrm{N}$ | $130^{\circ} 16.4{ }^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2200.0 | 85.0 |  | 0.384 | 6.0917 | 1.974 | 67.587 |  |
| V40/31-1 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2200.0 | 165 |  | 2.043 | 23.279 | 10.507 | 54.864 | 32.100 |
| V40/31-2 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2200.0 | 165 |  | 1.756 | 23.276 | 9.031 | 61.201 |  |
| V40/31-3 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2200.0 | 165 |  | 6.542 | 63.254 | 33.648 | 46.804 |  |
| V40/31-4 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2200.0 | 165 |  | 1.601 | 28.404 | 8.235 | 71.009 |  |
| V40/31-5 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2200.0 | 165 |  | 3.904 | 51.022 | 20.080 | 60.645 |  |
| V40/31-6 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2200.0 | 165 |  | 2.038 | 34.627 | 10.480 | 69.734 |  |
| V40/31-7 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2200.0 | 165 |  | 1.907 | 31.219 | 9.809 | 68.579 |  |
| V40/31-8 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2200.0 | 165 |  | 1.429 | 26.340 | 7.350 | 72.097 |  |
| V40/31-9 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2200.0 | 165 |  | 1.582 | 24.986 | 8.135 | 67.442 |  |
| V40/31-10 | $44^{\circ} 53.6^{\prime} \mathrm{N}$ | $130^{\circ} 11.8^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 |  |  |  | 1.166 | 14.503 | 5.998 | 58.640 |  |
| V41/13-1 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5640 | 2050.0 | 247 |  | 1.247 | 15.137 | 6.414 | 57.628 | 31.100 |
| V41/13-2 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5804 | 2050.0 | 247 |  | 1.131 | 16.673 | 5.817 | 65.115 |  |
| V41/13-3 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.5969 | 2050.0 | 247 |  | 4.629 | 51.414 | 23.808 | 53.693 |  |
| V41/13-4 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6133 | 2050.0 | 247 |  | 2.884 | 31.750 | 14.834 | 53.279 |  |
| V41/13-5 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6298 | 2050.0 | 247 |  | 7.817 | 88.204 | 40.205 | 54.418 |  |
| V41/13-6 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6462 | 2050.0 | 247 |  | 2.934 | 40.178 | 15.091 | 62.439 |  |
| V41/13-7 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6626 | 2050.0 | 247 |  | 1.979 | 27.247 | 10.177 | 62.647 |  |
| V41/13-8 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6791 | 2050.0 | 247 |  | 1.279 | 18.018 | 6.578 | 63.495 |  |
| V41/13-9 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.6956 | 2050.0 | 247 |  | 0.763 | 10.028 | 3.923 | 60.876 |  |
| V41/13-10 | $44^{\circ} 53.8^{\prime} \mathrm{N}$ | $130^{\circ} 15.7^{\prime} \mathrm{W}$ | 6.0 | 1990.7119 | 2050.0 | 247 |  | 1.299 | 12.363 | 6.680 | 45.969 |  |

Table 5: (continued).

| Mooring <br> ID | Latitude | Longitude | Coll. intvl. <br> $($ days $)$ | Compl. <br> date | Depth <br> $(\mathrm{m})$ | MAB | Total mass <br> $(\mathrm{mg})$ | Opal free <br> mass $(\mathrm{g})$ | Total VMF <br> $\left(\mathrm{mg} / \mathrm{m}^{2} / \mathrm{day}\right)$ | $\left.\begin{array}{c}\text { Opal free VMF } \\ (\mathrm{mg} / \mathrm{m} \\ \hline\end{array} \mathrm{day}\right)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | | Mean VMF |
| :---: |
| $\%$ opal |
| $\left(\mathrm{mg} / \mathrm{m}^{2} / \mathrm{day}\right)$ |

Table 6: Elemental fluxes from mooring V34.

|  |  | Compl. | Uncor. VMF | $\underset{\mathrm{Si}}{\mathrm{Remob} .}$ | Remob. Opal | $\begin{aligned} & \text { Corr. } \\ & \text { VMF } \end{aligned}$ | $\begin{gathered} \mathrm{Al} \\ \text { flux } \end{gathered}$ | $\begin{aligned} & \text { Corr. } \mathrm{Si} \\ & \text { flux } \end{aligned}$ | $\begin{aligned} & \text { Corr. P } \\ & \text { flux } \end{aligned}$ | $\begin{gathered} \mathrm{S} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \mathrm{V} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \mathrm{Cr} \\ \text { flux } \\ \hline \end{gathered}$ | Corr. Mn flux | Corr. total Fe flux | $\begin{gathered} \text { Hyd. } \\ \mathrm{Fe} \end{gathered}$ | $\begin{gathered} \text { Terr. } \\ \text { Fe } \end{gathered}$ | $\begin{array}{r} \mathrm{Cu} \\ \text { flux } \\ \hline \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \text { flux } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mooring | (m) | date | (mg/m² day) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| V34/15-1 | 2050 | 1990.564 | 18.000 | 3.4400 | 7.3616 | 25.362 | 0.13719 | 8.7447 | 0.046601 | 0.17212 | 0.0018001 | 0.00069998 | 0.0087281 | 0.16667 | 0.0000 | 0.16667 | 0.00056016 | 0.0051912 |
| V34/15-2 | 2050 | 1990.580 | 15.100 | 2.1800 | 4.6652 | 19.765 | 0.12012 | 4.2009 | 0.035086 | 0.11344 | 0.00047314 | 0.00085743 | 0.0085330 | 0.20275 | 0.053833 | 0.14891 | 0.00053617 | 0.0071231 |
| V34/15-3 | 2050 | 1990.597 | 27.800 | 4.6200 | 9.8868 | 37.687 | 0.18012 | 7.8230 | 0.24829 | 0.24035 | 0.0014698 | 0.0013723 | 0.0089596 | 0.20257 | 0.0000 | 0.20257 | 0.016370 | 0.017470 |
| V34/15-4 | 2050 | 1990.613 | 31.800 | 6.8200 | 14.595 | 46.395 | 0.21626 | 12.186 | 0.087571 | 0.15906 | 0.0018955 | 0.0016846 | 0.011607 | 0.25810 | 0.0000 | 0.25810 | 0.0000 | 0.020551 |
| V34/15-5 | 2050 | 1990.630 | 50.200 | 0.0005 | 0.0010700 | 50.201 | 0.25754 | 11.104 | 0.029343 | 0.46783 | 0.0024209 | 0.00070262 | 0.014800 | 0.49174 | 0.17292 | 0.31881 | 0.0041517 | 0.023551 |
| V34/15-6 | 2050 | 1990.646 | 52.500 | 7.8100 | 16.713 | 69.213 | 0.25631 | 16.905 | 0.11428 | 0.26186 | 0.0021689 | 0.0012304 | 0.010855 | 0.25539 | 0.0000 | 0.25539 | 0.0000 | 0.012092 |
| V34/15-7 | 2050 | 1990.663 | 31.700 | 3.5300 | 7.5542 | 39.254 | 0.17746 | 8.5978 | 0.13810 | 0.23929 | 0.0026254 | 0.0012748 | 0.014290 | 0.20317 | 0.0000 | 0.20317 | 0.0000 | 0.017700 |
| V34/15-8 | 2050 | 1990.679 | 32.400 | 6.5300 | 13.974 | 46.374 | 0.23256 | 15.057 | 0.13599 | 0.29414 | 0.0033339 | 0.0020498 | 0.010550 | 0.26725 | 0.0000 | 0.26725 | 0.0017350 | 0.022264 |
| V34/15-9 | 2050 | 1990.696 | 19.800 | 4.0700 | 8.7098 | 28.510 | 0.15723 | 8.5954 | 0.036589 | 0.15545 | 0.0021090 | 0.00091874 | 0.0070566 | 0.16339 | 0.0000 | 0.16339 | 8.5081e-05 | 0.010273 |
| V34/15-10 | 2050 | 1990.712 | 6.8000 | 0.7600 | 1.6264 | 8.4264 | 0.029205 | 1.1617 | 0.018171 | 0.030369 | 0.0000 | 0.00024295 | 0.0014946 | 0.026645 | 0.0000 | 0.026645 | 0.0000 | 0.0022748 |
| V34/30-1 | 2150 | 1990.564 | 149.50 | 14.1800 | 30.345 | 179.85 | 0.81858 | 65.234 | 0.16818 | 1.8271 | 0.012856 | 0.0095314 | 0.038611 | 1.9052 | 0.89240 | 1.0128 | 0.022430 | 0.067340 |
| V34/30-2 | 2150 | 1990.580 | 34.100 | 4.3200 | 9.2448 | 43.345 | 0.30444 | 12.689 | 0.076107 | 0.45488 | 0.0042254 | 0.0022285 | 0.048511 | 1.6538 | 1.2766 | 0.37720 | 0.010405 | 0.027495 |
| V34/30-3 | 2150 | 1990.597 | 24.600 | 7.1300 | 15.258 | 39.858 | 0.29293 | 14.007 | 0.065828 | 0.76152 | 0.0044018 | 0.0018738 | 0.023280 | 2.1081 | 1.7450 | 0.36305 | 0.054163 | 0.047300 |
| V34/30-4 | 2150 | 1990.613 | 44.000 | 6.6100 | 14.145 | 58.145 | 0.38202 | 18.453 | 0.094989 | 1.1560 | 0.0061944 | 0.0036039 | 0.063152 | 1.8438 | 1.3703 | 0.47348 | 0.013291 | 0.053487 |
| V34/30-5 | 2150 | 1990.630 | 60.500 | 0.0000 | 0.0000 | 60.500 | 0.43161 |  |  | 1.0128 | 0.0060639 | 0.0024365 |  | 2.6672 | 2.1334 | 0.53376 | 0.010528 | 0.092503 |
| V34/30-6 | 2150 | 1990.646 | 72.800 | 7.4000 | 15.836 | 88.636 | 0.49372 | 30.598 | 0.13218 | 0.88654 | 0.0087889 | 0.0057255 | 0.058849 | 2.4882 | 1.8776 | 0.61057 | 0.0071735 | 0.038193 |
| V34/30-7 | 2150 | 1990.663 | 52.500 | 6.2500 | 13.375 | 65.875 | 0.48611 | 22.971 | 0.11822 | 0.83676 | 0.0062302 | 0.0032074 | 0.056835 | 2.6833 | 2.0821 | 0.60115 | 0.19822 | 0.043268 |
| V34/30-8 | 2150 | 1990.679 | 33.500 | 4.5700 | 9.7798 | 43.280 | 0.32490 | 13.312 | 0.10627 | 0.47150 | 0.0051801 | 0.0017093 | 0.045111 | 1.7503 | 1.3485 | 0.40179 | 0.041545 | 0.049609 |
| V34/30-9 | 2150 | 1990.696 | 16.400 | 1.9000 | 4.0660 | 20.466 | 0.11571 | 5.3695 | 0.44419 | 0.22078 | 0.0012239 | 0.00062750 | 0.0096893 | 0.49078 | 0.34633 | 0.14445 | 0.026682 | 0.017488 |
| V34/30-10 | 2150 | 1990.712 | 27.900 | 5.2900 | 11.321 | 39.221 | 0.19076 | 10.100 | 0.083219 | 0.49186 | 0.0025695 | 0.0018075 | 0.036881 | 0.99197 | 0.75605 | 0.23591 | 0.0089201 | 0.025887 |
| V34/27-1 | 2250 | 1990.564 | 26.900 | 3.0400 | 6.5056 | 33.406 | 0.17973 | 8.1931 | 0.11918 | 0.41713 | 0.0060503 | 0.0013647 | 0.19063 | 4.7573 | 4.5351 | 0.22227 | 0.0048541 | 0.024647 |
| V34/27-2 | 2250 | 1990.580 | 22.800 | 3.8400 | 8.2176 | 31.018 | 0.24786 | 8.2383 | 0.081148 | 0.29024 | 0.0033483 | 0.0017515 | 0.049126 | 1.3165 | 1.0095 | 0.30703 | 0.0026360 | 0.044456 |
| V34/27-3 | 2250 | 1990.597 | 30.600 | 4.8500 | 10.379 | 40.979 | 0.29986 | 9.1536 | 0.073792 | 0.30589 | 0.0023588 | 0.0016246 | 0.031898 | 0.83020 | 0.45780 | 0.37240 | 0.0049403 | 0.013499 |
| V34/27-4 | 2250 | 1990.613 | 34.600 | 4.6000 | 9.8440 | 44.444 | 0.19182 | 7.9015 | 0.085046 | 0.29292 | 0.0047890 | 0.0011303 | 0.10083 | 2.2680 | 2.0305 | 0.23756 | 0.0030117 | 0.015806 |
| V34/27-5 | 2250 | 1990.630 | 70.300 | 12.7500 | 27.285 | 97.585 | 0.46931 | 23.046 | 0.17529 | 1.3614 | 0.0064698 | 0.0033558 | 0.17989 | 3.7935 | 3.2131 | 0.58038 | 0.012382 | 0.14362 |
| V34/27-6 | 2250 | 1990.646 | 75.900 | 6.5400 | 13.996 | 89.896 | 0.37645 | 17.025 | 0.12858 | 1.9200 | 0.0067004 | 0.0038311 | 0.063880 | 3.4423 | 2.9768 | 0.46554 | 0.023842 | 0.044570 |
| V34/27-7 | 2250 | 1990.663 | 51.700 | 4.7600 | 10.186 | 61.886 | 0.58830 | 16.021 | 0.11045 | 1.6203 | 0.0062300 | 0.0021910 | 0.072009 | 4.5661 | 3.8385 | 0.72753 | 0.33381 | 0.094343 |
| V34/27-8 | 2250 | 1990.679 | 60.600 | 7.3700 | 15.772 | 76.372 | 0.44377 | 15.912 | 0.095555 | 0.76839 | 0.0049288 | 0.0026595 | 0.18118 | 2.9587 | 2.4099 | 0.54880 | 0.10199 | 0.060407 |
| V34/27-9 | 2250 | 1990.696 | 28.500 | 3.5700 | 7.6398 | 36.140 | 0.27528 | 8.4878 | 0.12158 | 0.26327 | 0.0037892 | 0.0012624 | 0.091392 | 1.9970 | 1.6566 | 0.34043 | 0.011055 | 0.013854 |
| V34/27-10 | 2250 | 1990.712 | 20.100 | 2.4800 | 5.3072 | 25.407 | 0.26631 | 5.3706 | 0.080609 | 0.46819 | 0.0022726 | 0.0017152 | 0.062329 | 1.6355 | 1.3062 | 0.32933 | 0.017619 | 0.057750 |

Table 7: Comparison of elemental fluxes at north Cleft and Endeavour segments of the JDFR.

|  | Dec. <br> date | depth | Total flux | $\begin{gathered} \hline \mathrm{Al} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \hline \mathrm{Si} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \mathrm{S} \\ \text { flux } \end{gathered}$ | $\begin{aligned} & \hline \text { Mn } \\ & \text { flux } \end{aligned}$ | $\begin{gathered} \mathrm{Fe} \\ \text { flux } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{Cu} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \mathrm{Zn} \\ \text { flux } \end{gathered}$ | $\begin{gathered} \mathrm{Ca} \\ \text { flux } \end{gathered}$ | Va |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | (mg/m ${ }^{2} /$ day $)$ |  |  |  |  |  |  |  |  |  |
| This study | 1990.56-1990.71 | 2050 | 28.60 |  |  | 0.213 | 0.0096900 | 0.22400 | 0.0023400 | 0.013800 |  | 0.0018300 |
| V34 | 1990.56-1990.7 | 2150 | 51.60 |  |  | 0.812 | 0.042300 | 1.8600 | 0.039300 | 0.046300 |  | 0.0057700 |
|  | 1990.56-1990.7 | 2285 | 42.20 |  |  | 0.771 | 0.10200 | 2.7600 | 0.051600 | 0.051300 |  | 0.0046900 |
| This study | 1990.74-1991.34 | 1800 | 30.50 | 0.177 | 6.43 | 0.195 | 0.011000 | 0.0017300 | 0.00010500 | 0.0093000 | 2.39 | 0.00091000 |
| V43 | 1990.74-1991.34 | 2050 | 21.04 | 0.129 | 3.93 | 0.139 | 0.014700 | 0.059500 | 0.0011600 | 0.0068200 | 1.92 | 0.00072000 |
|  | 1990.74-1991.34 | 2150 | 30.11 | 0.254 | 6.82 | 0.201 | 0.038200 | 0.23600 | 0.00032200 | 0.0094700 | 2.30 | 0.0013500 |
|  | 1990.74-1991.34 | 2250 | 31.80 | 0.180 | 1.22 | 0.379 | 0.045300 | 0.19000 | 0.00039900 | 0.013000 | 0.17 | 0.0015000 |
| Dymond and | 1984.77-1985.44 | 1700 | 72.38 | 0.638 | 11.23 | n.d. | 0.0086800 | 0.40820 | 0.0020800 | 0.0052055 | 14.06 | 0.0089600 |
| Roth; 1988 | 1984.77-1985.44 | 1950 | 34.55 | 0.419 | 4.30 | 4.11 | 0.021500 | 2.0411 | 0.11780 | 0.32055 | 4.99 | 0.021600 |
|  | 1984.77-1985.44 | 2100 | 66.90 | 0.860 | 7.53 | 12.5 | 0.092500 | 5.9726 | 0.40000 | 1.2301 | 7.86 | 0.096160 |

## Appendix

Table A1: Time of recovery, splitting, and processing for sediment traps in which remobilization rates were calculated

|  |  |  | Remobilization in Supernate |  |  |  |  |  | Remobilization in Splitting Solution |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mooring | Date Trap Opened | Date <br> Recovered | $\begin{gathered} \text { Date } \\ \text { Sampled } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Vol. } \\ \text { (liters) } \\ \hline \end{gathered}$ | Duration | Label | $\begin{aligned} & \hline \text { Elements } \\ & \text { Sampled } \\ & \hline \end{aligned}$ | Equations | Date Split | Dilution | Date <br> Processed | Duration | Label | Elements <br> Sampled | Equations |
| V23 | 18 Aug 88 | 12 Sep 89 | 22 Jan 90 | 0.18 | Deployment \& Storage | $\mathrm{RF}_{\text {su }}$ | $\begin{gathered} \mathrm{Sal}, \mathrm{Si}, \mathrm{P}, \\ \mathrm{Fe}, \mathrm{Mn} \end{gathered}$ | $\begin{gathered} 1-5 \\ 5 \end{gathered}$ | 22 Jan 90 | unknown | Aug 91 | Remobilization in splitting solution unknown |  | $\begin{gathered} \text { not } \\ \text { sampled } \end{gathered}$ |  |
| V26 | 15 Aug 89 | 9 Jul 90 | 21 Mar 91 | 0.18 | Deployment \& Storage | $\mathrm{RF}_{\text {su }}$ | $\begin{gathered} \mathrm{Sal}, \mathrm{Si}, \mathrm{P}, \\ \mathrm{Fe}, \mathrm{Mn} \end{gathered}$ | $\begin{gathered} 1-5 \\ 5 \end{gathered}$ | 21 Mar 91 | unknown | Aug 91 | Remobilization in splitting solution unknown |  | not sampled |  |
| V34 | 18 Jul 90 | 17 Sep 90 | 9 Nov 90 | 0.18 | Deployment \& Storage | $\mathrm{RF}_{\text {su }}$ | $\begin{gathered} \mathrm{Sal}, \mathrm{Si}, \mathrm{P}, \\ \mathrm{Fe}, \mathrm{Mn} \end{gathered}$ | $\begin{gathered} 1-5 \\ 5 \end{gathered}$ | 9 Nov 90 | 4-15 | Aug 91 | In splitting solution between Nov. 90 and Aug. 91 | $\mathrm{RF}_{\text {spl }}$ | Sal, Si, P | 7-8 |
| V43 | 28 Sep 90 | 10 Jun 91 | 10 Jun 91 29 Sep 91 | 0.18 $\sim 0.06$ | Deployment <br> Storage | $R F_{\text {su }}$ $R F_{\text {st }}$ | Sal, Si, P, <br> $\mathrm{Fe}, \mathrm{Mn}$ <br> $\mathrm{Fe}, \mathrm{Mn}$ | $\begin{gathered} 1-5 \\ 5 \\ 6 \\ \hline \end{gathered}$ | 29 Sep 91 | unknown | $\begin{aligned} & \text { immediately } \\ & \text { upon } \\ & \text { splitting } \end{aligned}$ | No remobilization in splitting solution assumed |  | not sampled |  |

Table A2a: Concentrations of salinity, $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn in the supernates of the sediment trap cylinders for trap 13 on mooring V23 at the time of sample splitting.

| Mooring/ Trap | Sampling <br> Jar | Supernate at Recovery |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \text { Sal } \\ & \mathrm{ppt} \\ & \hline \end{aligned}$ | Si | P | Fe Mn |  |
|  |  |  |  | $\mu \mathrm{M}$ | nM |  |
| V23/13 | 1 |  |  |  |  |  |
| V23/13 | 2 | 38.70 | 201 | 6.900 | 74 | 8946 |
| V23/13 | 3 | 43.02 | 327 | 3.192 | 82 | 4613 |
| V23/13 | 4 | 44.49 | 254 | 7.306 | 0 | 2235 |
| V23/13 | 5 | 43.35 | 289 | 6.570 | 952 | 2240 |
| V23/13 | 6 | 42.98 | 214 | 1.865 | 0 | 1600 |
| V23/13 | 7 | 44.98 | 183 | 7.000 | 452 | 942 |
| V23/13 | 8 | 42.32 | 317 | 2.512 | 0 | 754 |
| V23/13 | 9 | 46.56 | 457 | 7.643 | 0 | 687 |
| V23/13 | 10 | 47.64 | 366 | 5.919 | 0 | 494 |
| Fill |  | 88.30 | 122 | 2.06 |  |  |
| Ambient SW |  | 34.60 | 183 | 2.96 |  |  |

Table A2b: Concentrations of salinity, $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn in the supernates of the sediment trap cylinders for traps 30,32 , and 36 on mooring V26 at the time of sample splitting.

| $\begin{gathered} \text { Mooring/ } \\ \text { Trap } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Sampling } \\ \text { Jar } \\ \hline \end{gathered}$ | Supernate at Recovery |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sal | Si | P | Fe | Mn |
|  |  | ppt | $\mu \mathrm{M}$ |  | nM |  |
| V26/30 | 1 |  | 247 | 4.32 | 2865 | 220 |
| V26/30 | 2 | 43.13 | 603 | 14.1 | 269 | 38 |
| V26/30 | 3 | 41.05 | 892 | 15.9 | 752 | 27 |
| V26/30 | 4 | 40.35 | 555 | 4.04 | 310 | 0 |
| V26/30 | 5 | 64.13 | 290 | 6.63 | 0 | 0 |
| V26/30 | 6 | 36.77 | 199 | 16.28 | 403 | 0 |
| V26/30 | 7 | 37.65 | 790 | 14.12 | 0 | 368 |
| V26/30 | 8 | 41.55 | 996 | 22.81 | 0 | 215 |
| V26/30 | 9 | 48.81 | 724 | 6.08 | 0 | 0 |
| V26/30 | 10 | no sample |  |  | , | 0 |
| V26/32 | 1 | 39.21 | 451 | 8.02 | 430 | 0 |
| V26/32 | 2 | 41.84 | 579 | 9.82 | 609 | 0 |
| V26/32 | 3 |  | 894 | 19.5 | 7395 | 626 |
| V26/32 | 4 | 49.44 | 825 | 7.27 | 1056 | 87 |
| V26/32 | 5 | 46.84 | 278 | 6.87 | 358 | 58 |
| V26/32 | 6 | 37.93 | 454 | 6.54 | - | 22 |
| V26/32 | 7 |  | 752 | 13.48 | 0 | 46 |
| V26/32 | 8 |  | 1008 | 18.7 | 430 | 26 |
| V26/32 | 9 |  | 386 | 6.35 | , | 0 |
| V26/32 | 10 |  |  |  | 0 | 0 |
| V26/36 | 1 |  | 480 | 5.04 | 1343 | 0 |
| V26/36 | 2 | 39.10 | 645 | 4.41 | 895 | 0 |
| V26/36 | 3 |  | 795 | 4.38 | 5694 | 448 |
| V26/36 | 4 | 40.97 | 835 | 14.35 | 127 | 0 |
| V26/36 | 5 |  | 823 | 4.28 | 2793 | 157 |
| V26/36 | 6 |  | 281 | 4.4 | 174 | 0 |
| V26/36 | 7 |  | 814 | 6.04 | 412 | 0 |
| V26/36 | 8 | 39.10 | 964 | 16.14 | 7395 | 1438 |
| V26/36 | 9 | 40.50 | 881 | 19.25 | 14414 | 1183 |
| V26/36 | 10 |  |  |  | 0 | 0 |
| Fill Sol. |  | 88.30 | 122 | 2.06 |  |  |
| Ambient SW |  | 34.60 | 181 | 2.97 |  |  |

Table A2c: Concentrations of salinity, $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn in the supernates of the sediment trap cylinders for traps 15,30 , and 27 on mooring V34 at the time of sample splitting, and the concentrations of salinity, Si , and P in the diluted splitting solution just prior to processing particles onto filters.

| Mooring/ Trap | Sampling Jar | Supernate at Recovery |  |  |  |  | Splitting Solution at Processing (t2) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sal | Si | P | Fe | Mn | Sal | Si | P |
|  |  | ppt | $\mu \mathrm{M}$ |  | nM |  | ppt | $\mu \mathrm{M}$ |  |
| V34/15 | 1 | 77.30 | 210 | 4.38 | 0 | 43.5 | 9.97 | 124 | 0.08 |
| V34/15 | 2 | 72.30 | 183 | 3.19 | 10.1 | 30.6 | 16.70 | 130 | 0.98 |
| V34/15 | 3 | 70.53 | 236 | 9.9 | 17.5 | 28.9 | 7.06 | 131 | 1.66 |
| V34/15 | 4 | 68.41 | 242 | 4.09 | 29.1 | 36.6 | 13.30 | 236 | 1.72 |
| V34/15 | 5 | 67.33 | 281 | 4.19 | 9.3 | 34.8 |  |  |  |
| V34/15 | 6 | 68.79 | 255 | 6 | 0 | 34.4 | 14.33 | 243 | 1.10 |
| V34/15 | 7 | 66.40 | 178 | 6.84 | 120 | 56.4 | 5.85 | 199 | 0.45 |
| V34/15 | 8 | 67.30 | 241 | 5.77 | 21 | 0 | 10.35 | 207 | 1.26 |
| V34/15 | 9 | 68.88 | 200 | 3.02 | 0 | 0 | 14.05 | 169 | 0.95 |
| V34/15 | 10 | 66.74 | 181 | 3.12 | 0 | 0 | 13.64 | 74 | 0.82 |
| V34/30 | 1 | 76.37 | 367 | 2.96 | 17.5 | 13.5 | 8.43 | 299 | 0.59 |
| V34/30 | 2 | 62.74 | 242 | 3.38 | 59 | 209 | 7.44 | 119 | 0.06 |
| V34/30 | 3 | 76.74 | 216 | 2.56 | 87 | 106 | 8.21 | 234 | 0.36 |
| V34/30 | 4 | 72.84 | 251 | 2.79 | 76 | 123 | 18.47 | 264 | 1.06 |
| V34/30 | 5 |  |  |  |  |  | 10.25 | 348 | 1.28 |
| V34/30 | 6 | 69.11 | 238 | 3.24 | 0 | 121 | 16.39 | 283 | 0.59 |
| V34/30 | 7 | 72.88 | 236 | 3.37 | 0 | 87 | 11.84 | 243 | 0.70 |
| V34/30 | 8 | 74.09 | 206 | 3.46 | 0 | 60 | 14.94 | 175 | 0.82 |
| V34/30 | 9 | 71.23 | 193 | 18.42 | 86 | 46 | 5.65 | 76 | 0.03 |
| V34/30 | 10 | 73.53 | 219 | 4.34 | 0 | 77 | 10.73 | 156 | 0.65 |
| V34/27 | 1 | 46.48 | 218 | 2.73 | 0 |  | 7.10 | 125 | 0.30 |
| V34/27 | 2 | 61.63 | 250 | 3.69 | 42 | 57.8 | 8.90 | 121 | 0.53 |
| V34/27 | 3 | 62.69 | 262 | 3.73 | 66 | 89 | 9.48 | 132 | 0.61 |
| V34/27 | 4 | 64.99 | 257 | 3.11 | 60 | 89 | 9.21 | 139 | 0.18 |
| V34/27 | 5 |  | 322 | 3.75 | 0 | 0 | 8.75 | 345 | 1.23 |
| V34/27 | 6 |  | 288 | 3.72 | 0 | 104 | 4.03 | 150 | 0.06 |
| V34/27 | 7 |  | 269 | 3.25 | 0 | 84 | 7.30 | 127 | 0.06 |
| V34/27 | 8 |  | 271 | 3.27 | 0 | 50 | 8.80 | 203 | 0.06 |
| V34/27 | 9 |  | 247 | 4.45 | 0 | 118 | 4.40 | 111 | 0.01 |
| V34/27 | 10 |  | 193 | 3.48 | 0 | 26.4 | 9.12 | 112 | 0.59 |
| Fill Sol. |  | 88.30 | 193 | 2.61 |  |  |  |  |  |
| Ambient SW | 1800 m | 34.60 | 181 | 2.88 |  |  |  |  |  |
| Ambient SW | Blw 1800 m |  |  | 2.97 |  |  |  |  |  |

Table A2d: Concentrations of salinity, $\mathrm{Si}, \mathrm{P}, \mathrm{Fe}$, and Mn in the supernates of the sediment trap cylinders for traps 17,30 , and 34 on mooring V43 at the time of recovery on board ship; and the volumes of the remaining supernates and the concentrations of Fe and Mn in the remaining supernates just prior to processing particles onto filters.

| $\begin{gathered} \text { Mooring/ } \\ \text { Trap } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Sampling } \\ \text { Jar } \\ \hline \end{gathered}$ | Supernate at Recovery |  |  |  |  | Splitting Solution at Processing (t2) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sal | Si | P | Fe | Mn | Sal | Si | P |
|  |  | ppt | $\mu \mathrm{M}$ |  | nM |  | ppt | $\mu \mathrm{M}$ |  |
| V43/17 | 1 | 54.98 | 168 | 5.84 | <61 | <21 | 0.059 | 177 | 26 |
| V43/17 | 2 | 56.24 | 207 | 26.55 | <61 | 43 | 0.054 | 367 | 117 |
| V43/17 | 3 | 45.35 | 330 | 6.84 | 107 | 43 | 0.076 | 661 | 91 |
| V43/17 | 4 | 36.45 | 230 | 4.33 | <61 | 63 | 0.051 | 371 | 72 |
| V43/17 | 5 | 54.21 | 139 | 5.61 | <61 | 63 | 0.070 | 645 | 45 |
| V43/17 | 6 | 56.39 | 248 | 4.53 | <61 | 57 | 0.067 | 260 | 63 |
| V43/17 | 7 | 50.05 | 226 | 6.85 | <61 | 37 | 0.052 | 1107 | 151 |
| V43/17 | 8 | 56.10 | 233 | 4.67 | <61 | <21 | 0.072 | 65 | <21 |
| V43/17 | 9 | 35.36 | 255 | 1.35 | <61 | <21 | 0.049 | 54 | <21 |
| V43/17 | 10 | no sample |  | 4.68 |  |  |  |  |  |
| V43/30 | 1 | 45.91 | 223 |  | 815 | <21 | 0.078 | 445 | $<21$ |
| V43/30 | 2 | 47.21 | 226 |  | 435 | <21 | 0.073 | 289 | <21 |
| V43/30 | 3 | 51.33 | 338 |  | 431 | 88 | 0.098 | 399 | 32 |
| V43/30 | 4 | 49.71 | 220 | 3.29 | 303 | 127 | 0.078 | 406 | 67 |
| V43/30 | 5 | 53.26 | 223 | 3.29 | 305 | 90 | 0.058 | 947 | 163 |
| V43/30 | 6 | 60.23 | 214 | 3.13 | 235 | 82 | 0.068 | 276 | 127 |
| V43/30 | 7 | 37.99 | 48 | 3.43 | 370 | 41 | 0.065 | 459 | 52 |
| V43/30 | 8 | 49.41 | 154 | 4.26 | 293 | <21 | 0.057 | 233 | <21 |
| V43/30 | 9 | 56.03 | 163 | 3.92 | <34 | 57 |  | <34 | 32 |
| V43/30 | 10 |  |  |  |  |  |  |  |  |
| V43/33 | 1 | 36.61 | 263 | 5.16 | 1205 | 910 | 0.082 | 12641 | 5692 |
| V43/33 | 2 | 54.82 | 293 | 4.74 | 850 | 116 | 0.084 | 163 | 84 |
| V43/33 | 3 | 54.33 | 346 | 7.54 | 830 | 164 | 0.079 | 727 | 220 |
| V43/33 | 4 | 35.35 | 210 | 7.87 | 1913 | 2902 | 0.072 | 1419 | 4491 |
| V43/33 | 5 | 46.10 | 260 | 3.63 | 523 | 196 | 0.083 | 400 |  |
| V43/33 | 6 | 51.00 | 205 | 3.62 | <34 | 200 | 0.087 | <34 | 132 |
| V43/33 | 7 | 54.30 | 303 | 4.43 | 1221 | 210 | 0.074 | 384 | 242 |
| V43/33 | 8 | 49.22 | 246 | 3.43 | 738 | 140 | 0.072 | 107 | 87 |
| V43/33 | 9 |  |  |  |  |  |  |  |  |
| V43/33 | 10 |  |  |  |  |  |  |  |  |
| V43/34 | 1 | 53.10 | 223 | 5.43 | 417 |  | 0.057 | 1741 | 93 |
| V43/34 | 2 | 44.13 | 201 | 4.65 | 936 | <21 | 0.048 | 3838 | 115 |
| V43/34 | 3 | 56.10 | 195 | 8.74 | 234 | 85 | 0.072 | 1288 | 212 |
| V43/34 | 4 | 54.30 | 212 | 15.24 | 473 | 140 | 0.058 | 897 | 108 |
| V43/34 | 5 | 55.34 | 181 | 5.48 | 370 | 174 | 0.057 | 915 | 119 |
| V43/34 | 6 | 60.21 | 181 | 4.91 | 302 | 100 | 0.059 | 788 | 181 |
| V43/34 | 7 | 52.18 | 171 | 1.53 | 110 | 107 | 0.062 | 1107 | 182 |
| V43/34 | 8 | 56.54 | 183 | 2.72 | 241 | 107 | 0.059 | 420 | 99 |
| V43/34 | 9 | 59.03 | 160 | 3.47 | 249 | 110 | 0.054 | 340 | 38 |
| V43/34 | 10 |  |  |  |  |  |  |  |  |
| Filling |  | 88.30 | 122 | 2.06 |  |  |  |  |  |
| Ambient |  | 34.60 | 181 | 2.97 |  |  |  |  |  |

Table A3: Si, P, Fe, and Mn in sediment trap supernates expressed as flux ( $\mathrm{mg} \mathrm{m}^{-2}$ day $^{-1}$ ).

| Mooring | Sample No. | Si | P | Fe | Mn |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\left(\mathrm{mg} / \mathrm{m}^{2} /\right.$ day $)$ |  |  |  |
| V23/13 | 2 | 0.12 | 0.0237 | 0.0008 | 0.0939 |
| V23/13 | 3 | 0.82 | 0.0022 | 0.0009 | 0.0484 |
| V23/13 | 4 | 0.44 | 0.0267 | 0 | 0.0235 |
| V23/13 | 5 | 0.62 | 0.0222 | 0.0102 | 0.0235 |
| V23/13 | 6 | 0.22 | -0.0056 | 0 | 0.0168 |
| V23/13 | 7 | 0.06 | 0.0249 | 0.0048 | 0.0099 |
| V23/13 | 8 | 0.77 | -0.0019 | 0 | 0.0079 |
| V23/13 | 9 | 1.54 | 0.0289 | 0 | 0.0072 |
| V23/13 | 10 | 1.06 | 0.0188 | 0 | 0.0052 |
| V26/30 | 1 | 0.41 | 0.0089 | 0.0278 |  |
| V26/30 | 2 | 2.32 | 0.0667 | 0.0026 | 0.0004 |
| V26/30 | 3 | 3.85 | 0.0772 | 0.0073 | 0.0003 |
| V26/30 | 4 | 2.04 | 0.0069 | 0.0030 | 0 |
| V26/30 | 5 | 0.76 | 0.0246 | 0 | 0 |
| V26/30 | 6 | 0.11 | 0.0790 | 0.0039 | 0 |
| V26/30 | 7 | 3.29 | 0.0663 | 0 | 0.0035 |
| V26/30 | 8 | 4.42 | 0.1181 | 0 | 0.0020 |
| V26/30 | 9 | 3 | 0.0198 | 0 | 0 |
| V26/32 | 1 | 1.48 | 0.0303 | 0.0042 | 0 |
| V26/32 | 2 | 2.18 | 0.0413 | 0.0059 | 0 |
| V26/32 | 3 | 3.88 | 0.0987 | 0.0717 | 0.0060 |
| V26/32 | 4 | 3.54 | 0.0269 | 0.0102 | 0.0008 |
| V26/32 | 5 | 0.59 | 0.0243 | 0.0035 | 0.0006 |
| V26/32 | 6 | 1.48 | 0.0215 | 0 | 0.0002 |
| V26/32 | 7 | 3.11 | 0.0630 | 0 | 0.0004 |
| V26/32 | 8 | 4.49 | 0.0939 | 0.0042 | 0.0002 |
| V26/32 | 9 | 1.15 | 0.0208 | 0 | 0 |
| V26/36 | 1 | 1.64 | 0.0128 | 0.0130 | 0 |
| V26/36 | 2 | 2.52 | 0.0090 | 0.0087 | 0 |
| V26/36 | 3 | 3.33 | 0.0089 | 0.0552 | 0.0043 |
| V26/36 | 4 | 3.55 | 0.0680 | 0.0012 | 0 |
| V26/36 | 5 | 3.48 | 0.0083 | 0.0271 | 0.0015 |
| V26/36 | 6 | 0.57 | 0.0090 | 0.0017 | 0 |
| V26/36 | 7 | 3.43 | 0.0187 | 0.0040 | 0 |
| V26/36 | 8 | 4.23 | 0.0784 | 0.0717 | 0.0137 |
| V26/36 | 9 | 3.79 | 0.0969 | 0.1398 | 0.0113 |
| V34/15 | 1 | 3.44 | 0.0340 | 0 | 0.0023 |
| V34/15 | 2 | 2.18 | 0.0210 | 0.0005 | 0.0016 |
| V34/15 | 3 | 4.62 | 0.2350 | 0.0009 | 0.0015 |
| V34/15 | 4 | 6.82 | 0.0690 | 0.0016 | 0.0019 |
| V34/15 | 5 | 0.0005 | 0.0018 |  |  |
| V34/15 | 6 | 7.81 | 0.0910 | 0 | 0.0018 |
| V34/15 | 7 | 3.53 | 0.1170 | 0.0064 | 0.0030 |
| V34/15 | 8 | 6.53 | 0.1020 | 0.0011 | 0 |
| V34/15 | 9 | 4.07 | 0.0190 | 0 | 0 |
| V34/15 | 10 | 0.76 | 0.0160 | 0 | 0 |

Table A3: (continued)

| Mooring | Sample No. | Si | P | Fe | Mn |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\left(\mathrm{mg} / \mathrm{m}^{2} /\right.$ day $)$ |  |  |  |
| V34/30 | 1 | 14.18 | 0.019 | 0.0009 | 0.0007 |
| V34/30 | 2 | 4.32 | 0.007 | 0.0031 | 0.0110 |
| V34/30 | 3 | 7.13 | 0 | 0.0046 | 0.0056 |
| V34/30 | 4 | 6.61 | 0.013 | 0.0041 | 0.0065 |
| V34/30 | 5 | 0 |  |  |  |
| V34/30 | 6 | 7.40 | 0.011 | 0 | 0.0064 |
| V34/30 | 7 | 6.25 | 0.024 | 0 | 0.0046 |
| V34/30 | 8 | 4.57 | 0.027 | 0 | 0.0031 |
| V34/30 | 9 | 1.90 | 0.418 | 0.0046 | 0.0024 |
| V34/30 | 10 | 5.29 | 0.049 | 0 | 0.0040 |
| V34/27 | 1 | 3.04 | -0.006 | 0 | 0 |
| V34/27 | 2 | 3.84 | 0.028 | 0.0022 | 0.0030 |
| V34/27 | 3 | 4.85 | 0.031 | 0.0035 | 0.0047 |
| V34/27 | 4 | 4.60 | 0.004 | 0.0032 | 0.0047 |
| V34/27 | 5 | 12.75 | 0.054 | 0 | 0 |
| V34/27 | 6 | 6.54 | 0.023 | 0 | 0.0055 |
| V34/27 | 7 | 4.76 | 0.006 | 0 | 0.0044 |
| V34/27 | 8 | 7.37 | 0.002 | 0 | 0.0026 |
| V34/27 | 9 | 3.57 | 0.044 | 0 | 0.0062 |
| V34/27 | 10 | 2.48 | 0.023 | 0.0014 |  |
| V43/17 | 1 | 0.06 | 0.0211 | 0.0007 | $1.00 \mathrm{E}-04$ |
| V43/17 | 2 | 0.30 | 0.1575 | 0.0013 | 0.0009 |
| V43/17 | 3 | 0.96 | 0.0266 | 0.0046 | 0.0009 |
| V43/17 | 4 | 0.30 | 0.0091 | 0.0012 | 0.0010 |
| V43/17 | 5 | -0.12 | 0.0195 | 0.0030 | 0.0009 |
| V43/17 | 6 | 0.54 | 0.0127 | 0.0011 | 0.0009 |
| V43/17 | 7 | 0.37 | 0.0272 | 0.0038 | 0.0009 |
| V43/17 | 8 | 0.45 | 0.0136 | 0.0003 | 0 |
| V43/17 | 9 | 0.45 | -0.0106 | 0.0002 | 0 |
| V43/30 | 1 | 0.32 | 0.0125 | 0.0120 | 0 |
| V43/30 | 2 | 0.35 | 0.0065 | 0 | 0 |
| V43/30 | 3 | 1.05 | 0.0077 | 0.0012 | 0.0012 |
| V43/30 | 4 | 0.33 | 0.0038 | 0.0057 | 0.0018 |
| V43/30 | 5 | 0.37 | 0.0042 | 0.0072 | 0.0017 |
| V43/30 | 6 | 0.36 | 0.0039 | 0.0040 | 0.0015 |
| V43/30 | 7 | -0.77 | 0.0034 | 0.0064 | 0.0007 |
| V43/30 | 8 | -0.06 | 0.0101 | 0.0043 | 0 |
| V43/30 | 9 | 0.03 | 0.0086 |  |  |
| V43/33 | 1 | 0.50 | 0.0146 | 0.0826 | 0.0409 |
| V43/33 | 2 | 0.80 | 0.0139 | 0.0110 | 0.0018 |
| V43/33 | 3 | 1.11 | 0.0322 | 0.0136 | 0.0030 |
| V43/33 | 4 | 0.18 | 0.0323 | 0.0294 | 0.0548 |
| V43/33 | 5 | 0.55 | 0.0056 | 0.0084 | 0.0023 |
| V43/33 | 6 | 0.25 | 0.0061 | 0 | 0.0031 |
| V43/33 | 7 | 0.86 | 0.0118 | 0.0164 | 0.0036 |
| V43/33 | 8 | 0.48 | 0.0047 | 0.0093 | 0.0020 |
| V43/33 | 9 |  |  |  |  |

Table A3: (continued)

|  |  | Si |  |  | P |  | Fe | Mn |
| :--- | :---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: |
| Mooring | Sample No. | $\left(\mathrm{mg} / \mathrm{m}^{2} /\right.$ day $)$ |  |  |  |  |  |  |
| $\mathrm{V} 43 / 34$ | 1 | 0.37 | 0.0182 | 0.0115 | 0.0003 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 2 | 0.18 | 0.0121 | 0.0232 | 0.0004 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 3 | 0.22 | 0.0403 | 0.0089 | 0.0020 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 4 | 0.31 | 0.0829 | 0.0090 | 0.0020 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 5 | 0.14 | 0.0188 | 0.0078 | 0.0025 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 6 | 0.17 | 0.0156 | 0.0066 | 0.0019 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 7 | 0.06 | -0.0075 | 0.0058 | 0.0020 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 8 | 0.16 | 0.0008 | 0.0045 | 0.0016 |  |  |  |
| $\mathrm{~V} 43 / 34$ | 9 | 0.03 | 0.0060 | 0.0042 | 0.0014 |  |  |  |


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